CENTRAL FLORIDA EXPRESSWAY AUTHORITY

Final Pond Siting Report March 2018

S.R. 408 Eastern Extension PD&E Study



PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with Metric Engineering, Inc. and I have reviewed or approved the evaluation, findings, opinions and conclusions as reported for:

PROJECT:	S.R. 408 Eastern Extension PD&E Study
FINANCIAL PROJECT NUMBER:	CFX-Project No. 408-254
LOCATION:	Orange County
CLIENT:	Central Florida Expressway Authority

This Pond Siting Report (PSR) includes a summary of data collection efforts, calculations, and an overall drainage review prepared for the conceptual analyses of the S.R. 408 Eastern Extension project in Orange County.

I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of transportation engineering and planning as applied through professional judgements and experience. This document is for planning purposes only and is not to replace any effort required for final design.

Florida Registered Engineer:

Name: Chandra S Raman, P.E.

Registration Number: FL # 58740

Signature:

Date:



Table of Contents

PROF	ESSIO	NAL ENGINEER CERTIFICATE	i
TABLE	E OF C	ONTENTS	ii
TABLE	ES AND	DACRONYMS	iii
APPE	NDICE	S	iv
EXEC	UTIVE	SUMMARY	1
	Existir	ng Drainage Conditions	1
	Propo	sed Drainage Conditions	2
	Summ	nary	
ALTEF	RNATI\	/E POND EVALUATION MATRIX	5
1.0	INTRO	DDUCTION	20
2.0	PROJ	ECT DESCRIPTION	20
3.0	DESI	GN CRITERIA	21
4.0	EXIST	TING CONDITIONS	22
	4.1	SOIL DATA	23
	4.2	LAND USE	24
	4.3	EXISTING CROSS DRAINS	24
	4.4	EXISTING DRAINAGE BASIN CHARACTERISTICS	25
5.0	PROF	POSED CONDITIONS	27
	5.1	METHODOLOGY OF POND DETERMINATIONS	27
	Pond Site Determination and Sizing		
	5.2	PROPOSED DRAINAGE BASINS AND PONDS	29
	5.3	TAILWATER DETERMINATION	35
	5.4	FLOODPLAIN IMPACTS/COMPENSATION	
	5.5	PROJECT CLASSIFICATION	
	5.6	FLOODING HISTORY AND MAINTENANCE CONCERN	
6.0	CONC	CLUSION	39



TABLES

Table-1 – Summary of Recommended Water Quality Treatment and Attenuation Ponds	3
Table-2 – Summary of Recommended Floodplain Compensation Ponds	4
Pond Evaluation Matrices	5
Table-3 – Summary of Existing and Proposed Condition Basin Limits	22
Table-4 – USDA NRCS Soil Survey Information	.23
Table-5 – Existing S.R. 50 Cross Drain General Information	.24
Table-6 – Preliminary Tailwater Elevations	.35
Table-7 – Floodplain Impact/Compensation Summary Table	.38
Recommended Pond Analysis Summary	.41

ACRONYMS

- PD&E Project Development and Environment
- CFX Central Florida Expressway Authority
- PSR Pond Siting Report
- SJRWMD St. Johns River Water Management District
- OFW Outstanding Florida Waters
- FDEP Florida Department of Environmental Protection
- FEMA Federal Emergency Management Agency
- FIRM FEMA Flood Insurance Rate Map
- FDOT Florida Department of Transportation
- USDA United States Department of Agriculture
- SHWT Seasonal High Water Table
- HGL Hydraulic Grade Line



APPENDICES

Appendix: A – Exhibits	A-1 to A-6
Appendix: B – FEMA Flood Insurance Rate Map	B-1 to B-4
Appendix: C – USDA NRCS Soil Report	C-1 to C-22
Appendix: D – S.R.408 Typical Section	D-1 to D-2
Appendix: E – Proposed Pond Site Maps	E-1 to E-21
Appendix: F – Pond Sizing Calculations	F-1 to F-67
Appendix: G – Excerpt from Existing S.R. 408 Plans	G-1 to G-11
Appendix: H – Existing S.R. 408 Permit Information	H-1 to H-15
Appendix: I – Excerpt Bithlo Area Stormwater Management Master Plan	I-1 to I-13
Appendix: J – Excerpt from BJM Associates, Inc	J-1 to J-7
Appendix: K – Big Econ River Basin Stormwater Management Master Plan	K-1 to K-3
Appendix: L – Excerpt from Orange County Public Schools	L-1 to L-2
Appendix: M – Excerpt from Harling Locklin & Associates, Inc	M-1 to M-12
Appendix: N – Excerpt from Kisinger Campo & Associates Corp	N-1 to N-2
Appendix: O – Correspondence	O-1 to O-9
Appendix: P – S.R. 50 Straight Line Diagram	P-1
Appendix: Q – Excerpt from S.R. 50 Original Construction Plans	Q-1 to Q-13
Appendix: R – Excerpt from Lochner	R-1 to R-17
Appendix: S – Excerpt from Comprehensive Engineering Services, Inc	S-1 to S-16
Appendix: T – Excerpt from CAD Engineering Design, Inc.	T-1 to T-2
Appendix: U – Excerpt from The Civil Design Group	U-1 to U-2
Appendix: V – Excerpt from Glace & Radcliffe, Inc	V-1
Appendix: W – Excerpt from Avalon II Plans	W-1 to W-4
Appendix: X – S.R. 50 Field Visit Photos	X-1 to X-11
Appendix: Y – Excerpt from Waterford Lakes Town Center	Y-1 to Y-2



EXECUTIVE SUMMARY

The purpose of the S.R. 408 Eastern Extension Project Development and Environment (PD&E) study is to develop a proposed improvement strategy that is technically sound, environmentally sensitive and publicly acceptable. As with every PD&E study, emphasis has been placed on the development, evaluation and documentation of detailed engineering and environmental studies including data collection, conceptual design, environmental analyses, project documentation and the preparation of a Pond Siting Report. The project is located in Orange County, Florida.

The Central Florida Expressway Authority (CFX) is presently evaluating the potential to expand S.R. 408 from its current eastern terminus at S.R. 50, locally known as East Colonial Drive, to S.R. 520 in northeast Orange County. This new seven-mile eastern extension of S.R. 408 would constitute the first stage towards providing a west-east high-speed corridor with future connectivity to I-95; enhancing safety, capacity and mobility for the region and CFX customers. After a comprehensive evaluation process, the preferred alternative was selected as being the most effective option within the project study area. Upon completion of the generation of various typical sections, horizontal alignment combinations, and public involvement effort a recommended alternative was selected. Please refer to the typical section in **Appendix-D**.

The proposed S.R. 408 Eastern Extension project is divided into three segments based on the land use characteristics. Segment 1 is more urban in nature and exhibits a higher traffic demand than Segments 2 and 3. Segment 1 is from beginning of the S.R. 50/S.R. 408 interchange to Avalon Park Boulevard. Segments 2 and 3 exhibit more of a rural tendency, beginning east of Avalon Park Boulevard to S.R. 520 at the east end of study area. The purpose of this Pond Siting Report (PSR) is to identify and discuss the stormwater management facilities for each of the 15 drainage basins within the project corridor. Two alternative pond sites were evaluated for each on-site drainage basin. Hydrology and pond sizing calculations are provided in **Appendix-F**.

Existing Drainage Conditions

The proposed S.R. 408 Eastern Extension corridor is located within the jurisdiction of the St. Johns River Water Management District (SJRWMD) and hydrologically within the Big Econ Drainage Basin. The project discharges into the Econlockhatchee (Econ) River, which is a tributary of the St. Johns River. The Econ River drainage basin drains from the south to the north. Since this is a new alignment, the proposed on-site drainage basins are located within various land uses of which are urban, built-up, and wooded/wetland. The drainage conditions for the urban and built-up land uses consists of curb and gutter and open swales that collect the runoff and discharge it to existing retention facilities. Stormwater runoff from the wooded areas drain into existing wetlands or low-lying areas that are connected to the Econ River tributaries.

The proposed S.R. 408 Eastern Extension corridor is a new alignment; therefore, there



are no existing cross drains or bridge crossings located along the project corridor. The corridor crosses over the Econ River, Econ River Tributaries, and wetlands. Runoff from the proposed corridor drains to low-lying areas, such as wetlands and creeks that are connected to the Econ River. The Econ River is listed as an Outstanding Florida Waters (OFW) per the Florida Department of Environmental Protection (FDEP). Projects that discharge into OFW require an additional 50% of treatment volume for proposed stormwater management facilities. The river is not listed for nutrient impairment; therefore, pollutant loading analysis is not required. The on-site drainage divides and basin limits are the same for existing and proposed conditions. A drainage map for existing condition was not prepared for this report since the on-site area foot print is the same as the proposed condition. Please refer to **Appendix-E** for the Project Overview Map.

The Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) for Orange County shows that a portion of the project lies within the 100-year floodplain areas Zone AE (100 year Base flood elevations are provided) and Zone A (100 year base flood elevations are not provided, areas with 1% change of flooding). Most of the project lies within flood Zone X (Areas of minimal flood hazard and above the 500-year flood zone). FEMA Map Nos. 12095C0280F, 129095C0285F, 12095C0295F and 12095C0315F, provide flood information for the project. Floodplain impacts occur throughout the project corridor. Refer to the FEMA Flood Insurance Rate Map in **Appendix-B**.

Proposed Drainage Conditions

Per the proposed typical section, roadway runoff will be mainly collected in shoulder gutter inlets and swales before it is piped to the recommended stormwater treatment pond. Water quality treatment and attenuation will be achieved through the construction of new wet detention ponds and expansion of existing ponds. Two alternative pond sites were identified for each basin. Based on the drainage evaluations, shown in the Pond Alternative Evaluation Matrices (**Page 5**), a recommended pond was identified for each basin. All on-site drainage basins are open basins. Two floodplain compensation ponds are proposed exclusively to provide compensation in Basin-11C. Some of the recommended stormwater ponds will provide additional floodplain compensation.

The project was divided into 15 on-site drainage basins. The drainage basins were divided based on high points of the proposed bridge overpass, which maintain flow connectivity to side streets. Scuppers may be used to collect runoff on the proposed bridges when the spread cannot be contained within the shoulder. Shoulder gutter inlets will be used to collect runoff from segments of the bridge with MSE walls and at high fill areas. Bridge drainage shall be evaluated during the design phase. Most of the offsite runoff flows into low lying areas such as wetlands and Econ River tributaries. The offsite runoff will be conveyed through the proposed cross drains. Some of the offsite runoff that drains into the project basin can be collected in by-pass swales at the toe of the embankment and directed to proposed cross drains per historical flow paths. There is enough right-of-way, 300 ft for the entire SR 408 corridor to provide by-pass swales.



other option is to collect offsite runoff in swales or ditch bottom inlets and route it through the stormwater ponds without providing treatment or attenuation.

Summary

The pond sizing analysis estimates right-of-way needs for the recommended pond using volumetric analysis, which accounts for water quality and attenuation. Please note that the pond location recommendations are based on preliminary data calculations, reasonable engineering judgment, environmental analysis and assumptions. This is a preliminary conceptual document; therefore, the pond sizes and locations may change during the final design as more information becomes available. Refer to **Table-1** for the recommended storm water ponds and Table-2 for the recommended floodplain compensation pond.

Refer to the Pond Alternative Evaluation Matrices (**Page 5**), for each on-site drainage basin. The Pond Alternative Evaluation Matrices summarize the on-site basin information, including jurisdictional agency, attenuation and treatment volume required, impacts, and justification for each recommended stormwater pond.

Basin	Recommended Ponds	Pond Selection Justification
1	Pond 1A, 1B and	Ponds 1A, 1B, and 1C are the recommended options, since they are located within existing CFX R/W and do not require R/W acquisition. Converting existing Pond-11 into 3 new ponds contribute to minor surface water impacts.
2		Pond 2B is the recommended option due to cost savings and willingness of the Orange County School Board to work with this project for land acquisition. Pond 2B has enough storage to provide compensation for the impacted Orange County Pond.
3-4	Pond 3A and Pond 4A	Ponds 3A and 4A are the recommended option, since the ponds are located on vacant lots. The right-of-way acquisition estimates for the vacant lots are more economical and the lots are closer to the onsite basin.
5	Pond 5B	Pond 5B is the recommended option since there are no wetland impacts and it can provide floodplain compensation in addition to treatment and attenuation.
6-8	Pond 6B	Pond 6B was selected as the preferred option, since it could provide floodplain compensation in addition to treatment and attenuation and is located within remnant parcels from the S.R. 408 corridor. The proposed SR 408 alignment will severe the access road (Sherman St and Caudle St) connecting homes south of the alignment. A large Pond 6B will be placed at the location of the homes that will be impacted by the proposed corridor.

Table-1 Summary of Recommended Water Quality Treatment & Attenuation Ponds



Table-1 Summary of Recommended Water Quality Treatment & Attenuation Ponds(Continued)

Basin	Recommended Ponds	Pond Selection Justification
9-10	-	Interconnected Ponds 9B and 10B are the recommended alternate pond sites due to cost savings and minor wetland impacts.
11A	Pond 11A1, Pond 11A2, Pond 11A3, and Pond 11A4	Pond Alternative-2 is the recommended option since all the infield ponds will be within existing CFX R/W, there are no impacts to floodplains or wetlands, and the parcel is more economical. Some of the offsite Pond 11A4 is located on a private property that will be impacted by the S.R. 408 corridor; therefore, the parcel could be purchased together with the roadway R/W acquisition.
11B	Pond 11B1	Pond 11B1 was selected as the recommended pond site due to minor wetland impacts. The property is owned by FDOT; therefore, the property will be easier to acquire.
11C	Pond 11C	Pond 11C is the recommended alternative since it is not located in a wetland, is more economical, and has no impacts to residential properties.
12	Pond 12A	Pond 12A is the recommended option since there are no impacts to residential properties, the parcel is larger, and the parcel is more economical.
13		Pond 13B is the recommended option, since the pond site is within the remnant parcels and does not have any wetland impacts.
14		Pond 14A is the recommended option since the pond site is located within remnant parcels, which is more economical.
15	Pond 15A	Pond Alternative-1, Pond 15A is the recommended option. This pond could provide flood relief for the surrounding area and provide water quality treatment for the proposed S.R. 408 corridor. Additionally it could provide compensation volume for the impacted Pond M-1.

Table-2 Summary of Recommended Floodplain Compensation Ponds

Basin	Recommended Ponds	Pond Selection Justification
11C	11C3 & 11C4	Both Ponds 11C3 and 11C4 are the recommended floodplain compensation pond. Need both ponds to compensate impacts caused by the proposed roadway. No floodplain impact caused by the pond berms.



Pond Alternative Evaluation Matrix



	Basin 1		
Jurisdiction	SJRWMD		
Open Basin: Use existing control structure from the meBasin Type and Outfall Location:Pond-11. Positive discharge via control structure into ewetlands to the east and into un-named Econ River Tri			
Required Treatment and Attenuation Volume	6.74 ac-ft		
-	nd 1C are located in the infield areas, where existing Pond-11 is osed roadway geometry converting into an interchange, the nd expanded into 3 new ponds.		
Pond ID	Alternative-1: Pond 1A, Pond 1B and Pond 1C		
Treatment and Attenuation Volume provided	6.74 ac-ft		
Surface Water Impact	3.55 ac		
Threatened or Endangered Species Impacts	None		
Floodplain	None		
Contamination	None		
Archeological Impacts	Low		
Major Utility Conflict Potential (Y/N)	None		
Pond Station	392+00, 400+00, 388+00		
Pond Right-of-way	8.14 ac		
Right-of-way Acquisition Estimates	None		
Location/Parcel Number	Existing CFX Property		
	and 1C are the recommended options, since they are located withir re R/W acquisition. Converting existing Pond-11 into 3 new ponds impacts.		

	Basin 2			
Jurisdiction	SJRWMD			
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.			
Required Treatment and Attenuation Volume	7.43 ac-ft			
Pond Alternative-1: Pond 2B, is locat is located on the west side of the Bri into wetlands, which are connected and will not impact either wetlands	dgeway Neighborhood. It will be a to a Econ River Tributary. The pon	wet pond and will discharge		
Pond Alternative-2: Pond 2C, is locat located. It is right next to S.R. 50 and located in the southwest corner of the	d it is a frontage property. This po	nd will discharge into wetlands		
Pond ID	Pond 2B Pond 2C			
Treatment and Attenuation Volume provided	7.43 ac-ft	7.43 ac-ft		
Jurisdictional Wetland Impact	None	None		
Threatened or Endangered Species Impacts	None	None		
Floodplain	None	None		
Contamination	None	None		
Archeological Impacts Low Low				
Archeological Impacts	Low	Low		
Archeological Impacts Major Utility Conflict Potential (Y/N)	Low None	Low		
Major Utility Conflict Potential				
Major Utility Conflict Potential (Y/N)	None	None		
Major Utility Conflict Potential (Y/N) Pond Station	None 420+00	None 440+00		

Pond Alternative-1: Pond 2B is the recommended option due to cost savings and willingness of the Orange County School Board to work with the project for land acquisition. Pond 2B has enough storage to provide compensation for the impacted Orange County Pond.

	Basin 3-4		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.		
Required Treatment and Attenuation Volume	4.87 ac-ft		
Pond Alternative-1: Pond 3A and Pond Palm Road. The ponds will be intercon connected ponds will discharge into w the west side of the pond. The existing flood elevation; therefore, there will b Pond Alternative-2: Pond 3B, is located An extended conveyance pipe system runoff into the pond, which could be of the pond. No major floodplain or wetl	nnected as a single stormwa vetlands that are connected g ground elevation at the po- be no floodplain impacts. d on a private property that along Lone Palm Road will costly. This pond will discha	ater management facility. The to a Econ River Tributary located on ond site is higher than the 100-year t is away from the project corridor. be required to carry the roadway rge into wetlands on the west side of	
located within the remnant parcels of the self-storage facility, Pond 4B and t be investigated during the final design to a Econ River Tributary.	the self-storage facility. De the existing pond could be r n phase. Pond 4B will discha	pending on the final acquisition of nerged together; this option should rge into wetlands that are connected	
Pond ID	3A and 4A	3B and 4B	
Treatment and Attenuation Volume provided	4.87 ac-ft	4.87 ac-ft	
Jurisdictional Wetland Impact	None	None	
Threatened or Endangered Species Impacts	None	None	
Floodplain	None	None	
Contamination	None	None	
Archeological Impacts	Moderate	Low	
Major Utility Conflict Potential (Y/N)	None	None	
Pond Station	450+00, 460+00	446+00, 464+00	
Pond Right-of-way	4.86 ac	5.43 ac	
Right-of-way Acquisition Estimates	\$133,343	\$1,045,353	
	Pond 3A: 23-22-31-0000-00-22 23-22-31-0000-00-021 23-22-31-0000-00-023	Pond 3B: 23-22-31-0000-00-079	
Location/Parcel Number	Pond 4A: 24-22-31-0000-00-010 24-22-31-0000-00-012 24-22-31-0000-00-13 24-22-31-0000-00-005	Pond 4B: Amsdell Storage Ventures XXII LLC 24-22-31-0000-00-049	

Pond Alternative-1: Ponds 3A and 4A are the recommended option, since the ponds are located on vacant lots. The right-of-way acquisition estimates for the vacant lots are more economical and the lots are closer to the onsite basin.



	Basin 5		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.		
Required Treatment and Attenuation Volume	3.52 ac-ft		
Pond Alternative-1: Pond 5A is located corridor. The pond site is on a private There will be no floodplain impacts du will be at the existing ground elevatior	property. The pond is located i e to the pond berm since the b	n FEMA floodplain Zone AE. back of the maintenance berm	
Pond Alternative-2: Pond 5B is located proposed corridor. The pond site is on quality, attenuation, and floodplain co A. There will be no floodplain impacts	a private property. This pond work of the property of the pond is located as the pond is the pond is located as the pond is located as th	will be utilized to provide water ed within FEMA floodplain Zone	
will be at the existing ground elevation			
		5B	
will be at the existing ground elevation	n.		
will be at the existing ground elevatior Pond ID Treatment and Attenuation Volume provided	n. 5A	5B	
will be at the existing ground elevatior Pond ID Treatment and Attenuation Volume	n. 5A 3.52 ac-ft	5B 4.07 ac-ft	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts	n. 5A 3.52 ac-ft 0.78 ac	5B 4.07 ac-ft None	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species	n. 5A 3.52 ac-ft 0.78 ac None	5B 4.07 ac-ft None None	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts Floodplain Contamination	n. 5A 3.52 ac-ft 0.78 ac None None	5B 4.07 ac-ft None None None	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts Floodplain Contamination Archeological Impacts	n. 5A 3.52 ac-ft 0.78 ac None None None	5B 4.07 ac-ft None None None None	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential (Y/N)	n. 5A 3.52 ac-ft 0.78 ac None None None Low	5B 4.07 ac-ft None None None None Low	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts Floodplain	n. 5A 3.52 ac-ft 0.78 ac None None None Low None	5B 4.07 ac-ft None None None Low None	
will be at the existing ground elevation Pond ID Treatment and Attenuation Volume provided Jurisdictional Wetland Impact Threatened or Endangered Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential (Y/N) Pond Station	n. 5A 3.52 ac-ft 0.78 ac None None Low None 487+00	5B 4.07 ac-ft None None None Low None 487+00	

Although, Pond 5A could be used as floodplain compensation pond if necessary. Both pond sites are located within conservation easements, and mitigation is expected.



	Basin 6-8		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.		
Required Treatment and Attenuation Volume	9.21 ac-ft		
Pond Alternative-1: Ponds 6A, 7A and 7B are lo proposed corridor. All of Pond 6A is located in p Board property. The ponds are not located wit from the S.R. 408 project. The site will have min than the 100-year flood elevation; therefore, th attenuation.	private property and part of 7A ar hin FEMA floodplains or wetlands nimal impacts to existing homes. his pond could also provide floodp	nd all of 7B are located in C 5. The pond site mostly con The normal water elevation blain compensation in addi	Drange County School Isists of remnant parcels n at Pond 6A is lower tion to treatment and
Pond Alternative-2: Pond 6B is located in Water The pond site is on a private property. The pone of remnant parcel from the S.R. 408 project and these properties. The Pond 6B site is located a Therefore, the larger Pond 6B will provide subs	d is not located within FEMA flood d some new home parcels that wi djacent to a floodplain and the SH tantial amount of floodplain comp	dplains or wetlands. The po Il be impacted by eliminati HWT is lower than the 100- pensation.	ond site mostly consists ing the access road to -year flood elevation.
Pond ID	6A, 7A, 7B	-	В
Treatment and Attenuation Volume provided	9.21 ac-ft	9.21	ac-ft
Jurisdictional Wetland Impact	None	Nc	one
Threatened or Endangered Species Impacts	None	No	one
Floodplain	None	Nc	one
Contamination	None	None	
Archeological Impacts	Low	Lc	w
Major Utility Conflict Potential (Y/N)	None	No	one
Pond Station	515+00, 526+00, 527+00	517	'+00
Pond Right-of-way	5.04 ac, 2.63 ac, 4.87 ac	19.7	'3 ac
Right-of-way Acquisition Estimates	\$562,910, \$249,535, \$411,427	\$1,15	5,892
Location/Parcel Number	Pond 6A: 19-22-32-7976-00-074 19-22-32-7976-00-080 19-22-32-7976-00-097 19-22-32-7976-00-092 19-22-32-7976-00-075 19-22-32-2484-00-050 19-22-32-2484-00-060 19-22-32-2484-00-220 Pond 7A: School Board of OC 19-22-32-2484-00-250 Pond 7B: School Board of OC 19-22-32-0000-00-007	19-22-32-7976-00-074 19-22-32-7976-00-072 19-22-32-7976-00-091 19-22-32-2484-00-110 19-22-32-2484-00-130 19-22-32-2484-00-150 19-22-32-2484-00-170 19-22-32-2484-00-190 19-22-32-2484-00-32 19-22-32-2484-00-34 19-22-32-2484-00-36	19-22-32-7976-00-075 19-22-32-7976-00-098 19-22-32-2484-00-100 19-22-32-2484-00-120 19-22-32-2484-00-140 19-22-32-2484-00-180 19-22-32-2484-00-31 19-22-32-2484-00-33 19-22-32-2484-00-35

Pond Alternative-2: Pond 6B was selected as the preferred option, since it could provide additional floodplain compensation in addition to treatment and attenuation, and is located within remnant parcels from the S.R. 408 corridor.

SJRWMD				
SJRWMD				
Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary and through pipes directly into Econ River.				
5.82 ac-ft				
rcels from the proposed S.R. 408 corridor. The site of henney Highway. The pond is not located within FE lite will impact any homes within the parcel. Pond that are north of proposed corridor. All of the hom	contains single family EMA floodplains or 10A is located on a private nes will be impacted within			
re within remnant parcels from the S.R. 408 corrido vill discharge directly into the Econ River. No wetla	or. The pond sites have nd or floodplain impacts are			
9A and 10A	9B and 10B			
5.82 ac-ft	5.93 ac-ft			
0.12	None			
None	None			
None	None			
None	None			
Low	Low			
None	None			
564+00, 575+00	568+00, 573+00			
5.48 ac	8.38			
\$578,690	\$379,750			
Pond 9A: 19-22-32-7876-04-020 19-22-32-7876-04-010 19-22-32-7880-02-120	Pond 9B: 19-22-32-7880-02-151 19-22-32-7880-02-161 19-22-32-7880-02-183			
Pond 10A: 19-22-32-7880-02-134 19-22-32-7880-02-135 19-22-32-7880-02-152 19-22-32-7880-02-163 19-22-32-7880-02-172 19-22-32-7880-02-160 19-22-32-7880-02-153 19-22-32-7880-02-133 19-22-32-7880-02-132 19-22-32-7880-02-136	Pond 10B: 19-22-32-7880-02-172 19-22-32-7880-02-181 19-22-32-7880-02-201 19-22-32-7880-02-212 19-22-32-7880-02-203 19-22-32-7880-02-180			
	Econ-River Tributary and through pipes directly in5.82 ac-ftlocated south of Old Chenney Highway just east of rrcels from the proposed S.R. 408 corridor. The site of henney Highway. The pond is not located within FE site will impact any homes within the parcel. Pond 3 that are north of proposed corridor. All of the hom podplain impacts are anticipated at this pond site loc d 10B will be interconnected. The ponds are locate re within remnant parcels from the S.R. 408 corridor will discharge directly into the Econ River. No wetlan there will be few residential homes impacted by the 9A and 10A9A and 10A5.82 ac-ft0.12NoneNoneLowNoneS64+00, 575+005.48 ac\$578,690Pond 9A: 19-22-32-7876-04-020 19-22-32-7880-02-134 19-22-32-7880-02-135 19-22-32-7880-02-152 19-22-32-7880-02-163 19-22-32-7880-02-153 19-22-32-7880-02-153 19-22-32-7880-02-153			

	Basin 11A				
Jurisdiction	SJRWMD				
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.				
Required Treatment and Attenuation Volume	5.27 ac-ft				
Pond Alternative-1: Basin-11A is the new interchange at the Chuluota Rd Extension. Three infield ponds and an offsite pond 11A4 are interconnected to provide required water quality treatment and attenuation. All infield ponds are located within the CFX R/W and the offsite pond is located on a private property. The Pond 11A4 site is currently a plant nursery. Minor impact to wetland and no impact to floodplain.					
Pond Alternative-2: A large single por Pond 11A5 is located on a private pro the parcel could be purchased togeth wetlands or floodplains.	operty that will be impacted by the	S.R. 408 corridor; therefore,			
Pond ID	Pond 11A1, Pond 11A2, Pond 11A3, and Pond 11A4 Pond 11A5				
Treatment and Attenuation Volume provided	5.27 ac-ft	5.27 ac-ft			
Jurisdictional Wetland Impact (ac)	0.24	None			
Threatened or Endangered Species Impacts	S None None				
Floodplain	None	None			
Contamination	None	None			
Archeological Impacts	Low	Low			
Major Utility Conflict Potential (Y/N)	None	None			
Pond Station	585+00, 590+00, 585+00, 583+00 587+00				
Pond Right-of-way	5.76 ac	5.37 ac			
Right-of-way Acquisition Estimates	\$41,585	\$45,803			
Location/Parcel Number	Concepts in Greenery 20-22-32-0000-00-014	20-22-32-0000-00-061 20-22-32-0000-00-059			
Remarks	All infield ponds located in the proposed CFX R/W and a single offsite pond located in private property.				

Pond Alternative-1: Pond Alternative-2 is the recommended option since all of the infield ponds will be within existing CFX R/W, there are will be minor wetland impacts and no floodplain impact. Most of Pond 11A4 is located on a private property that will be impacted by the S.R. 408 corridor; therefore, the parcel could be purchased together with the roadway R/W acquisition. Drainage conveyance to the infield ponds and offsite pond 11A4 will be much easier from the Chuluota Rd extension.

	Basin 11B		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. Positive discharge via control structure into wetlands part of the Econ-River Tributary.		
Required Treatment and Attenuation Volume	2.71 ac-ft		
Pond Alternative-1: Pond 11B1 is lo currently owned by FDOT. The site impacts are not anticipated at the p Pond Alternative-2: Pond 11B2 is lo Road Extension and proposed Pond treatment for Walgreens, Burger Ki	is mostly in a wooded area. Flo oond site. cated within the infield areas k 11-B1 will impact an existing s ng ,and other businesses along	bodplain impacts and wetland behind Walgreens. The Chuluota stormwater pond that provides	
could be used as a joint use pond b			
Pond ID	Pond 11B1	Pond 11B2	
Treatment and Attenuation Volume provided	2.71 ac-ft	2.71 ac-ft	
Jurisdictional Wetland Impact (ac)	None	0.64	
Threatened or Endangered Species Impacts	None	None	
Floodplain	None	None	
Contamination	None	None	
Archeological Impacts	Low	Low	
Major Utility Conflict Potential (Y/N)	None	None	
Pond Station	4020+00	4028+00	
Pond Right-of-way	3.98 ac	2.3 ac	
Right-of-way Acquisition Estimates	TBD	\$127,345	
Location/Parcel Number	FDOT Property 20-22-32-0000-00-031	20-22-32-4910-00-001 20-22-32-4910-00-002 20-22-32-4910-00-030	

Pond Alternative-1: Pond 11B1 was selected as the recommended pond site due to no wetland impacts. The property is owned by FDOT; therefore, the property will be easier to acquire.

	Basin 11C		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. Pond 11C2 will discharge into low land areas or floodplain areas of the Econ River. Pond 11C will discharge into Channel E an Econ River tributary.		
Required Treatment and Attenuation Volume	4.36 ac-ft		
408 project. This pond is located a	at the low point of the roadway s anticipated for this alternative	. Due the high SHWT elevation this	
	ately owned property. The site h cated close to a floodplain, but c		
Pond ID	11C2	11C	
Treatment and Attenuation Volume provided	3.07 ac-ft	4.36 ac-ft	
Jurisdictional Wetland Impact (ac)	N/A	None	
Threatened or Endangered Species Impacts	N/A	None	
Floodplain	None	None	
Contamination	N/A	None	
Archeological Impacts	N/A	Moderate	
Major Utility Conflict Potential (Y/N)	None	None	
Pond Station	610+00	628+00	
Pond Right-of-way	7.5 ac	5.7 ac	
Right-of-way Acquisition Estimates	\$211,686 \$119,531		
Location/Parcel Number	29-22-32-7882-00-220 29-22-32-7882-00-240	29-22-32-6721-00-030 29-22-32-6721-00-020	

Pond Alternative-2: Pond 11C is the recommended alternative since it will not have wetland impact, is more economical, and has no impacts to residential properties.



	Basin 11C			
Jurisdiction	SJRWMD			
Basin Type and Outfall Location:	Open Basin. Pond 11C2 and 11C3 will discharge into low land areas or floodplain areas of the Econ River. Pond 11C will discharge into Channel E an Econ River tributary.			
site is mostly located in floodplain low at the pond site and the SHW	C3 is located in a remnant parcel f and wetland adjacent to Channel T is between 2 to 3 feet below gro fore, no floodplain impacts due to ite.	E. The existing ground elevation i und. The maintenance berm will		
site is on a privately owned prope	nnant parcel from the S.R. 408 proj erty. The site has junk yard operatic oodplains. The pond site is hydraul flood elevation.	on currently. The site has no		
Pond ID	11C3	11C4		
Provided Floodplain Compensation	21.80 ac-ft	14.93 ac-ft		
Jurisdictional Wetland Impact (ac)	N/A	None		
Threatened or Endangered Species Impacts	N/A	None		
Floodplain	None	None		
Contamination	N/A	Moderate		
Archeological Impacts	N/A	N/A		
Major Utility Conflict Potential (Y/N)	None	None		
	633+00	635+00		
Pond Station	8.85 5.5 ac			
Pond Station Pond Right-of-way	8.85	5.5 ac		
	8.85 \$119,127	5.5 ac \$34,999		

	Basin 12		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. The alternate ponds will discharge into low-lying areas that connected to Econ River tributary (Channel A).		
Required Treatment and Attenuation Volume	4.10 ac-ft		
Pond Alternative-1: Pond 12A is loca mostly a wooded area and is near a anticipated. No impact to residentia	power distribution line. No impac l properties either. The site is loca	t to wetlands or floodplains are ted at station 645+00.	
Pond Alternative-2: Pond 12B is loca mostly a wooded area with several r anticipated. There will be impacts to 653+00.	esidential homes. No impact to w	etlands or floodplains are	
Pond ID	12A	12B	
Treatment and Attenuation Volume provided	4.10 ac-ft	4.10 ac-ft	
Jurisdictional Wetland Impact (ac)	None	None	
6	Gopher Tortoise	Gopher Tortoise	
Species Impacts	Gopher Tortoise None	Gopher Tortoise None	
Species Impacts Floodplain	-		
Species Impacts Floodplain Contamination	None	None	
Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential	None	None	
Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential (Y/N)	None None Moderate	None None Low	
Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential (Y/N) Pond Station	None None Moderate None	None None Low None	
Threatened or Endangered Species Impacts Floodplain Contamination Archeological Impacts Major Utility Conflict Potential (Y/N) Pond Station Pond Right-of-way Right-of-way Acquisition Estimates	None None Moderate None 645+00	None None Low None 653+00	

Pond Alternative-1: Pond 12A is the recommended option since there are no impacts to residential properties, the parcel is larger, and the parcel is more economical.

	Basin 13		
Jurisdiction	SJRWMD		
Basin Type and Outfall Location:	Open Basin. The alternate ponds will discharge into low laying areas that is connected to Econ River tributary (Channel-A).		
Required Treatment and Attenuation Volume	6.51 ac-ft		
Pond Alternative-1: Pond 13A is loc land. No impact to wetlands or floc		e site consists of cleared pasture pact to residential properties either	
Pond Alternative-2: Pond 13B is loc located on a remnant parcel from t floodplains or residential propertie	he S.R. 408 corridor. Minor we	tland impacts are anticipated. No	
Pond ID	13A	13B	
Treatment and Attenuation Volume provided	6.51 ac-ft	6.51 ac-ft	
Jurisdictional Wetland Impact (ac)	None	0.16	
Threatened or Endangered Species Impacts	None	None	
Floodplain	None	None	
Contamination	None	None	
Archeological Impacts	Low	Low	
Major Utility Conflict Potential (Y/N)	None	None	
Pond Station	678+00	678+00	
Pond Right-of-way	8.01 ac	10.45 ac	
Right-of-way Acquisition Estimates	\$24,227	\$29,786	
Location/Parcel Number	22-22-32-0712-00-000 22-22-32-0712-36-001 22-22-32-0712-36-013 22-22-32-0712-36-021	22-22-32-0712-21-010 22-22-32-0712-37-001 22-22-32-0712-14-010 28-22-32-0000-00-008	

parcels and does not have any wetland impacts. Pond 13A would be a complete new purchase and has minor wetland impacts.

	Basin 14			
Jurisdiction	SJRWMD			
Basin Type and Outfall Location:	Open Basin. The alternate ponds will discharge into low laying areas that is connected to Econ River tributary.			
Required Treatment and Attenuation Volume	1.91 ac-ft			
Pond Alternative-1: Pond 14A is locate the project corridor and west of C.R. 1 project. The pond site has no resident	3. The pond site is locate	d within remnant parcels	from the S.R. 408	
Pond Alternative-2: Pond 14B is locate the project corridor and west of C.R. 1 floodplain impacts are anticipated. Th would have to be a complete new pur	3. The pond site will have is site will not be impacte	e some residential impact	s. No wetland or	
Pond ID	14	1A	14B	
Treatment and Attenuation Volume provided	2.19 ac-ft		1.91 ac-ft	
Jurisdictional Wetland Impact (ac)	No	one	None	
Threatened or Endangered Species Impacts	None		None	
Floodplain	Nc	ne	None	
Contamination	None		None	
Archeological Impacts	Low		Moderate	
Major Utility Conflict Potential (Y/N)	None		None	
Pond Station	710+00		710+00	
Pond Right-of-way	2.57 ac		2.75 ac	
Right-of-way Acquisition Estimates	\$58,641		\$340,686	
Location/Parcel Number	22-22-32-0712-20-150 22-22-32-0712-20-201 22-22-32-0712-20-035 22-22-32-0712-20-043 22-22-32-0712-20-510 22-22-32-0712-20-560	22-22-32-0712-20-017 22-22-32-0712-20-013 22-22-32-0712-20-045 22-22-32-0712-20-520 22-22-32-0712-20-054 22-22-32-0712-20-058	22-22-32-0712-18-410 22-22-32-0712-18-370 22-22-32-0712-18-470 22-22-32-0712-18-330 22-22-32-0712-18-430 22-22-32-0712-18-290 22-22-32-0712-18-260	
	22-22-32-0712-20-750	22-22-32-0712-20-060	22-22-32-0712-18-230 22-22-32-0712-18-190	

Pond Alternative-1: Pond 14A is the recommended option, since the pond site will be within remnant parcels, which is more economical. Pond 14B would have to be a complete new purchase.

Basin 15					
Jurisdiction	SJRWMD				
Basin Type and Outfall Location:	Open Basin. The alternate Pond 15A will discharge into low laying areas that is connected to Econ River tributary. Pond 15B and Pond M1 will discharge into Channel KE which is a Econ River tributary.				
Required Treatment and Attenuation Volume	6.16 ac-ft				
Pond Alternative-1: Pond 15A is l project corridor in a wooded area site has no residential impacts. N	a. The pond site is in the r	emnant parcel from the SF			
Pond Alternative-2: Pond 15B and infield area where the project co- is required for this pond site. Exis impacted Pond M-1 can be comp could be interconnected and be a connected with Pond M-2 and Po 408 extends beyond the current	nnects to SR 50. The pond sting Orange County Pond rensated in the infield area used as a joint use pond to ond-M3 currently. The infi	ls are located at station 74 M-1 will be impacted by t as. As an alternative optio ogether with Pond M-2 and	0+00. No additional R/W he SR 408 project. The n Ponds 15B and M1 d Pond M-3. Pond M-1 is		
Pond ID	15A	·			
Treatment and Attenuation Volume provided	6.16 ac-ft	6.16 ac-ft			
Surface water Impact	None 2.24 ac				
Threatened or Endangered Species Impacts	None	No	one		
Floodplain	None	No	one		
Contamination	None	No	one		
Archeological Impacts	Low	Mod	lerate		
Major Utility Conflict Potential (Y/N)	None	No	one		
Pond Station	725+00	740)+00		
Pond Right-of-way	8.92 ac	4.3	7 ac		
Right-of-way Acquisition Estimates	\$115,988 TBD				
Location/Parcel Number	27-22-32-0000-00-007 21-22-32-0735-00-001 21-22-32-0735-00-020 21-22-32-0735-00-030 21-22-32-0735-00-010 21-22-32-0735-00-062 21-22-32-0735-00-061 21-22-32-0735-00-063	-	ounty BCC 0800-00-450 21-22-32-0735-00-010 21-22-32-0735-00-091 21-22-32-0735-00-082 21-22-32-0735-00-072 21-22-32-0735-00-070 21-22-32-0735-00-061		

Pond Alternative-1: Pond 15A is recommended for Basin 15. Pond 15A could provide treatment, attenuation, floodplain compensation and compensation for possible elimination for Orange County Pond M-1.



1.0 INTRODUCTION

The vision of this enhanced west-east corridor has been documented in prior concept studies prepared by CFX including the S.R. 408 Eastern Extension Concept Development and Evaluation Study completed in 2008. The limits of this study generally extend from the current terminus of S.R. 408 at S.R. 50 to the vicinity of the S.R. 50/S.R. 520 intersection. The project location and vicinity are shown in **Appendix-A**. The preferred alignment for Segment 1 and Segment 2/3 and the proposed typical sections are provided in **Appendix-D**. The S.R. 408 Eastern Extension is one of Florida's Strategic transportation investments to support future growth and create connections between global trade activities, from the Orlando International Airport, and the University of Central Florida to Cape Canaveral.

This report discusses and analyzes the stormwater management plan for the project. The report identifies potential pond locations and discusses the right-of-way requirements associated with the recommended pond sites. A description for each of the proposed pond sites is in Section 5.2 of this report. Recommended and alternate pond site exhibits are located in **Appendix-E**.

Within the project vicinity, S.R. 50 is functionally classified as a major arterial facility and provides an important connectivity function between the Orlando area to the west and I-95 just south of Titusville to the east. As traffic continues to grow within the study area due to the projected development in the area, it is essential to maintain adequate mobility for the region. A new expressway facility not only improves mobility but significantly reduces the existing exposure to at-grade conflict points associated with traffic signals and local access issues. In summary, the proposed S.R. 408 Eastern Extension Project greatly enhances Central Florida's regional expressway needs and provides the initial phase of the ultimate vision of an expressway connection from Orlando to I-95.

2.0 PROJECT DESCRIPTION

The CFX is presently evaluating the potential expansion of S.R. 408 from its current eastern terminus at S.R. 50 (East Colonial Drive) and Challenger Parkway to S.R. 520 in northeastern Orange County. The recommended seven-mile eastern extension of S.R. 408 would constitute the initial stage of providing a west-east high-speed corridor with future connectivity to I-95, enhancing safety, capacity and mobility for the region and CFX customers. After a comprehensive evaluation process, the preferred alternative was selected as being the most effective option within the project study area. Upon completion of the generation of various typical sections, horizontal alignment combinations, and public involvement effort a recommended alternative was selected. Please refer to the recommended alignment in **Appendix-D**.

The proposed S.R. 408 Eastern Extension project is divided into three segments based on the land use characteristics. Segment 1 is more urban in nature and exhibits a higher traffic demand than Segments 2 and 3. Segment 1 is from beginning of the S.R. 50/S.R.



408 interchange to Avalon Park Boulevard. Segments 2 and 3 exhibit more of a rural tendency, beginning east of Avalon Park Boulevard to S.R. 520 at the east end of the study area.

3.0 DESIGN CRITERIA

The design of stormwater management facilities for this project are governed by the rules and criteria set forth by the St. Johns River Water Management District (SJRWMD) and the FDOT. The following criteria was obtained from the 2013 SJRWMD Applicant's Handbook and 2016 FDOT Drainage Manual.

Water Quality and Pond Recovery

- Wet Detention (SJRWMD)
 - 1. Water quality treatment Greater of 1" over the total basin or 2.5" over the impervious area
 - 2. Recovery One-half the treatment volume within the first 24 to 30 hours
- Dry Retention (on-line) SJRWMD
 - 1. Treatment Greater of 1" over the basin or 1.25" over the impervious area
 - 2. Recovery Treatment volume within 72 hours
- Outstanding Florida Water (OFW): Treat an additional fifty percent of the runoff volume
- Econ River Hydrology Basin Criteria (SJRWMD)
 - 1. Mean annual storm (2.3-year return period) with a total 24-hour rainfall depth of 4.5 inches.
 - 2. 25-year return period

Water Quantity

• Open basin post-development peak discharges shall be at or below predevelopment peak discharge for the 25-year/24-hour storm event.

Pond Design (FDOT Criteria)

- Ponds shall be designed to provide a minimum 20-foot of horizontal clearance between the top edge of the normal pool elevation and the right-of-way line. Maintenance berm shall be at least 20-feet with a slope of 1:8 or flatter.
- Corners of ponds shall be rounded to provide an acceptable turning radius for maintenance equipment (30-foot minimum inside radius).
- At least 1-foot of freeboard is required above the maximum design stage of the pond below the front of the maintenance berm.

4.0 EXISTING CONDITIONS

The proposed S.R. 408 Eastern Extension corridor is located within the jurisdiction of the St. Johns River Water Management District (SJRWMD) and hydrologically within the Big Econ Drainage Basin. The project discharges into the Econ River, which is a tributary of the St. Johns River. The Econ River is an Outstanding Florida Waters. The Econ River drainage basin drains from the south to the north. The on-site drainage basins are all open basins draining to the Econ River. The S.R. 408 Eastern Extension corridor is divided into 15 basins for stormwater management. The basin limits are shown in **Table-3**. The basin divides were based on a conceptual S.R. 408 Eastern Extension profile with high points and low points. The same basin divide limits were used for the proposed condition as well. An existing condition drainage map was not prepared for this report, since the on-site basin limits and right-of-way width are the same for the existing and proposed condition. Offsite drainage patterns remain the same. A general description of each existing basin is provided in **Section 4.4**.

Basin Name	From Station	To Station	Outfall Location	
Basin 1	380+15	404+95	Basin 1 discharges to the east of the proposed ramp into the Unnamed Econ River Tributary(1).	
Basin 2	404+95	441+95	Basin 2 discharges into low areas of wooded forest that flows into the Unnamed Econ River Tributary(1).	
Basin 3-4	441+95	478+50	Basin 3-4 flows to the South into the Unnamed Econ River Tributary(1).	
Basin 5	478+50	498+00	B+00 Basin 5 discharges into the Unnamed Econ River Tributary(2).	
Basin 6-8	498+00	552+23	552+23 Basin 6-8 discharges into wetlands that flow interesting the Unnamed Econ River Tributary(2).	
Basin 9-10	552+23	579+95	Basin 9-10 discharge into wetlands that flow we into the Econ River.	
Basin 11A	579+95	602+80	Basin 11A discharges into wetlands that flow west into the Econ River.	
Basin 11B	4012+98	4037+37	Basin 11B discharges into wetlands that flow wes	

Table-3 Summary of Existing and Proposed Condition Basin Limits



Table-3 Summary	of Existing and	Proposed Condition	Basin Limits (continued	D
				·/

Basin Name	From Station	To Station	Outfall Location
Basin 11C	602+80	629+50	Pond 11C2 discharges into wetland that flow west into the Econ River. Pond 11C, 11C3 and Pond 11C4 discharge into Channel E.
Basin 12	629+50	661+10	Pond 12A discharges into Channel E and Pond- 12B discharges into Channel A.
Basin 13	661+10	701+95	Basin 13 discharges into Channel A.
Basin 14	701+95	714+10	Basin 14 discharges into wetlands that flows west into the Econ River.
Basin 15	714+10	746+00	Pond 15A discharges into Channel KE and Pond 15B discharges into Channel M.

4.1 SOIL DATA

The NRCS Soil Survey of Orange County published by United States Department of Agriculture (USDA) has been reviewed for the project. The soil survey map, obtained from the NRCS USDA Soil Survey, for the project is shown in **Appendix-A**. The soil report for this project is also provided in **Appendix-C**. In general, the surficial soils consist of fine sand, mucky fine sand, muck and poorly drained soil. In general, the groundwater is at a depth of 0' to 3.5' below the existing ground. **Table-4** outlines the most occurring soils within the offsite pond area.

Soil No.	Orange County USDA Soil Name	Depth to Water Table (inches)	Hydrologic Soil Group
3	Basinger Fine Sand	0	A/D
15	Felda Fine Sand	0 to 6	A/D
20	Immokalee Fine Sand	6 to 12	B/D
34	Pomello Fine Sand	24 to 42	А
37	St. Johns Fine Sand	6 to 12	B/D
42	Sanibel Muck	0	A/D
44	Smyrna-Smyrna, Wet, Fine Sand	6 to 18	A/D
51	Wabasso Fine Sand	6 to 18	B/D
53	Wauberg Fine Sand	0 to 6	D
54	Zolfo Fine Sand	24 to 42	А

Table-4 USDA NRCS Soil Survey Information



4.2 LAND USE

The existing land use along the proposed S.R. 408 Eastern Extension corridor consists mostly of residential developments and undeveloped areas. The residential areas consist of both multi-family and single-family residences. The undeveloped areas are mostly wetlands and upland forests with conservation easements. Please refer to **Appendix-A** for a Land Use Map.

4.3 EXISTING CROSS DRAINS

Considering this is a new alignment, there are not any existing cross drains or bridge structures for review. However, existing cross drains upstream and downstream of the proposed alignment were taken into consideration to maintain functionality and to verify the recommended improvements do not adversely impact the overall drainage function. Refer to **Table-5** for existing S.R. 50 cross drain information. The S.R. 50 Straight Line Diagram is in **Appendix-P** and identifies each S.R. 50 cross drain. The culvert size and 50-Year DHW elevations were obtained from the construction plans in **Appendix-Q**, **Appendix-R**, and **Appendix-S**. There is no evidence of scour or sedimentation for any existing cross drain along S.R. 50. Refer to **Appendix-X** for photos of the existing S.R. 50 cross drains.

Cross Drain ID	Pipe Description	50-Year DHW EL (ft)	Date of Construction
S.R. 50 CD-1	2-8'x6' CBC	58.57	2012
S.R. 50 CD-2	2-24" RCP	53.53	2012
S.R. 50 CD-3	2-12.95'x8.5' CBC	50.04	2012
S.R. 50 CD-4	1-30" RCP	54.68	2012
S.R. 50 CD-5	3-10'x6' CBC	43.70	1960
S.R. 50 CD-6	3-36" RCP	59.10	1960
S.R. 50 CD-7	1-4'x4' CBC & 1-54" RCP Jointed	59.10	1960
S.R. 50 CD-8	1-30" RCP	66.50	1960
S.R. 50 CD-9	1-8'x7' CBC	54.80	1960
S.R. 50 CD-10	1-10'x4' CBC	60.80	1960
S.R. 50 CD-11	1-24" RCP	61.60	1960

Table-5 Existing S.R. 50 Cross Drain General Information



4.4 EXISTING DRAINAGE BASIN CHARACTERISTICS

Basin 1 begins at station 380+15 and ends at 404+95, which is just south of the S.R. 408 and S.R. 50 interchange. This basin includes the existing S.R. 408 east and west bound lanes. Stormwater treatment and attenuation for Basin 1 is provided in existing Pond 11. This segment of project was initially permitted in 1987 by CFX with SJRWMD (Permit #4-095-20358-2). Subsequently, this permit was modified to accommodate various design modifications such as the recent S.R. 50 widening project at the S.R. 408 Interchange. Existing Pond 11 outfalls east towards the wetlands into Unnamed Econ River Tributary(1) that ultimately drains into the Econ River.

Basin 2 begins at station 404+95 and ends at station 441+95. The beginning of the basin includes the portion of S.R. 408 at the S.R. 50 interchange. The end of the basin cuts through part of the existing Winn-Dixie Supermarket. The middle part of the basin traverses through wooded areas. This basin also cuts through one of the three existing Orange County ponds (**Appendix-E**) that is located south of the Volkswagen Car Dealership. The existing Orange County ponds are wet retention ponds that were donated to the county by the Waterford Lakes development. Additional information about these ponds are not available at this time. Runoff from this basin generally flows into low areas of the wooded forest to the Unnamed Econ Tributary(1) and ultimately drains into the Econ River.

Basin 3-4 were merged as a single basin to evaluate alternative pond sites.

Basin 3, from station 441+95 to station 456+20, consists of upland forests, which are located within Flood Zone A. This basin contains Unnamed Econ River Tributary(1), which flows north to the Econ River and crosses S.R. 50 via an existing double 12.95' wide by 8.5' high box culvert crossing.

Basin 4, from station 456+20 to station 478+50, consists of residential and commercial developments as well as upland forests. The general flow of this basin is to the southeast and ultimately to the Econ River. The residential area includes the Deerwood Manufactured Home Community as well as single family housing. Compass Self Storage is located within the basin. There are SJRWMD permits for both Deerwood Manufactured Home Community and Compass Self Storage, 4-095-20418 and 40C-100527, respectively. The basin generally flows to the south to Unnamed Econ River Tributary(1).

Basin 5 begins at station 478+50 and ends at station 498+00. Basin 5 includes the Deerwood Manufactured Home Community east of Pell Street, upland forests and wetlands to Avalon Park Blvd. As previously stated, the Deerwood Manufactured Home Community is permitted under SJRWMD permit 4-095-20418. The upland forest and wetland areas are permitted under SJRWMD permit 40C-20959 as part of the Colonial Sunflower development. This basin discharges into Unnamed Econ River Tributary(2), which flows north to the Econ River and crosses Avalon Park Boulevard via an existing seven barrel 8' wide by 5' high box culvert crossing.



Basin 6-8, begins at station 498+00 and ends at station 552+23, which continues from Avalon Park Boulevard east to middle of Econ River. Basin 6-8 is a mixed land use of upland forests, wetlands, and residential areas. The upland forest and wetland areas are permitted under SJRWMD permit 40C-20959 as part of the Colonial Sunflower development. This basin consists of Unnamed Econ River Tributary(2), which flows north to the Econ River and crosses Faberge Drive via an existing four barrel 34" x 53" ERCP culvert crossing. The upland forest and wetland areas further east of the basin is permitted under SJRWMD permit 40C-20959 as part of the northeastern-most portion of the Colonial Sunflower development. The runoff from this basin flows south to the Econ River and crosses Faberge Drive via an existing four barrel 34" x 53" ERCP culvert crossing. The upland forest and wetland areas further east of the basin is permitted under SJRWMD permit 40C-20959 as part of the northeastern-most portion of the Colonial Sunflower development. The runoff from this basin flows south to the Econ River and crosses Faberge Drive via an existing four barrel 34" x 53" ERCP culvert crossing. The remaining segment of the basin that crosses a portion of the Econ River is in a floodway (Zone AE). The previous Old Cheney Highway bridge crossing the Econ River serves as the basin boundary. The existing bridge has since been removed.

Basin 9-10 were merged together as a single basin to evaluate alternative pond sites.

Basin 9, from station 552+23 to 569+20, crosses the Econ River and consists of floodplains (Zone AE). The previous Old Cheney Highway bridge crossing the Econ River serves as the basin boundary for these two basins. The existing bridge has since been removed.

Basin 10, from station 569+20 and to station 579+95, includes wooded areas and rural residential land uses from Hamilton Drive to Lockwood Drive. This basin generally drains west to the Econ River.

Basin 11 begins at station 579+95 and ends at station 629+50. This basin is a large basin, therefore, it is further sub-divided into Basins 11A, 11B and 11C. Basin 11B, from station 4012+98 to 4037+37, represents the C.R. 419 Extension and access road to East River High School, while Basins 11A and 11C represent the S.R. 408 Extension and interchange. Basin 11A is from station 579+95 to 602+80 while Basin 11C is from station 602+80 to 629+50. This basin includes rural residential, commercial, upland forests and wetland land uses. It follows the east bank of the Econ River before starting a gradual turn to the east and ending west of Pine Isle Drive. The runoff from this basin generally drains west to the Econ River.

Basin 12 begins at station 629+50, west of Pine Isle Drive and ends at station 661+10 near Cochran Trail. The basin also crosses an auto junk yard and small modular home community. Some of the basin runoff drains into Channel E and the rest of the basin runoff drains to Channel A; both channels drain into the Econ River.

Basin 13 begins at station 661+10 and ends at station 701+95. Picking up at Cochran Trail, Basin 13 continues east to North 5th Street. This basin is predominantly agricultural land use. The runoff from this basin generally flows west in Channel A, which flows into the Econ River.

Basin 14 begins at station 701+95 and ends at station 714+10. Continuing east from



North 5th Street, Basin 14 consists of rural residential areas and ends at County Road 13. The runoff from this basin generally flows west towards the Econ River.

Basin 15 begins at station 714+10 and ends at station 746+00. The basin traverses eastward through some residential areas and finally ties into S.R. 50. The basin mainly consists of wooded areas and some residential areas. The basin also impacts existing Orange County Pond M-1. Runoff from this basin generally drains into collection ditches that are a part of Channel KE and Channel M, which flow into the Econ River. The historical conveyance flow path and existing channels identified in the Bithlo Area Stormwater Management Master Plans at this basin location are depicted in the drainage overview map (**Appendix-E**).

5.0 PROPOSED CONDITIONS

The stormwater runoff from proposed impervious areas will be treated in existing and proposed stormwater facilities. The runoff from the proposed alignment will be collected in roadside swales and closed storm sewer systems, then directed to stormwater ponds for each respective basin. Water quality treatment and attenuation will be achieved from the construction of new wet detention ponds and the expansion of existing ponds. There is a total of 15 basins within the project limits.

The proposed design will incorporate a 300-ft right-of-way from the existing S.R. 408 interchange to the end of the project at S.R. 50. The C.R. 419 extension will maintain a right-of-way of approximately 102 ft from the interchange to S.R. 50.

Two alternative pond sites were evaluated for each basin. Based on the pond alternative evaluation matrix analysis, a preferred pond site was selected. The preferred pond sites were selected based on the cost for pond right-of-way acquisition, wetland and floodplain impacts, and site contamination. The final preferred pond sites for each basin are provided in the Pond Alternative Evaluation Matrices (**Page 5**).

5.1 METHODOLOGY OF POND DETERMINATIONS

Based on the available information, only hydraulically feasible and environmentally permittable pond sites were considered for the final preferred pond locations. Potential pond sites were analyzed and evaluated using the following parameters:

- Hydrologic and hydraulic factors such as existing ground elevations, soil types, estimated seasonal high water table (SHWT) established by a review of the USDA NRCS soils and geotechnical investigations, stormwater conveyance feasibility, allowable hydraulic grade line (HGL), and basin outfalls
- Cultural resource impacts
- Environmental resource impacts, including wetlands and threatened or endangered species
- Floodplain impacts
- Major utility conflict potential



• Hazardous materials and contamination

Please note that the information for environmental impacts, cultural resource impacts, and hazardous materials and contamination impacts are included in the Pond Alternative Evaluation Matrices (**Page 5**).

Pond Site Determination and Sizing

Most of the proposed pond sites are located on remnant parcels from the proposed S.R. 408 alignment. The alternative ponds sites were proposed in areas that have minimal impacts to wetlands, residential areas, and floodplains. Pond sites were also identified based on the ownership of the property; sites that are owned by CFX, Orange County, and the Orange County School Board are easier to acquire. All proposed ponds were designed as wet detention ponds.

Each pond size was estimated based on the best available data from each pond site location. Seasonal high water table (SHWT) elevations at each pond site were estimated based on the soil type from USDA NRCS Soil Survey for Orange County and SHWT from existing permits. Please refer to **Table-4** for soil type and the Pond Analysis Summary Table (**Page 41**) for estimated SHWT elevations for each respective pond.

The following method was used to determine the pond size:

- 1. Total basin area and impervious areas for pre and post development conditions were determined. Total basin areas for pre and post development conditions are the same.
- 2. Per CFXs' request, the entire 64' median was assumed as an impervious area for sizing the ponds for consideration of eventual build-out.
- 3. Pre and post development runoff volume was calculated using the SCS runoff calculation method, for 25yr-24hr storm (SJRMWD) and critical duration storms (FDOT) for 100yr-240hr and 100yr-8hr.
- 4. Maximum attenuation volume produced by the storm events mentioned above was calculated by the difference between post and pre development runoff.
- 5. Water quality volume based on SJRWMD criteria of 1" over the total basin or 2.5" over the impervious areas were calculated. An additional 50% treatment volume was added to the largest treatment volume since this project discharges into an OFW.
- 6. Both calculated attenuation volume and water quality treatment volume were added together to compute the total storage volume required for sizing the pond. This is a conservative approach to add both treatment and attenuation volume to size the pond.
- 7. Side slopes of 1:4 and 1-ft freeboard was used. The 1-ft freeboard is between the inside edge of the berm and the (treatment + attenuation) stage.
- 8. Maintenance berm width was kept at 20-ft wide.
- 9. Based on the SHWT elevation from USDA NRCS Soil Survey report and SHWT from existing project ponds. The ponds were sized using a volumetric method.



5.2 PROPOSED DRAINAGE BASINS AND PONDS

The preferred alternative was ultimately determined to be the most ideal corridor for the extension of S.R. 408. The roadway geometry is limited in order to minimize impacts and meet the requirements for the proposed design speed. The proposed design speed from the beginning of the project to the east side of Avalon Park Blvd is 65 mph and from the east side of Avalon Park Blvd to the end of the project the design speed is 70 mph. Different interchange layouts and considerations were made to provide alternative conceptual designs. Pond locations were determined once the alignment and the most effective interchange layouts were identified. All ponds were designed to be wet detention ponds and all on-site basins are open basins. The proposed corridor consists of many bridges. This has resulted in the profile being elevated. The elevated profile will accommodate the conveyance swales or closed drainage system above the proposed cross drain structure without any conflict, before discharging into respective stormwater treatment ponds.

Basin 1

This basin includes portions of the proposed on and off ramps and the new alignment that turns towards the east. Runoff from the proposed new alignment mainline and ramps will be treated in the same existing Pond-11 by expanding it. Due to the geometry of the proposed interchange, the existing Pond-11 will be expanded and divided into 3 separate infield ponds connected by equalizer pipes. The proposed ponds are named Pond 1A, 1B and 1C. The storage volume for all three ponds is sufficient enough to provide required treatment and attenuation for Basin-1. The existing outfall structure will remain at the same location, where it discharges to the wooded areas to the east. However, the control structure will have to be modified if necessary to accommodate additional runoff from the proposed alignment. The existing SJRWMD Permit #20358-24 for Pond-11 will need to be modified. An alternate pond site is not required since proposed Pond 1A, 1B, and 1C are located within CFX right-of-way. Refer to the Alternative Pond Site Map (Appendix-E) for the location of existing Pond-11 and the proposed Ponds 1A, 1B, and 1C. Existing Waterford Lakes Town Center Pond-98 (Permit # 19979-39) might be impacted by this project. Coordination with the Town Center should take place during the final design to mitigate the impact.

Basin 2

The proposed S.R. 408 Eastern Extension alignment will turn towards the east just south of the Volkswagen dealership. This basin will include on and off ramps from existing S.R. 408 to the proposed S.R. 408 Eastern Extension alignment. The new alignment will fill in one of the three wet retention ponds owned by Orange County. According to Orange County, these 3 ponds were donated to the county by Waterford Lakes. Additional information about these existing ponds are not available at this time. The impacted Orange County pond can be compensated in either one of the alternate Ponds 2B or 2C. The other option for compensation is to reshape the other two existing Orange County Ponds; however, reshaping the existing ponds were not considered as joint use ponds,



since they will create floodplain and wetland impacts. However, details about the existing ponds and using them as joint use ponds should be explored during the final design. The proposed alignment also will have minor impact to the existing University Medows Pond-A. This impact is very minor and this can be compensated in the proposed pond. Two alternative pond sites were identified for this basin as Pond 2B and Pond 2C. Runoff for Basin 2 will be collected in roadside swales and shoulder gutter inlets at the bridge approaches before discharging into the alternate ponds 2B or 2C. Pond 2B is located on property owned by the Orange County School Board and Pond 2C is located on a private property that contains a Winn-Dixie Supermarket. Based on the pond alternative evaluation matrix analysis, Pond 2B is the preferred pond site. Pond 2B was selected due to cost savings and willingness of the Orange County School Board to work with the project for land acquisition. Pond 2B also provides a large quantity of floodplain compensation.

Basin 3-4 were merged as a single basin to evaluate the alternative pond sites.

Two alternate pond sites, Pond 3A and 3B, were identified for Basin-3. Pond 3A is located on remnant parcels that will be impacted by the proposed S.R. 408 corridor. Pond 3B is located on a private property away from the project corridor. Drainage for Pond 3B could be conveyed through a stormsewer drainage system along Lone Palm Road south of the Waterford Creek Subdivision. Runoff for Basin 3 will be collected in a closed drainage system utilizing shoulder gutter due to the embankment requirements for the construction of the overpasses for Bridgeway Blvd. and Lone Palm Road. Three 12' wide x 6' high box culverts will be necessary to maintain flow of the wetlands from the south to the north in the middle section of the basin. Based on the pond alternative evaluation matrix analysis, Pond 3A is selected as the preferred pond site.

Two alternate pond sites, Ponds 4A and 4B, were identified for Basin-4. Pond 4A is located within vacant remnant parcels and Pond 4B is located on the remnant parcel of the self-storage facility. Based on the pond alternative evaluation matrix, Pond 4A is the preferred site. There is a possibility to merge the existing treatment pond (self-storage facility) with the proposed Pond 4B. Depending on the final acquisition of the self-storage facility, the merging of existing pond and proposed Pond 4B shall be investigated. Coordination with the Self-Storage Facility should take place during final design to reestablish the impacted drainage system. The roadway runoff will be collected in a closed drainage system utilizing shoulder gutter due to the embankment requirements for the construction of the overpasses for Lone Palm Road, Fricke Ave and Pel Street. The close proximity of Pond 4A to Pond 3A provides an opportunity to have single treatment facility for the combined basins. Based on the pond alternative evaluation matrix analysis, interconnecting both Ponds 3A and 4A is the preferred option due to its close proximity and cost. Combination of closed drainage system and conveyance swales will be required to drain the roadway runoff into selected pond sites. Conveyance swales and closed drainage system located at the elevated roadway profile will not be conflicting with cross drains while draining the runoff into the stormwater ponds.

The Deerwood mobile home community internal drainage system will be impacted by the



proposed roadway alignment. During the final design, necessary measures should be taken to minimize impact to this community's drainage system and to re-establish the impacted system.

Basin 5

Basin 5 begins at Pel Street and ends at Avalon Park Blvd. Two alternative pond sites, Pond 5A and Pond 5B, were identified for this basin. Both ponds are located within floodplains; compensation for the floodplain impacts could be provided in the ponds itself. The maintenance berms will tie to the existing ground; therefore, there will not be any anticipated floodplain impacts from the construction of these two ponds. The roadway runoff will be collected in a closed drainage system utilizing shoulder gutter due to the embankment requirements for construction of the overpasses for Pel Street and Avalon Park Blvd. Based on the pond alternative evaluation matrix, Pond 5B is the recommended pond location to serve Basin 5 since the pond site will not impact wetlands. Pond 5B will also be able to provide water quality, attenuation, and floodplain compensation. Pond 5A is identified as an alternate pond site.

Basin 6-8

Four pond sites are identified for this basin. A larger Pond 6B located south of the proposed corridor is the recommended site. The larger Pond 6B could provide the required treatment/attenuation volume and floodplain compensation for the entire basin. Pond 6B is located at the low point of the profile. The other alternative ponds are Pond 6A, 7A and 7B. Both Ponds 6A and 7A are located within the remnant parcels from the S.R. 408 corridor. Both ponds will be able to provide treatment, attenuation and some flood plain compensation since Pond 6A is adjacent to a floodplain. The roadway runoff will be collected in a closed drainage system utilizing barrier wall inlets and shoulder gutter inlets due to the embankment requirements for the construction of the overpasses at Avalon Park Blvd., Caudle St., and Colonial Dr. The western portion of the basin is in Flood Zone A and the ponds will be sized to include floodplain compensation. Avalon Park Subdivision Pond-C will be completely impacted by the proposed roadway alignment. The total impact to existing Pond-C is 2.2 ac-t. Compensation for this minor impact will be provided in the selected pond. The Avalon Park Permit #70394-1 will need to be modified for impacting existing Pond-C.

Pond 7B is located on an Orange County School Board property and does not have any significant impacts to wetland or floodplain. The roadway runoff will be collected in a closed drainage system utilizing barrier wall inlets and shoulder gutter inlets due to the embankment requirements for the construction of the overpasses at Colonial Dr. and Old Cheney Highway/Perdido Dr. Avalon Park subdivision Pond-J will not be impacted by the proposed S.R. 408 alignment.

Runoff from the bridge structure will be collected and conveyed to the recommended pond site through a closed drainage system. Bridge scuppers shall be used when the spread cannot be contained within the shoulder. Floodplain impacts and wetland impacts are not anticipated at the bridge location, since the bridge will completely span over the river and



floodplain. Only minor impacts are anticipated due to the bridge pier columns. No ponds were identified at the bridge location due to insufficient right-of-way availability and potential impact to wetlands and floodplains. Based on the pond alternative evaluation matrix, the preferred pond site for Basin 6-8 is Pond 6B. Pond 6B is a large pond that could provide required treatment, attenuation, large storage volume for floodplain compensation and compensation for impacted Avalon Park Pond C.

Bridge structures are not proposed at Sherman St and Caudle St. This will eliminate access to the homes located south of the SR 408 corridor. Since there will be no access to these home, it is our recommendation to purchase all the parcels and place stormwater Pond 6B as one alternative. For the second alternative, combination of Ponds 6A, 7A and 7B could be used.

Basin 9-10 were merged together and evaluated as a single basin

Basin 9 crosses the Econ River with a bridge structure. Runoff from the bridge will be collected and conveyed to one of the two alternate Ponds, 9A or 9B. Bridge scuppers shall be used when the spread cannot be contained within the shoulder. Both Ponds 9A and 9B are located within remnant parcels from the S.R. 408 corridor. Both ponds will have floodplain impacts and will be compensated for in the pond itself. Based on the pond alternative evaluation matrix, Pond 9B is the preferred pond site since it will have less impact to residential properties.

Basin 10 is divided between Hamilton Drive and Lockwood Drive. Two alternate pond sites were identified for this basin, Pond 10A and Pond 10B. Both ponds are located in the remnant parcel from the S.R. 408 alignment. Neither ponds have any environmental impacts. Runoff from the proposed S.R. 408 Eastern Extension alignment will be collected by shoulder gutters and will drain into either proposed ponds. Based on the pond alternative evaluation matrix, pond 10B is the preferred pond site since it will have less impact to residential properties.

Interconnecting Pond 9B and Pond 10B provides an opportunity for a single treatment facility. Based on the pond alternative evaluation matrix analysis, Pond 9B and Pond 10B were selected as the preferred option since there is less impact to residential properties, more economical, and the two ponds are in close proximity to be interconnected.

Basin 11A, Basin 11B and Basin 11C

Basin 11 is a large basin. For better evaluation, the overall Basin 11 is divided into Sub-Basins 11A, 11B and 11C. These basins are located between Lockwood Drive to just west of Palm Isle Drive. The basins span over a mile long and will require multiple ponds to meet the treatment and attenuation needs. Basin 11 is predominantly rural residential with some agriculture and wetlands. A portion of the S.R. 408 Eastern Extension alignment crosses a tributary of the Econ River and will require floodplain compensation. The proposed alignment will tie into the C.R. 419 Extension to provide direct access to and from C.R. 419. All the ponds will discharge to the Econ River tributaries.



Basin 11A, includes the S.R. 408 and C.R. 419 interchange areas and a small portion of the C.R. 419 extension. The infield ponds (Pond 11A1, Pond 11A2, and Pond11A3) are located within the proposed CFX R/W for the S.R. 408 corridor. Alternative 1 includes the three infield ponds and one offsite pond (Pond 11A4) that will be interconnected. Pond 11A4 is located on an existing plant nursery and will have some wetland impact. Alternative 2 will consist of an independent Pond 11A5. Pond 11A5 is located south of the interchange on a property that will be impacted by the S.R. 408 corridor. Most of Pond 11A5 is located on a private property that will be impacted by the S.R. 408 corridor; therefore, the parcel could be purchased together with the roadway R/W acquisition. Alternative 1 is selected as the recommended option since this option will use infield ponds that already within the road right-of-way and it will be cost effective.

Basin 11B will consist of the proposed C.R. 419 extension. The basin begins just before the proposed cross drain #7 and ends at S.R. 50. This basin includes the future access road to the East River High School. Two alternate pond sites have been identified for this basin, Pond 11B1 and Pond 11B2. Pond 11B1 is selected as the preferred pond site since the pond site is located within the parcel owned by the FDOT and there are less wetland impacts. Please refer to Pond Alternative Evaluation Matrices on **Page 5**.

Basin 11C is located south of the proposed S.R. 408 and C.R. 419 interchange. Two alternative pond sites were identified for this basin, Pond 11C and Pond 11C2. Pond 11C2 is located at the low point of the basin, however the pond area is mostly in a wetland. Due to high SHWT at this pond site, the pond could not provide sufficient storage volume for treatment and attenuation. Even though Pond 11-C is located closer to the higher point of the profile, it still could provide required treatment and attenuation storage. Since the low point of the roadway profile is still higher than the pond ground elevation, the roadway runoff could be conveyed to Pond 11C through a closed drainage system from the low point of the profile.

Pond 11C was selected as the preferred pond since it is more economical, and has no impacts to residential properties or wetlands. Please refer to Pond Alternative Evaluation Matrices (**Page 5**) for further details. Two additional ponds (Pond 11C3 and Pond 11C4) are proposed in this basin to provide floodplain compensation exclusively. Pond 11C4 site is currently used as an auto part junk yard; therefore, some contamination is expected at the site. Since this site is located within a floodplain and is impacted by the S.R. 408 corridor, it is practical to assume that the rest of the parcel could be used for a floodplain compensation pond. This option is only viable depending on the final sale of the parcel. Pond 11C3 is other floodplain compensation pond identified for this project. Since the roadway alignment in Basin 11C produce large amount of floodplain impact, it is our recommendation to use both Pond 11C4 and 11C3 as floodplain compensation ponds.

Basin 12

Basin 12 begins just west of Palm Isle Drive and ends south of Cochran Trail. This basin consists of rural residential, agricultural, and wetlands. This basin also crosses a tributary of the Econ River at the east end. This location will require floodplain compensation to mitigate the impacts of the mainline S.R. 408. Two alternate pond sites were identified for



this basin, Pond 12A and 12B. Both ponds are located within the remnant parcels from the S.R. 408 alignment. Based on the pond alternative evaluation matrix, Pond 12A was selected as the preferred pond location. Pond 12A will not impact residential properties, the parcel is larger, and the parcel is more economical.

Basin 13

Basin 13 begins south of Cochran Trail and ends at South 5th Street. This basin is predominantly agricultural. Runoff will be collected in roadside swales and conveyed to one of the two alternative ponds, Ponds 13A or 13B, identified for this basin. Both pond sites are vacant agricultural properties adjacent to the mainline. Pond 13B is located within remnant portions of property necessary for mainline S.R. 408. Pond 13B will have minor wetland impacts. Based on the pond alternative evaluation matrix, Pond 13B will be the preferred site, since it is located closer the low point of the profile and mainly consist of remnant parcel from S.R. 408.

Basin 14

Basin 14 begins at South 5th Street and ends at C.R. 13. This basin is predominantly rural residential. Two alternate pond sites are identified for this basin, Ponds 14A and 14B. These ponds will be placed within the remnant parcels from the S.R. 408 Eastern Extension corridor. No environmental impacts are identified for these ponds. Based on the pond alternative evaluation matrix, Pond 14A will be the preferred site. Pond 14A will have less impact to residential properties.

Basin 15

This is the last basin of the project. Two alternate ponds were identified for this basin, Pond 15A and Pond 15B. Pond 15B will be interconnected with modified Orange County Pond M-1, Pond M-2 and Pond M-3. The interconnected ponds could be used as a joint use ponds with Orange County. Based on the pond alternative evaluation matrix, Pond 15A is selected as the preferred option for this basin. Preliminary investigation suggests that Orange County Ponds M-2 and M-3 have additional storage capacity. The existing control structures for Ponds M-2 and M-3 will need to be modified to provide additional storage capacity. This basin includes on and off ramps from S.R. 50. The proposed roadway alignment in Basin 15 will impact portion of existing Orange County Pond M-1. Pond M-1 was constructed together with Pond M-2 and Pond M-3 by Orange County to provide flood relief for the adjacent areas and for the Bithlo South Basin. All three ponds are interconnected and discharge into Channel M. Please refer to Appendix-J for an excerpt from the Bithlo – Christmas Master Drainage Plan for additional information about Pond M-1. Based on our preliminary investigation, these ponds only provide flood attenuation and not water guality. Pond M-1 is connected to Channel KE which conveys runoff from north of S.R. 50 and drains to Channel M which eventually discharges to Econ River. The proposed roadway will sever the connectivity between Pond M-1 and Channel KE (Bithlo South Basin). Culvert #13 will be placed to reestablish connectivity between Pond M-1 and Channel KE (please refer to Location Hydraulic Report). The bypass ditch from Channel KE to Pond M-1 will be dissected by the westbound and eastbound ramps.



To re-establish the ditch connection 1-48" pipe will be placed. A portion of Pond M-1 will be filled in by the east bound lane. Compensation for filling in Pond M-1 will be provided in alternative Pond 15A by diverting flow from Channel KE and maintaining the historical flood relief in this area. Further investigation and coordination with Orange County is necessary during the final design. Please refer to the drainage maps for locations of the Orange County Ponds M-1, M-2, and M-3.

5.3 TAILWATER DETERMINATION

Preliminary tailwater elevations were determined by taking the average of the existing ground elevations and the 100-year elevations. These preliminary tailwater elevations at each pond location could be used for future pond designs and routing analyses. This tailwater elevation shall be verified based on survey data, and field indications such as stain marks shall be obtained during the design phase. Refer to **Table-6** for preliminary tailwater elevations.

Basin	Pond	100-year EL (ft)	DHW EL (ft)	Existing Ground EL (ft)	Tailwater EL (ft)	Source
	1A	-	60.20	61.0	60.60	SJRWMD Permit #20358
1	1B	-	60.20	61.0	60.60	SJRWMD Permit #20358
	1C	-	60.20	61.0	60.60	SJRWMD Permit #20358
2	2B	52.70	-	58.0	55.35	Big Econ Master Plan
2	2C	52.70	-	56.0	54.35	Big Econ Master Plan
	3A	52.70	-	55.0	53.85	Big Econ Master Plan
3-4	3B	52.70	-	56.0	54.35	Big Econ Master Plan
3-4	4A	52.70	-	55.0	53.85	Big Econ Master Plan
	4B	-	58.00	58.0	58.00	SJRWMD Permit #100527-1
5	5A	53.70	-	52.0	52.85	Big Econ Master Plan
5	5B	53.70	-	53.0	53.35	Big Econ Master Plan
	6A	53.04	-	55.0	54.02	SJRWMD Permit # 70394-1
6-8	6B	53.04	-	56.0	54.52	SJRWMD Permit # 70394-1
	7A	50.00	-	55.0	52.50	SJRWMD Permit #70394
	7B	50.00	-	55.0	52.50	SJRWMD Permit #70394
	9A	52.60	-	49.0	50.80	Big Econ Master Plan
9-10	9B	52.60	-	49.0	50.80	Big Econ Master Plan
9-10	10A	63.56	-	64.0	63.78	SJRWMD Permit #27625-4
	10B	52.60	-	49.0	50.80	Big Econ Master Plan
	11A1	63.56	-	63.0	63.28	SJRWMD Permit #27625-4
110	11A2	63.56	-	63.0	63.28	SJRWMD Permit #27625-4
11A	11A3	63.56	-	64.0	63.78	SJRWMD Permit #27625-4
	11A4	63.56	-	65.0	64.28	SJRWMD Permit #27625-4
110	11B1	63.56	-	60.0	61.78	SJRWMD Permit #27625-4
11B	11B2	63.56	-	63.0	63.28	SJRWMD Permit #27625-4

Table-6 Preliminary Tailwater Elevations

Basin	Pond	100-year EL (ft)	DHW EL (ft)	Existing Ground EL (ft)	Tailwater EL (ft)	Source
	11C	45.40	-	51.0	48.20	Bithlo Master Plan
11C	11C2	45.00	-	39.0	42.00	FEMA
	11C3	45.40	-	37.5	41.45	Bithlo Master Plan
	11C4	45.40	-	43.0	44.20	Bithlo Master Plan
12	12A	45.40	-	47.0	46.20	Bithlo Master Plan
12	12B	45.40	-	50.0	47.70	Bithlo Master Plan
13	13A	61.50	-	61.0	61.25	Bithlo Master Plan
13	13B	61.50	-	61.0	61.25	Bithlo Master Plan
14	14A	61.50	-	64.0	62.75	Bithlo Master Plan
14	14B	61.50	-	66.0	63.75	Bithlo Master Plan
15	15A	57.10	-	61.0	59.05	Bithlo Master Plan
15	15B	57.10	-	59.0	58.05	Bithlo Master Plan

Table-6 Preliminary Tailwater Elevations (Continued)

5.4 FLOODPLAIN IMPACTS/COMPENSATION

As previously mentioned, the project may impact the 100-year floodplain in three different ways:

- 1. Longitudinal roadway widening impacts resulting from filling the floodplain areas associated with Econlockhatchee River and its tributaries.
- 2. Impact due to proposed pond locations in floodplain.
- 3. Impact due to proposed cross drains in floodplain.

The longitudinal impact due to the recommended S.R. 408 Eastern Extension alignment cannot be avoided. During the final design phase of the project, every effort should be taken to minimize the floodplain impacts. Floodplain impacts could be compensated for by routing to swales at low profile locations, proposed stormwater ponds, and designated floodplain compensation ponds.

The FEMA's Flood Insurance Rate Map (FIRM) for Orange County shows that a portion of the project lies within the 100-year floodplain areas Zone AE and Zone A. Most of the project lies within flood Zone X. FEMA Map No. 12095C0280F, 129095C0285F, 12095C0295F, 12095C0290F and 12095C0315F, provide flood information for the project. Floodplain impacts occur throughout the project corridor and include the Econ River and its tributaries. Please refer to **Appendix-A** for a FEMA flood zone exhibit and **Appendix-B** for a FEMA Flood Insurance Rate Map.

Estimated 100-yr floodplain elevations were determined from the FEMA Map, the Big Econ Stormwater Management Master Plan, existing SJRWMD permits, and the Bithlo Area Stormwater Management Master Plan. The proposed bridge over the Econ River will not impact the floodplain since it spans over the entire river and floodplain. There will



be insignificant impacts due to bridge piers. Refer to the Location Hydraulics Report for a Bridge Hydraulics Evaluation. All of the floodplain impacts for this project stem from the proposed roadway fill. There are no floodplain impacts from the proposed floodplain compensation ponds. Pond maintenance berms located within floodplains tie to the existing ground; therefore, no fill will be produced above the existing ground.

Total floodplain impact due to roadway fill for the entire proposed project corridor is 100.28 ac-ft. Available compensation in the proposed stormwater ponds and floodplain compensation ponds are 107.47 ac-ft. Please refer to Table-7 for a summary of floodplain impacts and compensation. The dredge and fill volume are based on limited information available during the PD&E study. A detail evaluation has to be done during the final design. Based on the preliminary evaluation the project will provide more floodplain compensation than the impact. Therefore, a cup for cup compensation is provided by the project.

Two floodplain compensation pond sites were identified for this project in Basin 11C. The pond sites are Pond 11C3 and Pond 11C4. Both Pond 11C3 and Pond 11C4 are selected as the recommended floodplain compensation ponds. Beside this two floodplain compensation ponds, several stormwater ponds located adjacent to floodplains will also provide floodplain compensation. Please refer to **Table-7**. At certain segments of the project, for example at Basin 11C, the roadway profile is low enough to provide floodplain compensation should be evaluated during the design phase.

Runoff from within the corridor will be collected and conveyed to stormwater management facilities; therefore, reducing the overall impact to the remaining floodplains. The preliminary hydraulic evaluation indicates the flood elevation and limits will not change significantly; therefore, it is assumed that the project will not have a significant impact and the encroachment will be minimal.

SR 408 Eastern Extension-PD&E	Computed By	KS
CFX	Checked By	CR
	Date	3/14/2018

Floodplain Impact/Compensation Summary Table

		Average			Pond		Roadway		Available		
		Existing		Fill	Floodplain	Roadway	Floodplain		Compensation		
		Ground	100-Year	Depth	Impact Vol	Impact Area	Impact Vol (ac-	Total Impact	Vol in Pond (ac-	Method of Floodplain	
Basin	Pond ID	Elevation (ft)	Stage (ft)	(ft)	(ac-ft)	(ac)	ft)	Vol (ac-ft)	ft)	Hydraulic Connectivity	
1		NO IMPACT TO FLOODPLAIN									
2	Pond 2B	52.3	52.7	0.4	0	10.64	4.26	4.26	17.16	Adjacent to Floodplain	
	Pond 3A &										
3&4	Pond 4A	48	52.7	4.7	0	3.75	17.63	17.63	1.02	Adjacent to Floodplain	
5	Pond 5B	51.2	53.7	2.5	0	7.85	19.63	19.63	13.15	Within Floodplain	
6,7 and 8	Pond 6B	50.75	53.04	2.29	0	8.67	19.85	19.85	34.39	Adjacent to Floodplain	
9 & 10	NO IMPACT TO FLOODPLAIN										
11-A	NO IMPACT TO FLOODPLAIN										
11-B					NC) IMPACT TO FL	OODPLAIN				
		42.22	45.4	3.18	0	8.88	28.24	28.24	0.00	Not Connected	
11-C	11-C3	37.5	45.4	2	0	0	0.00	0.00	21.80		
	11-C4	43	45.4	3	0	0	0.00	0.00	14.93		
12		43.88	45.5	1.62	0	5.79	9.38	9.38	0.00	Not Connected	
13					NC	IMPACT TO FL	OODPLAIN				
14					NC	IMPACT TO FL	OODPLAIN				
15	Pond 15-A	59.2	59.5	0.3	0	4.35	1.30	1.30	5.02	Adjacent to Floodplain	
							Total:	100.28	107.47		



5.5 PROJECT CLASSIFICATION

The floodplain is in a medium density, semi-urbanized area and the encroachments are classified as "minimal". Minimal encroachment of a floodplain occurs when there is floodplain involvement, but the impacts on human life, transportation facilities, and natural and beneficial floodplain values are not significant and can be resolved with minimal efforts. Impacts that are resolved using minimal efforts, consist of applying the FDOT drainage design standards and following water management procedures to achieve results that do not increase or significantly change the flood elevation and the floodplain limits.

5.6 FLOODING HISTORY AND MAINTENANCE CONCERN

During a phone interview with the FDOT maintenance staff at the Oviedo Operations Center on 7/8/16, it was indicated that no areas of flooding concern were present along the S.R. 50 corridor. The staff member, Mike Danos, mentioned that there have been no reports of flooding or overtopping within the S.R. 50 corridor. The proposed S.R. 408 alignment is located just south of S.R. 50. Due to the close proximity of proposed S.R. 408 to existing S.R. 50, flooding history of S.R. 50 were used for this project.

6.0 CONCLUSION

This pond siting report has been prepared to provide pond site recommendations as part of the Project Development and Environment study for the proposed S.R. 408 Eastern Extension corridor in Orange County. The proposed seven-mile S.R. 408 Eastern Extension corridor is a new alignment, which consists of a four-lane divided rural roadway. The alignment will impact commercial properties, residential properties, and wooded areas. The final pond size calculations were determined by assuming the 64' median as impervious area. The recommended pond sites have been identified to:

- Minimize impact to residential and commercial properties.
- Minimize wetland and habitat impacts.
- Minimize floodplain impacts.
- Use remnant parcels from the S.R. 408 corridor. The final design team should maximize the usage of remnant parcels, which might change the pond shapes.

The following assumptions were made to determine the recommended pond sizes and locations:

- 1. The SHWT obtained from the Orange County soil report was used to size some of the ponds. During the final design, actual soil borings should be performed to determine the SHWT.
- 2. A preliminary profile was performed to verify that the recommended pond sites will be able to drain the respective on-site drainage basins. The existing ground was created from 1' contour Lidar, which was obtained from the SJRWMD. The profile was determined based on the existing ground elevations obtained from Lidar. The



Lidar does not provide accurate survey of the existing ground.

A volumetric analysis was used to size the ponds and accounts for both water quality treatment and attenuation. Please note that the pond location recommendations are based on preliminary data calculations, engineering judgment, and assumptions. This is a conceptual document and the pond locations may change during the final design as more detailed information and survey data become available. Refer to the Recommended Pond Analysis Summary Table (**Page 41**) for a summary of engineering data and analysis.



Recommended Pond Analysis Summary

Basin	Pond Name	Predominant Soil Type	Existing Ground Elevation (ft)	Estimated SHWT Elevation (ft)	Lowest edge of Proposed Road (ft)	Required Treatment and Attenuation (ac-ft)	Required Pond Area (ac)	Preliminary Pond Site (ac)	Treatment and Attenuation Depth (ft)	Outfall Location
	1A	Immokalee fine sand, St. Johns fine sand & Sanibel muck								Pond 1A, 1B, & 1C discharge to the east of the proposed
1	1B	Immokalee fine sand, St. Johns fine sand & Sanibel muck	61.5	58	67.51	6.74	4.1	8.14	1.2	ramp into the Unnamed Econ River Tributary(1).
	1C	Immokalee fine sand								
2	2В	Pomello fine sand	58.5	50.5	87.71	7.43	2.4	10.23	0.91	Pond 2B discharges into the Unnamed Econ River Tributary (1).
3 - 4	ЗA	Smyrna-Smyrna, wet, fine sand	55	50.5	75.71	4.87	2	4.86	1.82	Pond 3A and Pond 4A discharge into the Unnamed
	4A	Smyrna-Smyrna, wet, fine sand & Zolfo fine sand								Econ River Tributary (1).
5	5B	Smyrna-Smyrna, wet, fine sand	53	47.7	79.31	3.52	1.8	4.1	1.5	Pond 5B discharges into the Unnamed Econ River Tributary (2).
6-8	6B	Smyrna-Smyrna, wet, fine sand & Zolfo fine sand	57	50.4	81.71	9.21	3.3	19.73	0.53	Pond 6B discharges into surrounding wetlands that are connected to the Unnamed Econ River Tributary(2).
9 - 10	9B	Immokalee fine sand	49	48	90.41	5.82	4.3	8.38	0.91	Pond 9B & Pond 10B discharge into surrounding wetlands that flow into the
	10B	Zolfo fine sand								Econ River.
	11A1	Zolfo fine sand								
	11A2	Zolfo fine sand								Ponds 11A1, 11A2, 11A3, &
11A	11A3	Zolfo fine sand	63	60.5	64.5	5.27	2.6	5.76	1.14	11A4 are interconnected and discharge into wetlands that flow into the Econ River.
	11A4	Smyrna-Smyrna, wet, fine sand & Zolfo fine sand								

Recommended Pond Analysis Summary Table

-

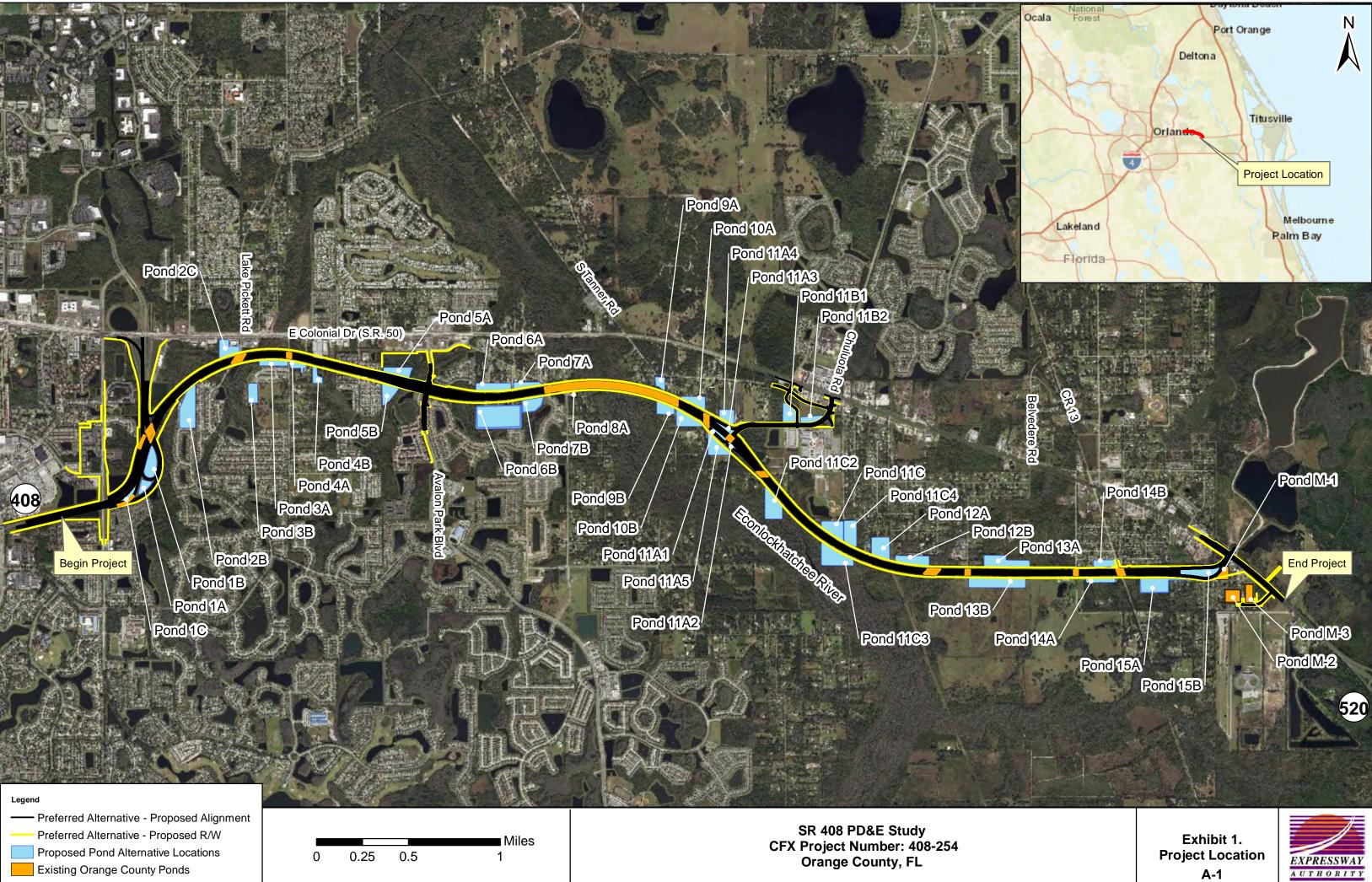
-

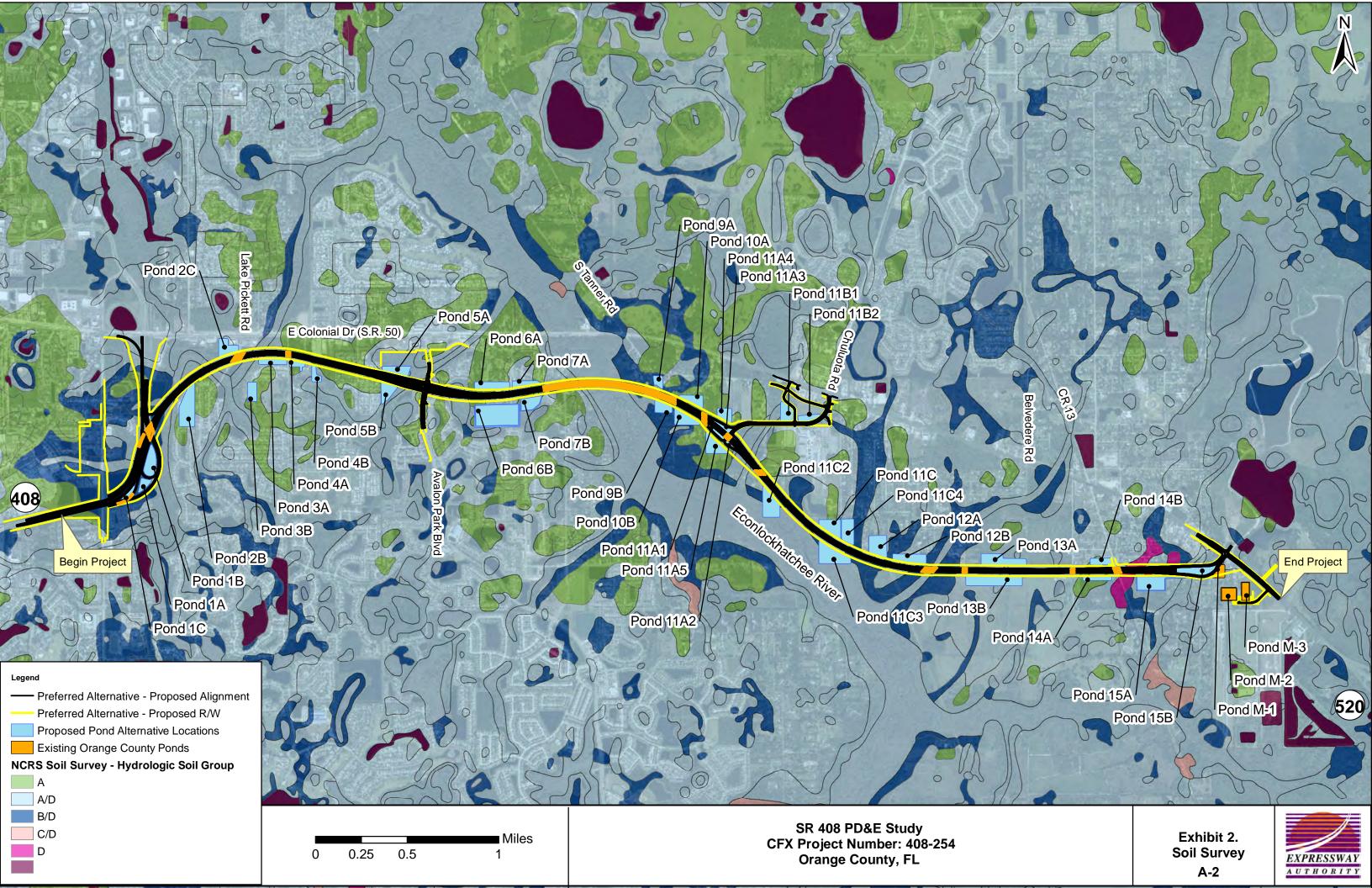
Basin	Pond Name	Predominant Soil Type	Existing Ground Elevation (ft)	Estimated SHWT Elevation (ft)	Lowest edge of Proposed Road (ft)	Required Treatment and Attenuation (ac-ft)	Required Pond Area (ac)	Preliminary Pond Site (ac)	Treatment and Attenuation Depth (ft)	Outfall Location	
11B	11B1	Smyrna-Smyrna, wet, fine sand	60	59	66.79	2.71	1.9	3.98	0.89	Pond 11B1 discharges into wetlands that flow into the Econ River.	
	11C	Smyrna-Smyrna, wet, fine sand & Wabasso fine sand	52	50	54.04	4.36	2.8	5.7	1	Pond 11C and Pond 11C4	
11C	11C3	Felda fine sand	37.5	35	53.39	N/A Floodplain Compensation Pond	N/A Floodplain Compensation Pond	8.85	N/A Floodplain Compensation Pond	discharge into Channel E.	
	11C4	St. Johns fine sand & Wabasso fine sand	43	41	52.73	N/A Floodplain Compensation Pond	N/A Floodplain Compensation Pond	5.5	N/A Floodplain Compensation Pond	Pond 11C3 discharges into wetlands that flow into the Econ River.	
12	12A	Smyrna-Smyrna, wet, fine sand & Basinger fine sand	48	47	54.02	4.1	3.2	6.88	0.73	Pond 12A discharges into Channel E and Pond 12B discharges into Channel A.	
13	13B	Smyrna-Smyrna, wet, fine sand & Pomello fine sand	61	60	78.8	6.51	4	10.45	0.79	Pond 13B discharges into surrounding vacant land that flows into Econ River.	
14	14A	Smyrna-Smyrna, wet, fine sand & Pomello fine sand	64	62	85.01	1.91	1.3	2.57	1.5	Pond 14A discharges into wetlands that flow into the Econ River.	
15	15A	Smyrna-Smyrna, wet, fine sand	60	53	68.17	6.16	2.6	8.92	1	Pond 15A discharges into wetlands that flow into Channel KE and eventually into Econ River.	

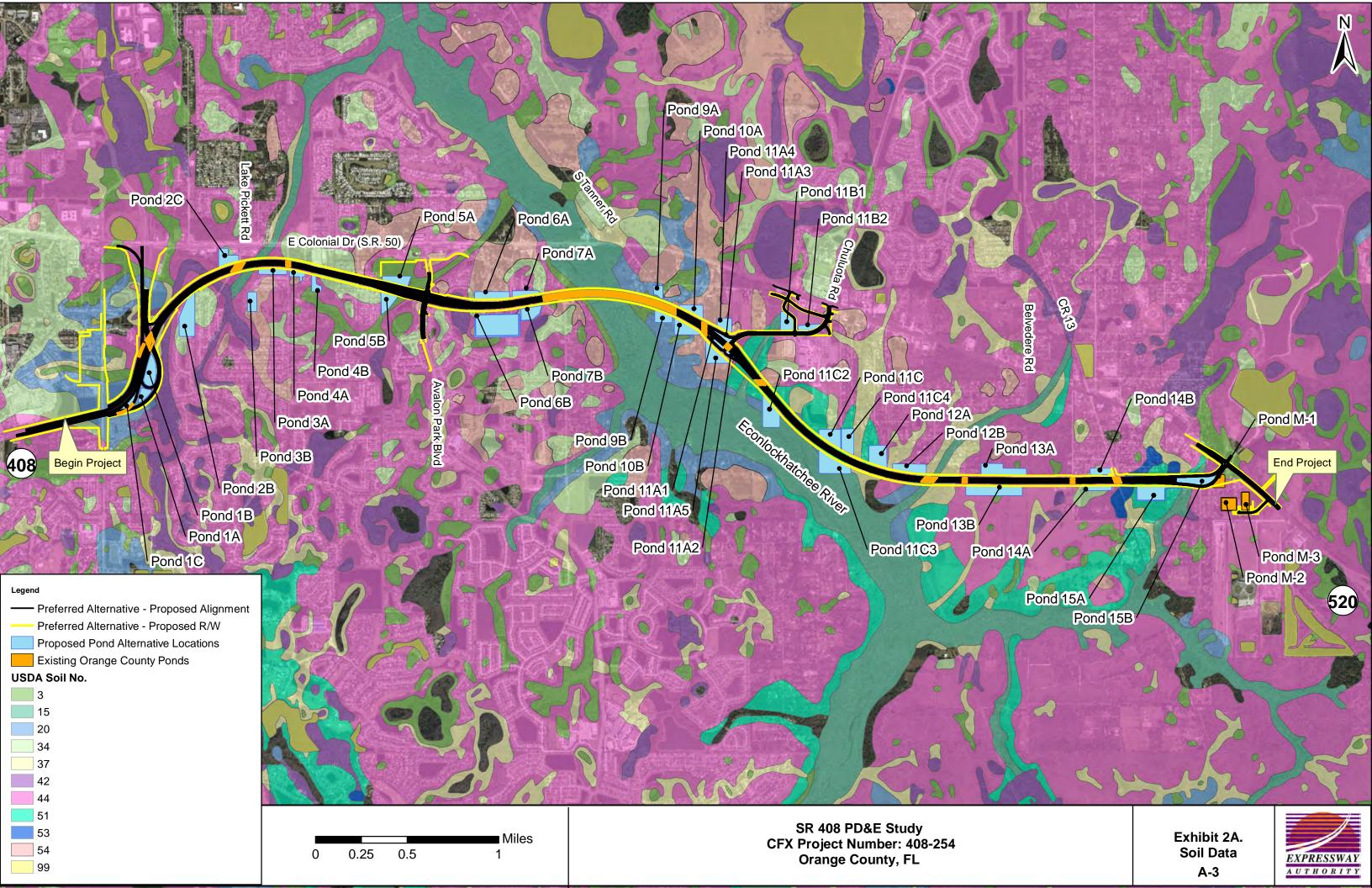
SR-408 Eastern Extension Project Development & Environment Study

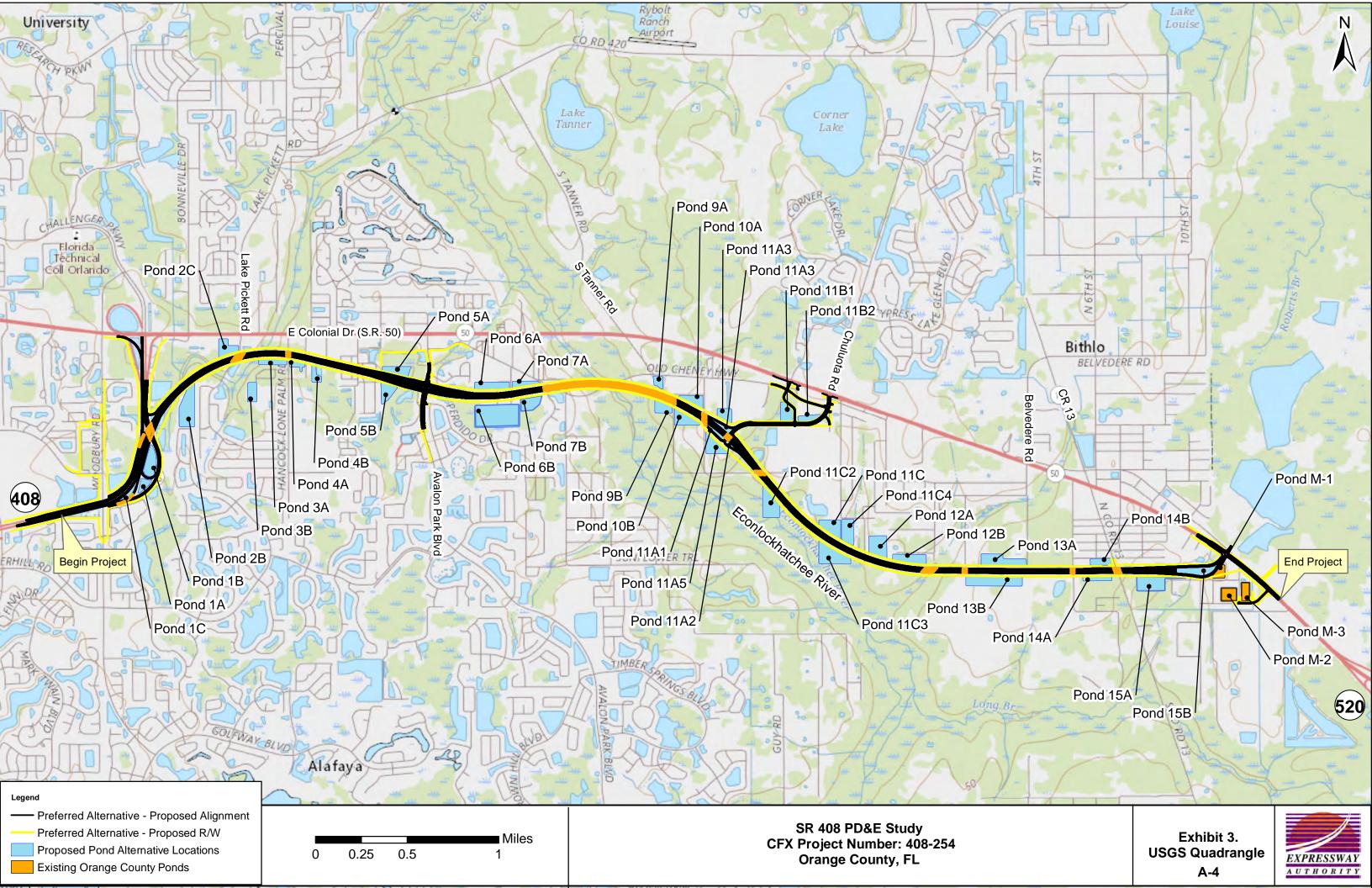
Appendix: A

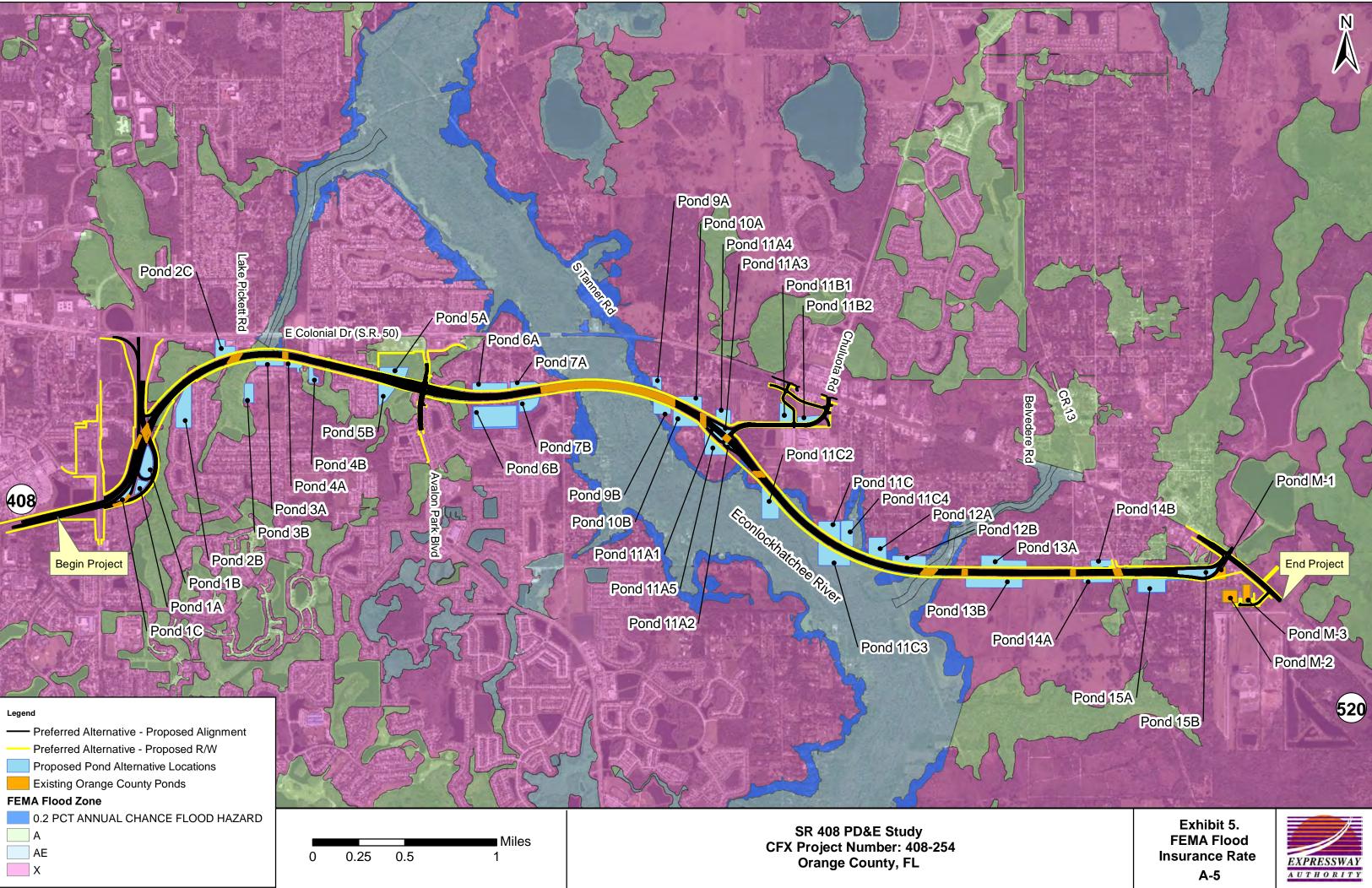
- Exhibit-1 Project Location Map
- Exhibit-2 Soil Survey
- Exhibit-2A Soil Data
- Exhibit-3 USGS Quadrangle Map
- Exhibit-4 Existing Land Use
- Exhibit-5-FEMA Flood Insurance Rate Map

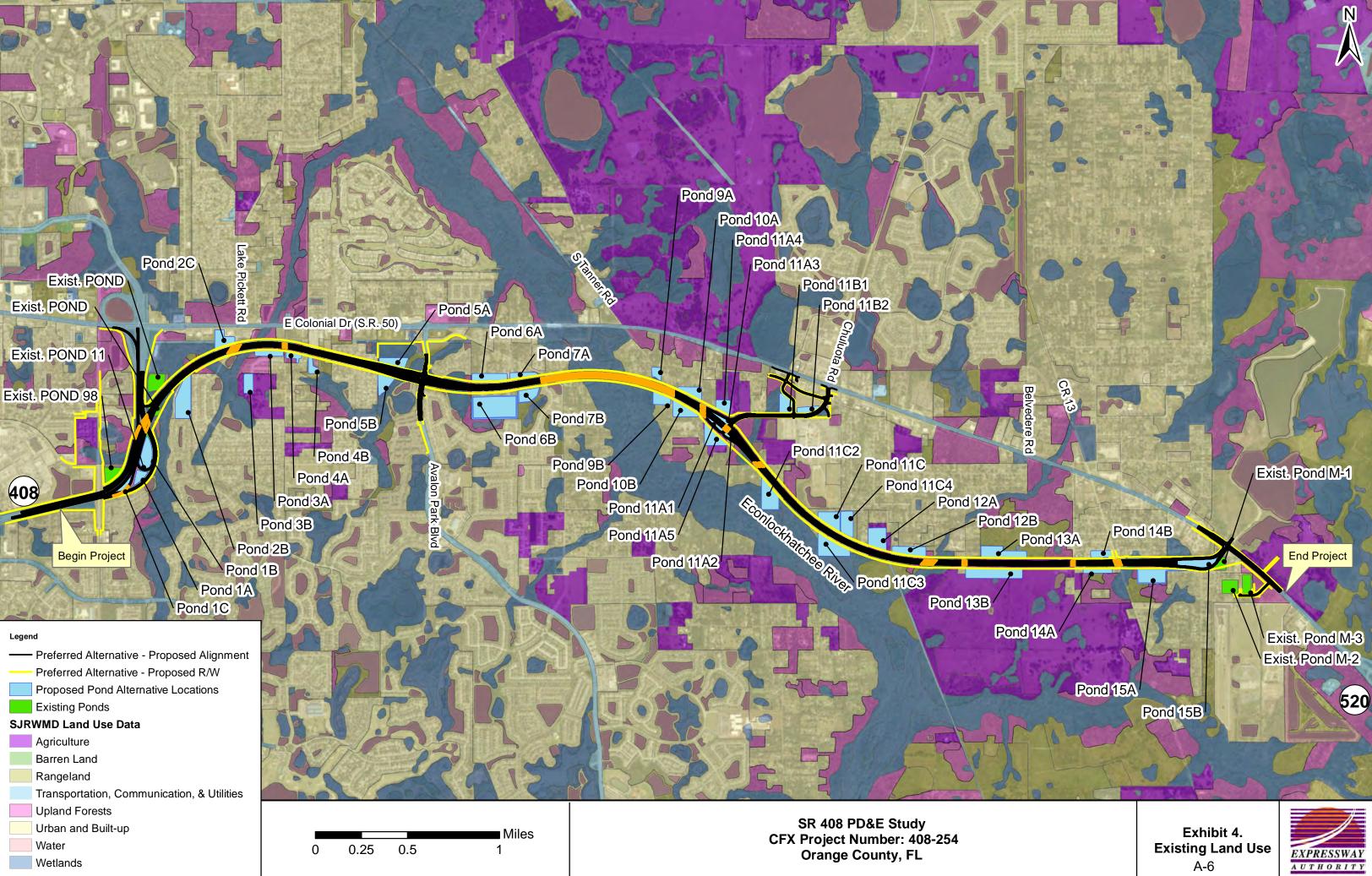












Appendix: B

FEMA Flood Insurance Rate Map

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or flood/plain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this unrefairling floodway. for this jurisdiction

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this junsdiction.

The projection used in the preparation of this map was State Plane Florida East FIPS Zone 0901. The horizontal datum was NAD83, GRS1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictors may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of Flood servations on this map are interenced to the North American Vertical Jacum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at the *InterNew* represence good or contact the National Geodetic Survey at the following the *InterNew* represence good or contact the National Geodetic Survey at the following the *InterNew* represence good or contact the National Geodetic Survey at the following the *InterNew* represence good or contact the National Geodetic Survey at the following the New represence of the InterNew represence of the InterNew represence of the InterNew represence of the InterNew represence of the National Section Section Section the New represence of the InterNew represence of the New represence of the

Spatial Reference System Division National Geodetic Survey, NCAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/

Base map information shown on this FIRM was provided in digital format by Orange County, Florida.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodpays that were transferred from the grevous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance SLady report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

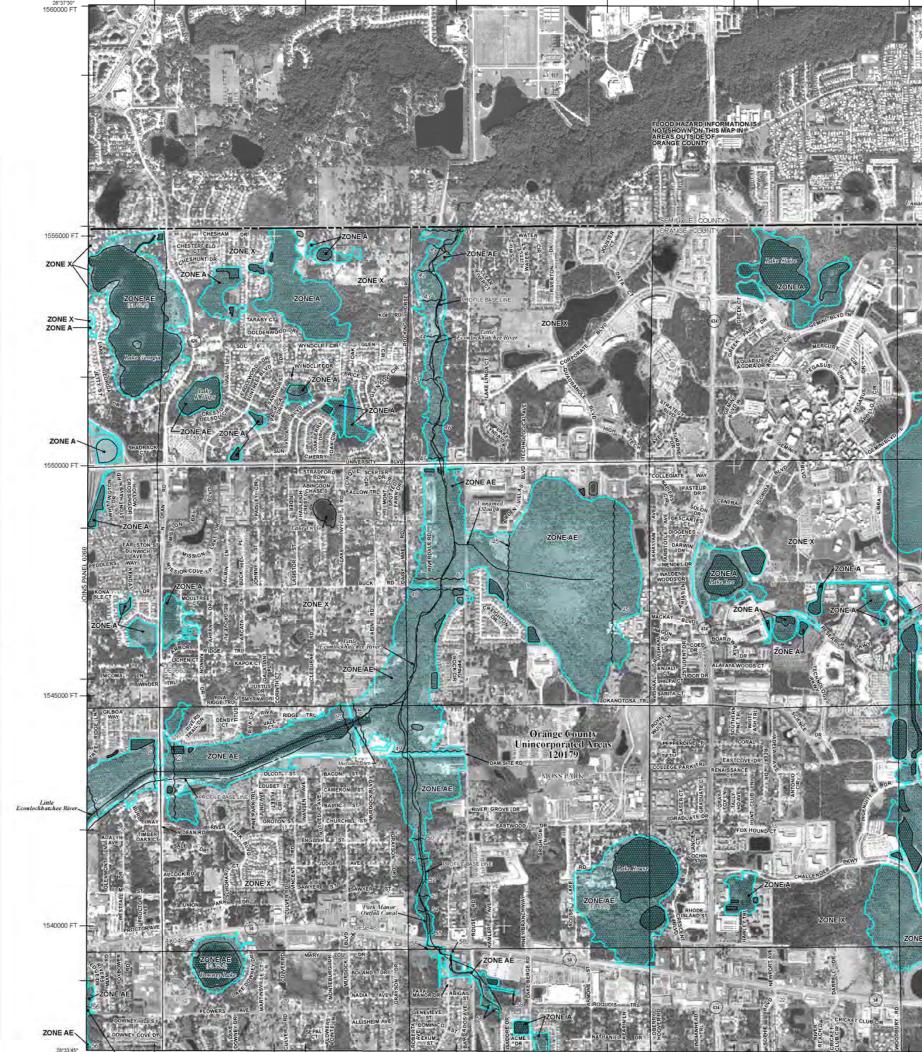
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

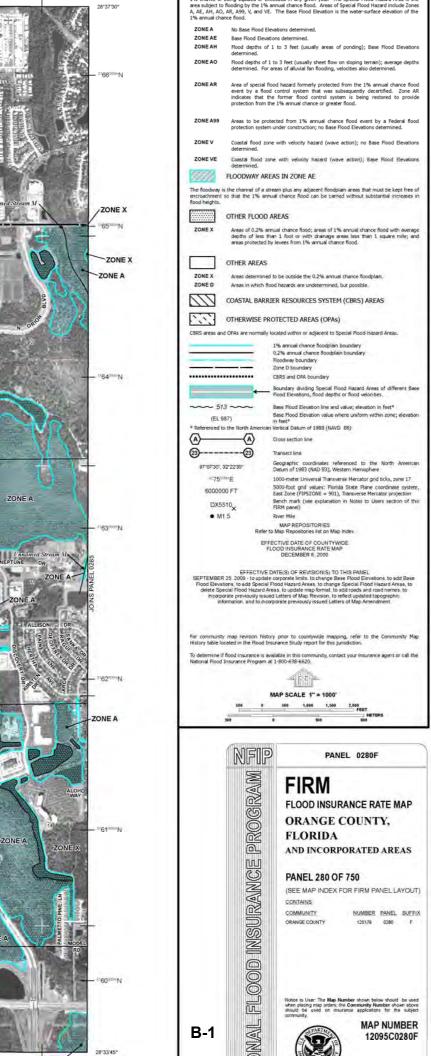
Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is provided.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gow/.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call **1-377-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <u>http://www.fema.gov/business/hfp/</u>.

Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhalcher River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.69	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.08
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econicokhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.88	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Weidva Riber	-0.88	-1.01	-0.94	0.07





ossible updated of additional flood nazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.07 North American Vertical Datum of 1988 (NAVD 86). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Sillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Sillwater Elevations table should be used for construction and/or flood/plain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jursiciton.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this junsdiction.

The **projection** used in the preparation of this map was State Plane Florida East FIPS Zone 0901. The **horizontal datum** was NAD33, GRS1960 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictione may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM

Flood elevations on this map are referenced to the North American Vertical Datum of 1986. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey verticate at <u>http://www.ngs.nosa.gov/</u> or contact the National Geodetic Survey at the following

Spatial Reference System Divisio National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.nga.gov/

Base map information shown on this FIRM was provided in digital format by Orange County, Florida.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

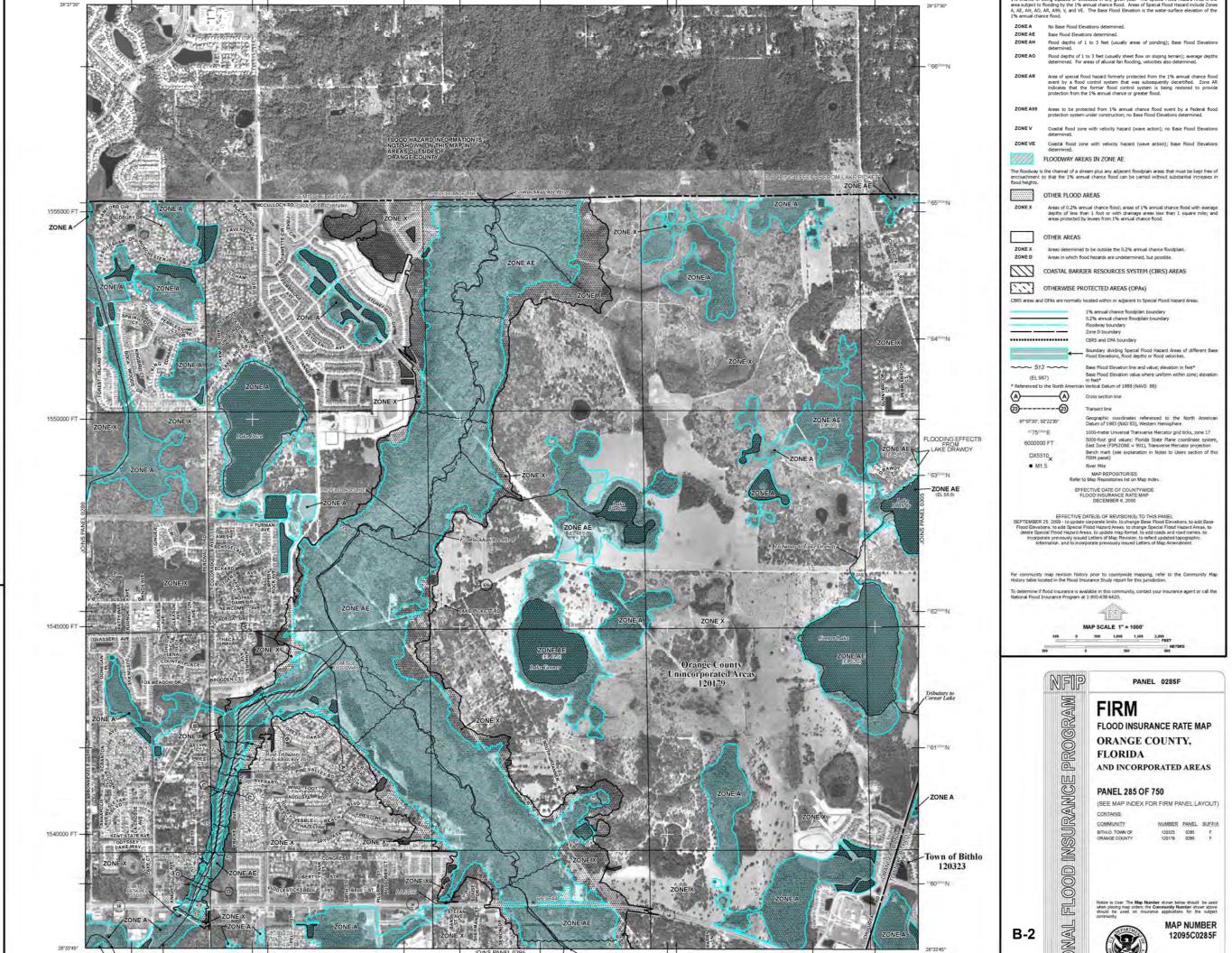
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously associated Letters of Map Change, a Flood Insurance Sludy report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-356-9620 and its weeting at <u>HIL/INWOWTES Clema good</u>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <u>http://www.fema.gov/business/infp/</u>.

Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.69	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econilockhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wektva River	-0.88	-1.01	-0.94	0.07



possible updated or adducital flood nazard filtormation

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of SIIIIvater Elevations tables contained within the Flood Insurance SIUdy (FIS) report that accompanies this FIRM. Users should be aware that SIFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain transagement.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0 North American Vertical Datum of 1988 (NAVD 86). Users of the FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or flood/aim management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was State Plane Florida East FIPS Zone 0901. The horizontal datum was NAD83, GRS1980 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across junsdiction boundance. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <u>http://www.ngs.nosa.gov/</u> or contact the National Geodetic Survey at the following address.

Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ns.naa.gov/

Base map information shown on this FIRM was provided in digital format by Orange County, Florida

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FROM for this jurisdiction. The floodpairs and floodways that were transferred from the previous FRIM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

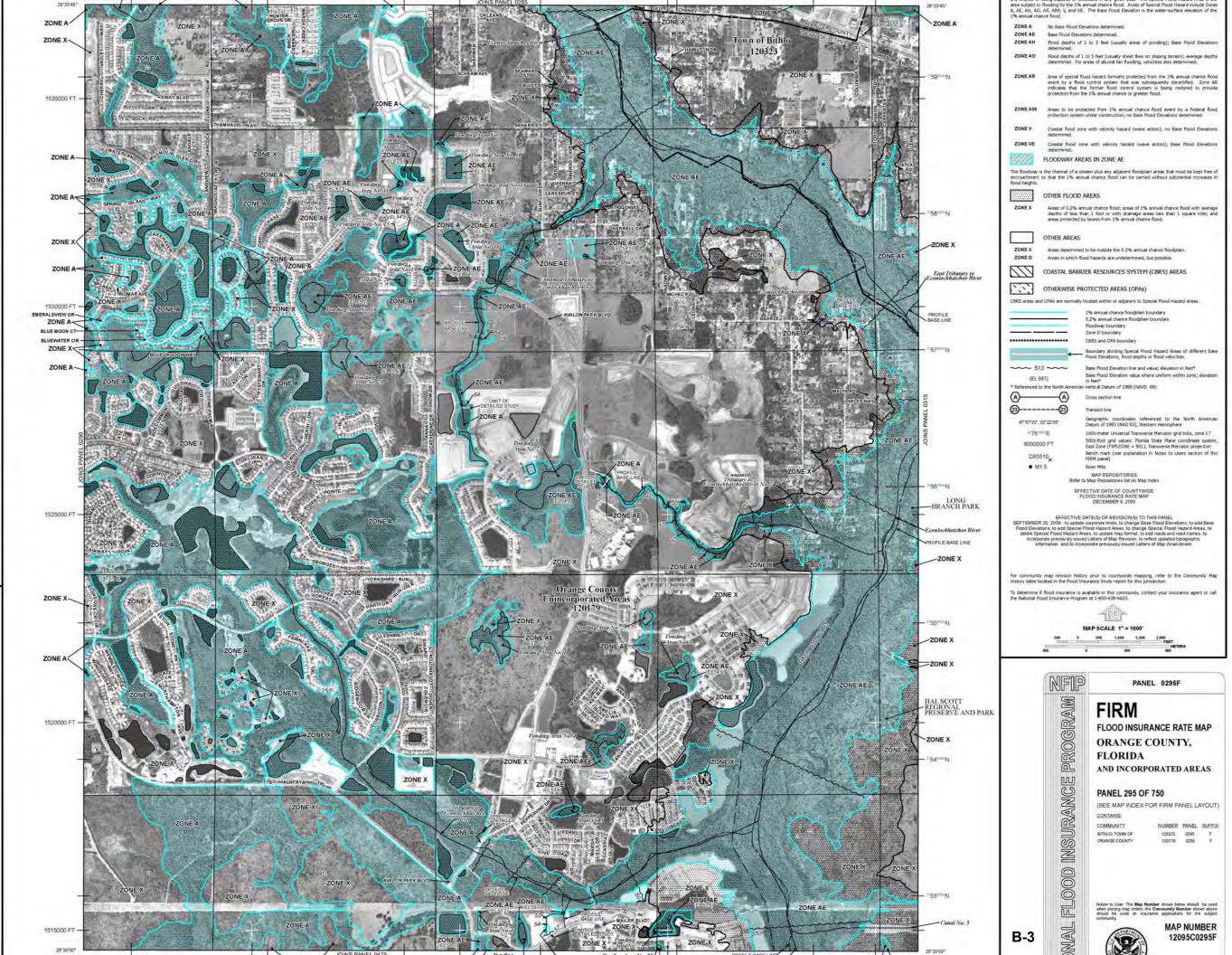
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Fload Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change. *Flood Insurance Study report.* and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <u>http://www.msc.fema.gov/</u>

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <u>http://www.fema.gov/business/nfip/</u>

Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.89	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econicokhatchee River	-0.92	-1.07	-5.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wekiva River	-0.88	-1.01	-0.94	0.07



possible updated of additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway' Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-floot elevations. These BFEs are intended for flood insurance range purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation that presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplein management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0 North American Vertical Datum of 1988 (NAVD 86). Users of this FIRM should be waver that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on the FIRM

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Frogram. Floodway widths, and other pertinent floodway data are provided in the Flood Insurance Study report for this jursicition.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this junsdiction.

The projection used in the preparation of this map was State Plane Florida East PIPS Zone 0901. The horizontal datum was NAD83, GRS1960 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictors may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1998. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <u>http://www.ngs.nosa.gov/</u> or contact the National Geodetic Survey at the following address.

Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/

Base map information shown on this FIRM was provided in digital format by Orange County, Florida.

This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplants and floodways that were transferred from the pevicous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

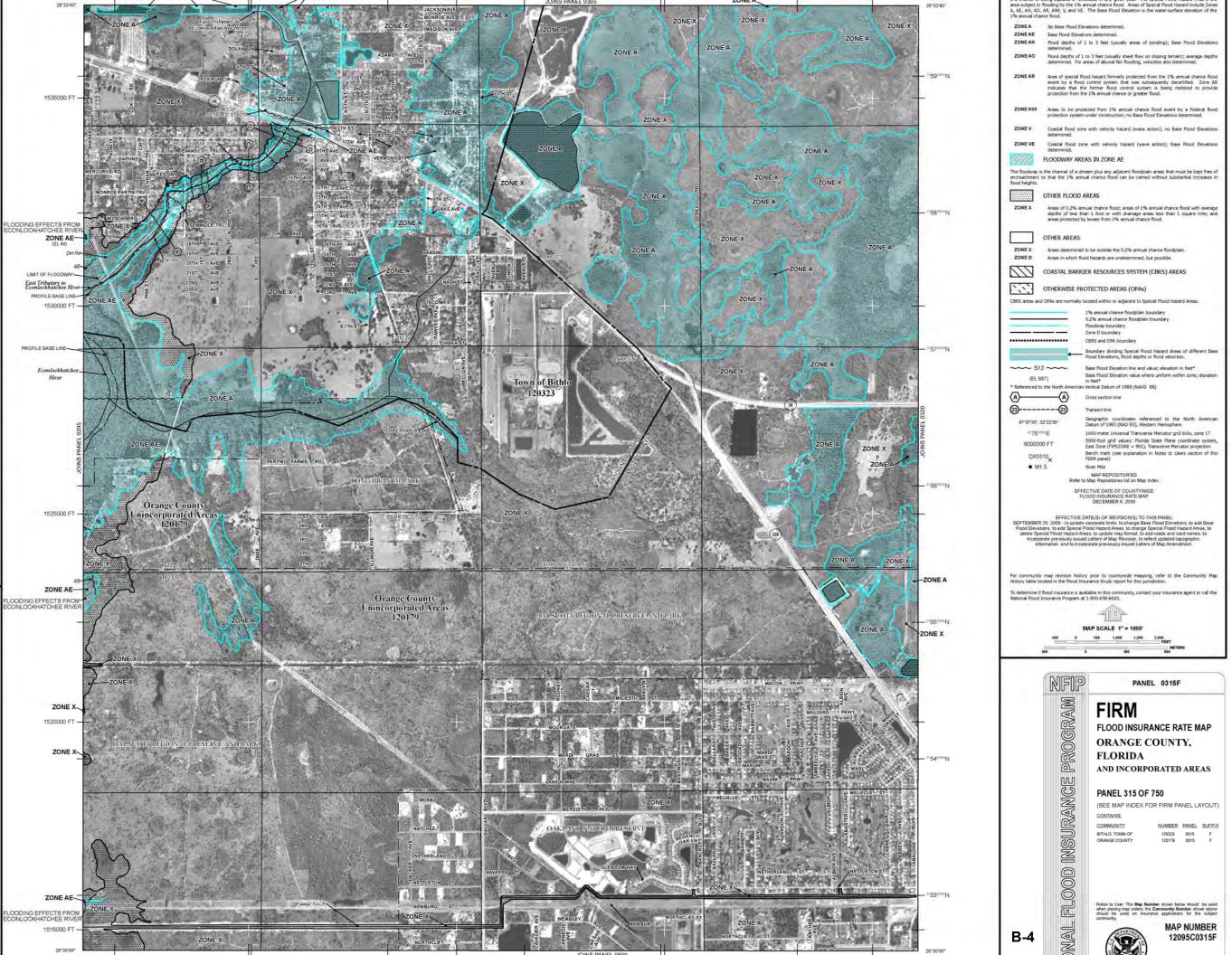
Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the country showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM Available products may include previously issued Letters of Map Change, a Flood Insurance Study report and/or digtal versions of this map. The FENA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <u>http://www.msc.fema.gov/</u>.

If you have questions about this map or questions concerning the National Flood Insurance Program in general, please call **1-877-FEMA MAP** (1-877-336-2627) or visit the FEMA website at <u>http://www.fema.gov/business/infp/</u>.

Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.69	0.02
Howell Branch	-0.96	+1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econicokhatohee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wekiva River	-0.88	-1.01	-0.94	0.07



Appendix: C

USDA NRCS Soil Report



USDA United States Department of Agriculture

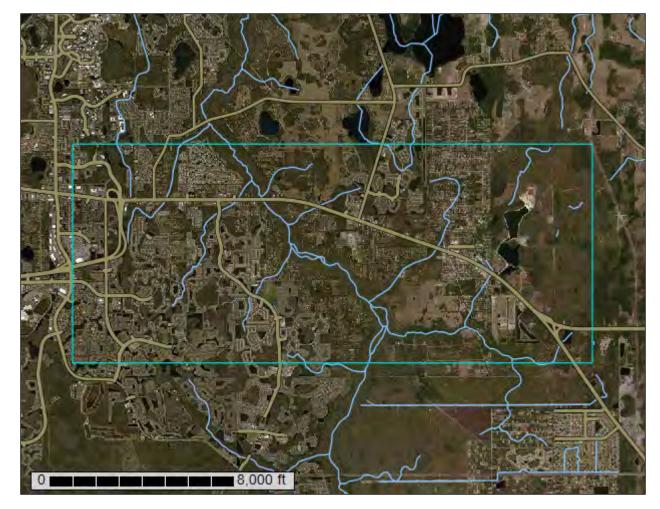


Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Orange County, Florida

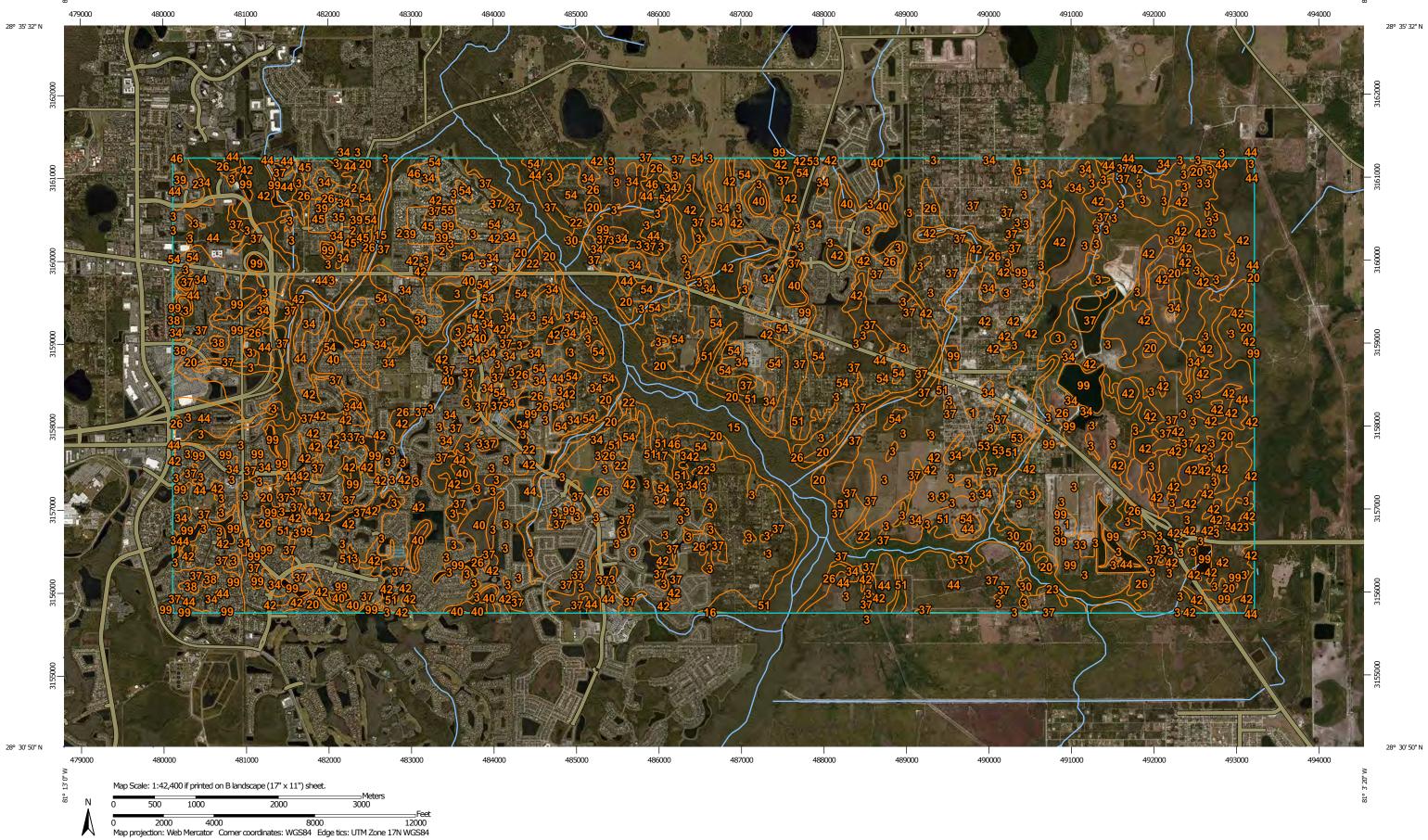
SR 408 Soil Data



May 27, 2016



Custom Soil Resource Report Soil Map



MA	P LEGEND	MAP INFORMATION
Area of Interest (AOI)	Spoil Area	The soil surveys that comprise your AOI were mapped at 1:20,000.
Area of Interest (AO) 👌 Stony Spot	Please rely on the bar scale on each map sheet for map
Soils Soil Map Unit Polygo	Very Stony Spot	measurements.
Soil Map Unit Lines	🖞 Wet Spot	Source of Map: Natural Resources Conservation Service
Soil Map Unit Points	△ Other	Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov
Special Point Features	Special Line Features	Coordinate System: Web Mercator (EPSG:3857)
() Blowout	Water Features	Maps from the Web Soil Survey are based on the Web Mercator
Borrow Pit	Streams and Canals	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the
Clay Spot	Transportation Rails	Albers equal-area conic projection, should be used if more accurate
Closed Depression	HH Rails	calculations of distance or area are required.
Gravel Pit	US Routes	This product is generated from the USDA-NRCS certified data as of
Gravelly Spot	Major Roads	the version date(s) listed below.
🔕 Landfill	Local Roads	Soil Survey Area: Orange County, Florida
Lava Flow	Background	Survey Area Data: Version 12, Nov 19, 2015
Marsh or swamp	Aerial Photography	Soil map units are labeled (as space allows) for map scales 1:50,000
Mine or Quarry		or larger.
Miscellaneous Wate	r	Date(s) aerial images were photographed: Mar 12, 2011—Feb
Perennial Water		20, 2015
Rock Outcrop		The orthophoto or other base map on which the soil lines were
Saline Spot		compiled and digitized probably differs from the background
Sandy Spot		imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.
Severely Eroded Sp	pt	
Sinkhole		
b Slide or Slip		
Sodic Spot		

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Arents, nearly level	16.4	0.1%
2	Archbold fine sand, 0 to 5 percent slopes	73.1	0.4%
3	Basinger fine sand, depressional, 0 to 1 percent slopes	1,106.2	6.2%
15	Felda fine sand, frequently flooded	1,060.0	5.9%
16	Floridana fine sand, frequently flooded	1.5	0.0%
17	Floridana mucky fine sand, depressional	13.6	0.1%
20	Immokalee fine sand	754.8	4.2%
22	Lochloosa fine sand	57.6	0.3%
23	Malabar fine sand	7.3	0.0%
26	Ona fine sand	193.0	1.1%
27	Ona-Urban land complex	4.8	0.0%
30	Pineda fine sand	28.5	0.2%
33	Pits	13.4	0.1%
34	Pomello fine sand, 0 to 5 percent slopes	986.4	5.5%
35	Pomello-Urban land complex, 0 to 5 percent slopes	19.4	0.1%
37	St. Johns fine sand	920.5	5.2%
38	St. Lucie fine sand, 0 to 5 percent slopes	34.7	0.2%
39	St. Lucie-Urban land complex, 0 to 5 percent slopes	29.9	0.2%
40	Samsula muck	145.3	0.8%
42	Sanibel muck	1,496.8	8.4%
44	Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes	9,067.4	50.9%
45	Smyrna-Urban land complex	80.9	0.5%
46	Tavares fine sand, 0 to 5 percent slopes	11.6	0.1%
51	Wabasso fine sand, 0 to 2 percent slopes	669.4	3.8%
53	Wauberg fine sand	26.8	0.2%
54	Zolfo fine sand, 0 to 2 percent slopes	717.2	4.0%
55	Zolfo-Urban land complex	11.2	0.1%
99	Water	277.9	1.6%
Totals for Area of Interest	'	17,825.4	100.0%

3-Basinger fine sand, depressional, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2v16v Elevation: 0 to 160 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Basinger, depressional, and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Basinger, Depressional

Setting

Landform: Depressions on marine terraces, drainageways on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 14 inches: fine sand Bh/E - 14 to 36 inches: fine sand Cg - 36 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 20.00 in/hr)

Depth to water table: About 0 inches Frequency of flooding: None Frequency of ponding: Frequent Calcium carbonate, maximum in profile: 1 percent Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0 Available water storage in profile: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL) Hydric soil rating: Yes

Minor Components

Smyrna, hydric

Percent of map unit: 5 percent

Landform: - error in exists on -

Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex

Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Samsula, muck

Percent of map unit: 3 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip, talf Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes Floridana, hydric

Percent of map unit: 2 percent Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Cypress Woodlands (MCV026CA), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL) Hydric soil rating: Yes

20—Immokalee fine sand

Map Unit Setting

National map unit symbol: bv7n Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Immokalee, non-hydric, and similar soils: 82 percent Immokalee, hydric, and similar soils: 10 percent Minor components: 8 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Immokalee, Non-hydric

Setting

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 35 inches: fine sand Bh - 35 to 67 inches: fine sand C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 6 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Description of Immokalee, Hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand

E - 5 to 35 inches: fine sand

Bh - 35 to 67 inches: fine sand

C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: Yes

Minor Components

Pineda

Percent of map unit: 4 percent
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

Wabasso

Percent of map unit: 4 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

34—Pomello fine sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2v16y Elevation: 0 to 180 feet Mean annual precipitation: 44 to 52 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 342 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Pomello and similar soils: 95 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pomello

Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve, riser Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 47 inches: fine sand Bh - 47 to 58 inches: fine sand Bw - 58 to 65 inches: fine sand C - 65 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 24 to 42 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: A Other vegetative classification: Sand Pine Scrub (R155XY001FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL) Hydric soil rating: No

Minor Components

Smyrna

Percent of map unit: 3 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Tavares

Percent of map unit: 1 percent
Landform: Ridges on marine terraces, flats on marine terraces
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Linear
Ecological site: Longleaf Pine-Turkey Oak Hills (R154XY002FL)
Other vegetative classification: Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)
Hydric soil rating: No

Bulow

Percent of map unit: 1 percent
Landform: Ridges on marine terraces
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Linear
Other vegetative classification: Sandy over loamy soils on knolls and ridges of mesic uplands (G155XB211FL)
Hydric soil rating: No

37—St. Johns fine sand

Map Unit Setting

National map unit symbol: bv87 Elevation: 30 to 150 feet Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

St. johns, non-hydric, and similar soils: 60 percent *St. johns, hydric, and similar soils:* 30 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of St. Johns, Non-hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)
Depth to water table: About 6 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

Description of St. Johns, Hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: B/D
Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 5 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Immokalee, non-hydric

Percent of map unit: 5 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

42—Sanibel muck

Map Unit Setting

National map unit symbol: bv8f Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Sanibel, undrained, and similar soils: 65 percent Sanibel, drained, and similar soils: 25 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Sanibel, Undrained

Setting

Landform: Marshes on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck *A - 11 to 15 inches:* fine sand *C - 15 to 80 inches:* fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Description of Sanibel, Drained

Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck *A - 11 to 15 inches:* fine sand *C - 15 to 80 inches:* fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 to 24 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

Minor Components

Hontoon, undrained

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

Samsula

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

44—Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2v171 Elevation: 0 to 150 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Smyrna, non-hydric, and similar soils: 76 percent *Smyrna, hydric, and similar soils:* 20 percent *Minor components:* 4 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Smyrna, Non-hydric

Setting

Landform: Flatwoods on marine terraces, flats on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 17 inches: fine sand Bh - 17 to 27 inches: loamy fine sand C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Description of Smyrna, Hydric

Setting

Landform: Flats on marine terraces, flatwoods on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand

E - 4 to 17 inches: fine sand

Bh - 17 to 27 inches: loamy fine sand

C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: Yes

Minor Components

Basinger, depressional

Percent of map unit: 2 percent Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL) Hydric soil rating: Yes

Pomona, non-hydric

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces Landform position (two-dimensional): Backslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Eaugallie, hydric

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces, flats on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R154XY003FL), Sandy soils on flats of mesic or hydric lowlands (G154XB141FL)

Hydric soil rating: Yes

Across-slope shape: Linear

Other vegetative classification: North Florida Flatwoods (R154XY004FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL)

Hydric soil rating: No

51—Wabasso fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2svzg Elevation: 0 to 130 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Wabasso and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wabasso

Setting

Landform: Flatwoods on flats on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits over loamy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 16 inches: fine sand Bh - 16 to 28 inches: fine sand E' - 28 to 32 inches: fine sand Btg - 32 to 48 inches: fine sandy loam Cg - 48 to 80 inches: loamy fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 12 to 63 inches to strongly contrasting textural stratification
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Minor Components

Basinger

Percent of map unit: 4 percent
Landform: Drainageways on flatwoods on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Convex, linear, concave
Across-slope shape: Linear, convex, concave
Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Felda

Percent of map unit: 4 percent
Landform: Flatwoods on drainageways on marine terraces
Landform position (three-dimensional): Tread, dip, talf
Down-slope shape: Linear
Across-slope shape: Concave, linear
Ecological site: Slough (R155XY011FL)
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)
Hydric soil rating: Yes

Riviera

Percent of map unit: 4 percent
Landform: Flatwoods on drainageways on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Linear, convex
Across-slope shape: Concave, linear
Ecological site: Slough (R155XY011FL)
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G156AC241FL)
Hydric soil rating: Yes

Boca

Percent of map unit: 3 percent
Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Tread, talf
Down-slope shape: Convex
Across-slope shape: Linear
Ecological site: South Florida Flatwoods (R155XY003FL)
Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

53—Wauberg fine sand

Map Unit Setting

National map unit symbol: bv8t Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Wauberg and similar soils: 94 percent Minor components: 6 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wauberg

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy and loamy marine deposits

Typical profile

- A 0 to 8 inches: fine sand
- E 8 to 28 inches: fine sand
- B 28 to 60 inches: sandy clay loam
- C 60 to 80 inches: sandy clay

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 6 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

54—Zolfo fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2w0q1 Elevation: 30 to 160 feet Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 324 to 365 days Farmland classification: Farmland of unique importance

Map Unit Composition

Zolfo and similar soils: 88 percent *Minor components:* 12 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Zolfo

Setting

Landform: Rises on marine terraces, knolls on marine terraces Landform position (two-dimensional): Summit, footslope Landform position (three-dimensional): Interfluve, side slope, riser Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 6 inches: fine sand E - 6 to 53 inches: fine sand Bh - 53 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)

Depth to water table: About 24 to 42 inches Frequency of flooding: None Frequency of ponding: None Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0 Available water storage in profile: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A Other vegetative classification: North Florida Flatwoods (R154XY004FL), South Florida Flatwoods (R154XY003FL), Sandy soils on rises and knolls of mesic uplands (G154XB131FL) Hydric soil rating: No

Minor Components

Myakka

Percent of map unit: 4 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Tavares

Percent of map unit: 3 percent

Landform: Ridges on marine terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Interfluve, tread, rise

Down-slope shape: Linear, convex

Across-slope shape: Linear

Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL) *Hydric soil rating:* No

Millhopper

Percent of map unit: 3 percent

Landform: Ridges on marine terraces, knolls on marine terraces, flatwoods on marine terraces

Landform position (two-dimensional): Shoulder, summit

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex, concave

Across-slope shape: Linear

Other vegetative classification: Upland Hardwood Hammock (R154XY008FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL) *Hydric soil rating:* No

Lochloosa

Percent of map unit: 1 percent Landform: Rises on marine terraces Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex

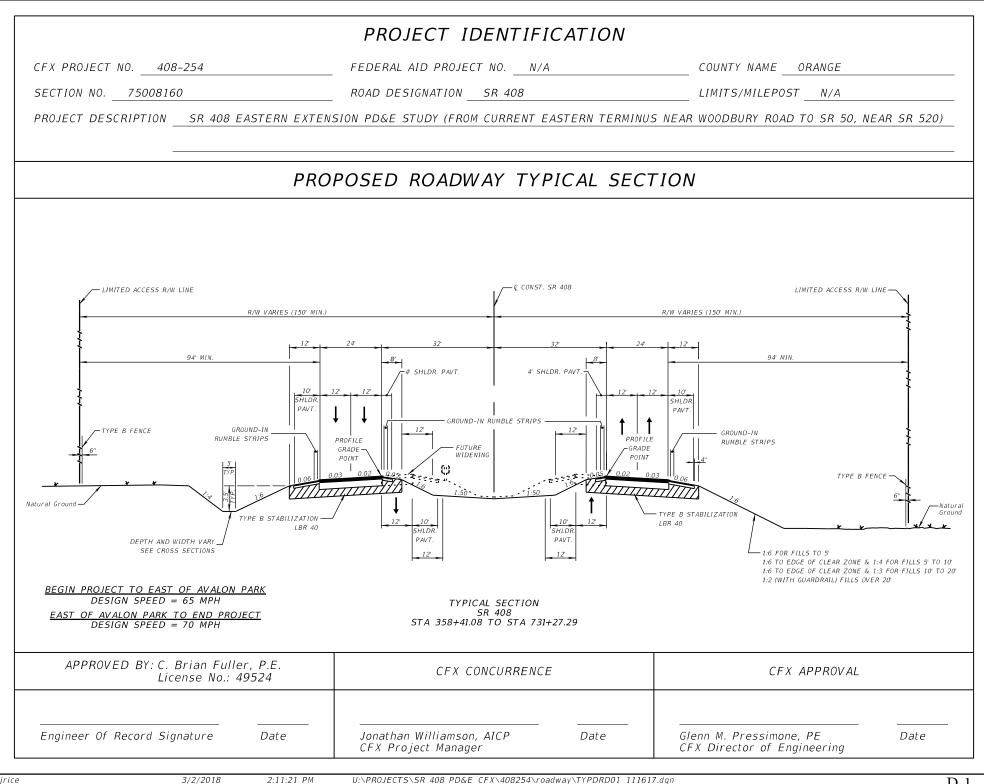
Across-slope shape: Linear Other vegetative classification: Sandy over loamy soils on rises and knolls of mesic uplands (G155XB231FL) Hydric soil rating: No

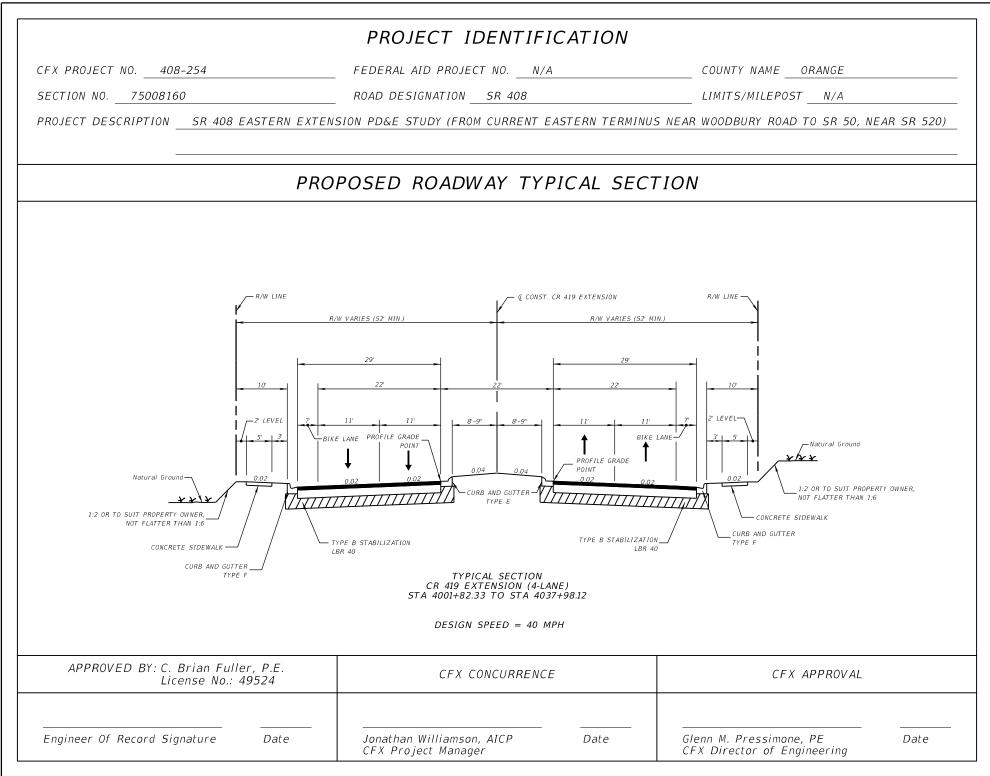
Malabar

Percent of map unit: 1 percent
Landform: Drainageways on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Linear, convex
Across-slope shape: Concave, linear
Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Appendix: D

SR 408 Typical Section



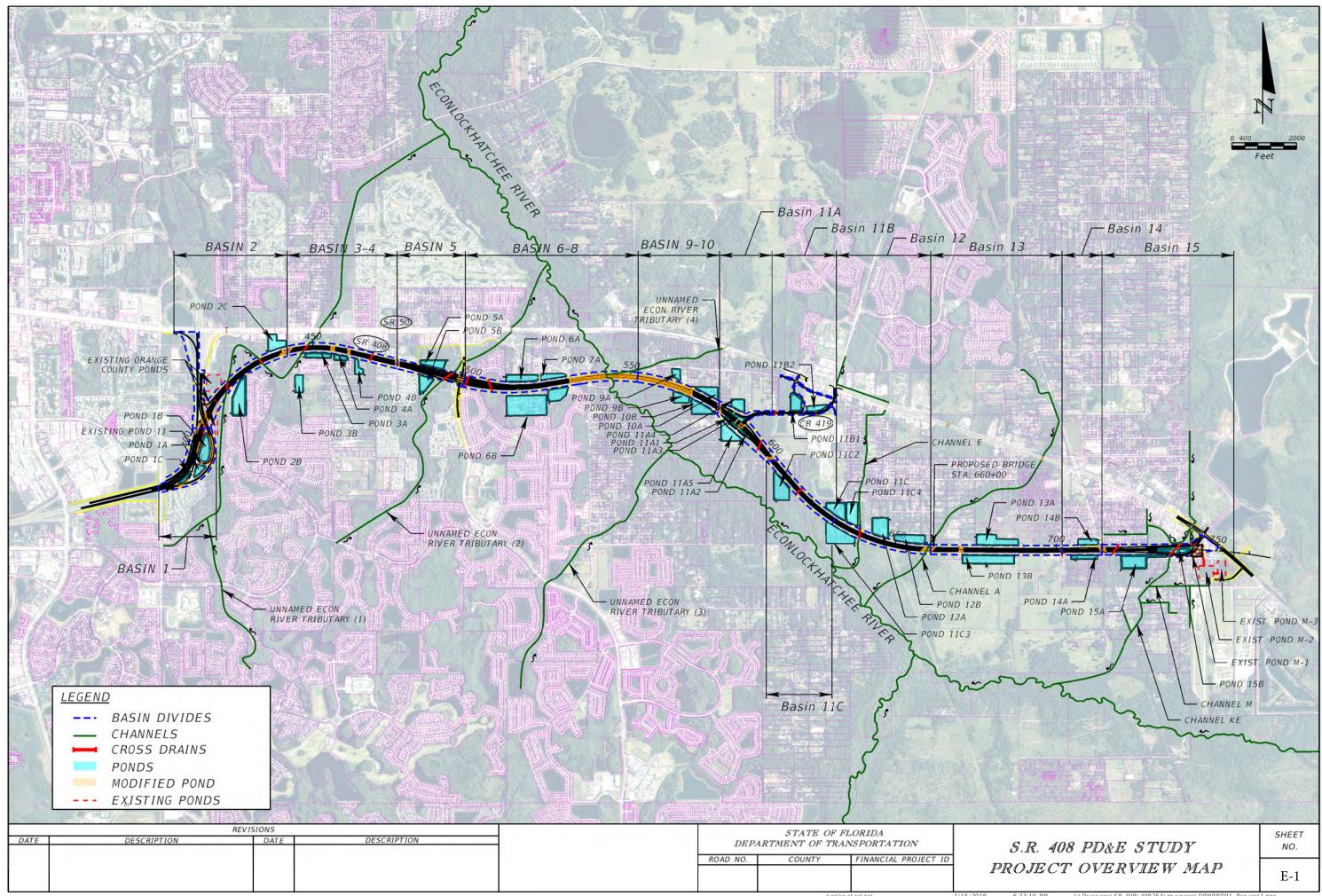


Appendix: E

Proposed Pond Site Maps

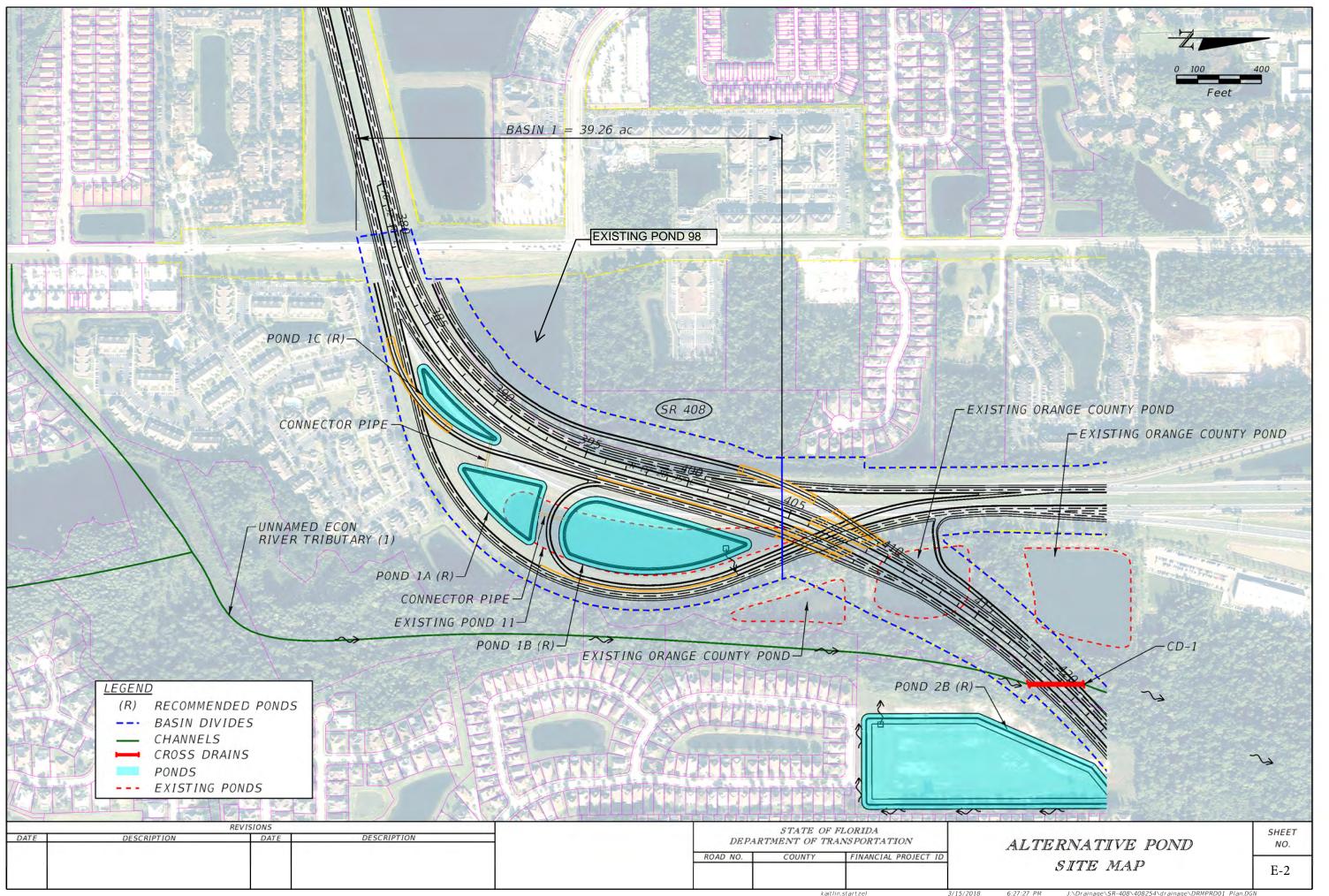
- Project Overview Map
- Alternative Pond Site Maps
- Alternative Pond Tax Maps
- Floodplain Maps
- Wetland Maps

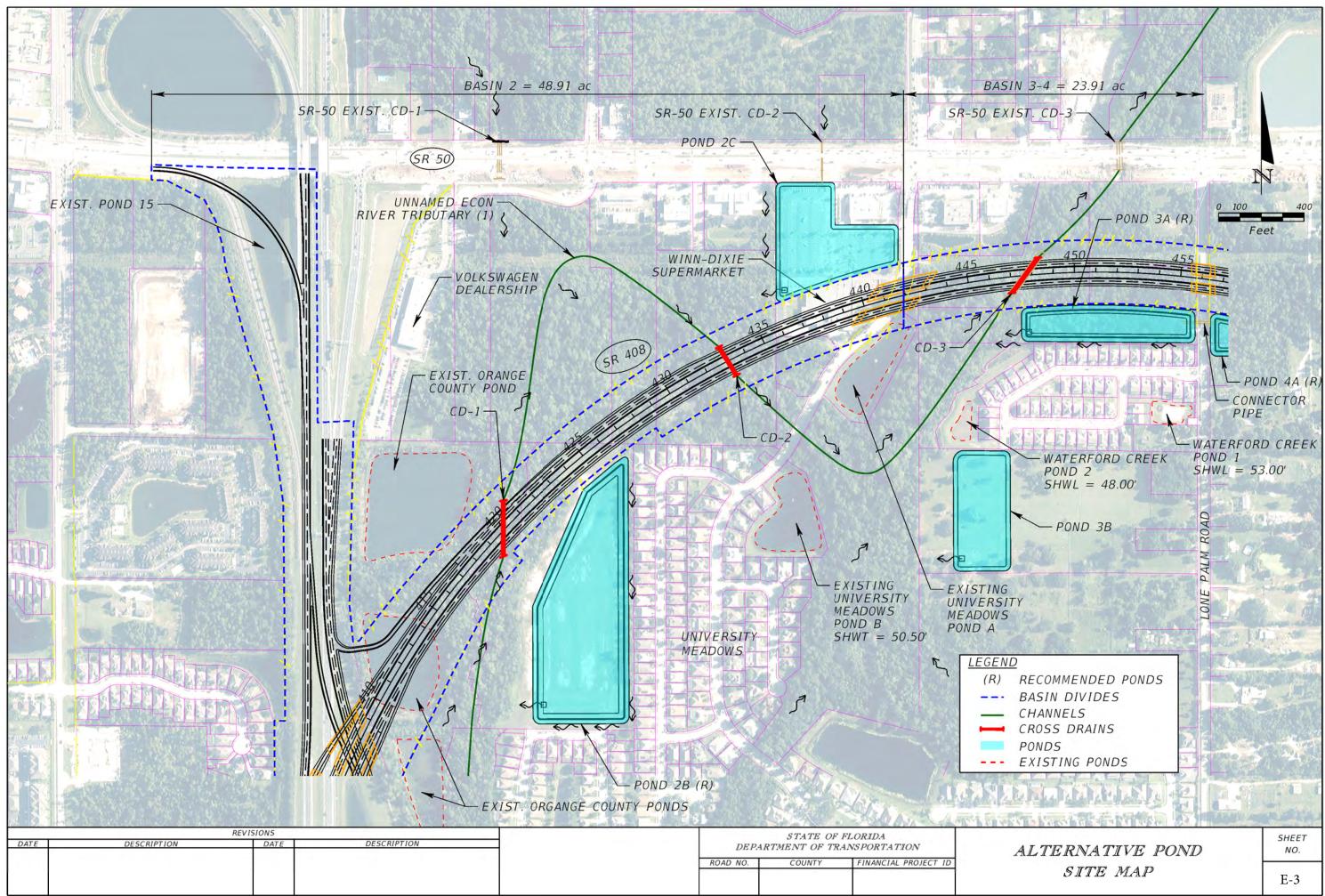
Project Overview Map

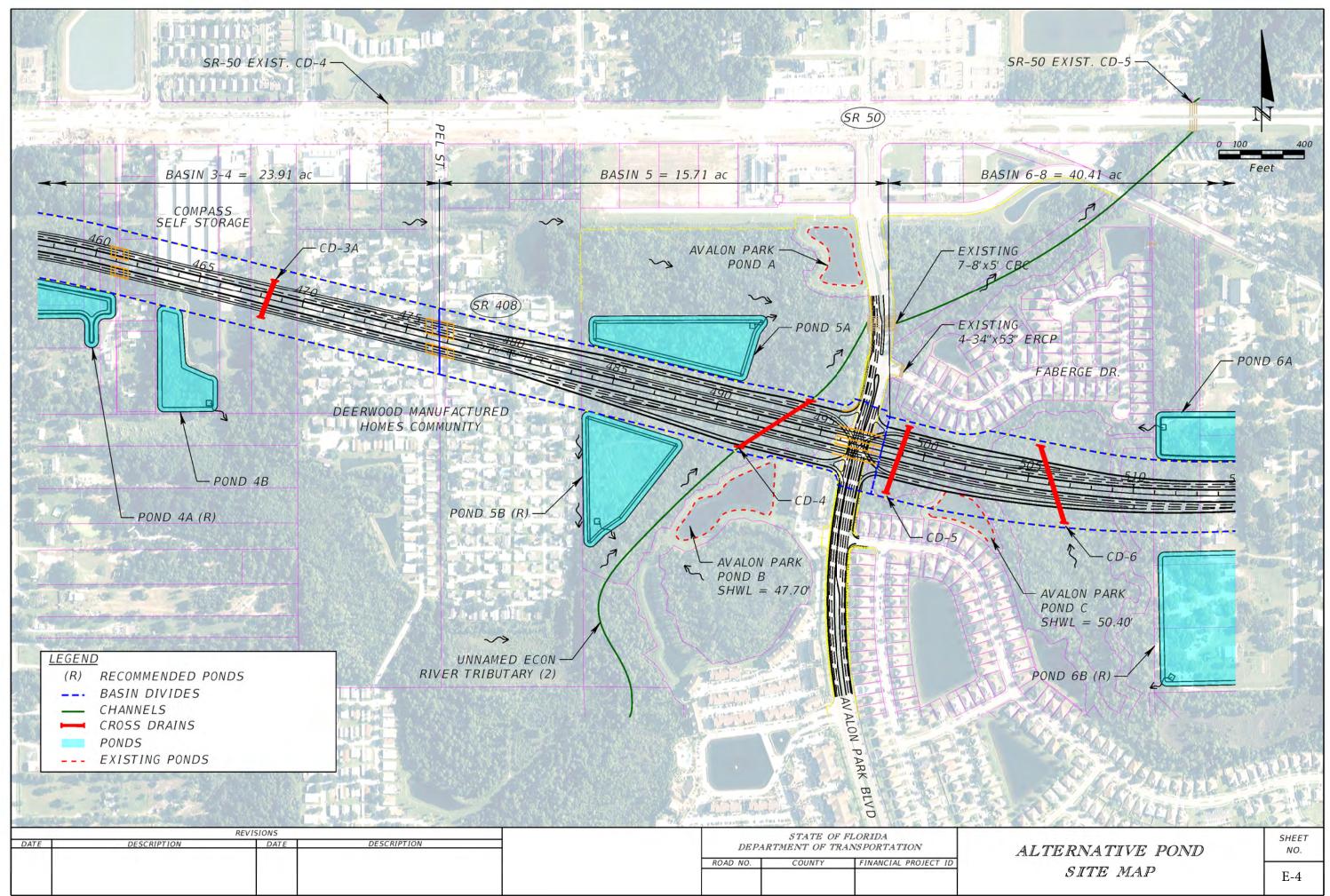


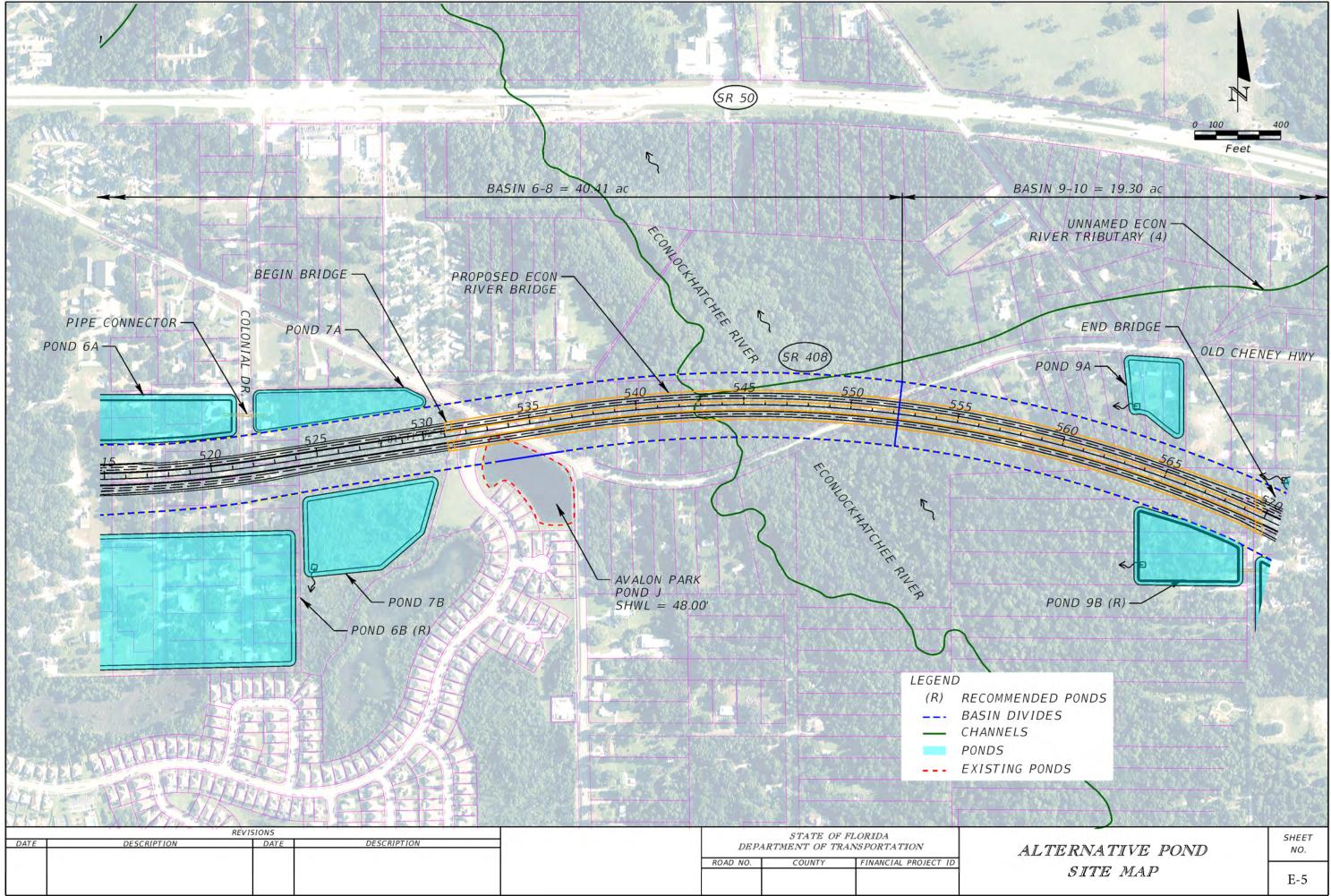
3/15/2018

Alternative Pond Site Maps



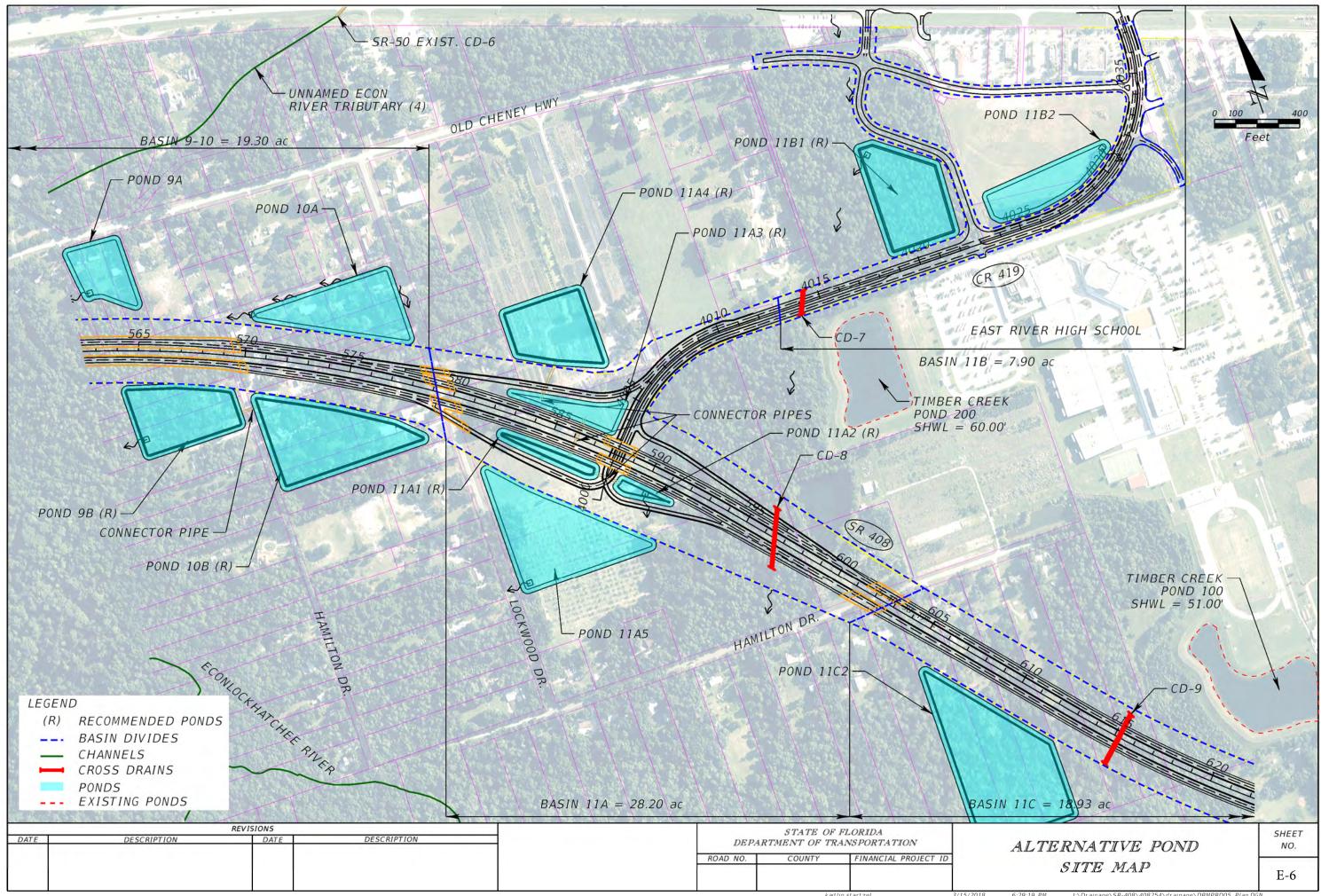


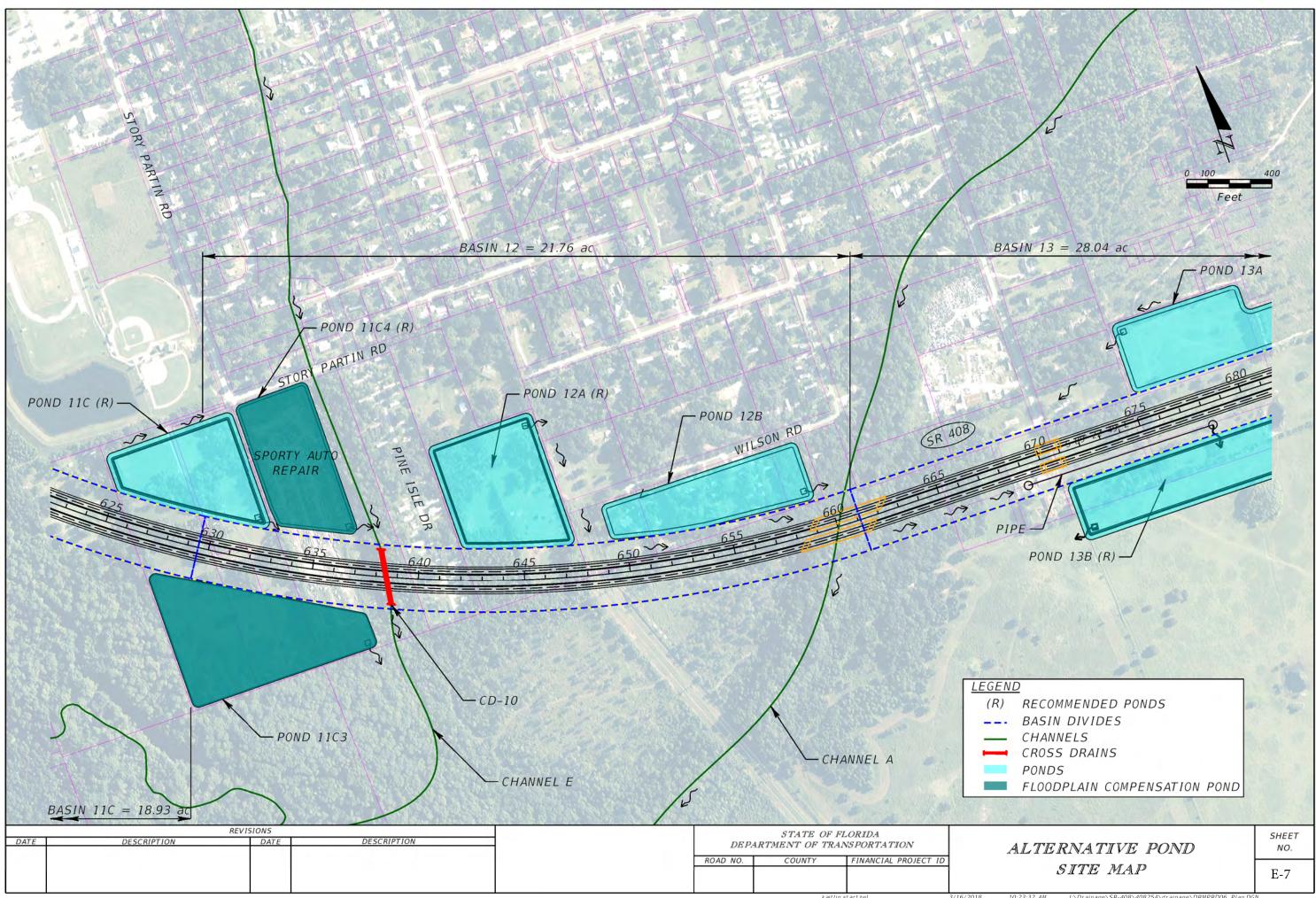




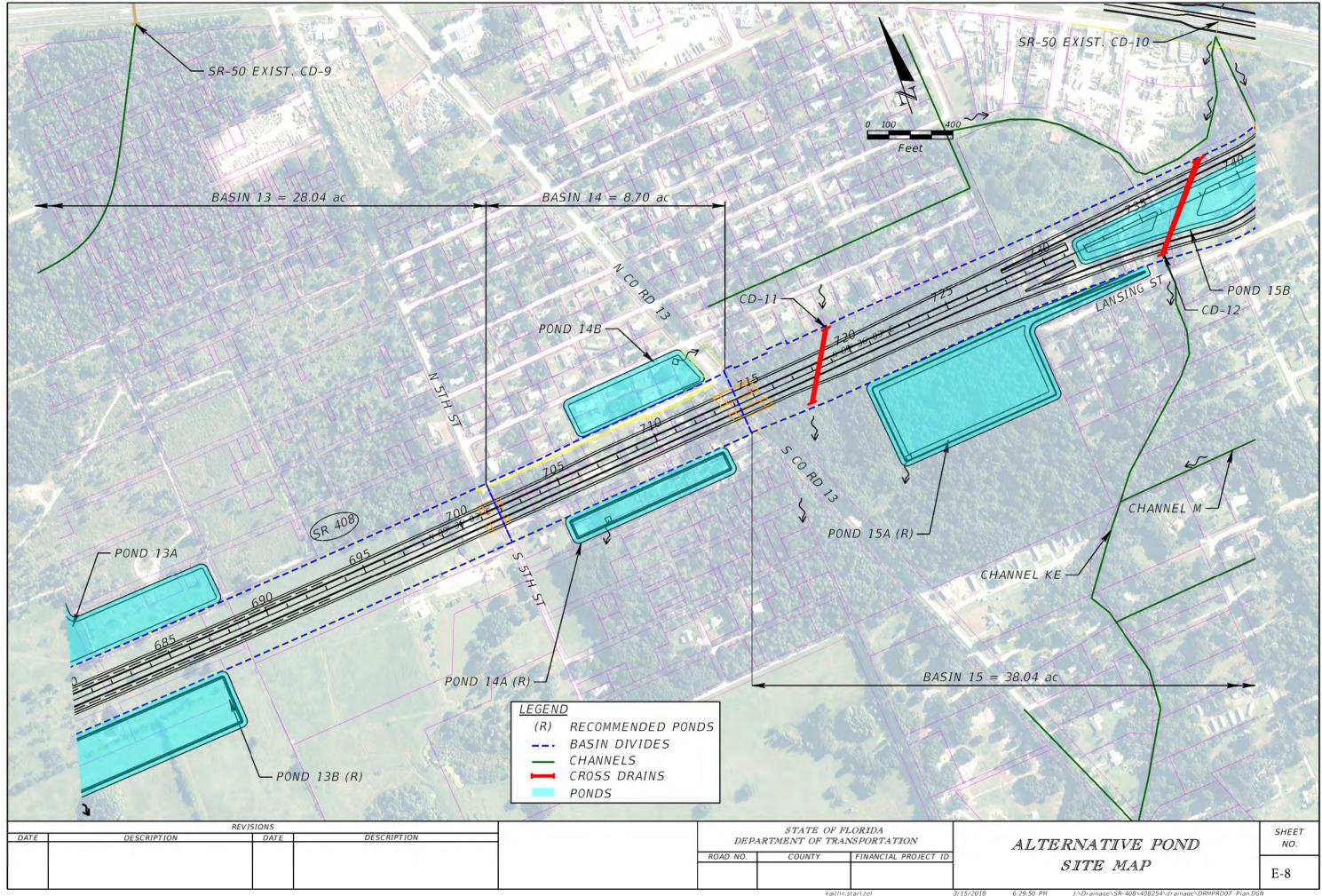
3/15/2018 6:2

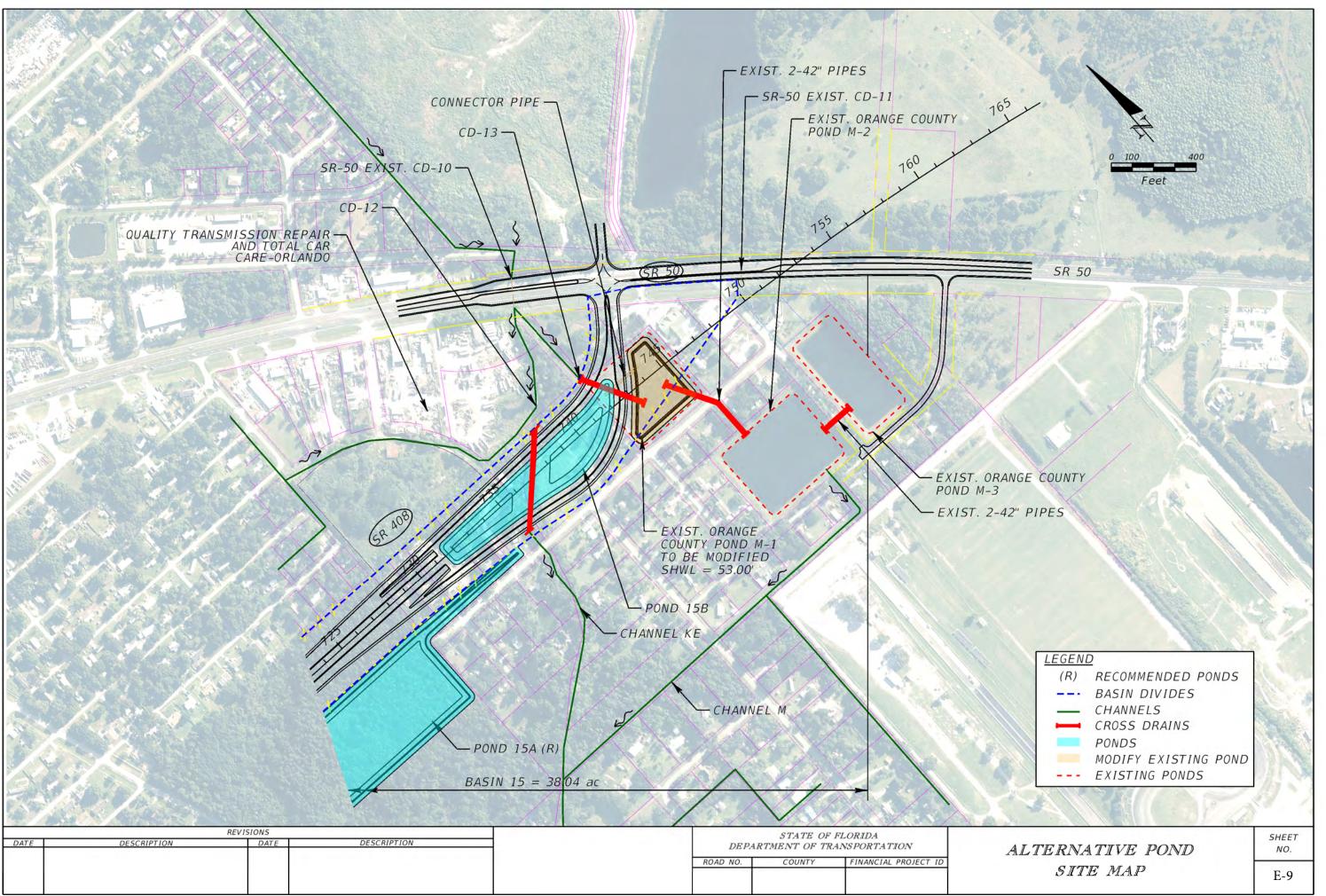
J:\Drainage\SR-408\408254\drainage\DRMPRD04_Plan.DGN



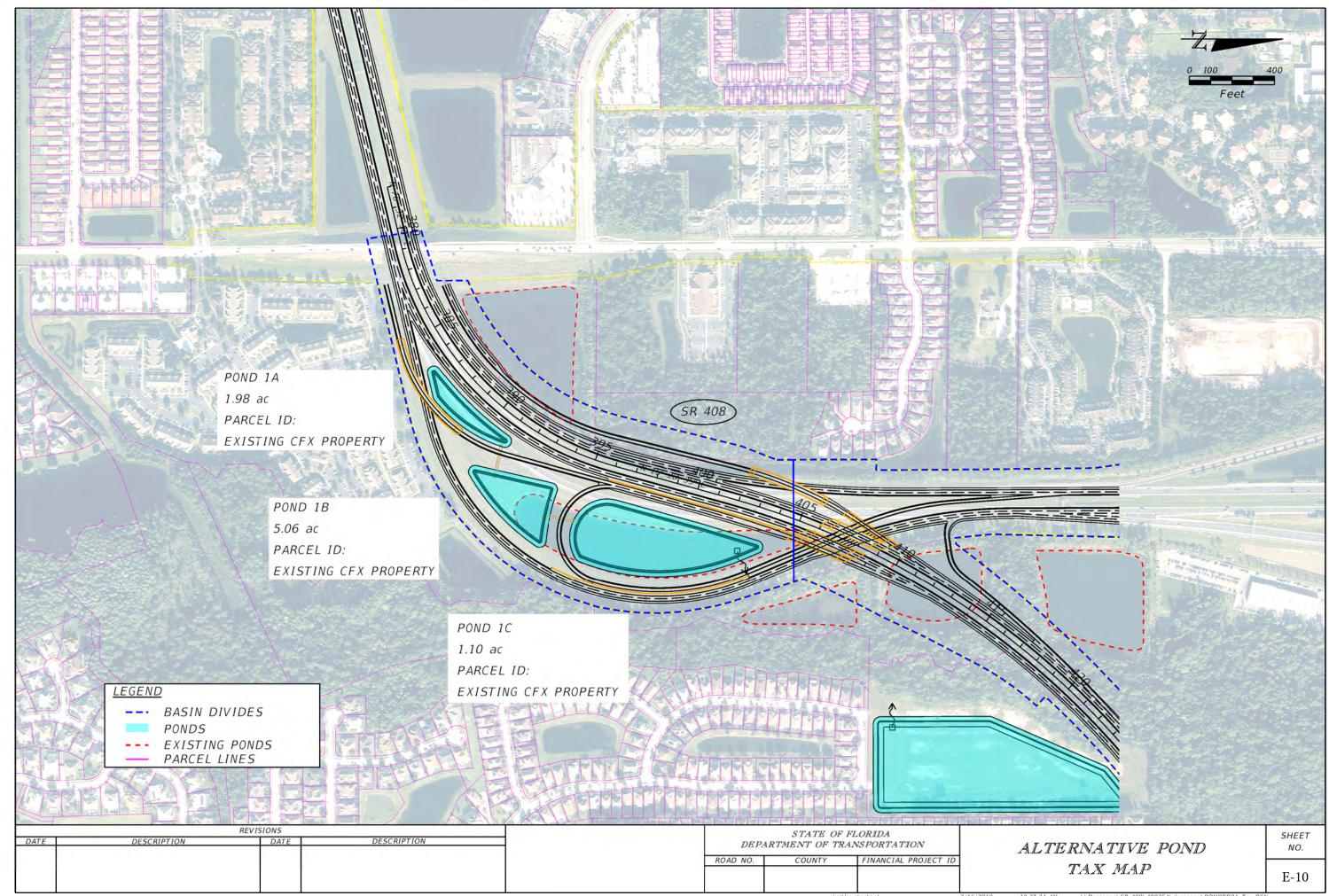


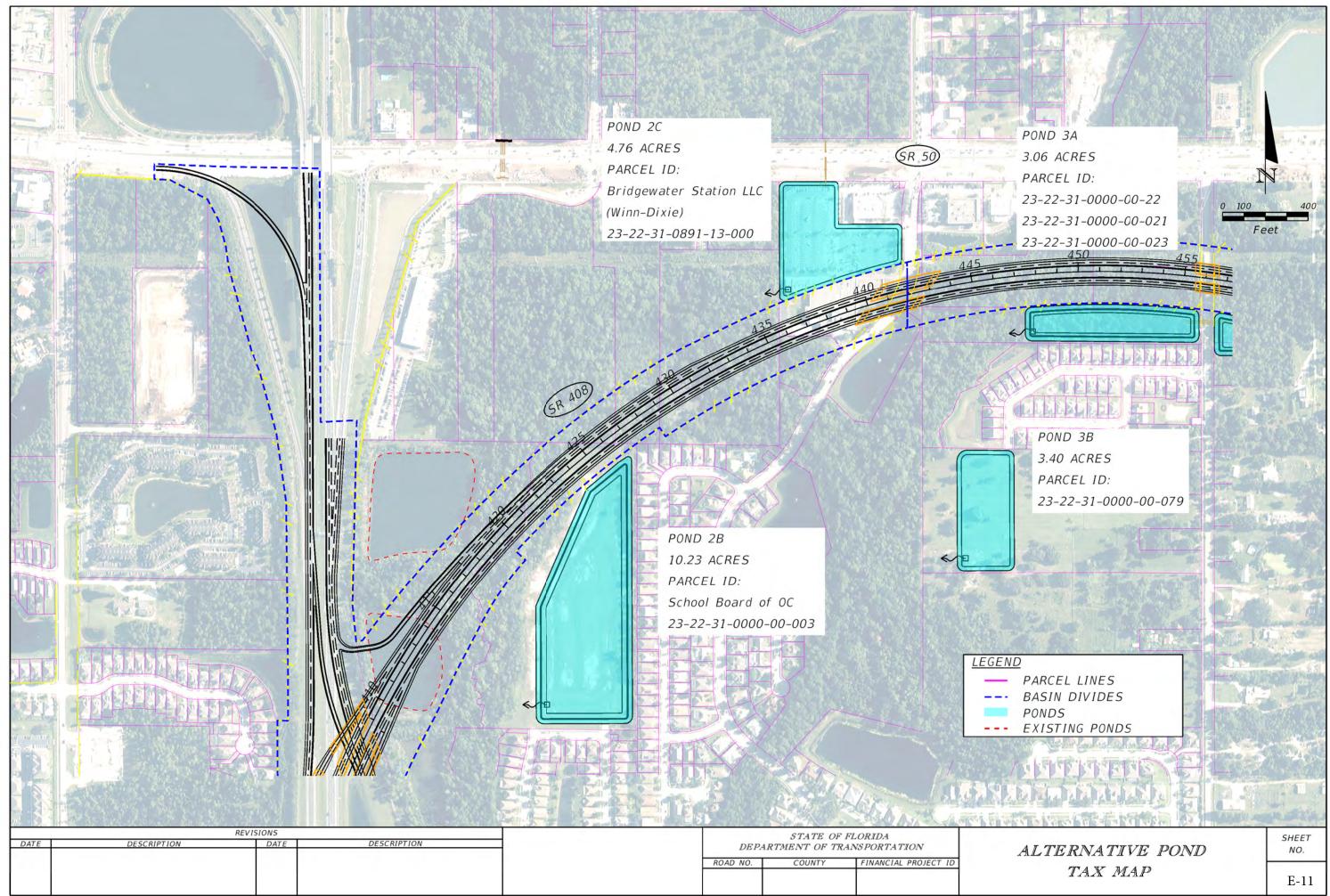
M J:\Drainage\SR-408\408254\drainage\DRMPRD06_Plan.D0

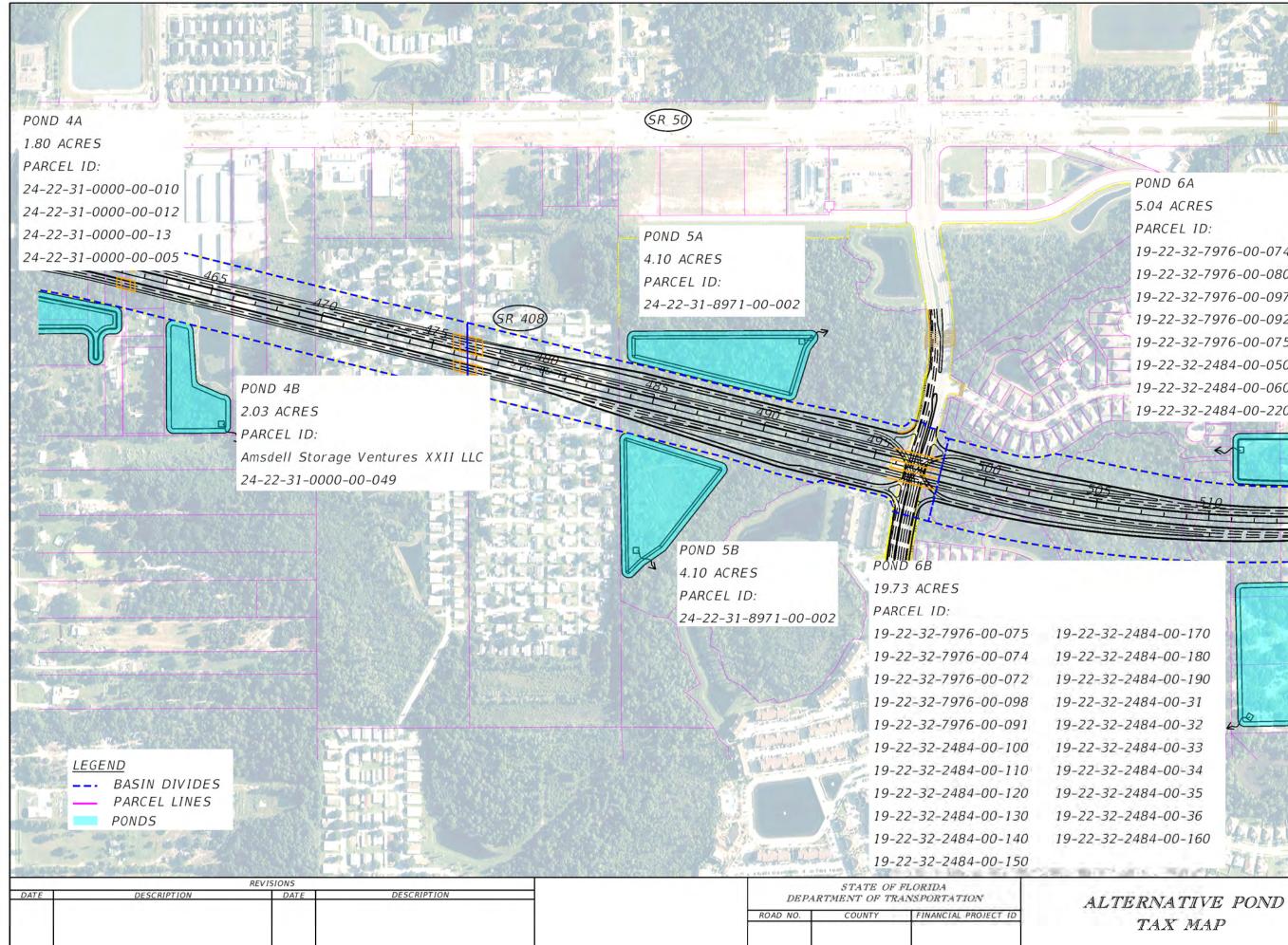




Alternative Pond Tax Maps





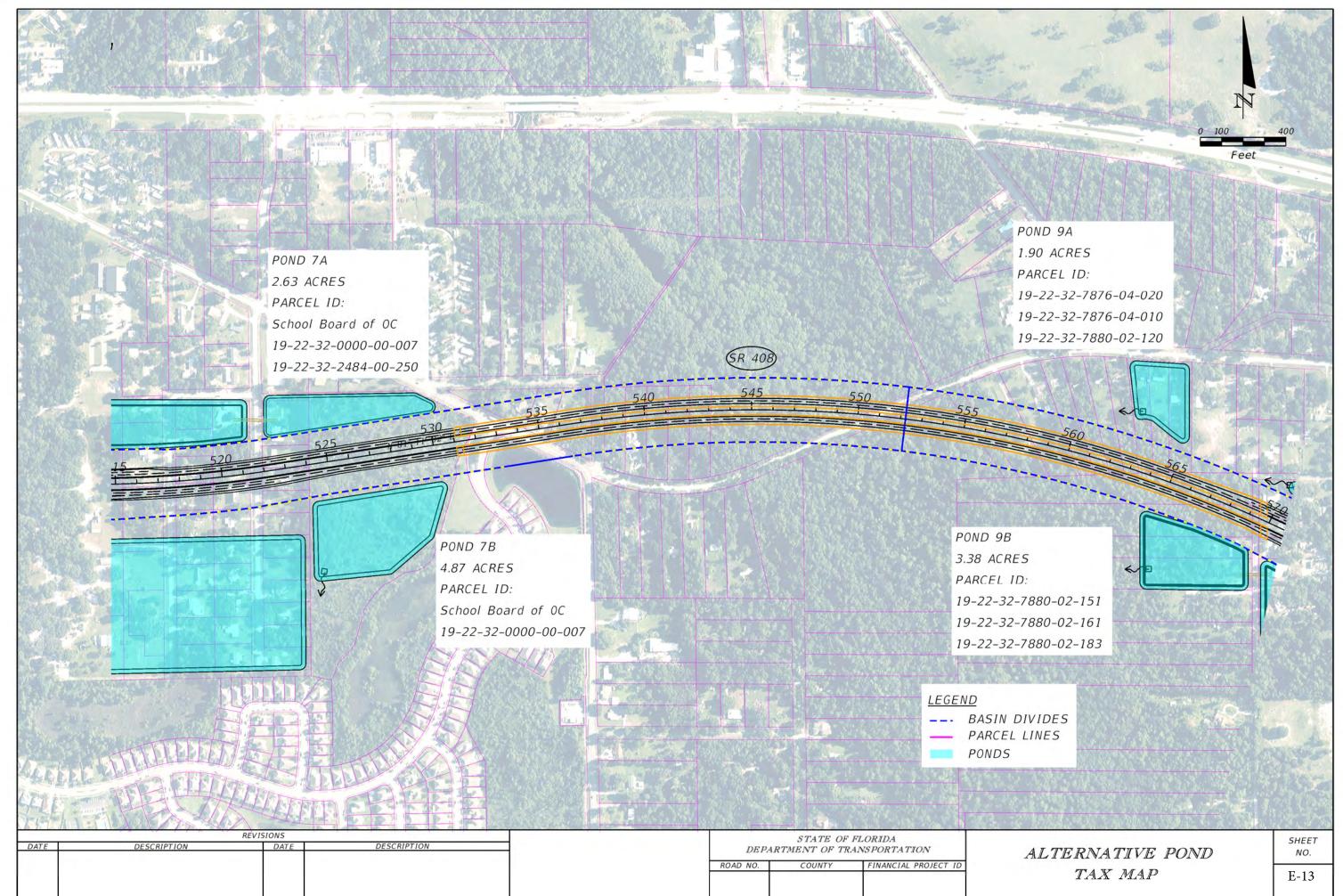


19-22-32-7976-00-074 19-22-32-7976-00-080 19-22-32-7976-00-097 19-22-32-7976-00-092 19-22-32-7976-00-075 19-22-32-2484-00-050 19-22-32-2484-00-060 19-22-32-2484-00-220

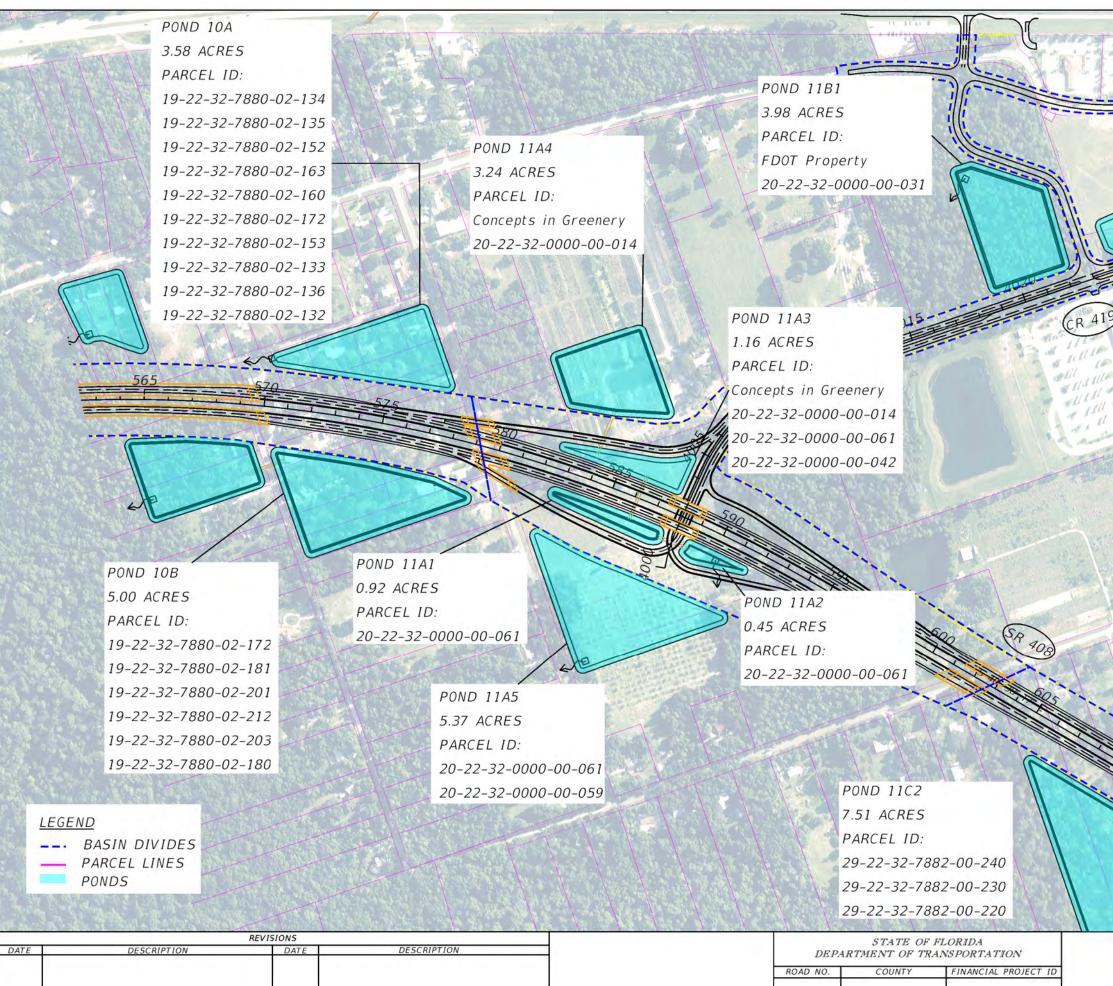
Feet

SHEET NO.

E-12



3/15/2018 6



POND 11B2 2.30 ACRES PARCEL ID: 20-22-32-4910-00-001 20-22-32-4910-00-002 20-22-32-4910-00-030

E-14

PON 8.0 PAF 22-POND 11C 22-5.70 ACRES 22-POND 11C4 PARCEL ID: 22. 5.52 ACRES 29-22-32-6721-00-030 PARCEL ID: POND 12B 29-22-32-6721-00-020 POND 12A 28-22-32-0000-00-015 5.33 ACRES 29-22-32-6721-00-010 6.88 ACRES PARCEL ID: PARCEL ID: 21-22-32-0734-00-970 28-22-32-0000-00-003 21-22-32-0734-00-960 21-22-32-0734-00-990 POND 13B 640 10.45 ACRES PARCEL ID: 22-22-32-0712-22-22-32-0712-. 22-22-32-0712-28-22-32-0000-POND 11C3 8.85 ACRES LEGEN PARCEL ID: 29-22-32-6721-00-030 29-22-32-6721-00-020 29-22-32-6721-00-010 28-22-32-0000-00-015 REVISIONS STATE OF FLORIDA DESCRIPTION DESCRIPTION DATE DATE DEPARTMENT OF TRANSPORTATION AI FINANCIAL PROJECT ID ROAD NO. COUNTY

	CHAN F	
	The second	4
ND 13A	TH	a fine and
1 ACRES	0 100	400
RCEL ID:	Feet	
-22-32-0712-00-000		
-22-32-0712-36-001		
-22-32-0712-36-013	/ FIL	
-22-32-0712-36-021		
		To the State
L		- Alle
	(80	
Le le		H
675		
620		a manual
	Æ	
	2	
A		
21-010		
37-001		
14-010		
00-008		0-10
D		3.54
 BASIN DIVIDES		
PARCEL LINES		
PONDS FLOODPLAIN COMPEN	SATION POND	
*		
LTERNATIVE I		SHEET NO.
TAX MAP		E-15

POND 14B 2.75 ACRES PARCEL ID: 22-22-32-0712-18-410 22-22-32-0712-18-370 22-22-32-0712-18-370 22-22-32-0712-18-470 22-22-32-0712-18-430 22-22-32-0712-18-290 22-22-32-0712-18-290 22-22-32-0712-18-290

> POND 14A 2.57 ACRES PARCEL 1D: 22-22-32-0712-20-150 22-22-32-0712-20-520 22-22-32-0712-20-017 22-22-32-0712-20-510 22-22-32-0712-20-013 22-22-32-0712-20-054 22-22-32-0712-20-013 22-22-32-0712-20-058 22-22-32-0712-20-045 22-22-32-0712-20-750 22-22-32-0712-20-043 22-22-32-0712-20-060

POND 15A 8.92 ACRES PARCEL ID: 27-22-32-0000-00-007 21-22-32-0735-00-001 21-22-32-0735-00-020 21-22-32-0735-00-030 21-22-32-0735-00-062 21-22-32-0735-00-061 21-22-32-0735-00-063

	3						5.0
		REVISIONS			STATE OF	FLORIDA	
DATE	DESCRIPTION	DATE	DESCRIPTION	DEPAK		ANSPORTATION	
				ROAD NO.	COUNTY	FINANCIAL PROJECT ID	

LEGEND

BASIN DIVIDES

PARCEL LINES

PONDS

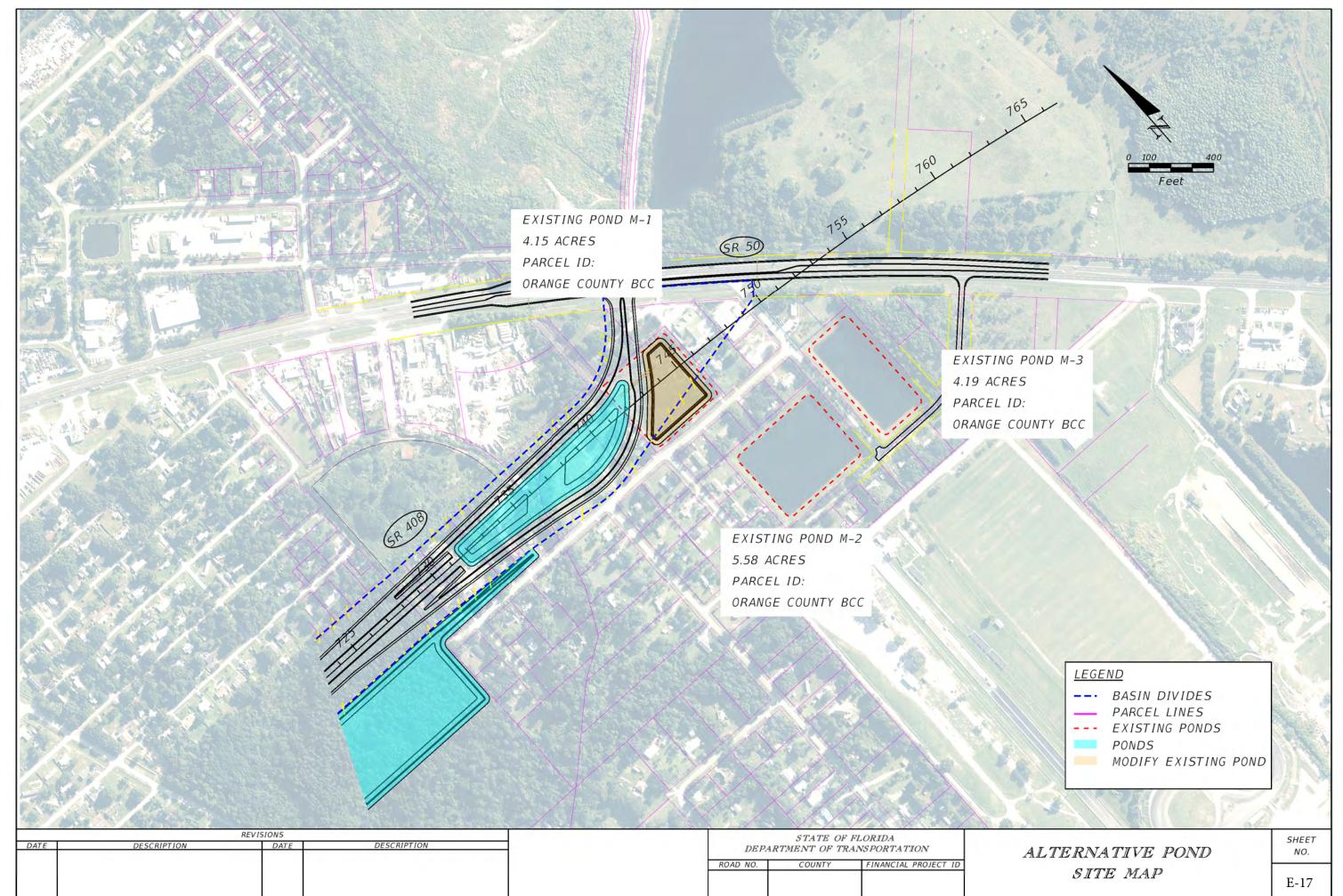
POND 15B 4.37 ACRES PARCEL ID: Orange County BCC 26-22-32-0800-00-450 21-22-32-0735-00-092 21-22-32-0735-00-091 21-22-32-0735-00-083 21-22-32-0735-00-082 21-22-32-0735-00-081 21-22-32-0735-00-072 21-22-32-0735-00-071 21-22-32-0735-00-070 21-22-32-0735-00-063 21-22-32-0735-00-061 21-22-32-0735-00-062 21-22-32-0735-00-010 21-22-32-0735-00-030

ALTERNATIVE POND TAX MAP SHEET NO.

E-16

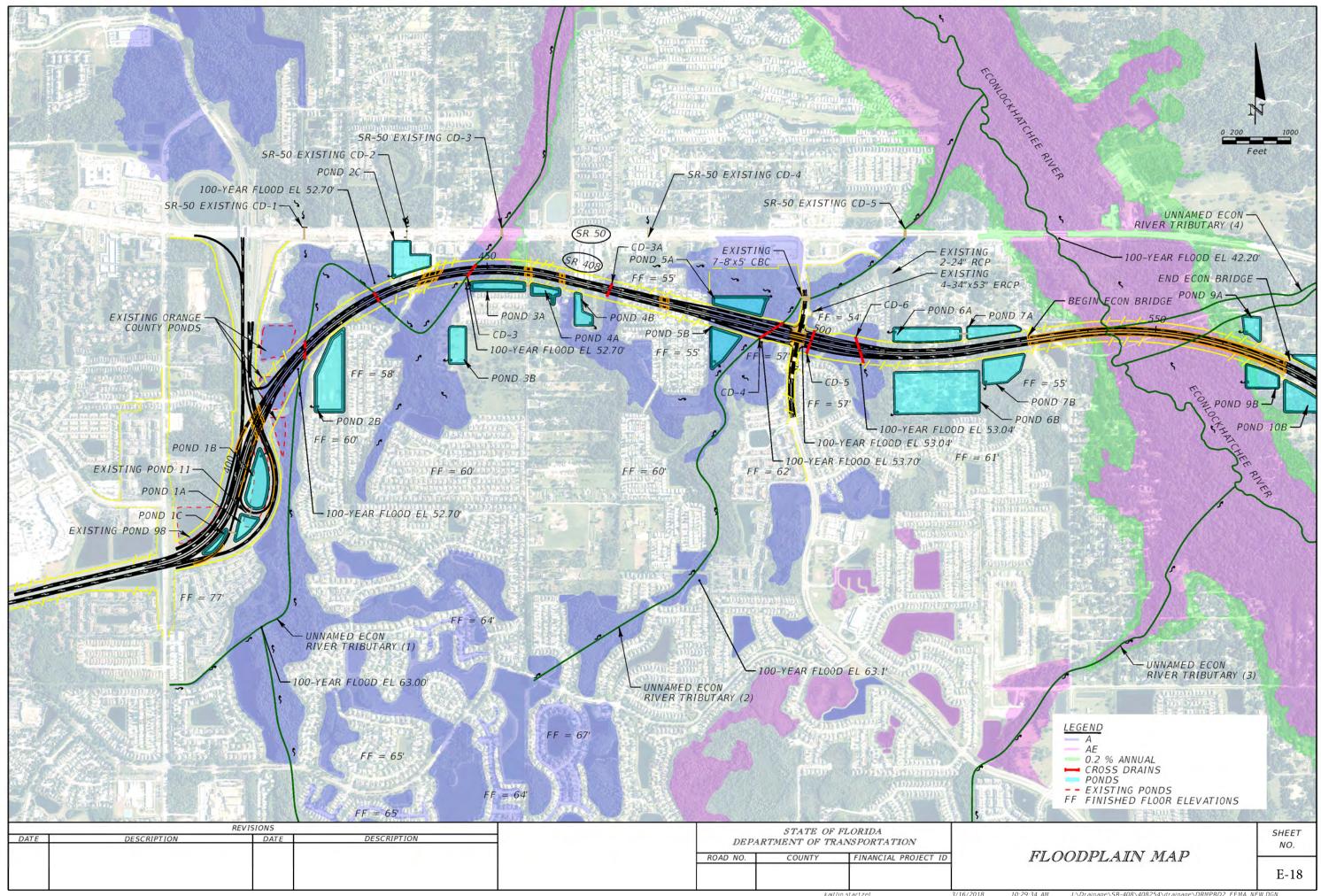
2:23 PN

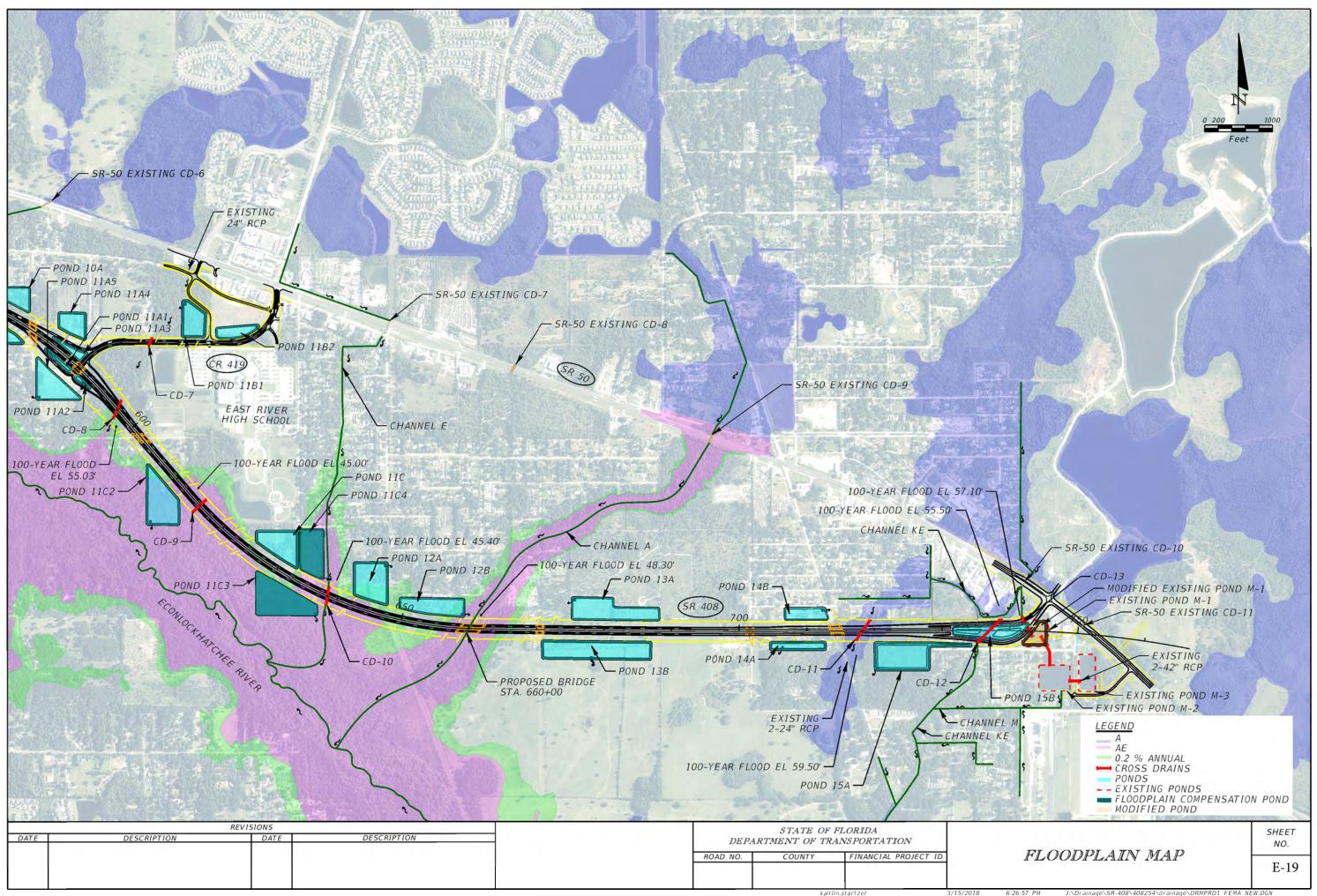
J:\Drainage\SR-408\408254\drainage\DRMPRD07_Tax.DGN



	3/	15/201	18
--	----	--------	----

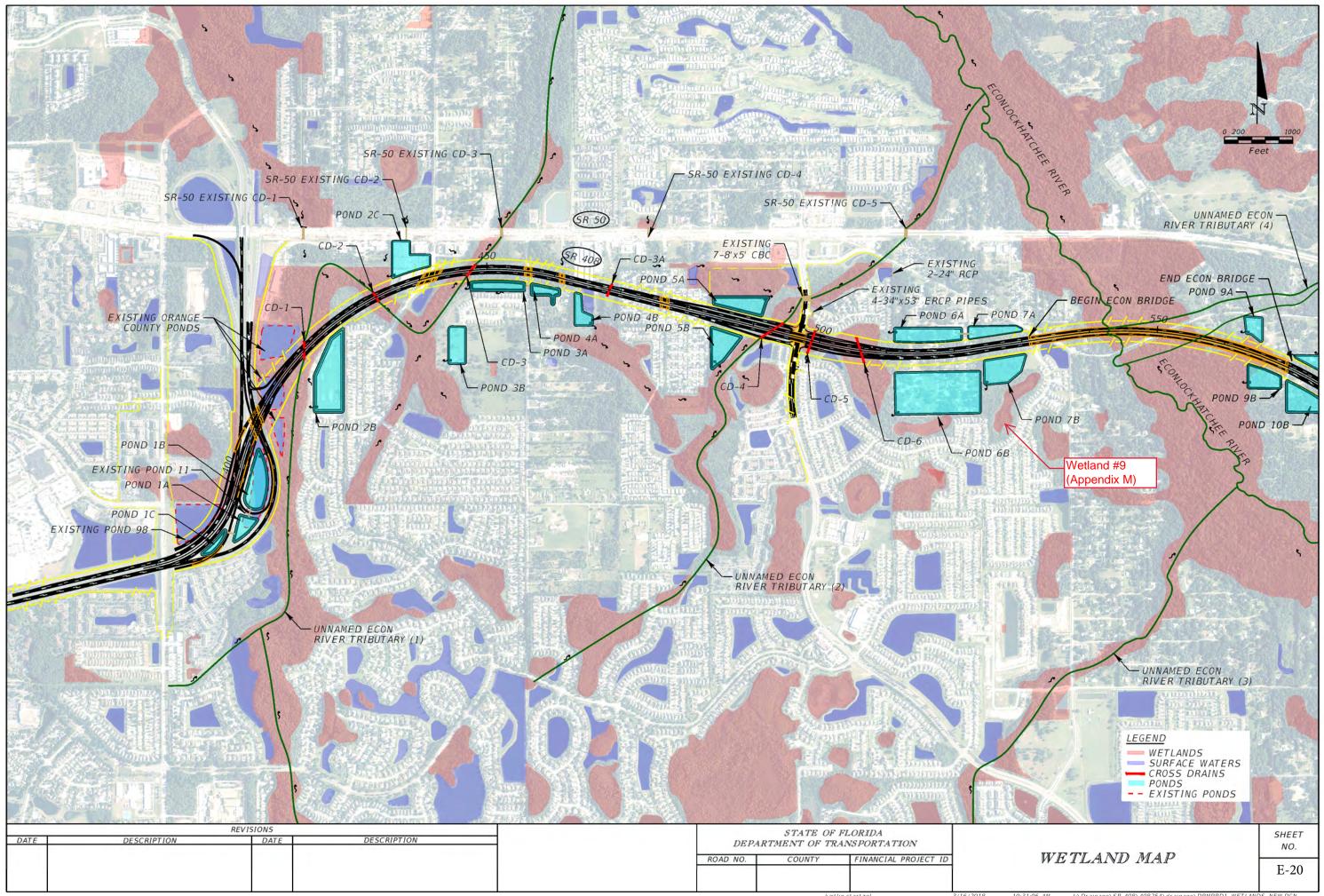
Floodplain Maps

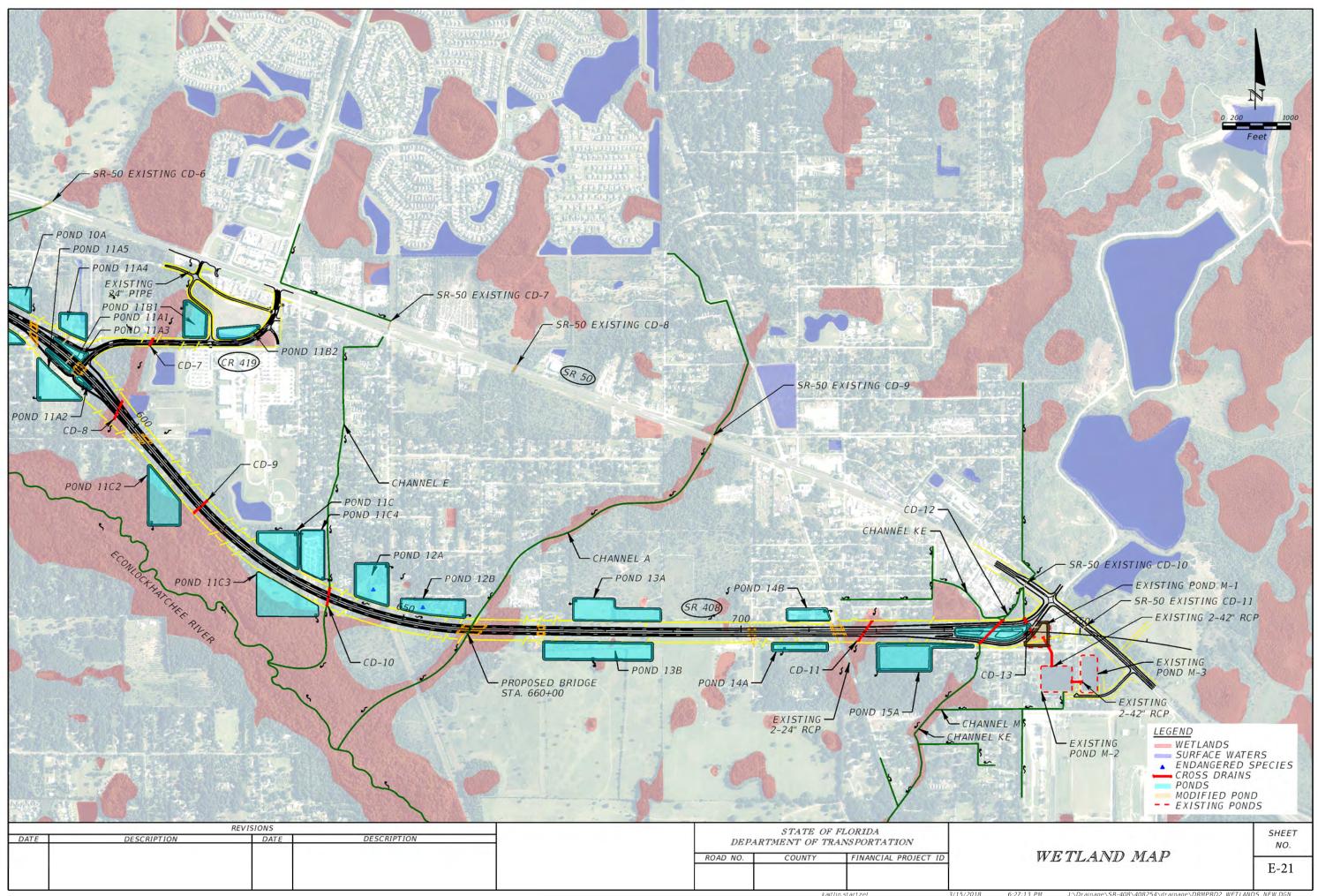




:\Drainage\SR-408\408254\drainage\D

Wetland Maps





:\Drainage\SR-408\408254\drainage\DRMPRD2_WETLAND NEW.DGN

Appendix: F

Pond Sizing Calculations

SR 408 Eastern Extension-PD&E CFX BASIN 1 POND 1A & 1B (EXISTING POND 11)

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	38015.00
End Station	40495.00
Length (ft)	2480.00

	Total Basin Area	l		
	<u>R/W Width (ft)</u>			<u>Area (ac)</u>
SR 408 (Ramps, ponds and infield Areas)	n/a	2480		39.26
			TOTAL AREA (AC)	39.26
	Existing Impervious	Area		
Description		Area		
Existing Impervious areas within the ba	asin limits	5.05		
То	tal Impervious Area	5.05	Acre	

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
Existing SR 50 and SR 408 Roadway					
On-site Roadway and Residential	B/D	98	5.05	494.90	
On-site Grassed Area	B/D	80	28.01	2,240.80	
Existing Infield Pond	B/D	100	6.20	620.00	
		TOTAL	39.26	3,355.70	
		COM	POSITE CN	85.5	

	Estimate of F	Runoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.70	6.95	22.73
100 yr, 240 hr	FDOT	18.00	1.70	16.11	52.71
100 yr, 8 hr	FDOT	8.00	1.70	6.27	20.51
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.70
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.95
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	22.73

	Proposed I	mpervious Area			
Description	Width (ft)	Length(ft)	Area		
SR 408 Proposed Pavement	assumed impervious media	n on mainline.	11.70		
	Total Impervious Ar	rea	11.70	Acre	

Existing Impervious areas on SR 408 already treated in existing FDOT Pond-11.

Existing roadway will be reconstructed therefore, the entire impervious areas in proposed condition needs to be treated. Existing Pond-11 will be modified to accommodate the proposed project.

Post Development

Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
Proposed SR 408 and Existing SR	50				
On-site Roadway	B/D	98	11.70	1,146.60	
On-site Grassed Area	B/D	80	19.39	1,551.20	
Proposed Pond Area	B/D	100	8.17	817.00	
		TOTAL	39.26	3,514.80	
		COM	POSITE CN	89.5	

	Estimate of F	Runoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.17	7.44	24.34
100 yr, 240 hr	FDOT	18.00	1.17	16.67	54.53
100 yr, 8 hr	FDOT	8.00	1.17	6.75	22.08
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.17
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.44
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	24.34

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) CN:	39.26 85.5		POST DEVELOF AREA (AC): CN:	
AGENCY	DESIGN	RU	NOFF VOLUME	(Vr)
	STORM	PRE	POST	INCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 Yr, 24 hr	22.73	24.34	1.60
FDOT	100 yr, 240 hr	52.71	54.53	1.83
FDOT	100 yr, 8 hr	20.51	22.08	1.57

MAXIMUM ATTENUATION VOLUME (AC-ET) 183			
	MAXIMUM ATTENUATION VOLUME (AC-	(FEI) 183	

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	39.26
Post Development Impervious Area (ac) =	11.70

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	4.91	Governs
2) 3.75" of Runoff Over Impervious Area =	3.66	
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.66	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maintenance Berm.

Per the existing permit, the Normal Water Level in existing Pond-11 is 3.5' below existing ground.
Existing Pond-11 berm = 61.5' and NWL = 58.0'
We will assume the SHWT elevations for the purpose of preliminary pond sizing to be at 3.5' below ground.
Pond Depth from top of Maint

	i top of Maint							
Be	erm to SHWT	3.5	ft					
<i>I</i> aintenance Berm (M	laint Berm) =	1	ft					
H = Dep	th to pond SHWT - Ma	intenance Be	rm	=	2.5	ft		
3) Use greater of rec	quired treatment volum	ie or attenuati	on volu	me.				
		Re	quired /	Attenuatio	n Volume	=	1.83	ac-ft
		R	equired	Treatmer	nt Volume	=	4.91	ac-ft
				Pea	k Volume	=	6.74	ac-ft
4) For purposes of p	oond area calculations,	assume a sq	uare po	ond.				

Volume =	LWH
----------	-----

where	H =	height (ft)
	L =	length of vertical sided pond
	VV =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume = H =	6.74 2.5	a ft	ic-ft			
		6.74	=		$L^2 x$	2.5
	Solving for L = Therefore W =		342.6 342.6	ft ft		

5) Increase dimensions to account for side slopes.

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes:	4	ft/ft
H:	2.5	ft
x =	20	ft
Length @ top of slope =	363	ft
Width @ top of slope =	363	ft

6) Add maintenance berms.

Assume 20' maintenance berm (add to each side)						
Length w/maint Berm =	403	ft				
Width w/maint. Berm =	403	ft				
Total Area =	3.72	acre				
Add 10 % Contingency	4.09	acre				
PRELIMINARY POND ARE	A REQUIRE	D FOR BASIN-1=	4.1	ACRES		

Basin 1 can provide required treatment and attenuation volume in proposed Pond 1A, Pond 1B and Pond 1C, which is by expanding the existing Pond-11.

Pond-11 can be expanded to accommodate the additional runoff from the new roadway alignment.

Existing Pond-11	6.20 acre
Proposed Pond 1A (expanding Pc	1.98 acre
Proposed Pond 1B (expanding Pc	5.06 acre
Proposed Pond 1C (Infield Area)	1.10 acre

Therefore, existing pond and infield areas has additional capacity and room for expansion. No new parcels required for this basin.

Flood plain impact is not anticipated in this basin.

Existing Ground Elevation =	61.5 ft
Normal Water Elevation =	58 ft (Existing Pond-11 NWL = 58' NAVD) Per the existing permit.
Lowest EOP Elevation =	67.51 ft
Total Pond Area=	8.14 acre

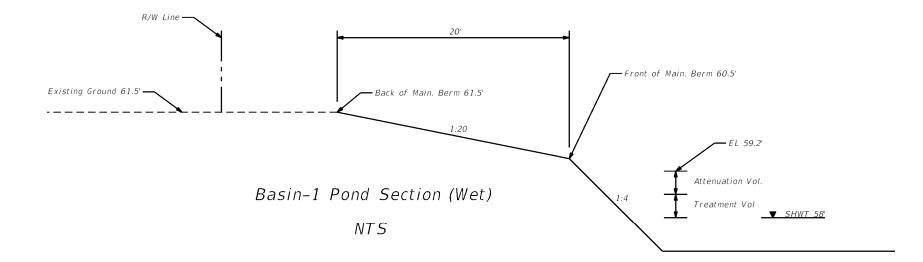
Pond Stage/Storage Calculations

			Ave Area		Storage (ac-	Total Storage
Stage	Description	Area (ac)	(ac)	Depth (ft)	ft)	(ac-ft)
58	Normal Water Level	5.26				0.00
59.5		5.80	5.53	1.50	8.30	8.30
60.5	Front Main Berm	6.17	5.99	1.00	5.99	14.28
61.5	Back Main Berm	8.14	7.16	1.00	7.16	21.44

Required Treatment and Attenuation Volume =

6.74 ac-ft

Provided treatment and attenuation volume = Provided treatment and attenuation Stage= 6.74 ac-ft 59.2 ft



SR 408 Eastern Extension-PD&E CFX BASIN 2

Computed By Checked By Date

KS CR 2/26/2017

Beginning Station	40495.00
End Station	44195.00
Length (ft)	3700.00

Total Basin Area		
R/W Width (ft)		<u>Area (ac)</u>
Existing roadway		8.71
Grass and Wooded Area		35.46
Existing infield Pond-15 (SW Quadrant of SR 405/SR 50 Interchange)		1.95
Existing Pond South of VW Dealership		2.79
	TOTAL AREA (AC)	48.91

Existing Impervio	us Area		
Description	Area		
Existing Impervious areas within the basin limits	8.71		
Total Impervious Area	8.71	Acre	

ATTENUATION VOLUME ESTIMATE

Pre-Development

		CON	IPOSITE CI	85.1	
		TOTAL	48.91	4,164.38	
Dealership	A/D	100	2.79	279.00	
Existing Pond-15 Existing Pond South of VW	A/D	100	1.95	195.00	
On-site Grassed Area	A/D	80	35.46	2,836.80	
On-site Roadway	A/D	98	8.71	853.58	
Soil Name			(ac)		
Land Use Description/	Soil Group	CN	Area	Product	

	Estimate of R	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.74	6.91	28.15
100 yr, 240 hr	FDOT	18.00	1.74	16.06	65.47
100 yr, 8 hr	FDOT	8.00	1.74	6.23	25.39
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (S	1.74
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.91
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	28.15

Proposed Impervious Area				
Description	Area			
SR 408 Proposed Alignment (Assuming impervious median from Sta 409+00 to 441+95)	18.09			
Total Impervious Area	18.09	Acre		

Post Development

Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
Proposed SR 408					
On-site Roadway	A/D	98.00	18.09	1,772.43	
On-site Grassed Area	A/D	80	28.87	2,309.92	
Existing Pond -15	A/D	100	1.95	195.00	
		TOTAL	48.91	4,277.35	
		CON	IPOSITE CI	N 87.5	

	Estimate of Runo	off Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.43	7.19	29.29
100 yr, 240 hr	FDOT	18.00	1.43	16.39	66.79
100 yr, 8 hr	FDOT	8.00	1.43	6.50	26.51
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (S	1.43
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.19
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	29.29

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) 48.91 CN: 85.1			POST DEVE AREA (AC): CN:	LOPED CONDIT 48.91 87.5	rion
AGENCY	DESIGN	RUI	NOFF VOLUM	E (Vr)	
	STORM	PRE	POST	INCREASE	
		(AC-FT)	(AC-FT)	(AC-FT)	
SJRWMD	25 Yr,24 hr	28.15	29.29	1.14	
FDOT	100 yr, 240 hr	65.47	66.79	1.32	
FDOT	100 yr, 8 hr	25.39	26.51	1.11	
MAXIMUM ATTENUATION VOLU	JME (AC-FT)	1.	32		

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	48.91
Post Development Impervious Area (ac) =	18.09

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	6.11	Governs
2) 3.75" of Runoff Over Impervious Area =	5.65	
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	6.11	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Used SHWT elevation from adjacent University Medows development Pond B. The SHWT elevation from permit plans = 50.5'

Pond Depth from top of Maint Berm to SHWT Maint Berm =	- 9		ft ft						
H = Depth to	o pond SHWT -	Maint Bern	n	=		8	ft		
3) Use greater of required tr	reatment volum	e or attenua	ation vol	lume.					
						Volume Volume		1.32 6.11	ac-ft ac-ft
					Peak	Volume	=	7.43	ac-ft
For purposes of pond are	ea calculations,	assume a s	square p	ond.					
Volume = LWH where	e H L W	=	-	· · /		ed pond d pond			
Since a square pond is being	g assumed, L =	W. Theref	ore, Vol	ume = L	_²H				
Volume = H =		-	ac-ft ft						
		7.43	3	=		L ² x	8		
	Solving for L = Therefore W =			01.1 01.1	ft ft				

5) Increase dimensions to account for side slopes.

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 8	ft/ft ft			
x =	64	ft			
Length @ top of slope = Width @ top of slope = <u>6) Add maintenance berms.</u>	265 265	ft ft			
Assume 20' maintenance berm (a	add to each side)				
Length w/maint berm = Width w/maint. Berm =	305 305	ft ft			
Total Area = Add 10 % Contingency	2.14 2.35	acre acre			
PRELIMINARY POND AREA REQUIRED FOR BASIN-2=					
Recommended Pond 2B					

Existing Ground Elevation =	58.5 ft
Normal Water Elevation =	50.5 ft
Lowest EOP Elevation =	87.71 ft
Pond R/W	10.23 ac

Pond Stage/Storage Calculations

Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	Storage (ac-ft)	Total Storage (ac-ft)
50.5	Normal Water Level	7.02				0.00
56.5		8.58	7.80	6.00	46.80	46.80
57.5	Front Main Berm	8.85	8.72	1.00	8.72	55.52
58.5	Back Main Berm	10.23	9.54	1.00	9.54	65.06

2.4

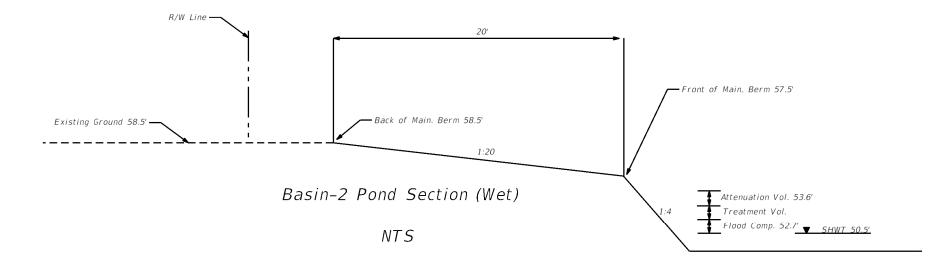
ACRES

Required Treatment and Attenuation Volume =	7.43 ac-ft
Stage of treatment and attenuation above 52.7'	53.61 ft
Flood plain Compensation between 50.5' to 52.7'	17.16 ac-ft

100-year Flood Elevation= 52.7 ft

The proposed pond will discharge into adjacent flood plain and provide flood connectivity and compensation.

Pond 2B has additional storage volume to provide compensation for the impacted Orange County Pond and minor impact to Unversity Meadows Pond B by the proposed SR 408 Extension.



SR 408 Eastern Extension-PD&E CFX BASIN 3-4

Computed By Checked By Date

2/26/2017

KS

CR

Beginning Station	44195.00
End Station	47700.00
Length (ft)	3505.00

т	otal Basin Area
R/W Width Proposed SR 408 Corridor	n (ft) <u>Area (ac)</u> 23.91
	TOTAL AREA (AC) 23.91

Existing Impervious Ar	ea	
Description	Area	
Existing Impervious areas within the basin limits	0.13	
Residential and commercial areas in Basin-4	4.99	
Total Impervious Area	5.12	Acre

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
Existing Roadway Woods (Fair)	A/D A/D	98 79	5.12 18.79	501.76 1,484.41	
		TOTAL	23.91	1,986.17	
		COM		83.1	

Estimate of Runoff Volume					
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	2.04	6.66	13.26
100 yr, 240 hr	FDOT	18.00	2.04	15.77	31.41
100 yr, 8 hr	FDOT	8.00	2.04	5.99	11.93
) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage	S	2.04
?) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	6.66
) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-f	Vr	13.26
	VI 1012 /000			VI	10.20

Proposed Impervious Area		
Description	Area	
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64' impervious median = 136')	10.94	
Total Impervious Area	10.94	Acre

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	A/D A/D	98 80	10.94 12.97	1,072.42 1,037.35	
		TOTAL	23.91	2,109.78	
		COM	POSITE CI	88.2	

	Estimate of Runoff Volume						
Summary Table:							
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)		
25 yr, 24 hr	SJRWMD	8.70	1.33	7.28	14.51		
100 yr, 240 hr	FDOT	18.00	1.33	16.49	32.86		
100 yr, 8 hr	FDOT	8.00	1.33	6.60	13.14		
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage	S	1.33		
2) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	7.28		
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-f	Vr	14.51		

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) 23.91 CN: 83.1		POST DEVELOPED CONDITION AREA (AC): 23.91 CN: 88.2			ONDITION
AGENCY	DESIGN	RUNOF	F VOLUME	E (Vr)	
	STORM	PRE	POST	NCREASE	
		(AC-FT)	(AC-FT)	(AC-FT)	
SJRWMD	25 Yr, 24 hr	13.26	14.51	1.25	
FDOT	100 yr, 240 hr	31.41	32.86	1.45	
FDOT	100 yr, 8 hr	11.93	13.14	1.22	
MAXIMUM ATTENUATION VOLU	JME (AC-FT)	1.45)		

St. John's River Water Management District Pollution Abatement Volume Requirement

Water quality and attenuation will be provided in either proposed Ponds 3A , 3B, 4A or 4B.

Post Development Total Area (ac) =	23.91
Post Development Impervious Area (ac) =	10.94

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	1
1) 1.5 " of Runoff Over Total Area =	2.99	
2) 3.75" of Runoff Over Impervious Area =	3.42	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.42	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

SHWT is from the Waterford Creek development permit # 129575. Took average SHWT from Pond-1 and Pond-2 Pond-1 = 53.0' and Pond-2 = 48.0' The average = 50.5'

Pond Depth from top of Maint Berm to SHWT Maint Berm =	6.5 1	ft ft						
H = Depth to	pond SHWT - Maint	Berm	=		5.5	ft		
3) Use greater of required treatme	ent volume or attenu	ation volum	<u>ne.</u>					
		Required Required					1.45 3.42	ac-ft ac-ft
			I	Peak \	/olume	=	4.87	ac-ft
4) For purposes of pond area calc	ulations, assume a	square pon	<u>d.</u>					
Volume = LWH where	H = L =	leng			sided po			
	W =	widt	h of vei	tical s	ided poi	nd		
Since a square pond is being assu	ımed, L = W. There	fore, Volum	$e = L^2 H$	4				
Volume = H =		4.87 ac-ft 5.5 ft	t					
		4.87	=		L ² x	5.5	i	
	ng for L = efore W =	-	196.4 196.4	ft ft				

5) Increase dimensions to account for side slopes.

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes:	4	ft/ft
H:	5.5	ft
x =	44	ft
Length @ top of slope =	240	ft
Width @ top of slope =	240	ft

6) Add maintenance berms.

Assume 20' maintenance berm (add to each side)

Length w/maint Berm =	280	ft
Width w/maint. Berm =	280	ft
Total Area =	1.80	acres
Add 10% Contingency	1.99	acres

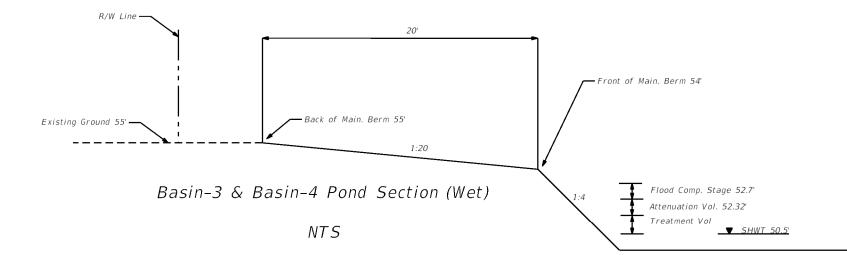
PRELIMINARY POND AREA REQUIRED FOR BASIN-3 and 4= 2.0 ACRES

Recommended Pond 3A and Pond 4A

Existing Ground Elevation =	55 ft
Normal Water Elevation =	50.5 ft
Lowest EOP Elevation =	75.71 ft
Pond R/W	4.86 ac

Pond Stage/Storage Calculations

					Storage	Total Storage
Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	(ac-ft)	(ac-ft)
50.5	Normal Water Level	2.20				0.00
53		3.15	2.68	2.50	6.69	6.69
54	Front Main Berm	3.43	3.29	1.00	3.29	9.98
55	Back Main Berm	4.86	4.15	1.00	4.15	14.12
Required Treatment and Atte Provided treatment and atter Provided treatment and atter	nuation volume =		ac-ft ac-ft ft			
	sation between 52.32' to 52.7'		ac-ft			
100-year Flood Elevation= 5						
	ion and floodplain comp storage on and flood compensation =	= 52.7	5.88 ft	ac-ft		



SR 408 Eastern Extension-PD&E CFX BASIN 5

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	47700.00
End Station	49800.00
Length (ft)	2100.00

Total Basin Area					
R/W Width (fi	<u>t)</u>	Area (ac)			
Proposed SR 408 Corridor	_	15.71			
	TOTAL AREA (AC)	15.71			
Existi	ng Impervious Area				
Description	Area				
Residential	3.74				

Total Impervious Area

3.74 Acre

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product
1/4 Residential Property Woods (Fair)	A/D AD	87 79	3.74 11.97	325.38 945.63
		TOTAL	15.71	1,271.01
		COMI	POSITE CN	80.9

			Estimate of Runoff Volume					
Agency	P (in)	S (in)	R (in)	Vr (ac-ft)				
SJRWMD	8.70	2.36	6.39	8.37				
FDOT	18.00	2.36	15.45	20.22				
FDOT	8.00	2.36	5.73	7.50				
S = (1000/CN) - 10		Soil Storage	S	2.36				
$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	6.39				
Vr = R/12 * Area		Runoff (ac-ft)	Vr	8.37				
	SJRWMDFDOTFDOTS = (1000/CN) - 10R = (P-0.2S)2/(P+0.8S)	$R = (P-0.2S)^{2}/(P+0.8S)$	SJRWMD 8.70 2.36 FDOT 18.00 2.36 FDOT 8.00 2.36 S = (1000/CN) - 10 Soil Storage R = (P-0.2S) ² /(P+0.8S) Runoff (in)	SJRWMD 8.70 2.36 6.39 FDOT 18.00 2.36 15.45 FDOT 8.00 2.36 5.73 S = (1000/CN) - 10 Soil Storage S R = (P-0.2S) ² /(P+0.8S) Runoff (in) R				

Proposed Impervious Area				
Description	Area			
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64' impervious median = 136') + Ramps	7.28			
Total Impervious Area	7.28	Acre		

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway	A/D	98	7.28	713.40	
On-site Grassed Area	A/D	80	8.43	674.43	
		TOTAL	15.71	1,387.83	
		СОМІ		I 88.3	

Agency SJRWMD FDOT FDOT	P (in) 8.70 18.00 8.00	S (in) 1.32 1.32 1.32	<u>R (in)</u> 7.29 16.51 6.61	Vr (ac-ft) 9.55 21.61 8.65
SJRWMD FDOT	8.70 18.00	1.32 1.32	7.29 16.51	9.55 21.61
		-		21.61
FDOT	8.00	1.32	6.61	8.65
	-			
(1000/CN) - 10		Soil Storage	S	1.32
(P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.29
· R/12 * Area		Runoff (ac-ft	Vr	9.55

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) CN:	15.71 80.9		POST DEVE AREA (AC): CN:	LOPED CONDITIO 15.71 88.3	
AGENCY	DESIGN	DESIGN RUNOFF VOLUME (Vr)			
	STORM	PRE	POST	INCREASE	
		(AC-FT)	(AC-FT)	(AC-FT)	
SJRWMD	25 yr, 24 hr	8.37	9.55	1.18	
FDOT	100 yr, 240 hr	20.22	21.61	1.39	
FDOT	100 yr, 8 hr	7.50	8.65	1.15	
MAXIMUM ATTENUATION VOLUM	/E (AC-FT)	. 1	.39		

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	15.71
Post Development Impervious Area (ac) =	7.28

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	1.96	
2) 3.75" of Runoff Over Impervious Area =	2.27	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	2.27	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per existing Avalon Park Blvd Permit, the Normal Water elevation in Pond B is 47.7 NAVD The existing Ground Elevation in this area is around 53 ft.

	p of Maint to SHWT int Berm =		5.3 ft 1 ft			
H =	Depth to pond SH	WT - Maint	Berm	=	4.3 ft	
3) Use greater of requ	ired treatment volu	ime or atten	<u>uation vol</u>	<u>ume</u> .		
					nuation Volume = atment Volume =	1.39 ac-ft 2.27 ac-ft
					Peak Volume =	3.66 ac-ft
4) For purposes of por	nd area calculation	s, assume a	a square p	ond.		
Volume = LWH	where	H = L = W =	lenç		rtical sided pond tical sided pond	
Since a square pond is	being assumed, L	. = W. Ther	efore, Vol	ume = L ²	²H	
	Volume = H =		3.66 ac-f 4.3 ft	ft		

	3.66	=		$L^2 x$
Solving for L =		192.6	ft	
Therefore W =		192.6	ft	

4.3

5) Increase dimensions to account for side slopes.

Side slopes:	4 ft/ft
H:	4.3 ft
x =	34.4 ft
Length @ top of slope =	227 ft
Width @ top of slope =	227 ft
6) Add maintenance berms.	

Assume 20' maintenance berm (add to each side)

Length w/maint berm = Width w/maint. Berm =	267 ft 267 ft
Total Area =	1.64 acres
Add 10% Contingency	1.80 acres

PRELIMINARY POND AREA REQUIRED FOR BASIN-5= 1.8 ACRES

Recommended Pond 5B

Existing Ground Elevation =	53 ft
Normal Water Elevation =	47.7 ft
Lowest EOP Elevation =	79.31 ft
Pond R/W	4.1 ac

Pond Stage/Storage Calculations

			Ave Area			Total Storage (ac-
Stage	Description	Area (ac)	(ac)	Depth (ft)	Storage (ac-ft)	ft)
47.70	Normal Water Level	2.61				0.00
49.20		2.82	2.72	1.50	4.07	4.07
52.00	Front Main Berm	3.24	3.03	1.80	5.45	9.53
53.00	Back Main Berm	4.10	3.67	1.00	3.67	13.20

Required Treatment and Attenuation Volume =

3.52 ac-ft 4.07 ac-ft

49.2 ft

Provided treatment and attenuation volume = Provided treatment and attenuation Stage=

attenuation Stage=

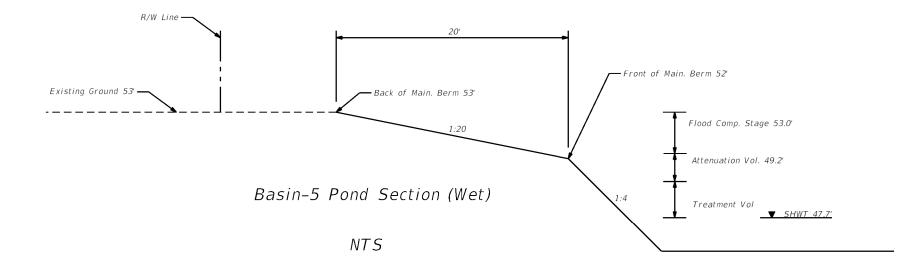
100-year Flood Elevation= 53.7 ft (Big Econ River Master Plan)

Pond 5B is hydraulically connected to 100 year floodplain

			Dredge Area	Dredge	Compensation
Description	Elevation	Area	(ac)	Height (ft)	(ac-ft)
Treatment + Attenuation	49.2	2.82	2.82		
Existing Ground Elevation	53	4.1	4.1	3.8	13.15
100-yr Flood Elevation	53.7				

No above ground maintenance berm, therefore no floodplain impact.

Please refer to Floodplain Impact/Compensation Calculation Summary Table.



SR 408 Eastern Extension-PD&E CFX BASIN 6-8 (merged as single basin)

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	49800.00
End Station	55223.00
Length (ft)	5423.00

	Total Basin	Area		
Proposed SR 408 Corridor	R/W Width (ft)	<u>Length (ft)</u>	<u>Area (sq-ft)</u>	<u>Area (ac)</u> 40.41
			TOTAL AREA (AC	40.41

Existing Impervious Area					
Description Residential	Width (ft)	Length(ft)	Area 3.86		
	Total Impervious Are	ea	3.86	Acre	

ATTENUATION VOLUME ESTIMATE Pre-Development Area Land Use Description/ Soil Group CN Product Soil Name (ac) 1/4 Residential Property A/D 84 3.86 324.24 Wooded area A/D 36.55 2,887.45 79 TOTAL 40.41 3,211.69 COMPOSITE CN 79.5

Estimate of Runo	off Volume			
Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
SJRWMD	8.70	2.58	6.22	20.95
FDOT	18.00	2.58	15.23	51.30
FDOT	8.00	2.58	5.56	18.74
S = (1000/CN) - 10		Soil Storage	S	2.58
R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.22
Vr = R/12 * Area		Runoff (ac-ft	Vr	20.95
-	Agency SJRWMD FDOT FDOT S = (1000/CN) - 10 R = (P-0.2S) ² /(P+0.8S)	$R = (P-0.2S)^{2}/(P+0.8S)$	Agency P (in) S (in) SJRWMD 8.70 2.58 FDOT 18.00 2.58 FDOT 8.00 2.58 S = (1000/CN) - 10 Soil Storage R = (P-0.2S) ² /(P+0.8S) Runoff (in)	Agency P (in) S (in) R (in) SJRWMD 8.70 2.58 6.22 FDOT 18.00 2.58 15.23 FDOT 8.00 2.58 5.56 S = (1000/CN) - 10 Soil Storage S R = (P-0.2S) ² /(P+0.8S) Runoff (in) R

Proposed Impervious Area				
Description	Width (ft)	Length(ft)	Area	
Proposed SR 408 Corridor (Prop median = 136') + Ramps	17.43			
	Total Impervious Ar	ea	17.43	Acre

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	A/D A/D	98 79	17.43 22.98	1,708.07 1,815.48	
		TOTAL	40.41	3,523.55	
		COM		87.2	

	Estimate of Runo	off Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.47	7.16	24.10
100 yr, 240 hr	FDOT	18.00	1.47	16.35	55.06
100 yr, 8 hr	FDOT	8.00	1.47	6.47	21.80
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage	S	1.47
2) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	7.16
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft	Vr	24.10

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC CN	/		POST DEVE AREA (AC): CN:	LOPED CONDITIO 40.41 87.2		
AGENCY	DESIGN	RUN	RUNOFF VOLUME (Vr)			
	STORM	PRE	POST	INCREASE		
		(AC-FT)	(AC-FT)	(AC-FT)		
SJRWMD	25 yr, 24 hr	20.95	24.10	3.15		
FDOT	100 yr, 240 hr	51.30	55.06	3.76		
FDOT	100 yr, 8 hr	18.74	21.80	3.06		
MAXIMUM ATTENUATION VOLU	JME (AC-FT)	3.7	76			

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	40.41
Post Development Impervious Area (ac) =	17.43

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	1
1) 1.5 " of Runoff Over Total Area =	5.05	
2) 3.75" of Runoff Over Impervious Area =	5.45	Govern
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	5.45	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per the Avalon Park Subdivision Permit the SHWT at this location is 50.4' NAVD. (Existing Avalon Pond C) Existing ground elevation at the Pond Location is = 57 '

Pond Depth from top of Maint			
Berm to SHWT	6	ft	
Maint Berm =	1	ft	

H = Depth to pond SHWT - Maint Berm = 5

3) Use greater of required treatment volume or attenuation volume.

Required Attenuation Volume =	3.76	ac-ft
Required Treatment Volume =	5.45	ac-ft

Peak Volume = 9.21 ac-ft

ft

4) For purposes of pond area calculations, assume a square pond.

Volume = LWH

where	H =	height (ft)
	L =	length of vertical sided pond
	W =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume = H =	9.21 5	ac ft	-ft			
		9.21	=		$L^2 x$	5
	g for L = ore W =		283.3 283.3	ft ft		

5) Increase dimensions to account for side slopes.

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 5	ft/ft ft		
x =	40	ft		
Length @ top of slope = Width @ top of slope =	323 323	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add	to each side)			
Length w/maint berm = Width w/maint. Berm =	363 363	ft ft		
Total Area =	3.03	acre		
Add 10% Contingency	3.33	acre		
PRELIMINARY	POND AREA REQUIRI	ED FOR BASIN-6=	3.3	ACRES
Recommended Pond 6B				
Existing Ground Elevation = Normal Water Elevation =		57 ft).4 ft		

Pond Stage/Storage Calculations

Lowest EOP Elevation =

Pond R/W

						Total Storage
Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	Storage (ac-ft)	(ac-ft)
50.4	Normal Water Level	16.11				0.00
52		16.64	16.38	1.00	16.38	16.38
56	Front Main Berm	18.00	17.32	4.00	69.28	85.66
57	Back Main Berm	19.73	18.87	1.00	18.87	104.52
Required Treatment and Attenuation	on Volume =	9.21	ac-ft			
Flood plain compensation provided		34.39	ac-ft			
Provided treatment and attenuation	n stage above 53.04'=	53.57	′ ft			

81.71 ft

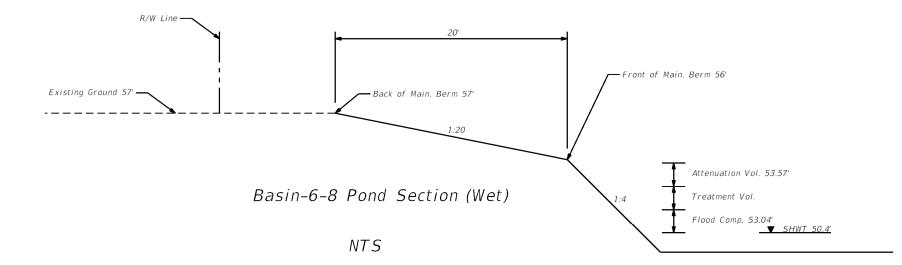
19.73 ac

100-year Flood Elevation= 53.04 ft (100-year stage at Avalon Subdivision Pond-C)

No above ground maintenance berm, therefore no floodplain impact.

Pond 6B will provide floodplain compensation in addition to providing treatment and attenuation.

Pond 6B will also able to provide compensation for impacted Avalon Park Pond-C.



SR 408 Eastern Extension-PD&E CFX BASIN 9-10

Computed By	KS
Checked By	CR
Date	

2/26/2017

Beginning Station	55223.00
End Station	57995.00
Length (ft)	2772.00

	Total Basin Area	
Proposed SR 408 Corridor	R/W Width (ft)	<u>Area (ac)</u> 19.30
		TOTAL AREA (AC) 19.30

	Existing Impervious Area	1	
Description		Area	
Old Cheney Hwy Residential		0.12	
Residential		2.31	
	Total Impervious Area	2.43 Acre	

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
On-site Roadway	B/D	98	0.12	12.15	
1/4 Residential Property	B/D	87	2.31	200.97	
Woods (Fair)	B/D	79	16.87	1,332.41	
		TOTAL	19.30	1,545.54	
		COM	POSITE CN	80.1	

Estimate of Runo	ff Volume			
Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
SJRWMD	8.70	2.49	6.29	10.12
FDOT	18.00	2.49	15.32	24.65
FDOT	8.00	2.49	5.63	9.06
S = (1000/CN) - 10		Soil Storage (in)	S	2.49
R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.29
Vr = R/12 * Area		Runoff (ac-ft)	Vr	10.12
	Agency SJRWMD FDOT FDOT S = (1000/CN) - 10 R = (P-0.2S) ² /(P+0.8S)	$R = (P-0.2S)^{2}/(P+0.8S)$	Agency P (in) S (in) SJRWMD 8.70 2.49 FDOT 18.00 2.49 FDOT 8.00 2.49 S = (1000/CN) - 10 Soil Storage (in) R = (P-0.2S) ² /(P+0.8S) Runoff (in)	Agency P (in) S (in) R (in) SJRWMD 8.70 2.49 6.29 FDOT 18.00 2.49 15.32 FDOT 8.00 2.49 5.63 S = (1000/CN) - 10 Soil Storage (in) S R = (P-0.2S) ² /(P+0.8S) Runoff (in) R

Proposed Impervious Area		
Description	Area	
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64' impervious median = 136')	11.12	
Total Impervious Area	11.12	Acre

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	B/D B/D	98.00 80	11.12 8.18	1,089.33 654.75	
		TOTAL	19.30	1,744.08	
		COM	POSITE CN	90.4	

P (in) 8.70	S (in)	_ () \	
	S (in)		
8.70	- ()	R (in)	Vr (ac-ft)
	1.07	7.54	12.13
18.00	1.07	16.78	26.99
8.00	1.07	6.85	11.02
	Soil Storage (in)	S	1.07
	Runoff (in)	R	7.54
	Runoff (ac-ft)	Vr	12.13
		Runoff (ac-ft)	Runoff (ac-ft) Vr

SUMMARY OF ATTENUATION ESTIMATES

	AREA (AC) 19.30 AREA (AC): 19.3): 19.30
AGENCY	DESIGN	RUN	OFF VOLUME	(Vr)
	STORM	PRE	POST	NCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 yr, 24 hr	10.12	12.13	2.00
FDOT	100 yr, 240 hr	24.65	26.99	2.34
FDOT	100 yr, 8 hr	9.06	11.02	1.95
MAXIMUM ATTENUATION VOLUME	(AC-FT)	2	.34	

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	19.30
Post Development Impervious Area (ac) =	11.12

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft]
1) 1.5 " of Runoff Over Total Area =	2.41	
2) 3.75" of Runoff Over Impervious Area =	3.47	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.47	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-9 and Basin-10 is between 6" to 24". We have assumed the SHWT is 1.0' below the existing ground and providing a 2.0' berm above existing ground.

Pond Depth from top of Maint Berm to	2	4			
SHWT Maint Berm =	3 1	ft ft			
	I	п			
H = Depth to po	ond SHWT - Maint	Berm =	2 ft		
3) Use greater of required treatment volu	me or attenuation	<u>i volume</u> .			
		Required Attenuati	ion Volume =	2.34	ac-ft
		Required Treatme		3.47	ac-ft
		Pe	eak Volume =	5.82	ac-ft
4) For purposes of pond area calculation Volume = LWH	·	re pond.			
where	H =	height (ft)			
	L =		ical sided pond		
	W =	width of vertic	cal sided pond		
Since a square pond is being assumed, L	. = W. Therefore,	Volume = L^2H			
Volume =	5.82	ac-ft			
H =	2	ft			
		5.82 =	$L^2 x 2$		
	o	055.0	<i>c</i> .		

Solving for L =	355.9	ft
Therefore W =	355.9	ft

5) Increase dimensions to account for side slopes.

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 2	ft/ft ft		
x =	16	ft		
Length @ top of slope = Width @ top of slope =	372 372	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add to ea	ach side)			
Length w/maint Berm = Width w/maint. Berm =	412 412	ft ft		
Total Area =	3.90	acres		
Add 10% Contingency	4.28	acres		
PRELIMINARY POND AREA REQU	UIRED FOR BASIN-9 a	nd Basin 10=	4.3	ACRES
Recommended Pond 9B and 10B				

Existing Ground Elevation =	49 ft
Normal Water Elevation =	48 ft
Lowest EOP Elevation =	90.41 ft
Pond R/W	8.38 ac

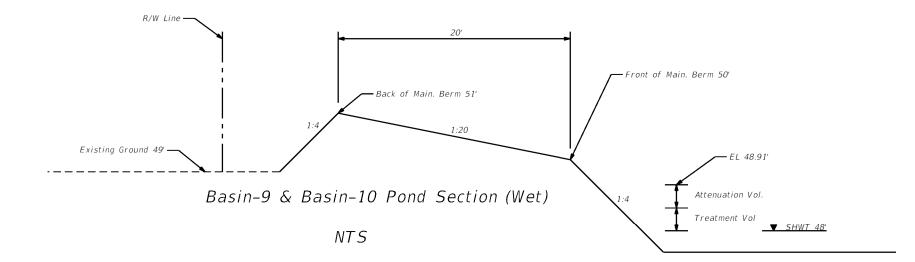
Pond Stage/Storage Calculations

			Ave Area		Storage	Total Storage
Stage	Description	Area (ac)	(ac)	Depth (ft)	(ac-ft)	(ac-ft)
48	Normal Water Level	6.32				0.00
49		6.60	6.46	1.00	6.46	6.46
50	Front Main Berm	6.90	6.75	1.00	6.75	13.21
51	Back Main Berm	8.38	7.64	1.00	7.64	20.85

Required Treatment and Attenuation Volume =	5.82 ac-ft
Provided treatment and attenuation volume =	5.93 ac-ft 48.91 ft
Provided treatment and attenuation Stage=	48.91 II

Pond Site located out side of the 100 year floodplain. FEMA 100-year flood elevation is 43.5' NAVD

The proposed pond will not impact flood plain since the ground elevation is higher than the 100-year stage.



SR 408 Eastern Extension-PD&E CFX **BASIN 11A**

Computed By	KS
Checked By	CR
Date	

2/26/2017

Beginning Station	57995.00
End Station	60200.00
Length (ft)	2205.00

Total Basin Area						
	R/W Width (ft)			<u>Area (ac)</u>		
Proposed SR 408 Corridor				28.20		
			TOTAL AREA (AC) 28.20		
	Existing Impervious Area					
Description		Area	1			
Residential		1.20)			
On-site Roadway		0.20)			
	Total Impervious Area	1.40	Acre			

ATTENUATION VOLUME ESTIMATE							
Pre-Development							
Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product			
1/4 Residential Property Woods (Fair) On-site Roadway Existing Pond	B/D B/D B/D B/D	87 80 98 100 TOTAL	1.20 24.86 0.20 1.94 28.20	104.40 1,988.80 19.60 194.00 2,306.80			
		CON	IPOSITE CI	N 81.8			
	Estimate	of Runoff Vo	olume				
Summary Table:							
Design Storm	Agency		P (in)	S (in)	R (in)	Vr (ac-ft)	
25 yr, 24 hr	SJRWMD		8.70	2.22	6.50	15.28	
100 yr, 240 hr 100 yr, 8 hr	FDOT FDOT		18.00 8.00	2.22 2.22	15.58 5.84	36.61 13.72	
1) Soil Storage (S)	S = (1000/CN) - 10			Soil Storage (in)	S	2.22	
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)			Runoff (in)	R	6.50	
3) Runoff Volume (Vr)	Vr = R/12 * Area			Runoff (ac-ft)	Vr	15.28	

Proposed Impervious Area					
Description	Area				
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64'					
impervious median = 136')+ Ramps and Portion of CR 419	10.93				
Total Impervious Area	10.93	Acre			

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	B/D B/D	98 80	10.93 17.27	1,071.32 1,381.45	
		TOTAL	28.20	2,452.77	
		COM	POSITE CN	87.0	

Estimate of Runoff Volume							
Agency	P (in)	S (in)	R (in)	Vr (ac-ft)			
SJRWMD	8.70	1.50	7.13	16.76			
FDOT	18.00	1.50	16.32	38.35			
FDOT	8.00	1.50	6.45	15.15			
S = (1000/CN) - 10		Soil Storage (in	i) S	1.50			
$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	7.13			
\/r = R/12 * Area		Runoff (ac-ft)	Vr	16.76			
			VI	10.10			
	Agency SJRWMD FDOT	Agency P (in) SJRWMD 8.70 FDOT 18.00 FDOT 8.00 S = (1000/CN) - 10 R = (P-0.2S) ² /(P+0.8S)	Agency P (in) S (in) SJRWMD 8.70 1.50 FDOT 18.00 1.50 FDOT 8.00 1.50 S = (1000/CN) - 10 Soil Storage (in R = (P-0.2S) ² /(P+0.8S) Runoff (in)	Agency P (in) S (in) R (in) SJRWMD 8.70 1.50 7.13 FDOT 18.00 1.50 16.32 FDOT 8.00 1.50 6.45 S = (1000/CN) - 10 Soil Storage (in) S R = (P-0.2S) ² /(P+0.8S) Runoff (in) R			

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION POST DEVELOPED C AREA (AC) 28.20 CN: 81.8					TION
AGENCY	GENCY DESIGN RUNOFF VOLUME (Vr)				
	STORM	PRE	POST	NCREASE	
		(AC-FT)	(AC-FT)	(AC-FT)	
SJRWMD	25 yr, 24 hr	15.28	16.76	1.47	
FDOT	100 yr, 240 hr	36.61	38.35	1.74	
FDOT	100 yr, 8 hr	13.72	15.15	1.44	
MAXIMUM ATTENUATION VOLUME (AC-FT) 1.74					

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	28.20
Post Development Impervious Area (ac) =	10.93

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	3.53	Governs
2) 3.75" of Runoff Over Impervious Area =	3.42	
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.53	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-11 is between 24" to 42". We have assumed the SHWT is 3.0' below the existing ground and are providing a 1.5' berm above existing ground.

Pond Depth from top of Maint		_				
Berm to SHWT	4.5	ft				
Maintenance Berm Depth =	1	ft				
H = Depth to pond SHWT	- Maintenance	Berm =	3.5	ft		
3) Use greater of required treatment vo	<u>olume or atten</u>	<u>uation volume.</u>				
		Required Attenua	ation Volume	=	1.74	ac-ft
					3.53	ac-ft
		Required Treatr		-	5.55	ac-n
		-	eak Volume	_	5.27	ac-ft
		Г	reak volume	-	5.27	ac-n
4) For purposes of pond area calculation	ons, assume a	a square pond.				
Volume = LWH						
where	H =	height (ft)				
	L =	length of ve	rtical sided p	ond		
	VV =	width of ver	tical sided po	ond		
Since a square pond is being assumed, $L = W$. Therefore, Volume = L^2H						

Volume = H =			ac-ft ft			
		5.27	=		$L^2 x$	3.5
	Solving for L = Therefore W =		256.1 256.1	ft ft		

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 3.5	ft/ft ft		
x =	28	ft		
Length @ top of slope = Width @ top of slope =	284 284	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add	to each side)			
Length w/maint berm = Width w/maint. Berm =	324 324	ft ft		
Total Area = Add 10% Contingency	2.41 2.65	acres acres		
PRELIMINARY POND AR	EA REQUIRED FOR	BASIN-11 A=	2.7	ACRES

Recommended Ponds 11A1, 11A2, 11A3 and 11A4. (Infield Ponds and Pond 11A4 will be interconnected)

Existing Ground Elevation =	63 ft
Normal Water Elevation =	60.5 ft
Lowest Point at the Interchange	64.5 ft
Pond R/W	5.76 ac

Pond Stage/Storage Calculations

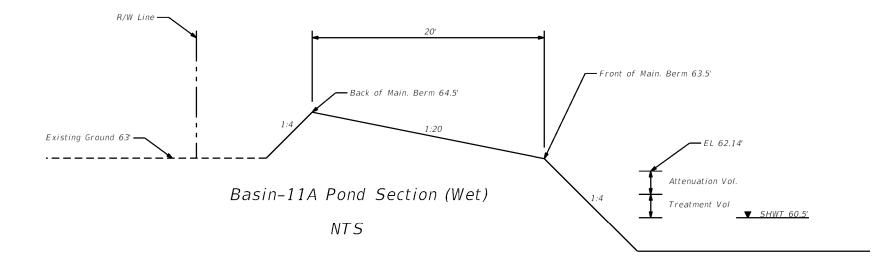
		Ave Area		Storage	Total Storage
Description	Area (ac)	(ac)	Depth (ft)	(ac-ft)	(ac-ft)
Normal Water Level	3				0
	3.43	3.22	2.50	8.04	8.04
Front Main Berm	3.78	3.61	1.00	3.61	11.64
Back Main Berm	5.76	4.77	1.00	4.77	16.41
	Normal Water Level Front Main Berm	Normal Water Level33.43Front Main Berm3.78	DescriptionArea (ac)(ac)Normal Water Level33.433.22Front Main Berm3.783.61	DescriptionArea (ac)(ac)Depth (ft)Normal Water Level3-3.433.222.50Front Main Berm3.783.611.00	Description Area (ac) (ac) Depth (ft) (ac-ft) Normal Water Level 3

5.27 ac-ft

Required Treatment and Attenuation Volume =

Provided treatment and attenuation volume =	5.27 ac-ft
Provided treatment and attenuation Stage=	61.64 ft

Ponds are located outside of the 100-year flood plain.



SR 408 Eastern Extension-PD&E CFX BASIN 11B

Computed By	KS	
Checked By	CR	
Date	2/	26/2017

Beginning Station	41315.00
End Station	43750.00
Length (ft)	2435.00

	Total Basin Area			
	R/W Width (ft)			<u>Area (ac)</u>
Proposed SR-419 Corridor				7.90
			TOTAL AREA (AC)	7.90
	Existing Impervious Area			
Description		Area		
Residential		0.00		
On-site Roadway		1.06		
	Total Impervious Area	1.06	Acre	

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
Woods (Fair)	A/D	79	6.84	540.36	
On-site Roadway	A/D	98	1.06	103.88	
		TOTAL	7.90	644.24	
		СОМ	POSITE CN	81.5	

Estimate of Runoff Volume							
Summary Table:							
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)		
25 yr, 24 hr	SJRWMD	8.70	2.26	6.47	4.26		
100 yr, 240 hr	FDOT	18.00	2.26	15.54	10.23		
100 yr, 8 hr	FDOT	8.00	2.26	5.81	3.82		
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	2.26		
?) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.47		
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	4.26		

Proposed Impervious Area					
Description	Area				
Curb and Gutter Roadway-not accounted for future Widening.	5.54				
Total Impervious Area	5.54	Acre			

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway	A/D	98	5.54	542.92	
On-site Grassed Area	A/D	79	2.36	186.44	
		TOTAL	7.90	729.36	
		COM	POSITE CN	92.3	

	Estimate of Runo	ff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	0.83	7.78	5.12
100 yr, 240 hr	FDOT	18.00	0.83	17.04	11.22
100 yr, 8 hr	FDOT	8.00	0.83	7.08	4.66
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	0.83
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.78
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	5.12

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION ARE/	A (AC) 7.90 CN: 81.5		POST DEVELO AREA (AC CN	·
AGENCY	DESIGN	RUN	OFF VOLUME ((Vr)
	STORM	PRE	POST	NCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 yr, 24 hr	4.26	5.12	0.86
FDOT	100 yr, 240 hr	10.23	11.22	0.98
FDOT	100 yr, 8 hr	3.82	4.66	0.84
MAXIMUM ATTENUATION VOLU	IME (AC-FT)	0.	98	

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	7.90
Post Development Impervious Area (ac) =	5.54

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	T
1) 1.5 " of Runoff Over Total Area =	0.99	
2) 3.75" of Runoff Over Impervious Area =	1.73	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	1.73]

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-11-A is between 6" to 18". We have assumed the SHWT is 1.0' below the existing ground and are providing a 2.5' berm above existing ground.

Pond Depth from top of Maint Berm to						
SHWT	3.5	ft				
Maint Berm =	1	ft				
H = Depth to pond SI	HWT - Maint B	Berm	=	2.5	ft	

3) Use greater of required treatment volume or attenuation volume.

Required Attenuation Volume =	0.98	ac-ft
Required Treatment Volume =	1.73	ac-ft
Peak Volume =	2.71	ac-ft

4) For purposes of pond area calculations, assume a square pond.

Volume = LWH

where	H =	height (ft)
	L =	length of vertical sided pond
	W =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume = H =	2.71 2.5	a ft	c-ft			
		2.71	=		$L^2 x$	2.5
	ing for L = efore W =		217.5 217.5	ft ft		

Add: x = [(Side Slopes x H) x 2] to each dimension

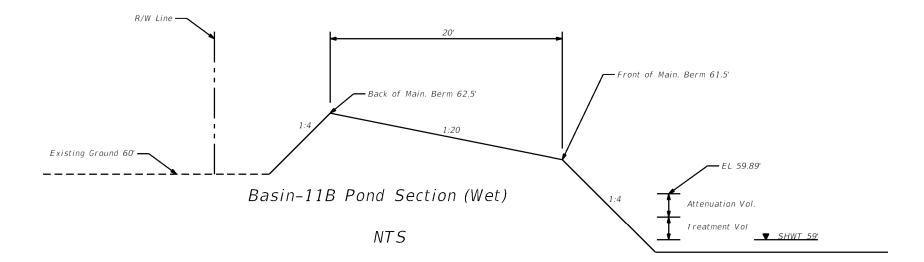
Side slopes:	4	ft/ft			
H:	2.5	ft			
× -	20	ft			
x =	20	п			
Length @ top of slope =	237	ft			
Width @ top of slope =	237	ft			
6) Add maintenance berms.					
Assume 20' maintenance berm (add to each s	side)				
Length w/maint berm =	277	ft			
Width w/maint. Berm =	277	ft			
T () A	4 77				
Total Area =	1.77	acres			
Add 10% Contingency	1.94	acres			
PRELIMINARY POND AREA	REQUIRED	-OR BASIN-11A=	1.9	ACRES	
Recommended Pond 11B1					
Existing Ground Elevation =		60 ft			
Normal Water Elevation =		59 ft			
Lowest EOP Elevation =	6	6.79 ft			
Pond R/W		3.98 ac			
Pond Stage/Storage Calculations					
i ond olage/olorage Calculations					
	-				<u> </u>

					Storage	Total Storage
Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	(ac-ft)	(ac-ft)
59	Normal Water Level	2.91				0.00
60.5		3.11	3.01	1.50	4.52	4.52
61.5	Front Main Berm	3.25	3.18	1.00	3.18	7.70
62.5	Back Main Berm	3.98	3.62	1.00	3.62	11.31
Required Treatment and Attenuation Vo	lume =	2.71	ac-ft			

Provided treatment and attenuation volume = Provided treatment and attenuation Stage=

2.71 ac-ft 59.89 ft

Pond located outside of the 100-year flood plain.



SR 408 Eastern Extension-PD&E CFX BASIN 11C

3) Runoff Volume (Vr)

Vr = R/12 * Area

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	60200.00
End Station	62950.00
Length (ft)	2750.00

	Total Basin Area				
	R/W Width (ft)			<u>Area (ac)</u>	
Proposed SR 408 Corridor				18.93	
			TOTAL AREA (AC)	18.93	
	Existing Impervious Area				
Description		Area			
Residential		1.52			
On-site Roadway		0.15			
	Total Impervious Area	1.67	Acre		

ATTENUATION VOLUME ESTIMATE							
Pre-Development							
Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product			
1/4 Residential Property Noods (Fair) Dn-site Roadway	B/D B/D B/D	87 80 98	1.52 17.26 0.15	132.46 1,380.60 14.70			
		TOTAL	18.93	1,527.76			
		СОМ	POSITE C	N 80.7			
	Estima	ate of Runoff	Volume				
Summary Table:							
Design Storm	Agency		P (in)	S (in)	R (in)	Vr (ac-ft)	
25 yr, 24 hr	SJRWMD		8.70	2.39	6.37	10.05	
100 yr, 240 hr	FDOT		18.00	2.39	15.42	24.32	
100 yr, 8 hr	FDOT		8.00	2.39	5.71	9.00	
1) Soil Storage (S)	S = (1000/CN) - 10			Soil Storage (in)	S	2.39	
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)			Runoff (in)	R	6.37	

Runoff (ac-ft)

10.05

Vr

Proposed Impervious Area		
Description	Area	
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64'		
impervious median = 136')	8.59	
Total Impervious Area	8.59	Acre

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	B/D B/D	98 80	8.59 10.34	841.41 827.53	
		TOTAL	18.93	1,668.95	
COMPOSITE CN 88.2					

	Estimate of R	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.34	7.27	11.47
100 yr, 240 hr	FDOT	18.00	1.34	16.48	26.00
100 yr, 8 hr	FDOT	8.00	1.34	6.59	10.39
 Soil Storage (S) 	S = (1000/CN) - 10		Soil Storage (in)	S	1.34
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.27
			<u> </u>		
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	11.47
, , , , ,			· · · · ·		

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) CN:	18.93 80.7		POST DEVELC AREA (AC CI	·	
AGENCY	DESIGN	RUN	OFF VOLUME	(Vr)	
	STORM	PRE	POST	INCREASE	
		(AC-FT)	(AC-FT)	(AC-FT)	
SJRWMD	25 yr, 24 hr	10.05	11.47	1.43	
FDOT	100 yr, 240 hr	24.32	26.00	1.68	
FDOT	100 yr, 8 hr	9.00	10.39	1.39	
MAXIMUM ATTENUATION VOLUME (AC-FT) 1.68					

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	18.93
Post Development Impervious Area (ac) =	8.59

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	2.37	
2) 3.75" of Runoff Over Impervious Area =	2.68	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	2.68	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-11-C is between 24" to 42". We have assumed the SHWT is 2.0' below the existing ground and are providing a 1.5' berm above existing ground.

Pond Depth from top of Maint			
Berm to SHWT	3.5	ft	
Maintenance Berm Depth =	1	ft	

H = Depth to pond SHWT - Maintenance Berm = 2.5 ft

3) Use greater of required treatment volume or attenuation volume.

Required Attenuation Volume =	1.68	ac-ft
Required Treatment Volume =	2.68	ac-ft

Peak Volume = 4.36 ac-ft

4) For purposes of pond area calculations, assume a square pond.

Volume = LWH

where	H =	height (ft)
	L =	length of vertical sided pond
	W =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume =	4.36		ac-ft ft			
H =	2.5		π			
		4.36	=		$L^2 x$	2.5
S	Solving for L =		275.6	ft		
7	Therefore W =		275.6	ft		

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 2.5	ft/ft ft		
x =	20	ft		
Length @ top of slope = Width @ top of slope =	296 296	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add t	o each side)			
Length w/maint berm = Width w/maint. Berm =	336 336	ft ft		
Total Area = Add 10% Contingency	2.59 2.84	acres acres		
PRELIMINARY POND AREA		FOR BASIN-11=	2.8	ACRES
Recommended Pond 11C				
Existing Ground Elevation = Normal Water Elevation = Low point in profile Pond R/W	5	52 ft 50 ft 4.04 ft 5.7 ac		

Pond Stage/Storage Calculations

			Ave Area		Storage	Total Storage
Stage	Description	Area (ac)	(ac)	Depth (ft)	(ac-ft)	(ac-ft)
50	Normal Water Level	4.32				0
51		4.50	4.41	1.00	4.41	4.41
52.5	Front Main Berm	4.80	4.65	1.00	4.65	9.06
53.5	Back Main Berm	5.70	5.25	1.00	5.25	14.31
Required Treatment and A	ttenuation Volume =	4.36	ac-ft			

4.36 ac-ft 51 ft

Provided treatment and attenuation volume =	
Provided treatment and attenuation Stage=	

Ponds are located outside of the 100-year flood plain.

Pond 11C4 will be used to provide floodplain compensation.

Pond 11C4 is hydraulically connected to 100 year floodplain

			Drodgo Aroo	Drodgo Hoight	Compens ation (ac-
			Dredge Area	Dredge Height	ation (ac-
Description	Elevation	Area	(ac)	(ft)	ft)
Normal Water Elevation	40	4.43	4.43		
Existing Ground Elevation	43	5.52	5.52	3	14.93
100-yr Flood Elevation	45.4				

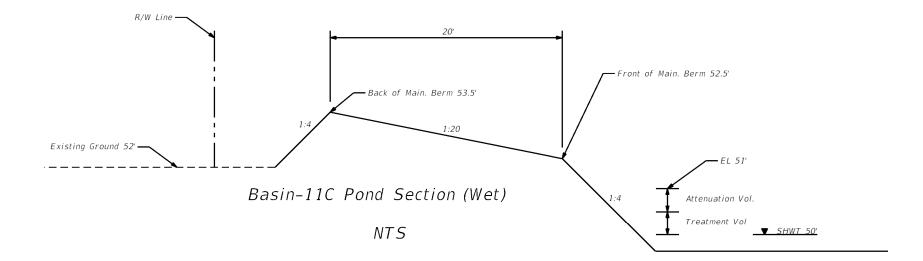
No above ground maintenance berm, therefore no floodplain impact.

Pond 11-C3 will be used to provide floodplain compensation.

Pond 11-C3 is hydraulically connected to 100 year floodplain

			Dredge Area	Dredge Height	Compens ation (ac-
Description	Elevation	Area	(ac)	(ft)	ft)
Normal Water Elevation	35	8.59	8.59		
Existing Ground Elevation	37.5	8.85	8.85	2.5	21.80
100-yr Flood Elevation	45.4				

No above ground maintenance berm, therefore no floodplain impact.



SR 408 Eastern Extension-PD&E CFX BASIN 12

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	62950.00
End Station	66110.00
Length (ft)	3160.00

	Total Bas	sin Area		
	R/W Width (ft)	Length (ft)	<u>Area (sq-ft)</u>	<u>Area (ac)</u>
Proposed SR 408 Corridor			TOTAL AREA (AC)	21.76 21.76

Existing Impervious Area					
Description Residential	Width (ft)	Length(ft)	Area 1.05		
	Total Impervious Ar	ea	1.05	Acre	

ATTENUATION VOLUME ESTIMATE Pre-Development Land Use Description/ Soil Group CN Area Product Soil Name (ac) 1/4 Residential Property Wood (Fair) A/D 87 1.05 91.35 A/D 84 1,739.64 20.71 TOTAL 21.76 1,830.99

COMPOSITE	CN

84.1

	Estimate of Ru	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.88	6.79	12.31
100 yr, 240 hr	FDOT	18.00	1.88	15.92	28.87
100 yr, 8 hr	FDOT	8.00	1.88	6.11	11.08
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.88
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.79
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	12.31
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	

Width (ft) (Proposed 4' lanes and	Length(ft) assume 64'	Area 9.87		
(Proposed 4' lanes and	assume 64'	9.87		
		9.87		
		0.07		
Total Impervious Are	ea	9.87	Acre	
Soil Group	CN	Area	Product	
		(00)		
A/D	98.00	9.87	966.86	
A/D	80	11.89	951.53	
	TOTAL	21.76	1,918.39	
	COMP	OSITE CN	88.2	
	Soil Group A/D A/D	Soil Group CN A/D 98.00 A/D 80 TOTAL COMPO	Soil Group CN Area (ac) A/D 98.00 9.87 A/D 80 11.89	Soil Group CN Area (ac) Product A/D 98.00 9.87 966.86 A/D 80 11.89 951.53 TOTAL 21.76 1,918.39 COMPOSITE CN 88.2

Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.34	7.27	13.19
100 yr, 240 hr	FDOT	18.00	1.34	16.48	29.89
100 yr, 8 hr	FDOT	8.00	1.34	6.59	11.94
) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.34
) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	7.27
) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	13.19

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) 21.76 CN: 84.1		POST DEVELOPED CONDITION AREA (AC): 21.76 CN: 88.2		
AGENCY	DESIGN	RUI	NOFF VOLUME	(Vr)
	STORM	PRE	POST	INCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 yr, 24 hr	12.31	13.19	0.88
FDOT	100 yr, 240 hr	28.87	29.89	1.02
FDOT	100 yr, 8 hr	11.08	11.94	0.86
MAXIMUM ATTENUATION VO	DLUME (AC-FT)		1.02	

٦

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	21.76
Post Development Impervious Area (ac) =	9.87

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft]
1) 1.5 " of Runoff Over Total Area =	2.72	
2) 3.75" of Runoff Over Impervious Area =	3.08	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.08]

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-12 is between 6" to 18". We have assumed the SHWT is 1.0' below the existing ground and are providing a 2.0' berm above existing ground.

Pond Depth from top of Maint			
Berm to SHWT	3	ft	
Maint Berm =	1	ft	

H = Depth to pond SHWT - Maint Berm = 2 ft

3) Use greater of required treatment volume or attenuation volume.

Required Attenuation Volume =	1.02	ac-ft
Required Treatment Volume =	3.08	ac-ft

Peak Volume =	4.10	ac-ft
---------------	------	-------

4) For purposes of pond area calculations, assume a square pond.

wł

Volume = LWH

nere	H =	height (ft)
	L =	length of vertical sided pond
	VV =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume = H =	4.10 2		ac-ft ft			
		4.10	=		$L^2 x$	2
	Solving for L = Therefore W =		298.8 298.8	ft ft		

Add: x = [(Side	Slopes x H) x 2] to each dimension
-----------------	------------------------------------

Side slopes:	4	ft/ft
H:	2	ft
x =	16	ft
Length @ top of slope =	315	ft
Width @ top of slope =	315	ft

6) Add maintenance berms.

Assume 20' maintenance berm (add to each side)

Length w/maint berm =	355	ft
Width w/maint. Berm =	355	ft
Total Area =	2.89	acres
Add 10% Contingency	3.18	acres

PRELIMINARY POND AREA REQUIRED FOR BASIN-12= 3.2 ACRES

Recommended Pond 12A

Existing Ground Elevation =	48 ft
Normal Water Elevation =	47 ft
Lowest EOP Elevation =	54.02 ft
Pond R/W	6.88 ac

Pond Stage/Storage Calculations

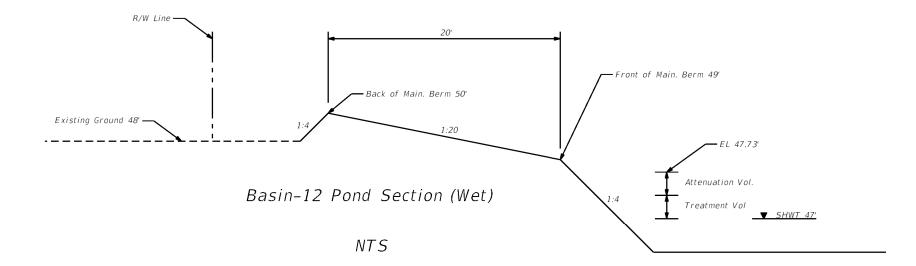
			Ave Area		Storage	Total Storage
Stage	Description	Area (ac)	(ac)	Depth (ft)	(ac-ft)	(ac-ft)
47	Normal Water Level	5.55				0.00
48		5.73	5.64	1.00	5.64	5.64
49	Front Main Berm	5.92	5.83	1.00	5.83	11.47
50	Back Main Berm	6.88	6.40	1.00	6.40	17.87

4.10 ac-ft

Required Treatment and Attenuation Volume =

Provided treatment and attenuation volume =	4.1 ac-ft
Provided treatment and attenuation Stage=	47.73 ft

Pond located outside of the 100-year flood plain.



SR 408 Eastern Extension-PD&E CFX BASIN 13

Computed By
Checked By
Date

KS CR

2/26/2017

Beginning Station	66110.00
End Station	70195.00
Length (ft)	4085.00

Total Basin Area		
R/W Width (ft)		<u>Area (ac)</u>
Proposed SR 408 Corridor		28.04
	TOTAL AREA (AC)	28.04

Existing Impervious Area							
Description		Area					
Residential		0.35					
	Total Impervious Area	0.35	Acre				

ATTENUATION VOLUME ESTIMATE

Pre-Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
1/4 Residential	A/D	87	0.35	30.45	
On-site Grassed Area	A/D	80	27.69	2,215.20	
		TOTAL	28.04	2,245.65	
		COM	POSITE CN	80.1	

Estimate of Runoff Volume

Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr/24 hr	SJRWMD	8.70	2.49	6.29	14.71
100 yr, 240 hr	FDOT	18.00	2.49	15.33	35.81
100 yr, 8 hr	FDOT	8.00	2.49	5.64	13.17
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	2.49
?) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	6.29
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	14.71

	Proposed Impervious Are	a	
Description		Area	
Proposed SR 408 Corridor (Prop impervious median = 136')	12.38		
	Total Impervious Area	12.38	Acre

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	A/D A/D	98.00 80	12.38 15.66	1,213.12 1,252.90	
		TOTAL	28.04	2,466.02	
		COM	POSITE CN	87.9	

	Estimate of Ru	Inoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.37	7.25	16.93
100 yr, 240 hr	FDOT	18.00	1.37	16.45	38.45
100 yr, 8 hr	FDOT	8.00	1.37	6.56	15.33
) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.37
) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	7.25
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	16.93

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) CN:	28.04 80.1	ł	POST DEVELC AREA (AC CI	
AGENCY	DESIGN	RUN	OFF VOLUME	(Vr)
	STORM	PRE	POST	NCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 yr, 24 hr	14.71	16.93	2.23
FDOT	100 yr, 240 hr	35.81	38.45	2.64
FDOT	100 yr, 8 hr	13.17	15.33	2.17
MAXIMUM ATTENUATION VOLUME	(AC-FT)	2.	64	

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	28.04
Post Development Impervious Area (ac) =	12.38

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft]
1) 1.5 " of Runoff Over Total Area =	3.51	
2) 3.75" of Runoff Over Impervious Area =	3.87	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	3.87	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the freeboard.

Per Soil Survey, SHWT at Basin-13 is between 0" to 18". We have assumed the SHWT is 1.0' below the existing ground and are providing a 2.5' berm above existing ground.

Pond Depth from top of Maint Berm to SHWT Freeboard =	3.5 1	ft ft				
H = Depth to por	nd SHWT - Free	eboard =	2.5	ft		
3) Use greater of required treatment	volume or atten	uation volume.				
			uation Volume = tment Volume =		2.64 3.87	ac-ft ac-ft
			Peak Volume =	:	6.51	ac-ft
4) For purposes of pond area calcula	tions, assume a	a square pond.				
Volume = LWH						
where	H = L = W =	-	ertical sided por ertical sided pone			
Since a square pond is being assume	ed, L = W. Ther	efore, Volume = L	² H			
Volume =	6.51	ac-ft				
H =	2.5	ft				
		6.51 =	L ² x	2.5		
	olving for L =	336.7	ft #			

Therefore W = 336.7 ft

Add: x = [(Side Slopes x H) x 2] to each dimension

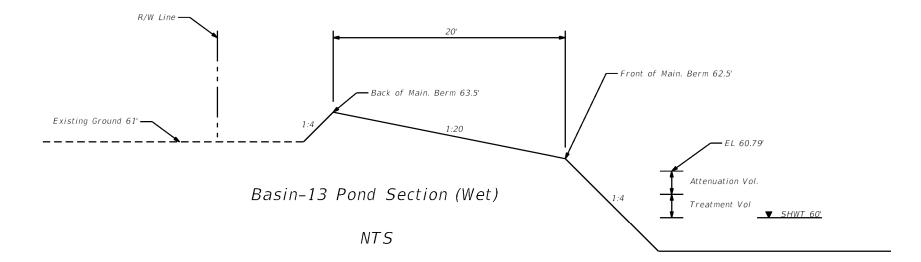
Side slopes: H:	4 2.5	ft/ft ft		
x =	20	ft		
Length @ top of slope = Width @ top of slope =	357 357	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add	to each side)			
Length w/maint berm = Width w/maint. Berm =	397 397	ft ft		
Total Area = Add 10% Contingency	3.61 3.97	acres acres		
PRELIMINARY POND	AREA REQUIRED	FOR BASIN-13=	4.0	ACRES
Recommended Pond 13B				
Existing Ground Elevation = Normal Water Elevation = Lowest EOP Elevation = Pond R/W	1	61 ft 60 ft 78.8 ft 0.45 ac		

Pond Stage/Storage Calculations

-			Ave Area		Storage	Total Storage
Stage	Description	Area (ac)	(ac)	Depth (ft)	(ac-ft)	(ac-ft)
60	Normal Water Level	7.93				0
61.5		8.42	8.175	1.5	12.2625	12.2625
62.5	Front Main Berm	8.75	8.585	1	8.585	20.8475
63.5	Back Main Berm	10.45	9.6	1	9.6	30.4475

Provided treatment and attenuation volume =	6.51 ac-ft
Provided treatment and attenuation Stage=	60.79 ft

Pond located outside of the 100-year flood plain.



SR 408 Eastern Extension-PD&E CFX

BASIN 14

Computed By	KS	
Checked By	CR	
Date		2/26/2017

Beginning Station	70195.00
End Station	71410.00
Length (ft)	1215.00

	Total Basin Area	
	R/W Width (ft)	<u>Area (ac)</u>
Proposed SR 408 Corridor		8.70
	TOTAL AREA (AC	8.70
	Existing Impervious Area	
Description	Area	
Residential	1.44	

	Total Impervious Area		1.44	Acre	
	ATTENUAT		ME ESTIMA	TE	
Pre-Development					
Land Use Description/	Soil Group	CN	Area	Product	

Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
1/4 Residential Property	A/D	87	1.44	125.28	
Woods (Fair)	A/D	79	7.26	573.54	
		TOTAL	8.70	698.82	
		COM	POSITE CN	80.3	

	Estimate of Ru	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	2.45	6.32	4.58
100 yr, 240 hr	FDOT	18.00	2.45	15.36	11.14
100 yr, 8 hr	FDOT	8.00	2.45	5.66	4.11
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	2.45
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	6.32
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	4.58

Proposed Impervious Area				
Description	Area			
Proposed SR 408 Corridor (Proposed 4' lanes and assume 64' impervious median = 136')	3.68			
Total Impervious Area	3.68	Acre		

Post Development

Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product	
On-site Roadway On-site Grassed Area	A/D A/D	98.00 80	3.68 5.02	360.82 401.45	
		TOTAL	8.70	762.27	
		COM	POSITE CN	87.6	

	Estimate of Ru	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	1.41	7.21	5.23
100 yr, 240 hr	FDOT	18.00	1.41	16.41	11.90
100 yr, 8 hr	FDOT	8.00	1.41	6.52	4.73
) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	1.41
) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)		Runoff (in)	R	7.21
) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	5.23

SUMMARY OF ATTENUATION ESTIMATES

PRE DEVELOPED CONDITION AREA (AC) CN:	8.70 80.3		POST DEVELC AREA (AC Cl	
AGENCY	DESIGN	RUN	OFF VOLUME	(Vr)
	STORM	PRE	POST	INCREASE
		(AC-FT)	(AC-FT)	(AC-FT)
SJRWMD	25 yr, 24 hr	4.58	5.23	0.64
FDOT	100 yr, 240 hr	11.14	11.90	0.76
FDOT	100 yr, 8 hr	4.11	4.73	0.62
MAXIMUM ATTENUATION VOLUM	IE (AC-FT)	().76	

St. John's River Water Management District Pollution Abatement Volume Requirement

Post Development Total Area (ac) =	8.70
Post Development Impervious Area (ac) =	3.68

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	1.09	
2) 3.75" of Runoff Over Impervious Area =	1.15	Governs
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	1.15	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

The top of the treatment and attenuation volume are constrained to berm elevation minus the Maint Berm.

Per Soil Survey, SHWT at Basin-14 is between 6" to 42". We have assumed the SHWT is 2.0' below the existing ground and are providing a 2.0' berm above existing ground.

Pond Depth from top of Maint Berm to SHWT Maint Berm =	4	ft ft			
H = Depth to por	nd SHWT - Maint	Berm =	3	ft	
3) Use greater of required treatme	nt volume or atte	enuation volume.			
		Required Attenu Required Treat			ac-ft ac-ft
		I	Peak Volume =	1.91	ac-ft
4) For purposes of pond area calc	ulations, assume	a square pond.			
Volume = LWH					
where	H = L = W =		vertical sided po ertical sided po		
Since a square pond is being assu	med, L = W. The	erefore, Volume =	^E L ² H		
Volume = H =		ac-ft ft			
		1.91 =	$L^2 x$	3	
	Solving for L =	166.5	ft		

166.5

ft

Therefore W =

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 3	ft/ft ft		
x =	24	ft		
Length @ top of slope = Width @ top of slope =	191 191	ft ft		
6) Add maintenance berms.				
Assume 20' maintenance berm (add to	each side)			
Length w/maint berm = Width w/maint_Berm =	231 231	ft ft		
Total Area =	1.22	acres		
Add 10% Contingency	1.34	acres		
PRELIMINARY POND AREA	REQUIRED	FOR BASIN-14=	1.3	ACRES
Recommended Pond 14A				
Existing Ground Elevation = Normal Water Elevation = Lowest EOP Elevation =	8	64 ft 62 ft 5.01 ft		
Pond R/W		2.57 ac		

Pond Stage/Storage Calculations

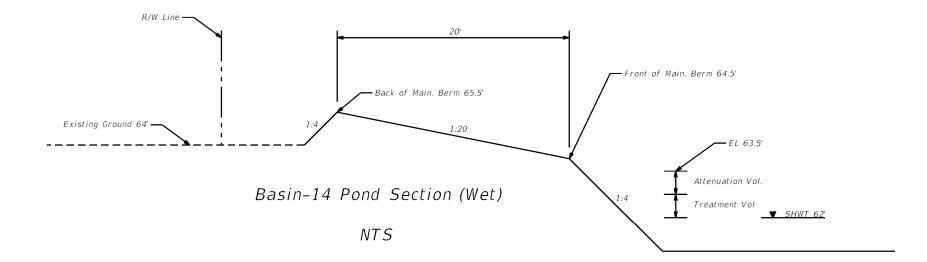
Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	Storage (ac-ft)	Total Storage (ac-ft)
62	Normal Water Level	1.34				0.00
63.5		1.58	1.46	1.50	2.19	2.19
64.5	Front Main Berm	1.74	1.66	1.00	1.66	3.85
65.5	Back Main Berm	2.57	2.16	1.00	2.16	6.01

1.91 ac-ft

Required Treatment and Attenuation Volume =

Provided treatment and attenuation volume =	2.19 ac-ft
Provided treatment and attenuation Stage=	63.5 ft

Pond located outside of the 100-year flood plain.



SR 408 Eastern Extension-PD&E CFX

BASIN 15

Computed By	
Checked By	
Date	

KS

CR

2/26/2017

Beginning Station	71410.00
End Station	74600.00
Length (ft)	3190.00

Total Basin Area					
R/W Width (ft)	<u>Area (ac)</u>				
Existing Pond M-1	3.11				
Grass and Wooded Area	26.18				
Grassed Area	4.26				
1/2 acre Residential lots	4.49				
	TOTAL AREA (AC) 38.04				

Existing Impervious Area					
Description	Area				
Existing Impervious areas within the basin limits	4.49				
Total Impervious Area	4.49	Acre			

ATTENUATION VOLUME ESTIMATE

Pre-Development

Pre-Development					
Land Use Description/	Soil Group	CN	Area	Product	
Soil Name			(ac)		
Existing SR 50					
1/2 acre Residential lots	A/D	84	4.49	377.50	
On-site Grassed Area	A/D	80	4.26	340.80	
On-site Pond-M1	A/D	100	3.11	311.00	
Grass and Wooded Area	A/D	79	26.18	2,067.90	
		TOTAL	38.04	3,097.20	
		COM	POSITE CN	81.4	

	Estimate of R	unoff Volume			
Summary Table:					
Design Storm	Agency	P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD	8.70	2.28	6.46	20.47
100 yr, 240 hr	FDOT	18.00	2.28	15.52	49.21
100 yr, 8 hr	FDOT	8.00	2.28	5.79	18.36
1) Soil Storage (S)	S = (1000/CN) - 10		Soil Storage (in)	S	2.28
2) Runoff (R)	$R = (P-0.2S)^2/(P+0.8S)$		Runoff (in)	R	6.46
3) Runoff Volume (Vr)	Vr = R/12 * Area		Runoff (ac-ft)	Vr	20.47

	Proposed Imp	ervious Area	1			
Description			Area			
Proposed SR 408 Corridor(Prop impervious median = 136')	osed 4' lanes and assun	ne 64'	10.97			
	Total Impervious Area		10.97	Acre		
Post Development						
Land Use Description/ Soil Name	Soil Group	CN	Area (ac)	Product		
Proposed SR 408 and Existing S	<u>R 50</u>					
On-site Roadway On-site Grassed Area	A/D A/D	98.00 79	10.97 27.07	1,075.16 2,138.45		
		TOTAL CON	38.04 MPOSITE CI	3,213.61 N 84.5		
	E dias		\/			
	Estim	ate of Runoff	volume			
Summary Table:						
Design Storm	Agency		P (in)	S (in)	R (in)	Vr (ac-ft)
25 yr, 24 hr	SJRWMD		8.70	1.84	6.83	21.64
100 yr, 240 hr 100 yr, 8 hr	FDOT FDOT		18.00 8.00	1.84 1.84	15.97 6.15	50.62 19.50
1) Soil Storage (S)	S = (1000/CN) - 10			Soil Storage (in)	S	1.84
2) Runoff (R)	R = (P-0.2S) ² /(P+0.8S)			Runoff (in)	R	6.83
3) Runoff Volume (Vr)	Vr = R/12 * Area			Runoff (ac-ft)	Vr	21.64
	SUMMARY OF ATTEN	UATION EST	IMATES			
PRE DEVELOPED CONDITION AREA (AC) CN:	<u>38.04</u> 81.4			POST DEVELOPI AREA (AC): CN:		TION
AGENCY	DESIGN STORM		RL PRE (AC-FT)	INOFF VOLUME (V POST (AC-FT)	r) INCREASE (AC-FT)	
SJRWMD	25 yr, 24 hi		20.47	21.64	1.18	
FDOT	100 yr, 240 l		49.21	50.62	1.41	
FDOT	100 yr, 8 hi	ſ	18.36	19.50	1.14	
MAXIMUM ATTENUATION VOL	JME (AC-FT)			1.41		

St. John's River Water Management District	
Pollution Abatement Volume Requirement	

Post Development Total Area (ac) =38.04Post Development Impervious Area (ac) =10.97

The Basin Discharges it Econ River which is an OFW. Additional 50% treatment volume is required The basin is an Open Basin.

Wet Detention	Ac-Ft	
1) 1.5 " of Runoff Over Total Area =	4.76	Govern
2) 3.75" of Runoff Over Impervious Area =	3.43	
WET DETENTION POLLUTION ABATEMENT VOLUME REQUIRED =	4.76	

ESTIMATE POND RIGHT OF WAY REQUIREMENTS

<u>The top of the treatment and attenuation volume are constrained to Berm elevation minus the Maint Berm.</u> Existing Ground Elevation = 60 ft Per the Bithlo Drainage Master Plan SHWT in Pond M-1 = 53 ft

Pond Depth from top of Maint				
Berm to SHWT	7	ft		
Maint Berm =	1	ft		
			-	

H = Depth to pond SHWT - Maint Berm = 6 ft

3) Use greater of required treatment volume or attenuation volume.

Required Attenuation Volume =	1.41	ac-ft
Required Treatment Volume =	4.76	ac-ft
Peak Volume =	6.16	ac-ft

4) For purposes of pond area calculations, assume a square pond.

Volume = LWH

where	H =	height (ft)
	L =	length of vertical sided pond
	W =	width of vertical sided pond

Since a square pond is being assumed, L = W. Therefore, Volume = L^2H

Volume = H =	6.16 6		ac-f ft	ft			
		6.16		=		$L^2 x$	6
	Solving for L = Therefore W =			211.5 211.5	ft ft		

Add: x = [(Side Slopes x H) x 2] to each dimension

Side slopes: H:	4 6	ft/ft ft		
x =	48	ft		
Length @ top of slope = Width @ top of slope =	260 260	ft ft		
6) Add maintenance Berms.				
Assume 20' maintenance Berm (ac	ld to each side)			
Length w/maint Berm = Width w/maint. Berm =	300 300	ft ft		
Total Area = Add 10% Contingency	2.06 2.27	acres acres		
PRELIMINARY POND A	REA REQUIRED FO	OR BASIN-15=	2.6	ACRES
				viation of Damad

Recommended Pond 15A - Will provide compensation for possible elimination of existing Pond M-1

Existing Ground Elevation =	60.00 ft
Normal Water Elevation =	53.00 ft
Lowest EOP Elevation =	68.17 ft
Pond R/W (Infield Pond)	8.92 ac

Pond Stage/Storage Calculations

Stage	Description	Area (ac)	Ave Area (ac)	Depth (ft)	Storage (ac-ft)	Total Storage (ac-ft)
53.00	Normal Water Level	5.32				0.00
60.00		6.95	6.14	7.00	42.95	42.95
61.00	Front Main Berm	7.27	7.11	1.00	7.11	50.06
62.00	Back Main Berm	8.92	8.10	1.00	8.10	58.15

6.16 ac-ft

6.16 ac-ft

54 ft

Required Treatment and Attenuation Volume =

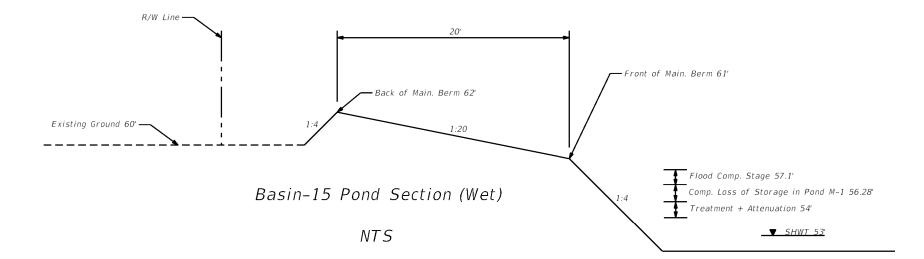
Provided treatment and attenuation volume = Provided treatment and attenuation Stage=

If Pond M-1 were to be eliminated the total loss in storage volume is 14.01 ac-ft (between stage 54' and 56.28') Compensating lost storage volume for Pond-M1 in Pond 15A will result in pond stage at = 56.28 ft

100-year Flood Elevation= 57.1 ft at Existing Pond M-1 (Bithlo Stormwater Masterplan)

Flood plain Compensation between 56.28' to 57.1' = 5.02 ac-ft

The 15 A pond has additional storage capacity to compensate for the lost storage in existing Orange County Pond M-1 due to the proposed SR 408 alignment and to provide additional flood plain compensation.

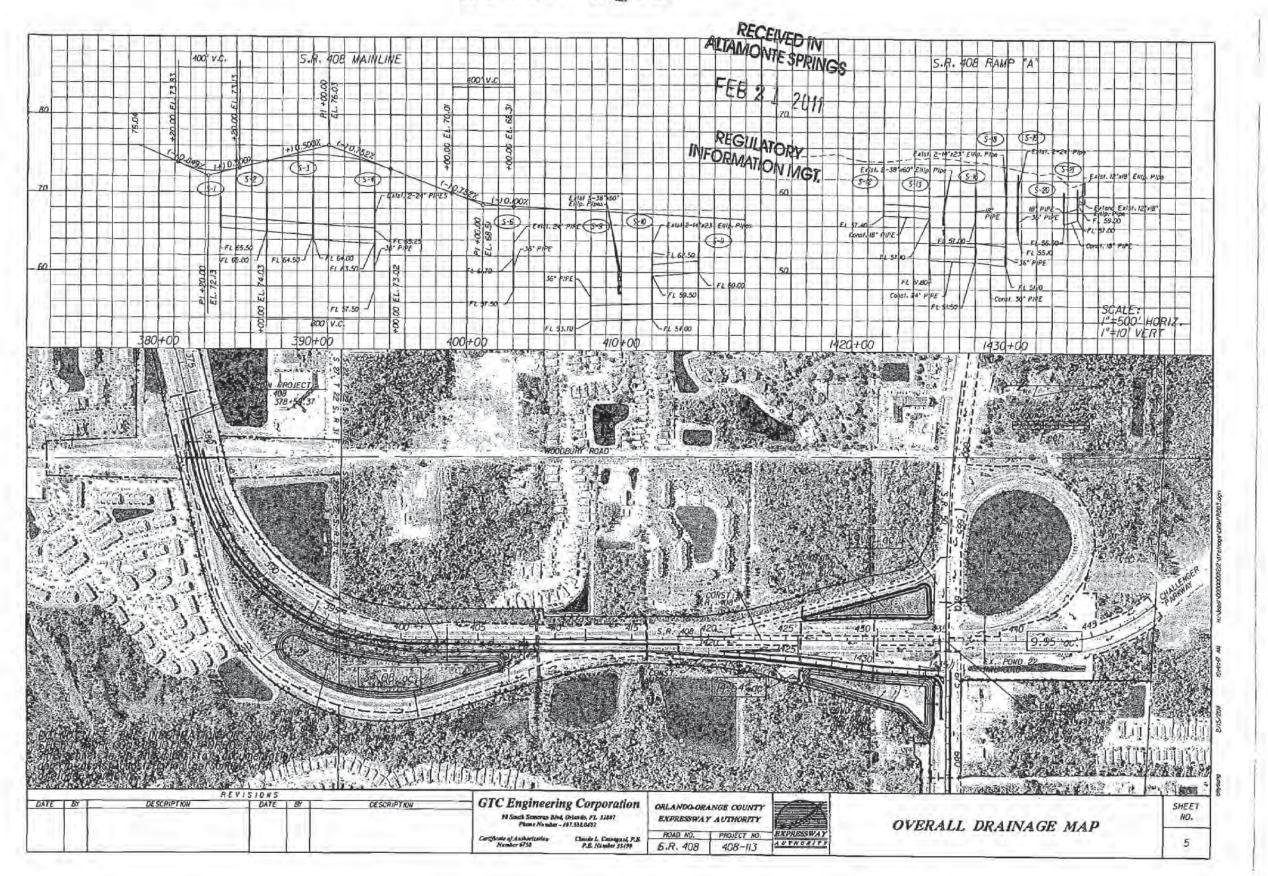


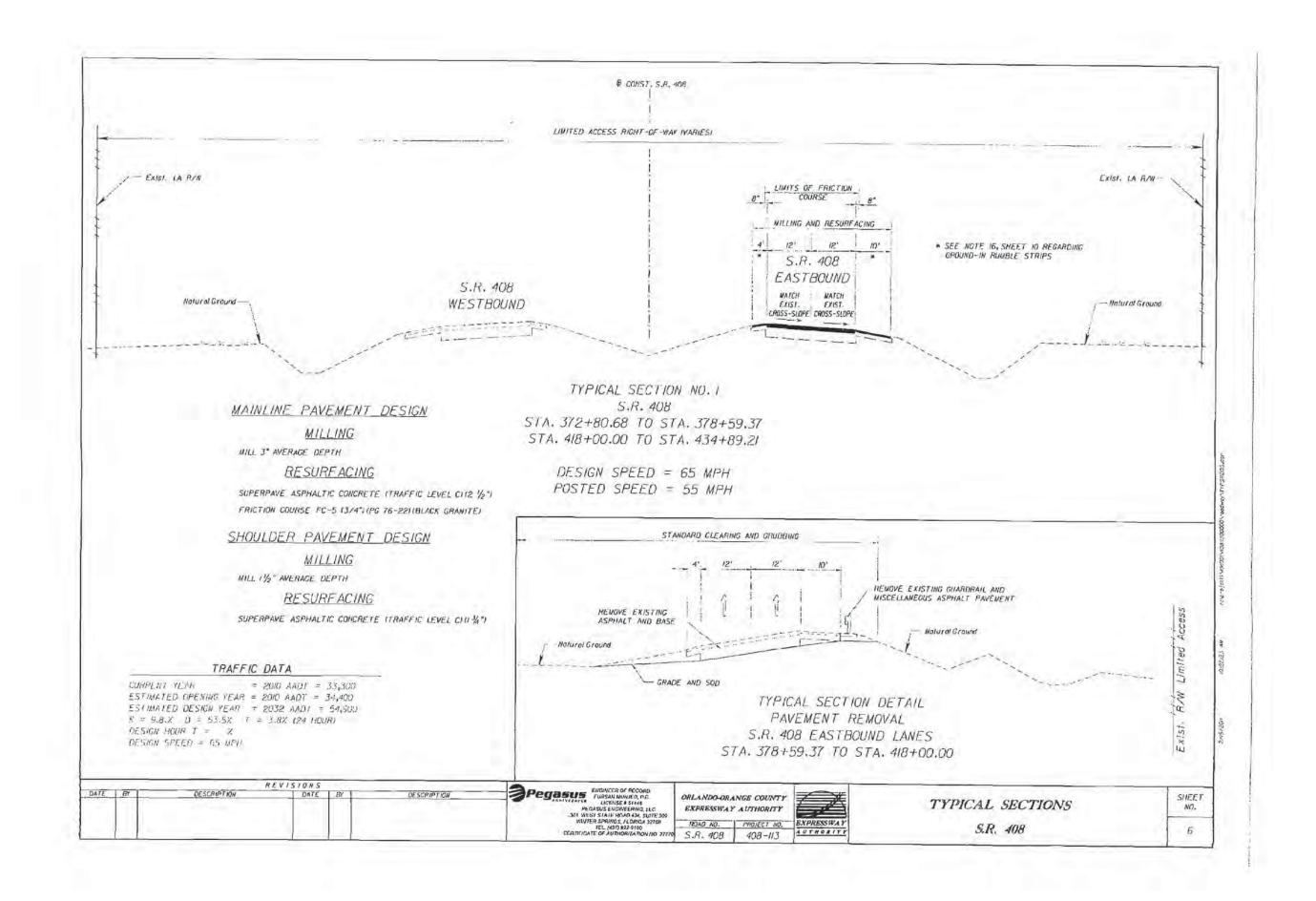
Appendix: G

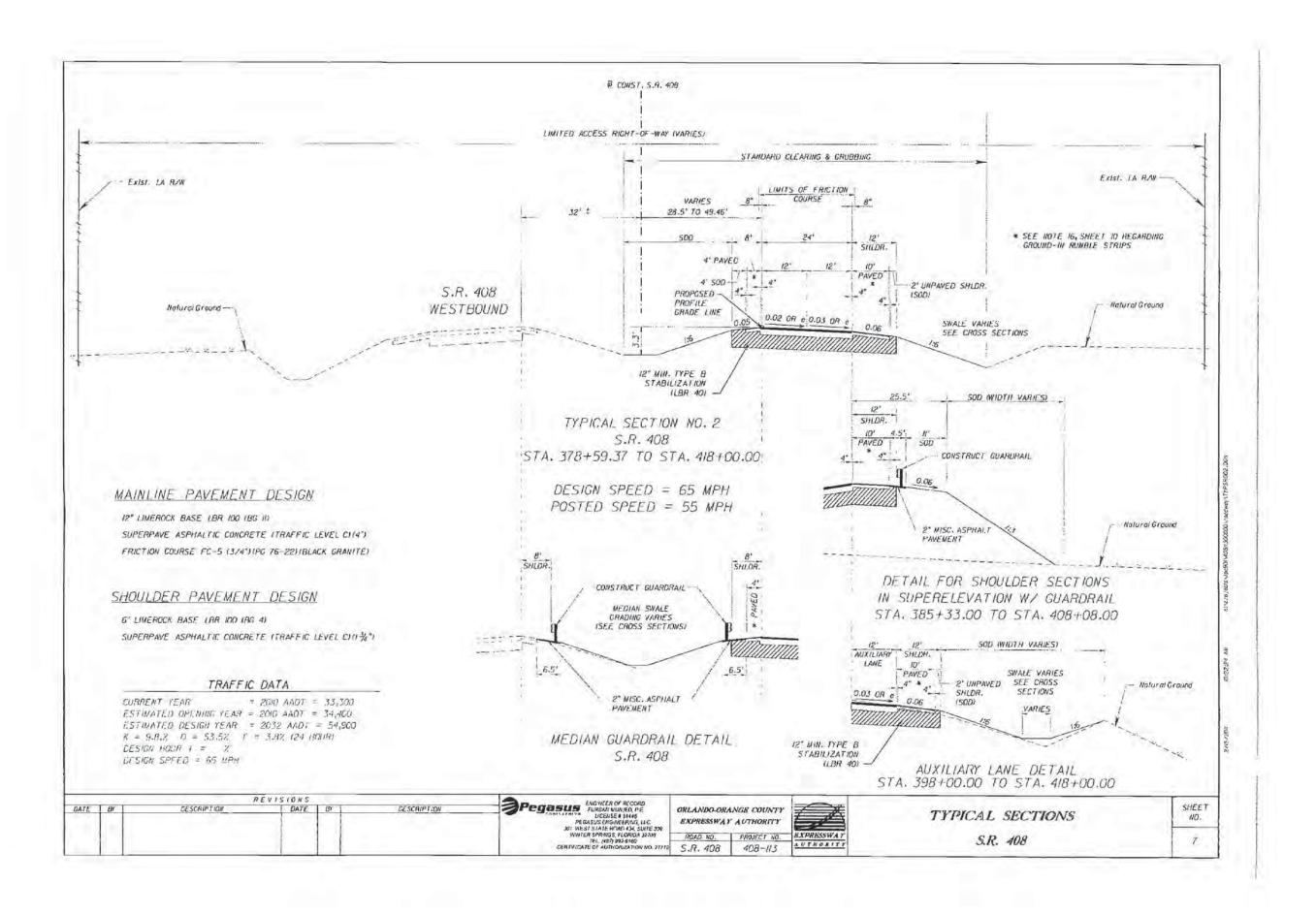
Excerpt from Existing SR.408 Plans

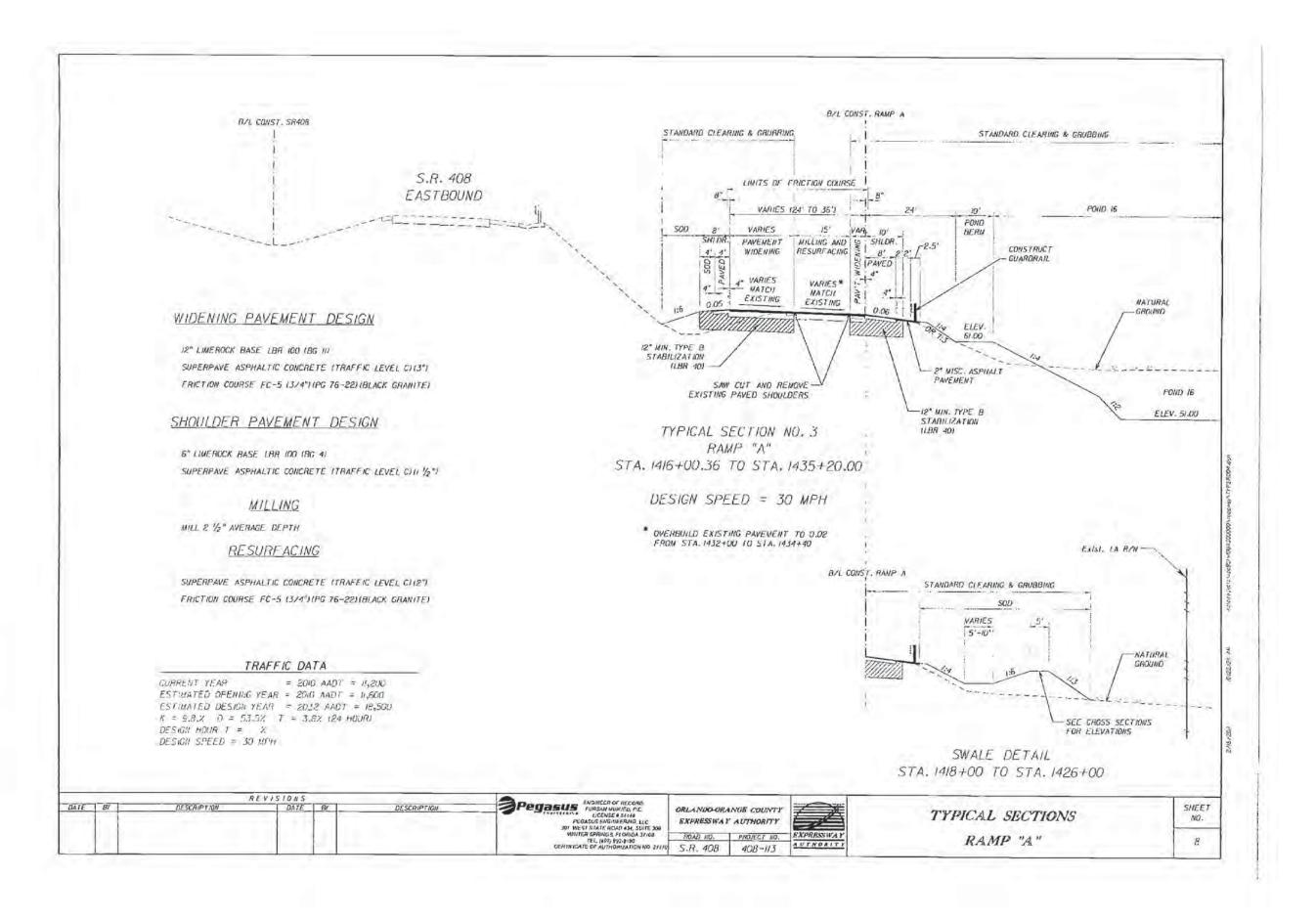


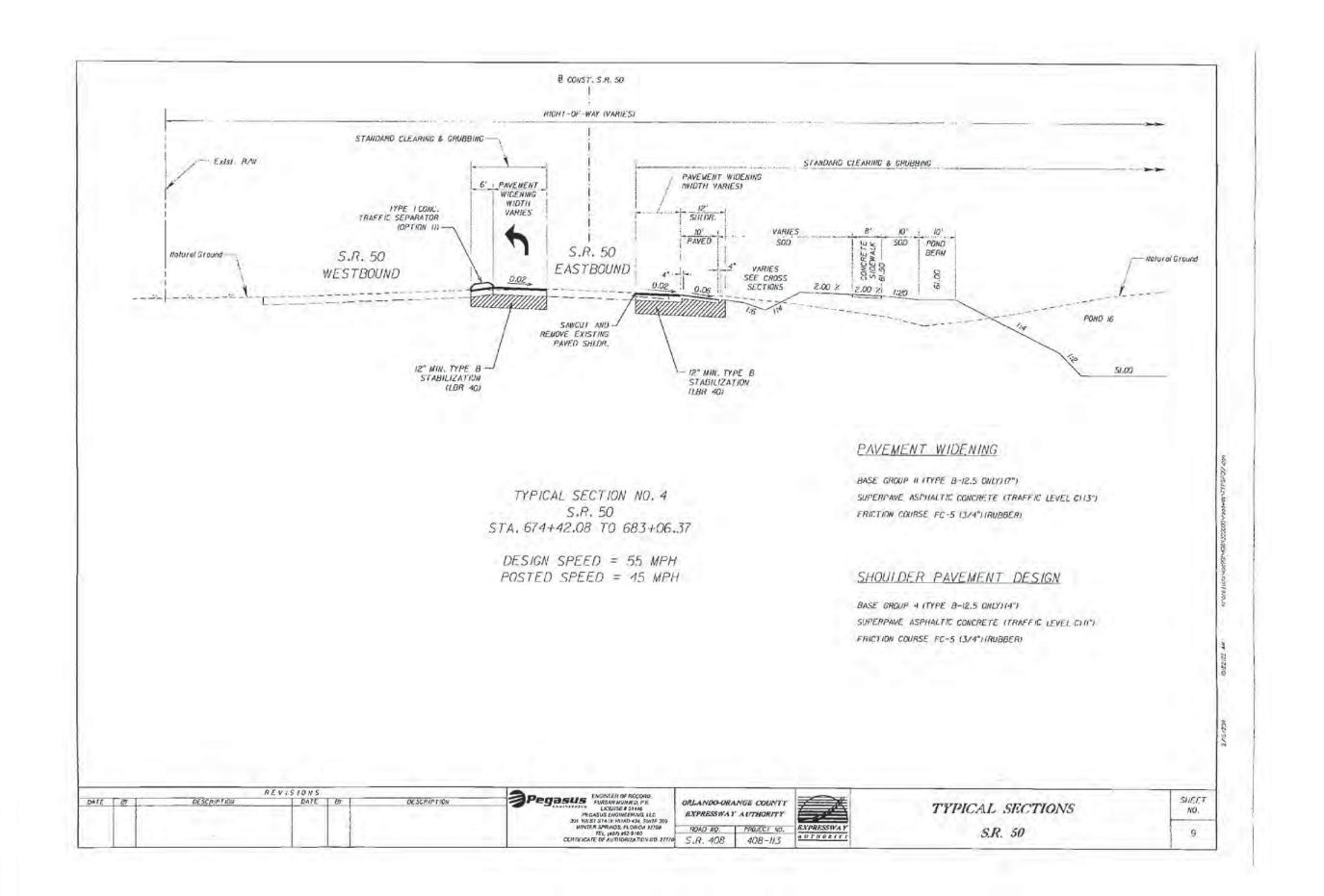
20358=24-=



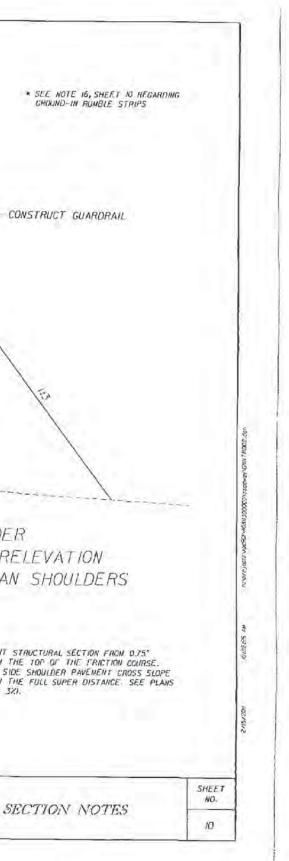


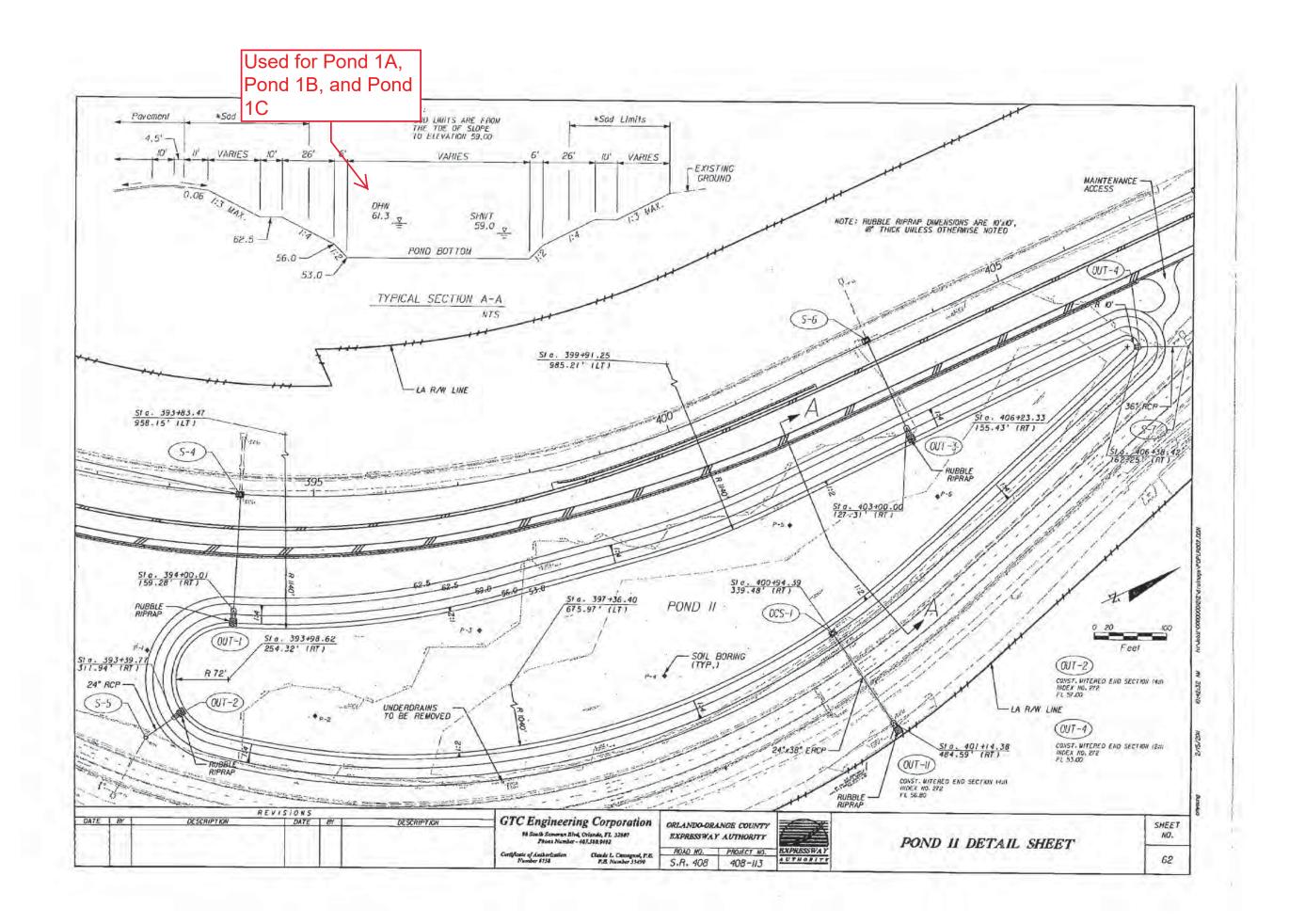


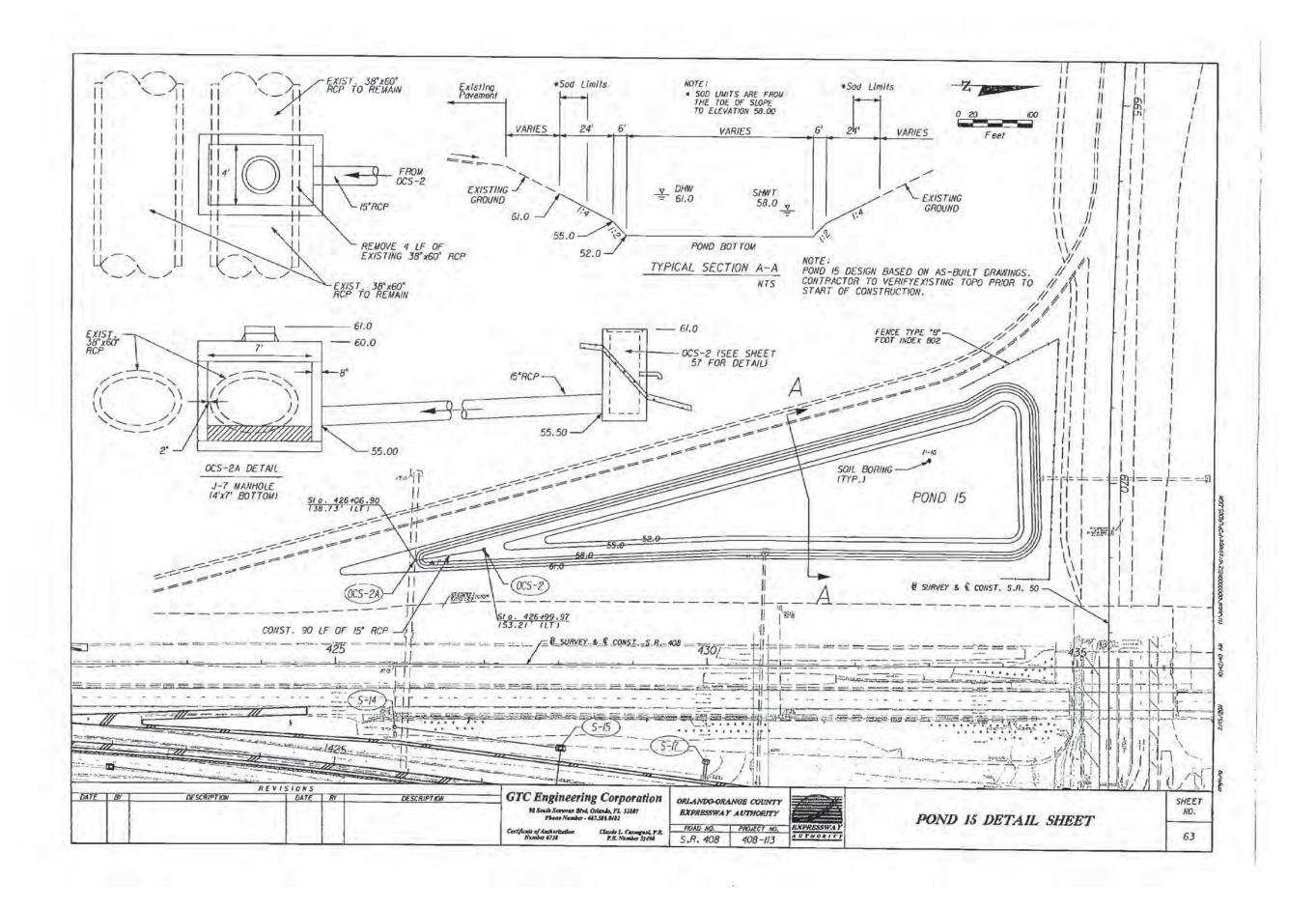




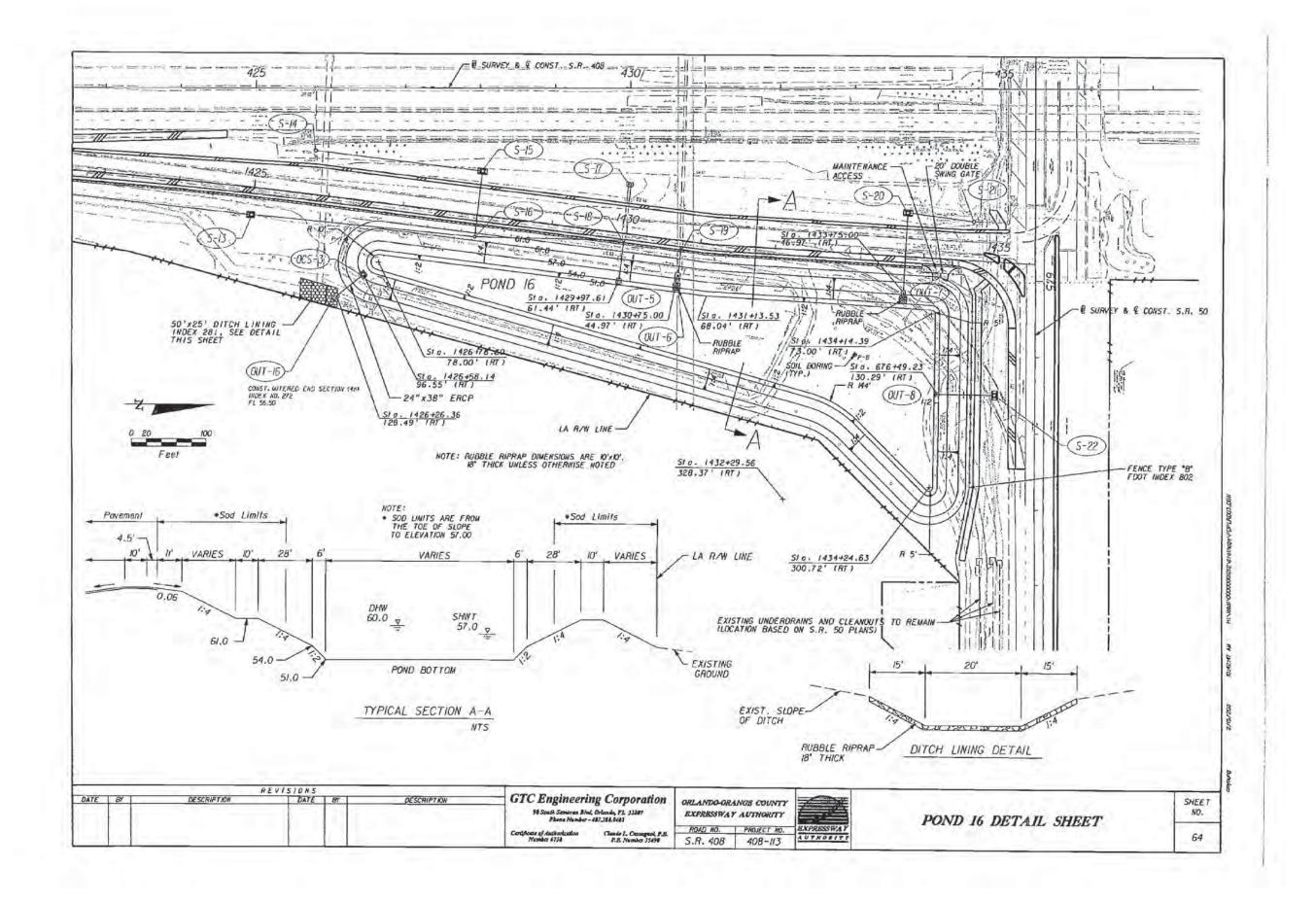
	TYPICAL SECTION NOTES				
h.	BITUMINOUS PRIME COAT IS TO BE APPLIED TO ALL LIMEROCK BASES ON WHICH PAVEMENT IS TO BE PLACED AT A RATE NOT LESS THAN OUS GALLONS PER SOUARE YARD, OR AS DIRE BY THE ENGINEER. PAYMENT FOR THE PRIME COAT IS INCIDENTAL TO AND IS INCLUDED IN O ITEMS OF RELATED WORK.	CTED THER	1.2	25.5'	
2.	TACK COAT IS TO BE APPLIED BETWEEN ALL PAVEMENTS COURSES AT A RATE OF 0.04 GALL PER SQUARE YARD, UN AS DIRECTED BY THE ENGINEER. PAYMENT FOR THE TACK COAT IS INCIDENTAL TO AND IS INCLUDED IN OTHER ITEMS OF RELATED WORK.	095		2'	
З,	ALL PERMANENT SOD AREAS, EXCEPT POND BOTTOMS, SHALL RECEIVE A 6 INCH FINISH SOIL I IPER 162-3-1011 TO BE PAND FOR UNDER 120-6.	LAYER,	SHL	LDR.	
4.	NONE OF THE EXISTING LIMEROCK BASE THAT IS REMOVED IS TO BE USED IN THE CONSTRU OF THE NEW LIMEROCK BASE. ALL EXISTING LIMEROCK THAT IS TO BE REMOVED IS TO BE INCORFORATED IN THE STABILIZED PORTION OF THE SUBGRADE.	IC F ION	TRAVEL LANE 10 PAVI	and second the second second second	
5.	ALL NEWLY-CONSTRUCTED SLOPES TO BE SODDED AS SOON AS PRACTICAL TO MINIMIZE EROSA	D₩.	LIMITS OF		
5.	ROADSIDE SWALES SHALL BE SODDED TO A MINIMUM OF 2 FOOT DEPTH.		FRICTION COURSE	1"	
7.	AREAS DUISIDE THE LINITS OF CONSTRUCTION AND WITHIN THE RIGHT-OF-WAY MAY BE SELL CLEARED AND GRUBBED AS DESIGNATED BY THE ENGINEER.		MAINLINE 4"	Ta	
в.	ALL DISTURBED AREAS, EXCEPT ROADWAY PAVEMENT AND POWD BOTTOMS, WITHIN THE LINITS CONSTRUCTION, SHALL BE GRADES AND SODDED.	OF	PAVEMENT		
9.	THE FRICTION COURSE IS TO BE MADE WITH BLACK GRAVITE AGGREGATE DULY ISEE SPECIAL	PROVISIONSI.	-520.05 ** 0.0	In the	
10.	COORDINATE MILLING AND RESURFACING CONSTRUCTION OPERATIONS TO PREVENT PONDING OF ON ROADWAY.	WATER	SE S	mil	
11+	MILLING OPERATIONS MAY INCLUDE REMOVAL OF LIMEROCK OR SDIL CEMENT BASE, REMOVAL OF BE INCIDENTAL TO THE CORRESPONDING MILLING EXISTING ASPHALT PAVEMENT PAY TIEM.	BASE SHALL			
12.	IN AREAS WHERE BASE COURSE IS EXPOSED, CONTRACTOR SHALL REMOVE MY LODSE OR BRO ROLL EXPOSED BASE COURSE WITH WINIMUM 2 PASSES OF A 5 TO 12 TON ROLLER, APPLY PRI INSTALL NEW ASPHALT IASPHALT SHALL BE INSTALLED DURING THE SAME OPERATION.	KEN ASPHALT, ME CDAT, AND	2" M	ISC. ASPHALT	
13.	THE FRICTION COURSE DVERLAP SHALL BE INSTALLED TO THE DIMENSION PROVIDED IN THE SECTIONS (B'IWITH & 0.5 INCH TOLERENCE.	TYPICAL	PAVE	EMENT	
14.	ALL FENCE PUSIS ARE TO BE SET IN CONCRETE OR BOLTED TO WALL TOPS PER INDEX NO.	802.			
15.	AT LOCATIONS WHERE FENCE IS INSTALLED OUTSIDE AREAS DESIGNATED FOR CLEARING AND THE CONTRACTOR SHALL CLEAR THE FENCE LINE SUFFICIENTLY TO ALLOW AN UNDESTRUCTED INSTALLATION. CLEARING REDUREMENTS FOR ACCESS AND INSTALLATION EQUIDMENT IS TO BE BY THE CONTRACTOR AND SHALL BE MINIMIZED. IN WETLAND AREAS CLEARING SHALL BE LIMIT	DETERMINED		Natural Graund	
16.	MAINLINE INSIDE AND DUTSIDE SHOULDERS SHALL HAVE GROUND-IN HUMBLE STRIPS AS PER I INDEX NO. 518, SHEET 2 OF 2. SHOULDER GROUND-IN RUMBLE STRIPS SHALL BE LONGITUDINAL	FUOT STANDARD		L <u>V</u> V V	
Π.	AT THE CONTRACTOR'S OPTION, BASE MATERIAL MAY BE USED IN LIEU OF STABILIZED SUBGR PAVED SHOULDERS, AT NO ADDITIONAL COMPENSATION.			and the second sec	
18.	THE CONTRACTOR SHALL GRADE THE AREA ADJACENT TO THE BASE OF THE WALLS TO ENSU	IRE DRAINAGE	МА	INLINE SHOULD	
19.	ALL A-8 WATERIAL IS TO BE STOCKPILED AND USED IN THE EMBANKMENT OR FINISH SOIL LA WITH INDEX NOS. 500 & 505.	YER IN ACCORDANCE		SIDE OF SUPEI	
20.	BASED ON THE CONTRACTOR'S TECHNOOLES, A SEPERATE PASS BY THE WILLING MACHINE MAY MEET DROP-OFF CLEARANCE REQUIREMENTS. ALL ASSOCIATED COSTS SHALL DE INCLUDES IN CORRESPONDING ASPHALT MILLING PAY ITEM NUMBERS.	BE REQUIRED TO THE COST FOR	SIMILAR FOR	CROWNED MEDIA N.T.S.	
21.	SHOULDER CROSS SLOPES AT SUPER-ELEVATION LOCATIONS SHALL BE PER DOCEA STANDARDS			14.1.5.	
22.	SHOULDER UN THE HIGH SIDE SHALL BE SLOPED IN THE SAME DIRECTION AS PAVEMENT WHI SLOPE IS GREATER THAN 0.05 FOOT PER FOOT.	EN PAVEMENT			
23.	FOR STABILIZING AT INTERSECTIONS, TURNOUTS AND GRADED CONNECTIONS, SEE STANDARD WI TYPICAL SECTIONS FOR DEPTH AND L.B.H.	DEX 515. SEE	** PROVIDE A 25' LONG VERTICAL TRANSITION OF THE SHOULDE BELOW THE TOP OF THE HIGH SIDE FRICTION COURSE, TO F EHD THE VERTICAL SHOULDER PAVEMENT TRANSITION WHEN		
24.	ACTUAL WIDTH OF BASE WIDENING WAY VARY DUE TO ACTUAL EXISTING PAVEMENT WIDTH. CON ELECT TO PLACE UNIFORM WIDTH BASE WIDENING STRIP AT NO ADDITIONAL COST.	TRACTOR MAY	EQUALS OF AND REEP IT FLUSH WITH FOR LOCATIONS. INOTE, WHEN SE > 92,	THE FRICTION COURSE THROUGH THE SHOULDER CROSS SLOPE =	
25.	THE TOP LIFT OF THE ASPHALTIC CONCRETE STRUCTURAL CONRSE IS TO NICLUDE THE PG 76	-22 BINDER.			
-	REVISIONS	A			
DATE BY		Pegasus Engineers of Record FURSAN NUNNED, P.C. UCENSET 5146	ORIANDO-ORANGE COUNTY		
		PEGASUS ENGINEERING, LLC TPI WHST STATE ROAD CIA, SUITE 300 WINTER SPANIOS, FLORIDA 37/08 TEL. (407) VIZ.21160 CENTRICATE OF AUTORNALATION NO. 37770	EXPRESSWAY AUTHORITY ROAD HO. PROJECT NO. EXPRESSWAY S.R. 408 408-113	TYPICAL	
			S.R. 408 408-113		

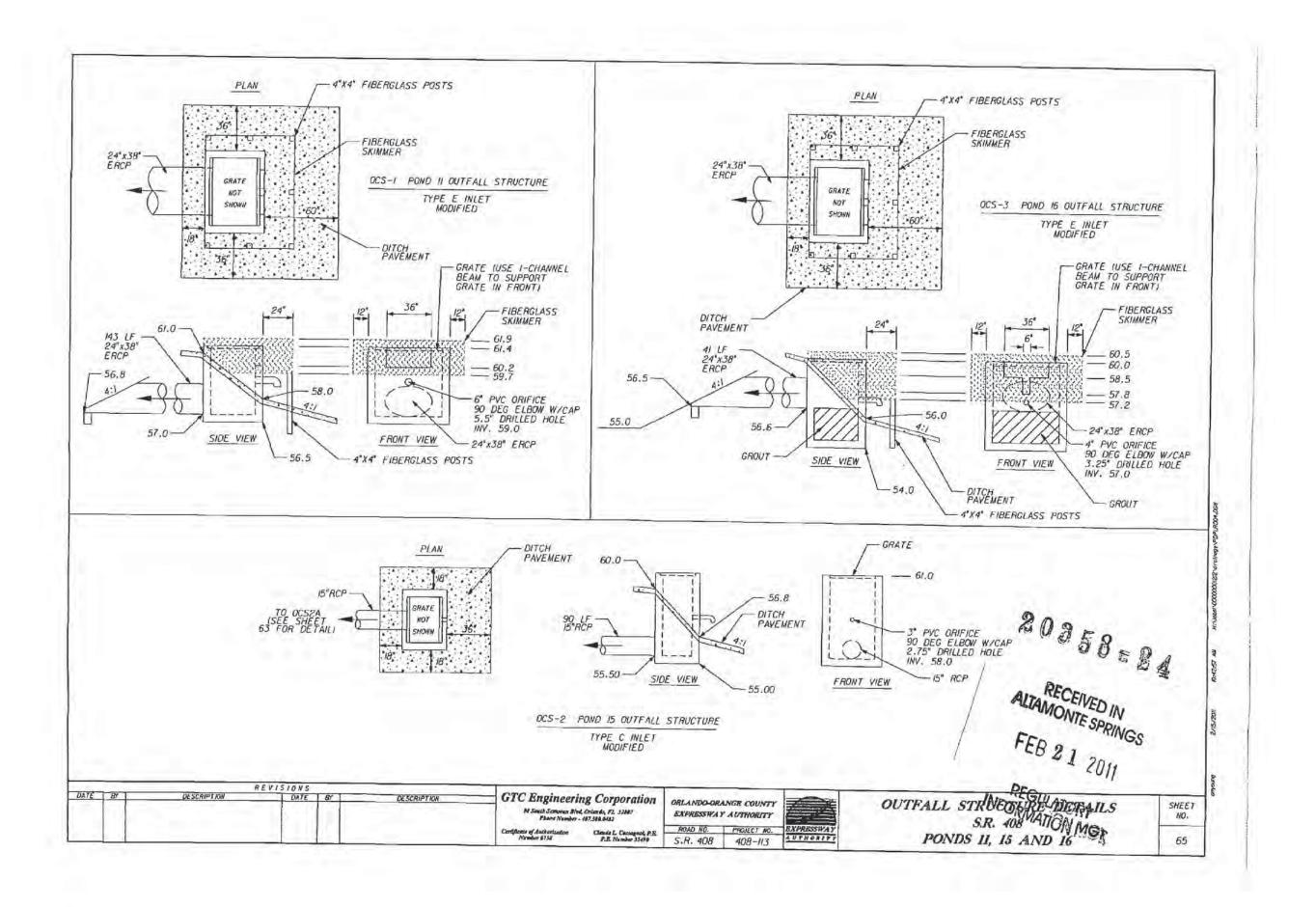






G-9





G-11

Appendix: H

Existing SR.408 Permit Information

Drainage Design Documentation & Calculations

S.R. 408 at S.R. 50



Prepared for: Orlando-Orange County Expressway Authority

Prepared by: 20358 ~ 24 GTC Engineering Corporation

February, 2011

RECEIVED FEB 2 1 2011 ALTAMONTÉ

GTC Engineering Corporation

98 South Semoran Blvd. - Orlando, FL 32807 Phone 407-380-0402 - Facsimile 407-380-0483



S.R. 408 at S.R. 50, OOCEA Project #408-113 Orange County, Florida Drainage Design Documentation

Contents

Section 1.0	General Information	
1.1	Project Location	2
1.2	Purpose	
1.3	Existing Drainage Pattern	
1.4	Tailwater	
	1.4.1 Pond Design	2
	1.4.2 Storm Sewer Design	2
1.5	Floodplain Impacts and Mitigation/Floodway Involvement	3
1.6	Rules and Regulations	3
	1.6.1 Stormwater Pond Design Criteria	3
1.7	Previously Permitted Project Information	4
Section 2.0	Pre-Development Analysis	
Section 3.0	Post-Development Analysis	7
Section 4.0	Floodplain Analysis	.10
Section 5.0	Crossdrain Analysis	10
Section 6.0	On-site Conveyance Analysis	10
Section 7.0	References	.10

Figures

Figure 1: Location MapFigure 2: USGS Quadrangle MapFigure 3: SCS Soils MapFigure 4: FEMA Flood Insurance Rate Map

Appendices

Appendix A:	Existing Condition Basin Data
Appendix B:	Proposed Condition Basin Data
Appendix C:	Existing ICPR Calculations
Appendix D:	Proposed ICPR Calculations
Appendix E:	Orifice Calculations
Appendix F:	Drainage Maps
Appendix G:	Storm Sewer Calculations
Appendix H:	Backup Information from Prime Design, Inc, H.W. Lochner and
	SJRWMD

20358-24

RECEIVED FEB 2 1 2011 ALTAMONTE





SECTION 1.0 - GENERAL INFORMATION

1.1 PROJECT LOCATION

The proposed project is located on SR 408 from just west of the bridge with Woodbury Road to the interchange with SR 50, a distance of approximately 1.1 miles. It is located in Sections 23 and 26, Township 22 South, Range 31 East of Orange County, Florida. The proposed project will include the realignment of the eastbound lanes of S.R. 408, the addition of turn lanes at the off ramp to SR 50, and modifications to three existing detention areas. The drainage design accommodates the proposed improvements in all ponds.

Note: This project is based on the NGVD '29 Datum.

1.2 PURPOSE

The purpose of this report is to document the drainage analysis for expanding and/or revising the existing permitted pond sites within the roadway right of way, and to meet the water quantity and water quality needs of the proposed roadway improvements.

1.3 EXISTING DRAINAGE PATTERN

The project is located within the Econlockhatchee River Basin of the St Johns River Water Management District. The existing stormwater management systems outfall to adjacent wetland systems and canals that flow to the Econlockhatchee River.

1.4 TAILWATER

1.4.1 Pond Design

The tailwater used in the pond design is based on stain marks in the existing drainage system.

1.4.2 Storm Sewer Design

The design of the storm sewer system is based on the stage of the 10-year 24-hour storm event at the time of peak inflow.



1.5 FLOODPLAIN IMPACTS AND MITIGATION/FLOODWAY INVOLVEMENT

The portion of SR 408 included in the project area lies outside of the 100-year floodplain as defined by FEMA (see FEMA exhibit, effective date of September 25, 2009 in Appendix A). There is a wetland area directly east of SR 408 which is classified as Zone A (areas within the 100-year floodplain).

1.6 RULES & REGULATIONS

The stormwater management criteria for the mainline and ramps are based on regulations from the St Johns River Water Management District (SJRWMD) and the Florida Department of Transportation (FDOT). In general, the stormwater collection systems for this project will include utilization of roadway swales and storm sewers with ditch bottom inlets, gutter inlets, and curb inlets. The stormwater management facilities consist of wet detention facilities to treat and attenuate the stormwater runoff. Off-site drainage systems are maintained using existing cross drains.

Permits required for this project:

- SJRWMD Environmental Resource Permit
- NPDES Stormwater Permit

1.6.1 Stormwater Pond Design Criteria

The major stormwater attenuation design criteria will require post development discharge rates not to exceed predevelopment discharge rates for the 25-year 24-hour event and the mean annual storm event. For this project, SJRWMD will require water quality treatment based on the type of treatment system proposed, i.e. wet detention (see SJRWMD Basis of Review (BOR)). Pond control elevations for Ponds 15 and 16 were set one-foot below the permitted dry bottom elevation. Pond 11 was set based on existing evidence of high water marks in the drainage system (staining on existing culverts and structures). The proposed Design High Water (DHW) elevation for ponds shall not exceed the low edge of pavement within the basin and shall not exceed base clearance requirements (3' for mainline, 1' for ramps) for a period greater than 24 hours. Ponds not constrained by pavement shall provide one foot of freeboard from the top of berm to the DHW elevation. The ponds are sized based on the SJRWMD 25-year 24-hour (8.60 inch rainfall) runoff volume. The pond layout shall meet applicable SJRWMD criteria as well as FDOT criteria as defined in the FDOT Drainage Manual and the Stormwater Management Facilities Handbook.

<u>Water Quantity Criteria</u> – The water quantity aspects will meet the requirements of the St. Johns River Water Management District (SJRWMD) with appropriate drainage features and stormwater management plan, for a project located within an open drainage basin. The peak allowable post development discharge from the project must be less than or equal to the peak rate at which water leaves the site under existing conditions. The 25-year 24 hour design storm event and mean



annual storm event will be used as required by the SJRWMD (25-year 24-hour rainfall 8.60", mean annual rainfall 4.5"). This criteria is outlined in the Applicants Handbook for Management and Storage of Surface Waters, Rule 40C-4 F.A.C.

<u>Water Quality Criteria</u> – The water quality aspects of the proposed stormwater management system will be designed in accordance with the SJRWMD criteria for a wet detention system. Since the Econlockhatchee River is considered an Outstanding Florida Water (OFW) at this location, the ponds will be designed to retain 3.75" inches of runoff from impervious area or the first 1.5" inch of runoff from the entire basin, whichever is greater. This criteria is outlined in the Applicants Handbook for Regulation of Stormwater Management Systems, Rule 40C-42.

<u>Pond Layout Guidelines</u> – The ponds are designed with side slopes generally at 1:4(V:H). Maintenance berms are flat. A ten foot maintenance berm is provided for Pond 11 to maximize fill requirements. A ten foot maintenance berm is provided for Pond 16 due to pond volume constraints. No maintenance berm is provided for Pond 15 due to pond volume constraints. The existing Pond 15 has no maintenance berm. All ponds have a minimum 1:4 slope from the top of bank to the normal water elevation, which in a meeting with OOCEA was deemed acceptable for maintenance purposes for this project.

<u>Pond Recovery</u> – Stormwater management systems shall be designed so that the outfall structures shall bleed down one-half the treatment volume within 24 to 30 hours following a storm event, but no more than one-half of this volume will be discharged within the first 24 hours. This criteria is outlined in the Applicants Handbook for Regulation of Stormwater Management Systems, Rule 40C-42.

1.7 PREVIOUSLY PERMITTED PROJECT INFORMATION

Some of the information in this report was gathered from projects previously permitted by SJRWMD. The original design of the S.R. 408 project was completed by Prime Engineers (Permit #4-095-20358-2) in 1987 for OOCEA. The as-built plans for the original design were used to determine the inverts, pipe lengths and sizes for the interconnected pond system at the interchange of S.R. 408 and S.R. 50, as well as the stage/area information for the existing ponds. The widening of S.R. 50 at the interchange with S.R. 408 was designed by H.W. Lochner, Inc. for FDOT (Project #239203-4-52-01) and permitted by SJRWMD in 2004 (Permit #4-095-86445-3). For their design, they performed storm routings using revised basin information for the interconnected pond system. Their calculations were used to determine the basin areas, CN, and TC's for the existing condition.

4



SECTION 2.0 – PREDEVELOPMENT ANALYSIS

The existing typical section consists of a four-lane expressway with open swales and closed storm sewer systems that collect the roadway runoff and discharging into existing permitted ponds. The project alignment is located entirely within Orange County, Florida and within the regulatory boundaries of the SJRWMD.

Predevelopment Basins

Basin 1100

Basin 1100 is located where the eastbound and westbound lanes of SR 408 bifurcate and runs from Station 380+20 to 416+00 of the centerline of SR 408. The basin area drains to the existing Pond 11 located between the eastbound and westbound lanes. This pond is not functioning as intended in the permit, and was originally permitted as a dry bottom pond with underdrains. The pond discharges through a control structure to the wetland east of the eastbound lanes of SR 408.

Basins 5001, 5005

These basins are located on the west side of the center line of SR 408 and drain to the existing Pond 15 located west of the alignment. This pond was permitted as a dry detention facility using underdrains and is not functioning as intended in the permit. The pond discharges through two 24" RCP culverts under SR 408 into Pond 16. Basin 5001 includes the area of SR 50 between Station 664+00 to 671+66 of the centerline of SR 50. Basin 5005 runs from approximately 421+50 to 435+63 of the centerline of SR 408 and includes the pond area, the westbound lanes and a portion of the eastbound lanes of SR 408.

Basins 5000, 5002, 5004

These basins are located on the east side of the center line of SR 408 and drain to the existing Pond 16 located east of the off ramp (to SR 50). This pond is not functioning as intended in the permit, and was originally permitted as a dry bottom pond with underdrains. The pond discharges to the wetland area east of the pond. Basin 5000 runs from approximately 425+76 to 434+60 of the centerline of SR 408 and includes the median area between the eastbound and westbound travel lanes. Basin 5002 runs from approximately Station 1416+00 to 1425+76 of the baseline of Ramp "A" of SR 408 and includes a portion of the eastbound lanes of SR 408, the ramp pavement and roadway swales east of the ramp. Basin 5004 runs from approximately to 1423+70 to 1433+10 of the baseline of Ramp "A" of SR 408 and includes a portion of the ramp approximately to 1423+70 to 1433+10 of the baseline of Ramp "A" of SR 408 and includes a portion of the ramp approximately to 1423+70 to 1433+10 of the baseline of Ramp "A" of SR 408 and includes a portion of the ramp approximately to 1423+70 to 1433+10 of the baseline of Ramp "A" of SR 408 and includes a portion of the ramp approximately to 1423+70 to 1433+10 of the baseline of Ramp "A" of SR 408 and includes a portion of the eastbound lanes of SR 408, the ramp pavement, grassed swale to the west of the ramp and the Pond 16 area.

Basin 5003

This basin is located on the southeast corner of the SR 408/SR 50 interchange and drains to the existing Pond 17 located south of SR 50. This pond is a dry detention facility which discharges to



an existing box culvert east of the pond which outfalls to the wetland south of SR 50. Basin 5003 includes the grassed area north of Pond 16 and west of the turn lanes, the turn lanes onto SR 50 and the east bound lanes of SR 50 from Station 673+11 to Station 681+00 of the centerline of SR 50. This basin was not included in the routing.

Basins 8000, 8001

These basins are located northwest of the interchange at SR 408 and SR 50 and drain to Pond 19, a wet detention facility. This pond discharges through a control structure under SR 50 into Pond 15. Basin 8000 includes the pond area a portion of the westbound lanes of SR 408 and the on-ramp to SR 408 Westbound from westbound SR 50. Basin 8001 includes the westbound lanes of SR 50 from approximately Station 647+30 to 664+00 of SR 50.

Basin 8002

This basin is located at the northeast corner of the SR 408/SR 50 Interchange and runs from Station 435+60 to 449+55 of the centerline of SR 408. This area drains to the existing Pond 22. Pond 22 discharges through a cross drain under SR 408 into Pond 19. Basin 8002 includes the eastbound lanes of SR 408 and the pond area.

Basin	Node	Area (ac.)	Impervious Area (ac.)	CN ¹	Tc (min.)
1100	11	34.08	6.72	93	40
5001*	15	1.85		95.9	10
5005*	15	7.96	+	87	36
5000*	16	0.72	1	85.4	10
5002*	16	2.10		94.2	10
5004*	16	5.21	-	91	23.3
8000*	19	3.09		92.1	45.6
8001*	19	19.04	1. etc. 1	91.5	30
8002*	22	9.95	1 S-4	90.2	66.7

Table 1 – Existing Hydrologic Information	Table 1	- Existing	Hydrologic	Information
---	---------	------------	------------	-------------

* Information from H.W. Lochner Calculations, (SJRWMD Permit

#4-095-86445-3), impervious area not available

¹ CN value includes impervious area



SECTION 3.0 – POST DEVELOPMENT ANALYSIS

The proposed improvements will consist of the realignment of the eastbound lanes of SR 408, the widening of the off-ramp to SR 50, and the addition of a turn lane onto SR 50, with runoff collected and directed to stormwater treatment facilities. Three ponds (Ponds 11, 15, and 16) will be converted from dry retention to wet detention facilities. Ponds 11 and 16 will be regraded and discharge structures replaced. Pond 15 will be regraded and a control structure with orifice will be constructed to maintain the established normal water level. Pond 17 will be eliminated and the associated drainage area will be collected in Pond 16. Ponds 19 and 22 will remain in their existing condition. There are no new proposed ponds within this project. Ponds 11, 15 and 16 discharge to an Outstanding Florida Waterbody (OFW).

Post Development Basins

Basin 1100

This basin is located from Station 380+20 to 416+00 of the centerline of SR 408. The eastbound lanes will be realigned further west to follow the existing alignment of the westbound lanes. This basin area will drain to the regraded Pond 11 which will be located east of the realigned eastbound lanes. The control structure for Pond 11 will be replaced. No additional impervious area is proposed for this basin.

Basin 5001_5005

This basin is located at the southwest corner of the SR408/SR 50 interchange and drains to Pond 15 located west of the alignment. Basin 5001_5005 includes the area of SR 50 between Station 664+00 to 671+65 of the centerline of SR 50, the area of SR 408 from approximately 421+46 to 435+63 of the centerline of SR 408, the pond area, the westbound lanes and a portion of the eastbound lanes of SR 408. No additional impervious area is proposed for this basin.

Basin 1600

This basin is located on the east side of the center line of SR 408 and drains to Pond 16 located east of the off ramp to SR 50. Basin 1600 runs from approximately Station 425+75 to 435+63 of the centerline of SR 408 and includes the median area between the eastbound and westbound travel lanes, a portion of the eastbound lanes of SR 408, the ramp pavement and roadway swales east of the ramp, the grassed swale to the west of the ramp, the area of SR 50 from Station 676+75 to 681+00 of the centerline of SR 50, and the Pond 16 area. The ramp area is proposed to be widened along with an addition of a turn lane onto SR 50. Pond 16 will be enlarged to the north and regraded. The existing control structure will be replaced with a drop structure and pipe which will discharge to the existing wetland to the east.



S.R. 408 at S.R. 50, OOCEA Project #408-113 Orange County, Florida Drainage Design Documentation

Basins 8000, 8001

These basins are located northwest of the interchange at SR 408 and SR 50 and drain to Pond 19, a wet detention facility. This pond discharges through a control structure under SR 50 into Pond 15. Basin 8000 includes the pond area a portion of the westbound lanes of SR 408 and the on-ramp to SR 408 Westbound from westbound SR 50. Basin 8001 includes the westbound lanes of SR 50 from approximately Station 647+30 to 664+00 of SR 50. No improvements are proposed for these basins.

Basin 8002

This basin is located at the northeast corner of the SR 408/SR 50 Interchange and runs from Station 435+60 to station 449+55 of centerline of SR 408. This area drains to the existing Pond 22. Pond 22 discharges through a cross drain under SR 408 into Pond 19. Basin 8002 includes the eastbound lanes of SR 408 and the pond area. No improvements are proposed for this basin.

Basin	Node	Area (ac.)	Impervious Area (ac.)	CN ¹	Tc (min.)
1100	11	34.08	6.72	93	23
5001_5005	15	9.81	3.63	91	10
1600	16	14.54	5.17	90	17
8000*	19	3.09		92.1	45.6
8001*	19	19.04		91.5	30
8002*	22	9.95		90.2	66.7

Table 2 – Proposed Hydrologic Information

*Information from H.W. Lochner Calculations, (SJRWMD Permit #4-095-86445-3), impervious area not available

¹ CN value includes impervious area



S.R. 408 at S.R. 50, OOCEA Project #408-113 Orange County, Florida Drainage Design Documentation

Table 3 - Proposed Hydraulic Information

		25 Year-24	Hour Storm		1	Mean Ann	ual Storm	
	Peak S	tage (ft)	Peak Disc	harge (cfs)	Peak S	tage (ft)	Peak Disc	harge (cfs)
Pond	Existing	Proposed	Existing	Proposed	Existing	Proposed	Existing	Proposed
Pond 11	63.0	61.3	14.6	12.8	62.3	60.4	1.6	1.6
Pond 15	61.0	61.0	16.4	16.6	59.9	59.8	4.7	3.9
Pond 16	60.1	60.0	23.6	18.8	59.6	58.9	5.3	3.8

Table 4 - Water Quality Volumes

Basin	1.5" of Runoff from Basin (ac-ft)	3.75" of Runoff from Impervious Area (ac-ft)	Water Quality Volume Required (ac-ft)	Water Quality Volume Provided (ac-ft)
Pond 11	4.26	2.10	4.26	4.41
Pond 15	1.23	1.13	1.23	1.25
Pond 16	1.82	1.62	1.82	1.93

Table 5 - Post Development Basin Design Characteristics

Basin	Control Elevation	Pond Bottom Elevation	Top of Berm Elevation	Proposed Peak Stage 25-year 24-hour
Pond 11	59.0	53.0	62.5	61.3
Pond 15	58.0	52.0	62.0	61.0
Pond 16	57.0	51.0	61.0	60.0



SECTION 4.0 – FLOODPLAIN ANALYSIS

There will be no floodplain impacts as a result of the proposed construction.

SECTION 5.0 - CROSS DRAIN ANALYSIS

The three existing cross drains within the project will not be affected by the proposed construction. These cross drains are as follows: 3-38"x60" ERCP at Station 408+85, 2-36" RCP at Station 416+00, and 2-38"x60" ERCP at Station 426+00. The locations of these cross drains both horizontally and vertically were taken into account in the design of the proposed storm sewer systems.

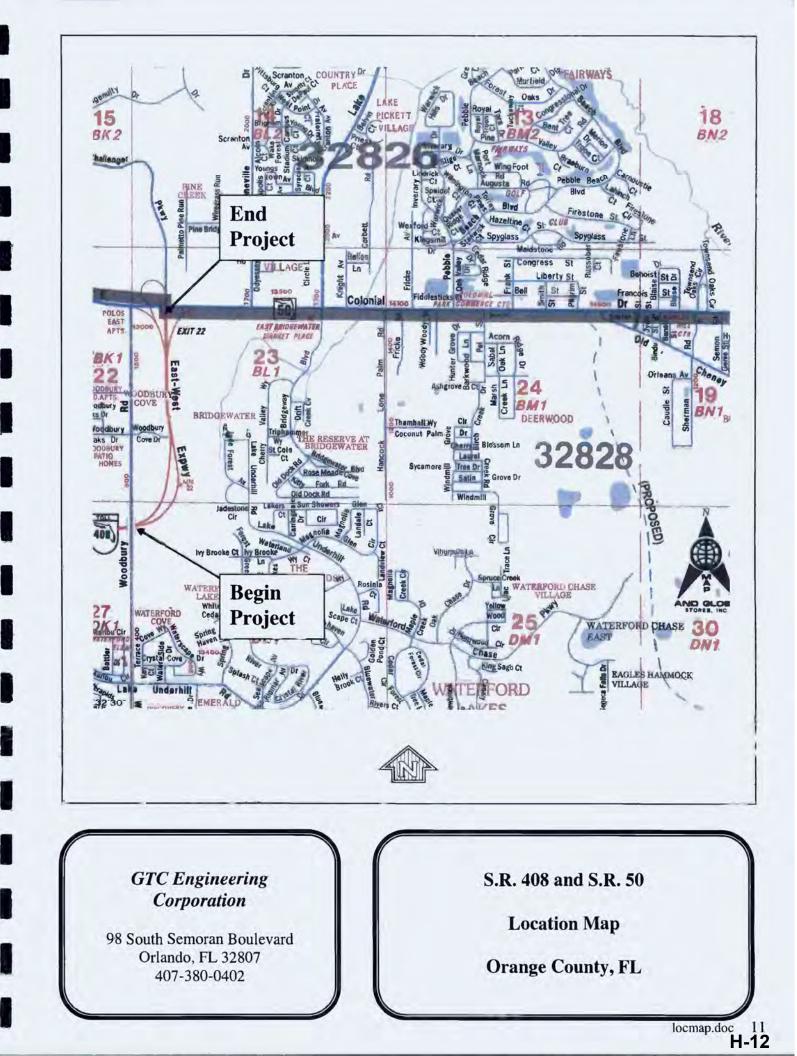
SECTION 6.0 - ON-SITE CONVEYANCE ANALYSIS

The on-site conveyance for this project uses roadside and median ditches to collect runoff and convey it to the treatment areas. Ditch bottom inlets located in the median outfall to the roadside ditches. The design of the storm sewer system is based on the tailwater from the receiving pond at the 10 year peak inflow stage. The software program ASAD was used for storm sewer design. ASAD uses the Rational Method to calculate peak flows and Manning's formula to calculate pipe losses in a storm sewer system. Peak flows are calculated using IDF (Intensity Duration Frequency) curves developed by the FDOT for short duration, high intensity storms which represent typical small storms within various zones within the FDOT. This project is located in Zone 7. ASAD does not account for storage within a system and can only use a single tailwater elevation for the starting water surface elevation. See Appendix H for calculations and results.

SECTION 7.0 – REFERENCES

- Florida Department of Transportation (FDOT) Drainage Manual/Handbook (2009)
- FDOT Plans Preparation Manual (2010)
- St. Johns River Water Management District Applicants Handbook for Management and Storage of Surface Waters, Rule 40C-4 F.A.C.
- Orange County Aerials dated 2010
- SCS Soils Data
- FEMA firmettes
- USGS Quadrangle Maps

10



Basin 100

Added Impervious Area - Sta. 514+75 to Sta. 515+90, LT – 0.14 acres

An inlet (S-100) was added at Sta. 514+75 to capture 0.14 acres of impervious area to offset the impervious area added to Basin 1 (0.14 acres).

The additional new impervious area of 0.14 acres, combined with the permitted impervious area of 2.92 acres, totals 3.06 acres and equates to 4.58% of the impervious area within Basin 100. The required treatment volume for Pond 100 increases 4.69% from 0.61 ac-ft (permitted) to 0.64 ac-ft of required volume. The permitted treatment volume provided in Pond 100 is 0.66 ac-ft, which still exceeds the new required amount of 0.64 ac-ft.

No changes to the pond configuration, weir elevation or control elevation are required. The 25yr/24hr maximum discharge increased from 16.23 cfs to 19.01 cfs, but is still less than the allowable discharge of 24.56 cfs.

Basin 200

Added Right Turn Lane – Sta. 539+80 to Sta. 543+50, LT – 0.10 acres Added Left Turn Lane – Sta. 555+80 to Sta. 559+00 - 0.06 acres Added Impervious Area - Sta. 558+00 to Sta. 559+00, LT & RT – 0.28 acres

In addition to the right and left turn lanes, the eastern basin boundary for Basin 200 was shifted from Sta. 558+00 to Sta. 559+00 by removing S-301 and S-302 in order to offset the added impervious area in Basin 300 of 0.21 acres.

The additional new impervious area of 0.44 acres, combined with the permitted impervious area of 8.06 acres, totals 8.50 acres and equates to 5.18% of the impervious area within Basin 200. The required treatment volume for Pond 200 increases 5.08% from 1.68 ac-ft (permitted) to 1.77 ac-ft of required volume. The permitted treatment volume provided in Pond 200 is 2.14 ac-ft, which still exceeds the new required amount of 1.77 ac-ft.

No changes to the pond configuration, weir elevation or control elevation are required. However, due to a change at the pond outfall, the control structure was revised from a weir to a drop structure. The 25yr/24hr maximum discharge decreased from 35.14 cfs to 27.68 cfs and is still less than the allowable discharge of 92.97 cfs.

Basin 300

Added Right Turn Lane – Sta. 571+45 to Sta. 579+00 – 0.21 acres Removed Impervious Area - Sta. 558+00 to Sta 559+00, LT & RT – (0.28 acres)

Basin 300 drains to Pond 1 which was permitted under Permit No. 4-095-27073-2. The western basin boundary for Basin 300 was shifted from Sta. 558+00 to Sta. 559+00 by removing S-301 and S-302 in order to offset the added impervious area in Basin 300 of 0.21 acres. The impervious area originally permitted for Basin 300 has subsequently decreased by 0.07 acres and no modification of Permit No. 4-095-27073-2 is required.

Page 2 of 4

The additional new impervious area is 0.00 acres, which is 0.00% of the impervious area within Basin 300.

Basin 400

Added Impervious Area - Sta. 588+50 to Sta 588+90, LT & RT - 0.09 acres

The western basin boundary for Basin 400 was shifted from Sta. 588+90 to Sta. 588+50 due to a slight profile adjustment.

The additional new impervious area of 0.09 acres, combined with the permitted impervious area of 8.84 acres, totals 8.93 acres and equates to 1.01% of the impervious area within Basin 400. The required treatment volume for Pond 400 increases 1.08% from 1.84 ac-ft (permitted) to 1.86 ac-ft of required volume. The permitted treatment volume provided in Pond 400 is 2.33 ac-ft, which still exceeds the new required amount of 1.86 ac-ft.

No changes to the pond configuration, weir elevation or control elevation are required. The 25yr/24hr maximum discharge increased from 15.07 cfs to 19.03 cfs and is still less than the allowable discharge of 104.44 cfs.

Basin 500A

Added Right Turn Lane – Sta. 626+90 to Sta. 632+80, RT - 0.16 acres Added Right Turn Lane – Sta. 633+00 to Sta. 636+60, LT - 0.10 acres Added Left Turn Lane – Sta. 639+80 to Sta. 643+00 – 0.09 acres Added Left Turn Lane – Sta. 646+80 to Sta. 652+00 – 0.03 acres Added Left Turn Lane – Sta. 653+50 to Sta. 656+50 – 0.08 acres Added Right Turn Lane – Sta. 654+00 to Sta. 660+20, RT - 0.17 acres Added Right Turn Lane – Sta. 661+00 to Sta. 663+50, LT - 0.07 acres Removed Right Turn Lane – Sta. 661+00 to Sta. 662+50, LT - (0.04 acres)

The additional new impervious area of 0.66 acres, combined with the permitted impervious area of 11.90 acres, totals 12.56 acres and equates to 5.25% of the impervious area within Basin 500. The required treatment volume for Pond 500 increases 5.34% from 2.48 ac-ft (permitted) to 2.62 ac-ft of required volume. The permitted treatment volume provided in Pond 500 is 2.67 ac-ft, which still exceeds the new required amount of 2.62 ac-ft.

No changes to the pond configuration, weir elevation or control elevation are required. The 25yr/24hr maximum discharge increased from 57.67 cfs to 57.70 cfs and is still less than the allowable discharge of 104.17 cfs.

Basin 700

Added Impervious Area – Sta. 681+50 to Sta. 681+90, LT & RT – 0.09 acres Added Left Turn Lane – Sta. 681+50 to Sta. 681+90 – 0.01 acres Added Left Turn Lane – Sta. 690+60 to Sta. 694+00 – 0.09 acres Added Left Turn Lane – Sta. 691+75 to Sta. 693+80 – 0.06 acres Added Right Turn Lane – Sta. 692+80 to Sta. 700+00, LT – 0.23 acres Added Left Turn Lane – Sta. 693+80 to Sta. 700+65 – 0.14 acres Added Right Turn Lane – Sta. 701+00 to Sta. 705+00, RT – 0.11 acres Removed Left Turn Lane – Sta. 689+00 to Sta. 691+75 – (0.09 acres)

Page 3 of 4

The western basin boundary for Basin 700 was shifted from Sta. 681+90 to Sta. 681+50 due to a slight profile adjustment.

The additional new impervious area of 0.64 acres, combined with the permitted impervious area of 7.83 acres, totals 8.47 acres and equates to 7.56% of the impervious area within Basin 700. The required treatment volume for Pond 700 increases 7.39% from 1.63 ac-ft (permitted) to 1.76 ac-ft of required volume. The permitted treatment volume provided in Pond 700 is 1.69 ac-ft, which is less than the new required amount of 1.76 ac-ft. Therefore, the weir elevation has been increased from 49.10 feet to 49.20 feet. The new treatment volume provided in Pond 700 is 1.88 ac-ft, which exceeds the new required amount of 1.76 ac-ft.

No changes to the pond configuration or control elevation are required. The 25yr/24hr maximum discharge increased from 46.30 cfs to 48.10 cfs (Pond 700 and Pond 800 combined) and is still less than the allowable discharge of 134.81 cfs (Basin 700 and Basin 800 combined).

Basin 800

Added Left Turn Lane – Sta. 716+20 to Sta. 718+00 – 0.05 acres Added Left Turn Lane – Sta. 728+00 to Sta. 728+50 – 0.02 acres Added Left Turn Lane – Sta. 731+80 to Sta. 732+80 – 0.02 acres Removed Left Turn Lane – Sta. 728+00 to Sta. 728+50 – (0.02 acres)

The additional new impervious area of 0.07 acres, combined with the permitted impervious area of 5.73 acres, totals 5.80 acres and equates to 1.21% of the impervious area within Basin 800. The required treatment volume for Pond 800 increases 1.65% from 1.19 ac-ft (permitted) to 1.21 ac-ft of required volume. The permitted treatment volume provided in Pond 800 is 1.25 ac-ft, which exceeds the new required amount of 1.21 ac-ft.

No changes to the pond configuration, weir elevation or control elevation are required. The 25yr/24hr maximum discharge increased from 46.30 cfs to 48.10 cfs (Pond 700 and Pond 800 combined) and is still less than the allowable discharge of 134.81 cfs (Basin 700 and Basin 800 combined).

Project Summary

The combined additional new impervious area for the project is 2.04 acres, an increase of 4.31% over the permitted impervious area. These changes meet the Modification of Permits requirements under Section 40C-4.331 (1) (b) F.A.C. No additional wetlands are impacted by the addition of turn lanes.

Please find enclosed one set of SR 50 Construction Plans and one set of Drainage Design Documentation (Basin Calculations and ICPR Analysis). In addition, the required permit application fee of \$270.00 for an Individual ERP Letter Modification is enclosed.

If you have any questions or need any additional information for your review, please contact Ms. Theresa (Tracy) Ellison with H.W. Lochner, Inc. at 727-572-7111, extension 8355.

Sincerely

Mannah Hernańdez District Permit Coordinator FDOT District Five Copies: Patrick Muench, Chris Dabson, Jack Box/HWL, permit file

Page 4 of 4

Appendix: I

Excerpt from Bithlo Area Stormwater Management Master Plan



Executive Summary

1.0 Purpose of Study

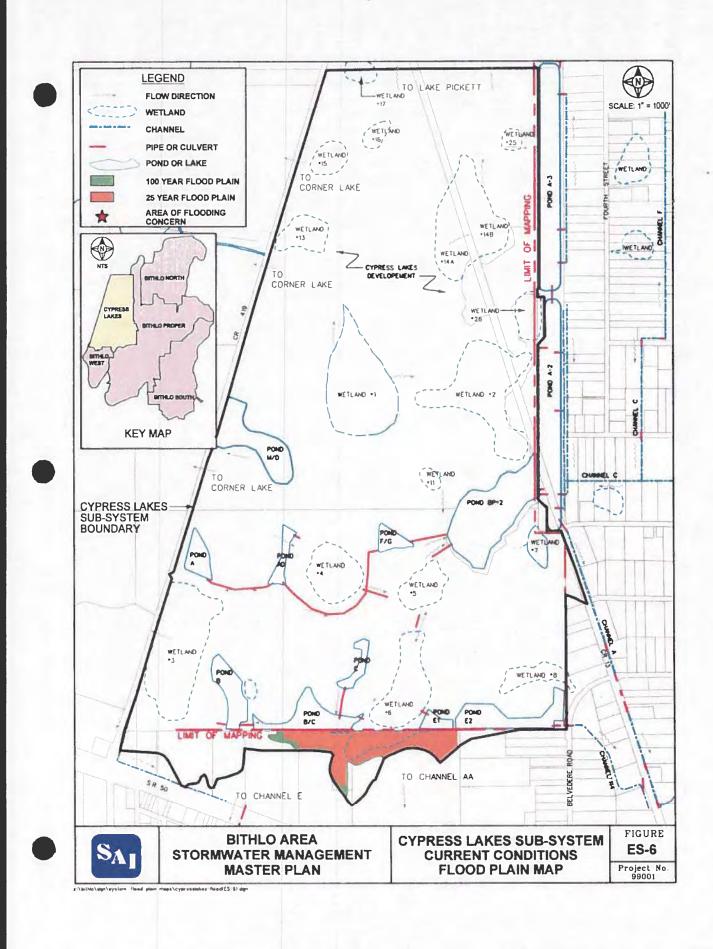
In March 1987, a Stormwater Management Master Plan (Master Plan) was prepared for the Bithlo and Christmas Areas by Ghioto, Singhofen & Associates, Inc (GSA). Since that time, Orange County has implemented numerous elements of the 1987 Master Plan. The purpose of this study is to prepare an update to the 1987 Master Plan. The primary objectives include (1) evaluation of the current conditions with respect to flooding, (2) evaluation of the effectiveness of implementing the remaining elements of the 1987 Master Plan, and (3) development of additional design alternatives, as necessary, to address flooding concerns. As part of this process, the 1987 stormwater model was to be updated from the EXPLC computer model to the Interconnected Channel and Pond Routing (ICPR v2.20) computer model.

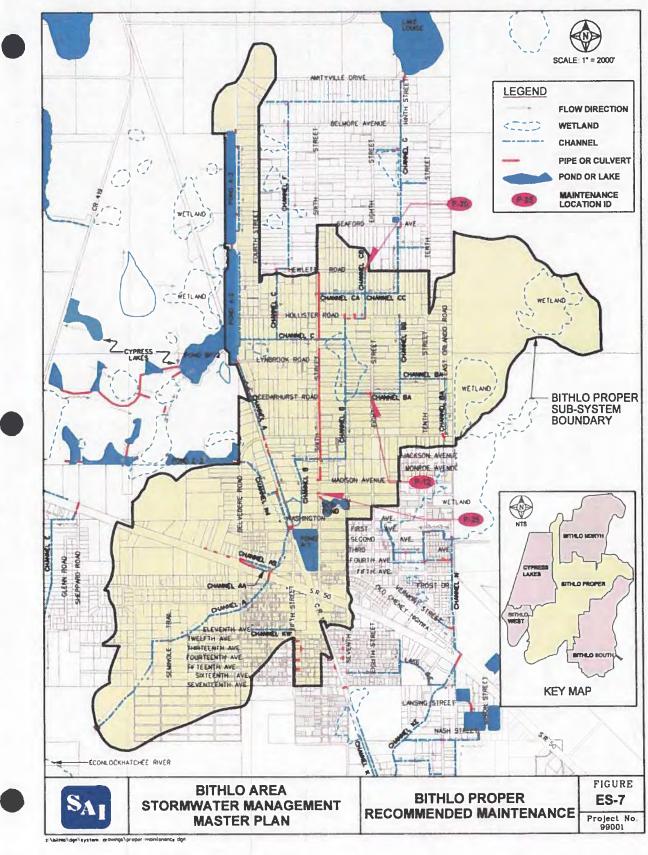
2.0 The Study Area

The study area (Figure ES-1) consists of approximately 4,540 acres and has been segmented into five separate drainage sub-systems for discussion, analysis and design purposes. These subsystems are named Bithlo Proper, Bithlo North, Bithlo West, Bithlo South, and Cypress Lakes. The 1987 GSA study included the first three sub-systems. For this update to the Master Plan, the original Bithlo Proper was subdivided to create Bithlo South and Cypress Lakes was added to account for a new development.

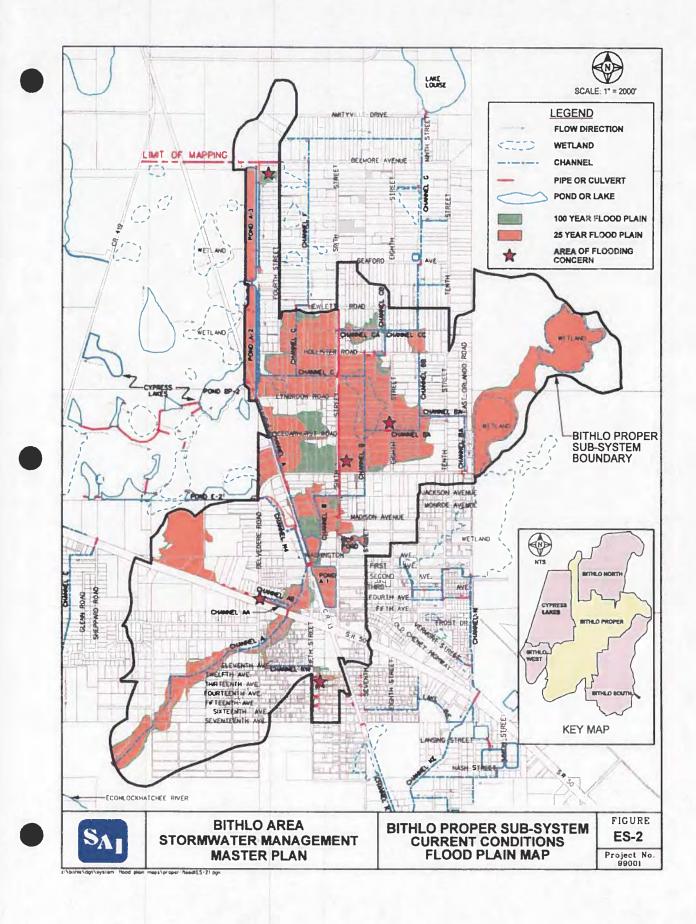
Bithlo Proper – Bithlo Proper is the largest of the five sub-systems, consisting of approximately 1,700 acres. It is generally located in the central portion of the overall study area and drains to the south into the Econlockhatchee (Econ) River. Land use in this system north of State Road (S.R.) 50 is primarily low density residential with commercial areas along the highway. South of S.R. 50, land use is primarily rangeland and upland forest with some low-density residential use. Channel A, primary drainage features in this sub-system, originates in the north central portion of the study area and travels south along County Road (C.R.) 13, crosses under Old Cheney Highway and S.R. 50, and subsequently discharges into the Econ River. The Channel B system, including several lateral channels, provides drainage conveyance for the northeast part of the Bithlo Proper system. Channel B connects to Channel A at C.R. 13 about midway between Belvedere Road and S.R. 50. Hydraulic connections exist between Bithlo Proper, Bithlo North, Bithlo South, and Cypress Lakes, however, these sub-systems are presented separately for discussion purposes. The Cypress Lakes sub-system provides the most significant contribution of off-site drainage to Bithlo Proper. The Cypress Lakes sub-system and its discharge locations are discussed below.







1-3



1-4



Section 3 — Bithlo Proper

This section presents a detailed discussion of drainage conditions in the Bithlo Proper Sub-System (Figure 3.1). The major drainage features within this sub-system are Channels A, N4, B, C, and KW. For discussion purposes, the information is presented for each major drainage feature separately. The following sections present a description of the drainage feature, the results of the existing conditions analysis, the results of incorporating the remaining elements of the 1987 Master Plan, and an evaluation of alternatives to correct predicted flooding problems. As stated previously, all structures and a number of roadways located within the predicted 100year flood plain were surveyed in 2001/2002 by LSTS. All references to structure flooding in this report are based on this survey information.

An inventory of drainage structures and conveyances at major crossings and outfalls in the drainage system is presented in Technical Appendix. The tabulated information includes geometry, construction materials, location, and Orange County Commissioner district for culverts, weirs, and drop structures. A summary of the structure inventory is presented in Table 3.1. This summary table also includes a Location ID for use in referencing the location on the drainage system map, Figure 3.1.

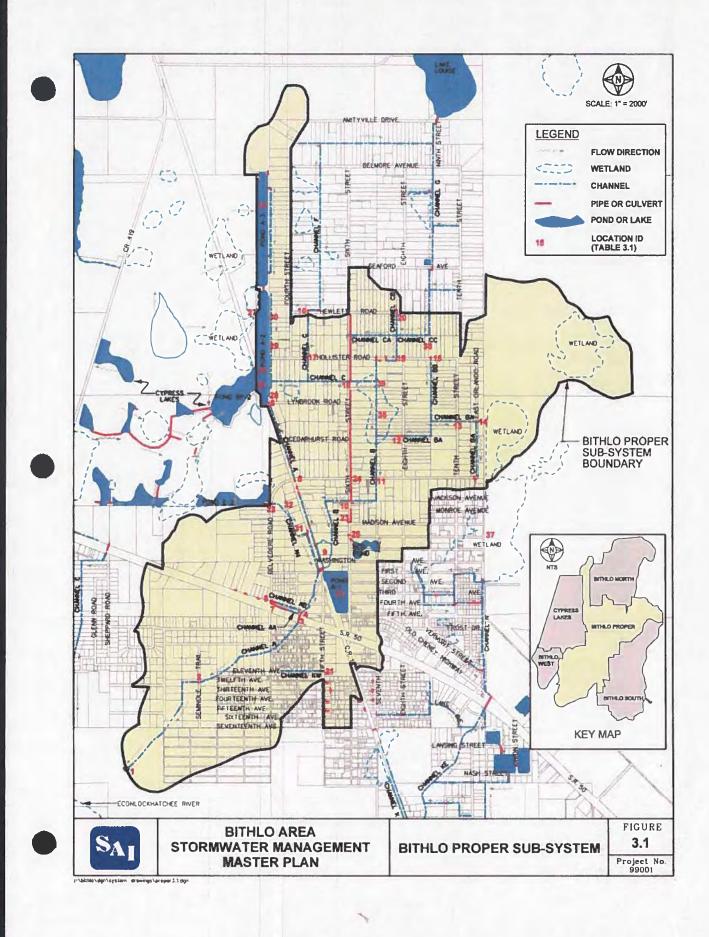
3.1 Channel A Drainage System

The Channel A drainage system includes Channels A, AA, AB, and N4. Channel A originates at the north end of the Bithlo Area west of Fourth Street and conveys stormwater south to the east side of C.R. 13, under Belvedere Road, to a wetland area between C.R. 13 and Sixth Street. The wetland then discharges water southwest under C.R. 13 then under Old Cheney Highway and S.R. 50, then through an extended reach of natural channel and ultimately discharges under a utility easement to the Econ River. Channels AA and AB discharge into Channel A from the east along either side of Old Cheney Highway.

The 1987 Master Plan predicted flooding at Old Cheney Highway, at a portion of C.R. 13 south of Belvedere Road including residential yards along the road, Belvedere Road at C.R. 13, and extensive road and lot flooding east of C.R. 13 between Belvedere Road and Lynbrook Road. This flooding in turn created a backwater effect on Channel C resulting in flooding of that area.

Since 1987, all of the previously recommended Channel A improvements appear to have been implemented. These have included installation of Ponds A-1, A-2, and A-3, culvert additions and replacements, and channel modifications along C.R. 13 between Pond A-2 and Pond A-1. In addition, a revised Channel N4 system was implemented to address the relatively large volume of water received from the northwest region of the study area (currently referred to as Cypress Lakes). The originally recommended Channel N4 system diverted water from the northwest toward the south (away from the upper portion of Channel A) to S.R. 50 and into the lower portion of Channel A. The modified version of Channel N4 that was implemented instead diverts water from this area to the east under Belvedere Road and south along the south side of C.R. 13 to a point where it converges with Channel A.





I-6

3.1.1 Current Conditions Analysis

The results of the current conditions model indicate that the referenced improvements have adequately eliminated the flooding problems along C.R. 13, the west end of Belvedere Road, and road flooding south of Lynbrook Road. Old Cheney Highway, which was previously predicted to overtop during the 10-year and 25-year storm events, is now predicted to only overtop during the 100-year storm. Only one structure along the Channel A System is predicted to flood during the 100-year storm; a garage building located northeast of Pond A-3. The house located on the same lot does not flood.

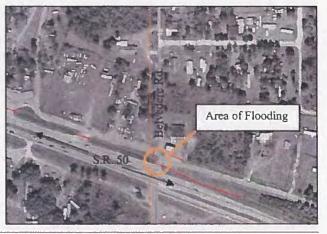


It should be noted that the previously implemented improvements along the northern reach of Channel A will not function as predicted in the 1997 Master Plan. This is primarily due to the following two conditions:

- (1) Pond A-2 receives additional stormwater drainage from the west. The 1987 design elements were developed based on information from the 1984 aerial photogrammetry indicating that the old C.R. 13 served to hydraulically separate stormwater from the west. However, according to Sam Carr of Consul-Tech Engineering, Inc., sections of old C.R. 13 have since been "cut out" allowing stormwater to flow from the west and into Pond A-2. Mr. Carr also indicated that this represented existing conditions prior to implementation of the Cypress Lakes development.
- (2) The area of the constructed Pond A-2 is approximately 2 acres smaller than that specified in 1987. While this contributes to increased stages in the pond, the additional flow from the west has the most significant impact.

While not apparently causing additional flood problems, these conditions result in increased stages in the pond as well as in Channel A along C.R 13 to the south and along Channel C to the east (as compared to the stages predicted in 1987).

Also, based on new information, the Cypress Lakes development is hydraulically connected to a wetland area to the south which subsequently discharges via overland flow to the roadside swale (Channel AA) along the north side of S.R. 50 then to Channel A. The current model indicates that this discharge causes water to overtop Belvedere Road at S.R. 50 for all storm events with the exception of the mean annual event. The flood depth is



Bithlo Stormwater Management Master Plan Update

Singhofen & Associates, Inc.



1-7



		1.2	Annual Event				ear Event				Year Event				Year Event		100-Year Storm Event					
	Node		Cun	rent	Pro	ject	Cur	rent	Pro	Ject	Cur	rent	Project		Cur	rent	Pro	Ject	Cur	rent	Pro	oject
LOC	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
Channel	A										T					10.01		leiej	1.0	10.02		1 leist
1	NA-015	Power Easement, N.	40.2	325	40.2	322	40.5	492	40.5	489	40.7	620	40.7	615	41.5	762	41.5	744	42.8	1027	42.B	1005
2	NA-060	Seminole Trl., W.	48.2	256	48.2	253	48.6	377	48.6	372	48.8	465	48.8	458	49.1	564	49.1	549	49.5	719	49.4	697
2	NA-070	Seminole Trl., E.	48.4	253	48.4	250	49.6	373	49.6	369	50.5	461	50.4	454	50.7	556	50.7	541	50.9	703	50.9	682
3	NA-110	SR 50, N.	57.0	204	57.0	204	58.3	310	58.3	310	59.04	379	59.05	380	59.5	425	59.5	425	60.3	499	60.3	499
4	NA-115	Old Chanay Hwy., N.	57.1	192	57.1	191	58.4	295	58.4	290	59.2	373	59.2	369	60.0	395	60.0	393	61.0	446	61.0	447
	NA-130	CR 13, W.	60.1	182	60.1	182	60.4	280	60.4	280	60.6	345	60.6	345	60.9	386	60.9	387	81.5	446	61.5	447
33	NA-140	Pond A-1	60.3	10	60.3	10	60.8	15	60.8	15	61.1	22	61.1	22	61.4	27	61.4	27	62.0	34	62.0	34
5	NA-220	Beivedere Rd., N.	65.6	58	65.6	58	66.6	80	66.6	80	66.9	81	66.9	81	67.3	83	67.3	83	68.4	91	68.4	91
6	NA-230	Just S. of Pond A-2	67.1	56	67.1	56	87.9	87	67.9	87	68.2	93	68.2	93	68.4	90	68.4	90	68.8	106		106
34	NA-240	Pond A-2	67.6	56	67.6	56	68.7	86	68.7	86	69.2	91	69.2	91	69.6	86					68.8	
35	NA-250	Pond A-3	68.6	11	68.6	11	69.3	29	69.3	29	69.8	34	69.8	34			69.6	86	69.9	74	69.9	74
Channel	AA						00.0	20	00.0	23	09.0	34	09.0	34	70.4	38	70,4	38	71.3	42	71.3	42
7	NAA-020	Belvedere Rd., W.	63.2	12	60.9	14	64.1	14	61.6	22	64.3	22	62.0	25	64.5	31	63.0	35	64.6	52	64.3	53
Channel	AB			-						1				~~			00.0	00	04.0	- 32	04.3	55
8	NAB-030	Belvedere Rd., W.	63.5	9	63.3	20	64.5	14	63.3	20	64.6	20	63.8	20	64.6	24	64.4	22	64.7	31	64.6	31
Channel	B					5.8						1			1	-		-				
9	NB-010	Wetland, E. of CR 13	60.3	142	60.3	142	60.8	206	60.8	206	61.1	249	61.1	249	61.3	270	61.3	271	62.0	296	62.0	297
10	NB-040	Sixth St., E.	64.9	76	64.9	78	65.3	79	65.3	79	65.7	82	65.7	82	66.2	91	66.2	91	66.7	98	66.7	98
11	NB-070	Belvedere Rd., N.	66.6	59	66.6	59	67.3	64	67.3	64	68.2	71	68.2	71	68.8	79	68.8	79	69.3	85	89.3	85
-	NB-080	Channel B/BA confluence	67.5	50	67.5	50	68.0	62	68.0	62	68.6	73	68.6	73	69.0	84	69.0	84	69.4	98	69.4	98
Channel	BA																				00.4	
12	NBA-010	Eighth St., W.	68.3	12	68.3	12	68.8	13	68.8	13	69.0	11	69.0	11	69.1	10	69.1	10	69.4	10	69.4	10
12	NBA-020	Eighth St., E.	68.5	29	68.5	29	69.1	32	69.1	32	69.2	49	69.2	49	69.2	71	69.2	71	69.4	105	69.4	105
13	NBA-040	Tenth St., W.	68.5	16	68.5	16	69.1	23	69.1	23	69.2	24	69.2	24	69.3	25	69.3	25	69.5	26	69.5	26
14	NBA-060	East Orlando Rd., W.	66.2	2	66.2	2	66.3	3	66.3	3	66.4	4	86.4	4	66.4	4	66.4	4	86.5	5	60.5	5

Table 3.2 Maximum Stages and Flows at Selected Locations in the Bithio Proper Sub-System (Current and Project Conditions).



Bithlo Stormwater Management Master Plan Update



6.3 Channel L/M Drainage System

The Channel L/M drainage system (Figure 6.1) includes Channels L and M. Channel L begins at Wellon Avenue and conveys water westward under Rawles Street before discharging into the main leg of Channel KE approximately 1000 feet upstream of C.R. 13. With the exception of limited ponding at Wellon Street, the 1987 GSA study predicted no lot or road flooding associated with this channel. Recommended improvements included cleaning of the channel only.

Channel M originates south of S.R. 50 at an overflow spillway serving as a high water bypass for runoff in the Channel N system. Runoff is conveyed south into Pond M-1 where it is held until elevation 67.5 where it then discharges to Ponds M-2 and M-3 which are equalized by a culvert under Union Street. Stormwater then discharges south under Nash Street, then west under Wellon Street before arriving at its confluence with Channel KE. The 1987 study predicted no flooding concerns in this area. The channel, culvert, and pond improvements constructed in this area are based on recommendations in the 1987 study for a bypass system addressing increased flows from the north (Channel N). As discussed above, the high stage overflow weir was, however, constructed at an elevation that prevents any bypass flow from Channel KE.

6.3.1 Current Conditions Analysis

The results of the current conditions analysis agree with that predicted in the 1987 study. There is no structure or road flooding during any of the five storm events. During the 100-year storm, overland flow may occur across a wooded area where water travels out of bank from Channel KE and into the western reach of Channel M.

Maximum Stages and Flows at selected locations within the Bithlo South Sub-system are presented on **Table 6.2**. An Evaluation of Flood Conditions along the Channel L/M system is presented on **Table 6.5**. Current conditions flood profiles are included for Channel L on Figure 6.9 and Channel M on Figure



6.10. Sheets 9 and 10 present and the current conditions flood plains (25-year and 100-year) and the flood evaluation results for structures, lots, and roads. A flood plain summary for the Bithlo South Sub-system is presented on Figure 6.3.

6.3.2 Evaluation of 1987 Master Plan Remaining Elements

The elements recommended in the 1987 GSA study for Channels L and M have apparently been implemented and are functioning as previously predicted.

6.3.3 Design Alternatives Evaluation – Revisions to the Master Plan

There are currently not flooding concerns in this area.

Singhofen & Associates, Inc.





					Annual Event				ear Event				Year Event				Year Event		100-Year Storm Event				
	T		Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	oject	
LOC	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	
Channel	к		12 23								1								1				
2	NKE-020	C.R. 13, S.	46.4	277	46.4	283	46.8	431	46.8	431	47.0	536	47.0	533	47.1	621	47.1	621	47.34	784	47.35	787	
24	NK-110	Wetland, W. of CR13	59.5	28	59.5	32	59.6	46	59.6	54	59.7	59	59.7	71	59.7	71	59.7	84	59.8	97	59.8	110	
25	NK-130	Wetland, E. of CR13	60.3	5	60.3	5	60.4	10	60.4	10	60.5	14	60.5	14	60.5	18	60.5	18	60.6	43	60.6	24	
Channel	KE												4 200 -							4			
2	NKE-020	C.R. 13, S.	46.4	277	46.4	283	46.8	431	46.8	431	47.0	536	47.0	533	47.1	621	47.1	621	47.34	784	47.35	787	
2	NKE-030	C.R. 13, N.	47.9	244	47.9	247	48.8	375	48.8	366	49.4	465	49.3	449	49.8	537	49.7	523	50.6	668	50.5	659	
	NKE-040	Confluence w/ Chan. L	51.1	236	51.2	239	51.8	361	51.7	353	52.2	447	52.1	432	52.5	516	52.5	502	52.8	642	52.8	633	
	NKE-060	Confluence w/ Chan. M	52.4	213	52.4	215	53.1	327	53.0	317	53.5	404	53.4	386	53.8	467	53.8	449	54.2	575	54.1	565	
3	NKE-080	Lansing St., N.	54.4	169	54.4	173	55.3	256	55.2	250	55.8	311	55.7	299	56.1	353	56.0	340	56.6	410	56.6	409	
	NKE-090	Confluence w/ Chan. N	55.10	165	55.15	169	56.0	250	56.0	243	56.5	304	56.4	291	56.9	346	56.8	330	57.3	399	57.3	397	
4	NKE-120	Fairfield St., W.	57.6	33	56.7	34	58.7	48	57.3	55	59.5	55	57.7	67	60.4	59	58.2	116	60.7	58	58.8	144	
5	NKE-143	14th Ave., N.	58.7	10	58.7	10	59.2	16	59.1	16	59.8	20	59.4	20	60.9	21	59.6	24	61.5	24	60.0	31	
6	NKE-165	8th St., W.	59.2	9	58.0	10	59.7	13	58.3	16	60.2	16	58.5	20	60.5	19	58.8	24	60.9	22	59.5	30	
7	NKE-220	7th St., E.	61.8	8	60.6	8	61.9	12	60.9	13	62.0	15	61.0	17	62.1	17	61.2	20	62.2	20	61.4	25	
7	NKE-225	7th St., W.	63.7	8	1 G. 4	5.21	63.8	11	1 5 1	1.91	63.8	14	1		63.8	15			63.9	18	-	(e.).	
7	NKE-225Z	7th St., W.	e.		61.5	8	intera. I	-	61.9	12			62.1	16	-	÷.	62.3	19	1.0		62.6	24	
	NKE-235	Between 14th & 15th	65.2	7	62.8	8	65.2	10	63.1	17	65.2	12	63.3	18	65.3	14	63.5	19	65.3	16	63.8	24	
8	NKE-245	Between 13th & 14th	65.3	6	63.5	7	65.5	9	63.8	11	65.6	11	64.0	14	65.7	12	64.1	16	65.9	14	64.4	21	
9	NKE-255	Between 12th & 13th	65.4	5	64.2	6	65.6	7	64.5	9	65.8	9	64.7	12	66.0	10	64.9	14	66.3	12	65.2	17	
10	NKE-265	Between 11th & 12th	65.4	4	64.6	4	65.7	7	64.9	7	66.0	8	65.1	9	66.2	9	65.3	10	66.6	11	65.5	17	
Channel	it f							ł		(* . ·]								1					
11	NL-020	Rawles St., E.	52.3	13	52.3	13	52.9	21	52.9	21	53.2	30	53.1	29	53.3	33	53.3	33	54.0	42	54.1	42	
-	NL-030	Wellon St., W.	55.5	11	55.5	11	55.7	20	55.7	20	55.8	24	55.8	23	55.9	27	55.9	27	56.0	37	56.0	38	

Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).

Bithlo Stormwater Management Master Plan Update





		Wellon St., E. Pond M-2 Pond M-3 Pond M-1										Year Event				Year Event				Year Event		
1000			Cur	rent	Pro	ject	Current		Project		Current		Project		Current		Project		Current		Pro	ject
LOC	Node ID	Location	Stage (ft)	Flow (cfs)																		
hannel	M														1							
12	NM-030	Wellon St., E.	53.9	26	53.8	23	54.3	43	54.2	38	54.7	58	54.7	59	55.0	71	55.1	76	55.5	95	55.7	107
26	NM-050	Pond M-2	53.9	8	53.6	5	54.4	14	54.3	12	54.8	19	54.8	24	55.0	23	55.2	35	55.5	30	55.9	53
27	NM-060	Pond M-3	53.9	3	53.6	2	54.4	5	54.3	5	54.8	6	54.8	8	55.0	7	55.2	9	55.5	10	55.9	11
28	NM-070	Pond M-1	57.7	10	57.4	0	57.8	15	57.8	13	57.8	19	57.9	26	57.9	22	58.0	35	57.9	28	58.2	51
22	NM-080	Overflow spillway, S.	57.7	0	57.4	0	57.8	0	57.8	6	57.8	0	57.9	15	57.9	0	58.0	24	57.9	0	58.2	36
hannel	N						1															1.
14	NN-010	S.R. 50, S.	57.3	126	57,4	131	57.9	192	57.8	186	58.2	232	58.1	217	58,4	266	58.2	243	58.7	319	58.5	284
15	NN-015	S.R. 50, N.	61.1	117	61.1	117	61.8	178	61.8	178	62.3	214	62.3	214	62.6	246	62.6	246	63.1	294	63.1	294
15	NN-020	Old Cheney Hwy., N.	61.1	93	61.1	93	61.9	143	61.9	143	62.3	171	62.3	171	62.6	195	62.6	195	63.2	236	63.2	236
17	NN-050	Struct from wetland, N.	61.5	20	61.5	20	62.3	38	62.3	38	62.7	52	62.7	52	63.1	63	63.1	63	63.6	84	63.6	84
18	NN-110	Third Ave., N.	62.0	1	62.0	1	62.9	1	62.9	1	63.4	1	63.4	1	63.9	1	63.9	1	64.5	1	64.5	1
19	NN-150	Third Ave., N.	62.0	10	62.0	10	63.3	15	63.3	15	64.0	21	64.0	21	64.4	25	64.4	25	65.0	33	65.0	33
Channel	NA								1 24													
20	NNA-030	Intersect 4th & 10th, W.	61.9	19	61.9	19	63.2	24	63.2	24	63.8	34	63.8	34	64,1	38	64.1	38	64.5	49	64.5	49
	NNA-070	4th St., N.	61.6	21	61.6	21	62.5	25	62.5	25	63.0	27	63.0	27	63.3	27	63.3	27	63.8	28	63.8	28

Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).

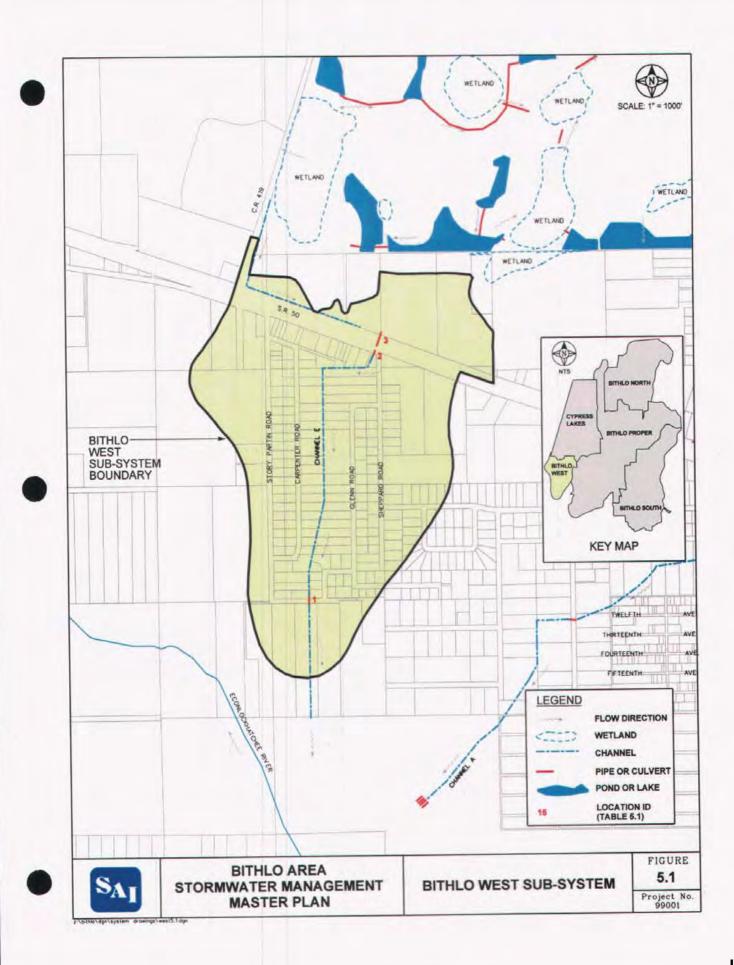
Notes: 1. Flow represents the peak outflow at the referenced node.

2. Results are from the Bithlo Current Conditions model <EXIST> and the Bithlo Project Conditions model <B-PROJ1>.

3. The simulated storms are all 24-hr duration storms.

4. The LOC ID numbers associated with each location are included for the purpose of cross referencing to the system map (refer to Figure 6.1)







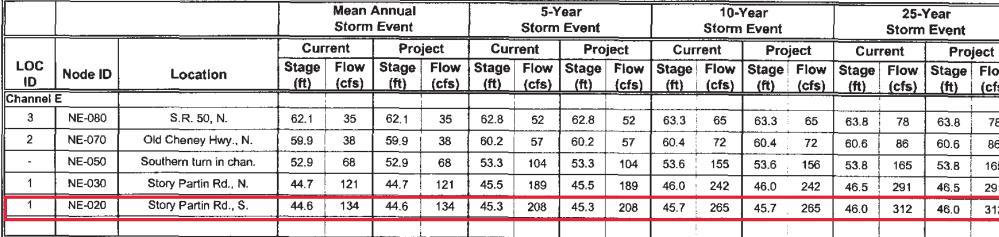


Table 5.2 Maximum Stages and Flows at Selected Locations in the Bithlo West Sub-System (Current and Project Conditions).



			Year Event	
t	Cur	rent	Pro	ject
ow fs}	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
78	65.0	106	65.0	106
6	61.4	132	61.4	131
65	54.2	295	54.2	295
91	47.4	364	47.4	364
12	46.5	398	46.5	398

Bithlo Stormwater Management Master Plan Update

Appendix: J

Excerpt from BJM Associates, Inc. Bithlo – Christmas Master Drainage Plan

4-095-0302 AGM3



in the first to be a second first to

Bound Reports 1720



ORDS

SYSTEM KE

in neuroutin

BITHLO - CHRISTMAS

MASTER DRAINAGE PLAN AUG 30 1996 4-095-0302 AG-M 3

BITHLO DRAINAGE IMPROVEMENTS

Section 26, Township 22 South, Range 32 East Orange County, Florida.

APPLICATION No. 4-095-0302AGM3

MODIFICATION OF PERMIT No. 4-095-0302GM2E Response #2 to

ST. JOHNS RIVER WATER MANAGEMENT DISTRICT

Prepared for

ORANGE COUNTY STORMWATER MANAGEMENT DEPARTMENT 4200 S. JOHN YOUNG PARKWAY ORLANDO, FLORIDA 32839-9205

AUGUST 1996

Engineers • Land Planners • Surveyors 506 Wymore Road • Winter Park, FL 32789 • (407) 645-5566

20.72°a6

BIM ASSOCIATES, INC.

Engineers

Land Planners

Surveyors

August 30, 1996

Ms. Stephanie R. Smith, P.E. Department of Resource Management St. John's River Water Management District 618 E. South Street Orlando, Fl 32801



RE: System KE of Bithlo Christmas Master Drainage Plan Application No. 4-095-0302AGM3

Dear Ms. Smith,

We are submitting five (5) copies of the requested for additional information in response to your comments dated May 2, 1996 as follows:

1. Based on the response to question 2 in the first RAI, the total pond area at elevation 52.8 should be 9.9 acres. A rough measurement of the two ponds indicates that the area is about 6.5 acres. In our meeting on April 16, it was discussed that the design and sizing of the ponds was based on a volume rather than an area requirement. However, to meet the volume requirement, the pond stage had to be increased and this increase may have some adverse impacts to the up- and downstream conditions. Please provide either additional pond area to meet the master plan requirements or provide calculations to show that the volume provided is equivalent to the volume required (based on the master calculations) and that the increase in the pond stage will not have an adverse impact to the permitted master drainage system for the Bithlo area. [40C-4:301(1)(a)4,6; (2)(a)4,6; amended 6/7/93 F.A.C.]

RESPONSE: Attached calculations show the increase in the pond stage of pond M-2 will not have an adverse impact to the permitted master drainage system for the Bithlo area.

2. Since the addition of Pond M-2 East is a new proposal and was not part of the master plan, it seems that the connecting pipes and inlets between the two ponds are part of this proposal. If so, please indicate with shading. [40C-4.301(1)(a)4,6; (2)(a)4,6; amended 6/7/93 F.A.C.]

RESPONSE: The connecting pipes and inlets between two ponds have been indicated with shading (see proposed pond M-2 East plan).

aps.eng.bithlo.app.smith.itr

506 Wymore Road

Winter Park, Fla. 32789

Ph. 407.645.5566_{J-3}

page 2

Staff has reviewed your response to comment 4 and 5 of the RAI dated March 1, 1996. Although no mitigation was needed for the loss of wetland functions associated with the Nash/Union Street roadside ditches, they were identified, accounted for, and evaluated in both permits 4-095-0302GM2 and 12-095-0051GM. Please use a similar approach to account for the RHPZ (wetland and upland component) within the; east side of the Union Street, west side of Avenue D, and north side Nash Street roadside ditches and any proposed encroachments. Please Complete Table One of Section E of the ERP permit application form. [40C-4.301(1)(a)4,6; (2)(a)4,6; amended 6/7/93 F.A.C. and subparagraph Chapter 40C-41(5)(d)(1),(4) and (5), F.A.C.]

RESPONSE: In accordance with a meeting on August 20, 1996 between Bernard J. Martin, P.E. of BJM Associates, Inc. and Elizabeth R. Johnson of S.J.R.W.M.D., the ditches at Union Street, Avenue D, Nash Street were determined to be non-jurisdictional.

If you need further information, please call me at (407) 645-5566.

Bernard J. Martin, P.E.

S/incerely,

3.

dc: Michael J. Drozeck, P.E. Ørange County Stormwater Management Department

DRAINAGE CALCULATIONS

8

100

in star etter

i,

(mail)

DRAINAGE CALCULATIONS POND M-1 & POND M-2 BITHLO

The original design of the Bithlo Master Storm drainage system envisioned the use of existing pond M-1 (4510) and the excavation of a proposed new pond M-2 (4420).

BJM Associates reconfigured the geometry of proposed pond M-2 to avoid damages to existing homes which had been constructed in the interim time period between the study date and the current time.

Although the reconfigured pond provides comparable storage volumes, St. Johns Water Management District wished BJM to evaluate the backwater conditions the reconfigured pond would have on the existing pond M-1.

PROCEDURE

BJM Associates retrieved the original data, input and output files for the relative ponds and the associated reaches.

Attached herein are the original input and output files for the relative ponds and reaches.

BJM then routed the 25 year 24 hours storm event through the designed system to compare with the previous study output.

SUMMARY

There is no discernable difference between the anticipated headwaters in the original design and the proposed design.

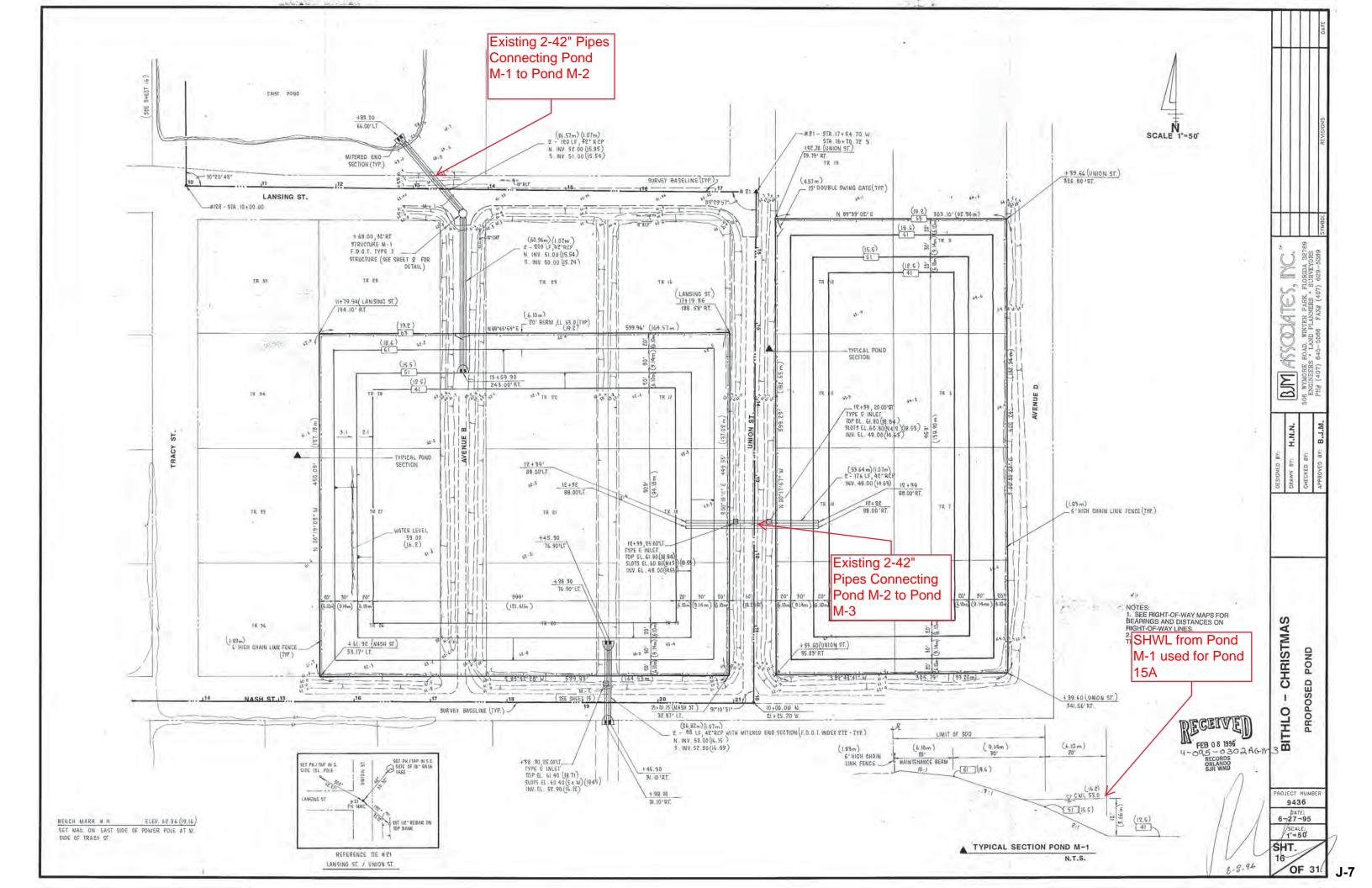
 ORIGINAL DESIGN PROPOSED

 POND M-1 ELEV
 60.5
 59.61

 POND M-2 ELEV
 57.8
 57.98

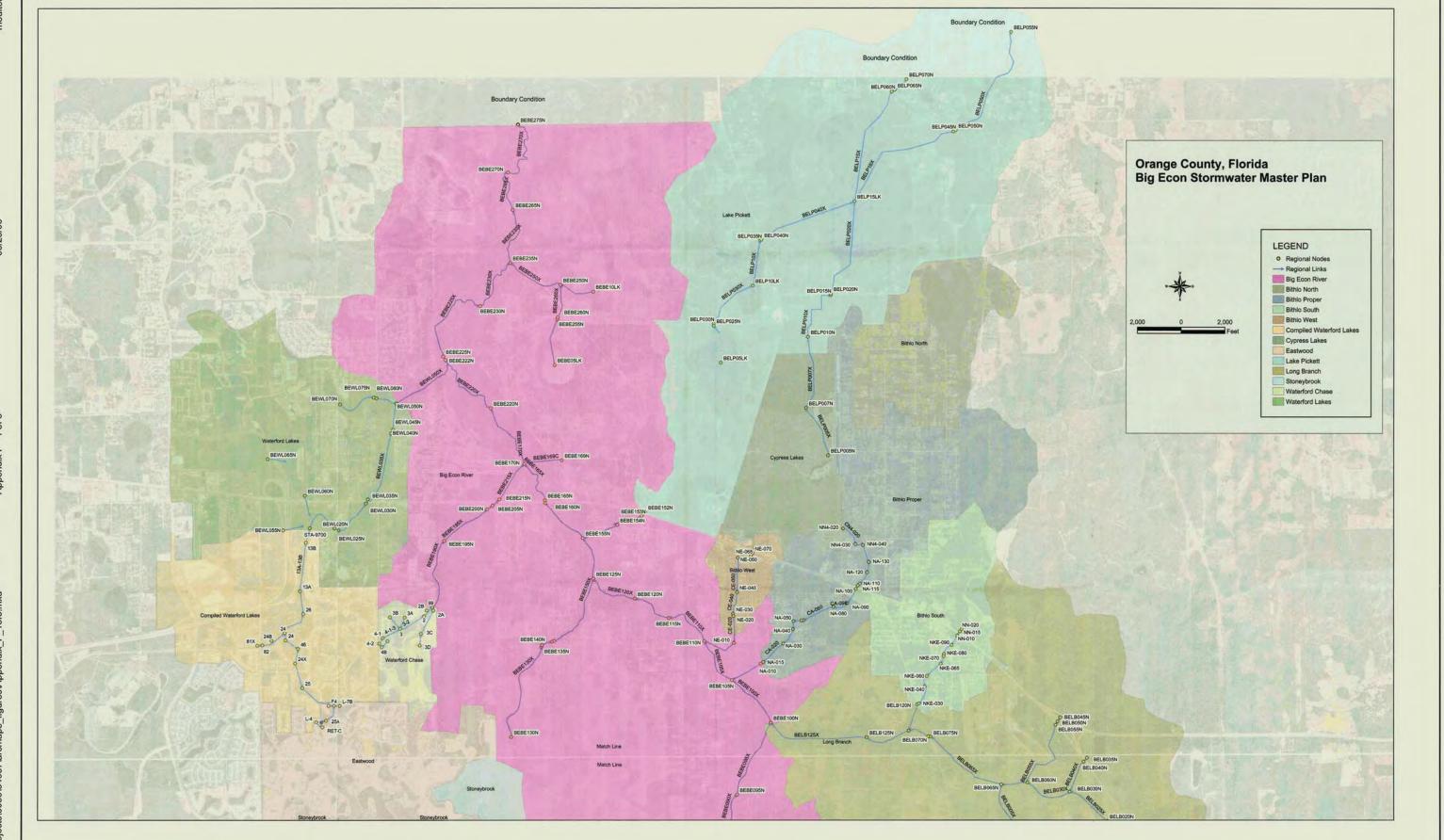
 POND M-2
 130 CFS
 111.18 CFS

 DISCHARGE
 130 CFS
 111.18 CFS



Appendix: K

Excerpt from Big Econ River Basin Stormwater Management Master Plan





Appendix F - 1 of 3 Model Schematic

Table 5-1 Big Econ Stormwater Management Master Plan Orange County, Florida Existing Conditions Results

1.1		1.1	Contraction of the second			Mean Ann				10 Year - 24				25 Year - 24				100 Year - 24		1.1	
del ID	U/S Node	D/S Node	Critical Elevation	Location	U/S Stage ³	D/S Stage	Flooding	Flow ²	U/S Stage	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ⁴	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	Comments
E010C	BEBE010N	the second se	65.8	Wewahoolee Road	62.4	61.8	1-22-21	89	63.9	62.3		170	64.5	62.4		197	65.2	62.5		224	
E011C	BEBE010N	BEBE015N	65.8	Wewahootee Road	62.4	61.8	1002.001	172	63.9	62.3	-	347	64.5	62.4		416	65.2	62.5		498	
E010W	BEBE010N	BEBE015N	65.8	Wewahootee Road - Overflow	62.4	61.8		0	63.9	62.3	~	0	64.5	62.4		0	65.2	62.5		0	
			57.6	Wewanoolee hoad - Overnow	61.8	55.2		393	62.3	56.8	4.1	732	62,4	57.3	-	863	62.5	58.1	0.5	1011	
E015X	BEBE015N	BEBE020N		Destine Prides Faultistant				998	56.8		1		57.3	57.3			the second s				
E020X	BEBE020N	BEBE025N	62.1	Beeline Bridge Equivalent	55.2	55.2	1			56.8		1967				2338	58.1	58.1	1.1	3067	
E020W	BEBE020N	BEBE025N	62,15	Beeline - Overflow	55.2	55.2		0	56.8	56.8	-	0	57.3	57.3	•	0	58.1	58.1		0	
E025X	BEBE025N	BEBE030N	56.6		55.2	53.8		992	56.8	55.8		1931	57.3	56.4		2291	58.1	57,2	0.5	3023	
E030X	BEBE030N	BEBE035N	57.4		53.8	53.6	1 + - + - + - + - + - + - + - +	971	55.8	55.7	1	1861	56.4	56.3		2186	57.2	57.0	· · · · · · · · · · · · · · · · · · ·	2961	
E035X	BEBE035N	BEBE040N	50.2		53.6	52.5	2.3	2300	55.7	54.8	4.6	4418	56.3	55.4	5.2	5169	57.0	56.1	5.9	6007	Hal Scott - flooding not a pro
E040X	BEBE040N	BEBE045N	49.8		52.5	52.1	2.3	2371	54.8	54.2	4.4	4758	55.4	54.8	5.0	5638	56.1	55.5	5.7	6735	Hal Scott - flooding not a pro
	BEBE045N	BEBE050N	48.3		52.1	45.5	1000000	2519	54.2	48.1		5187	54.8	48.8	0.5	6181	55.5	49.8	1.5	7516	Hal Scott - flooding not a pro
E045X			and the second design of the s		45.5	44.7	-	2529	48.1	47.4	0.4	5310	48.8	48.1	1.1	6360	49.8	49.2	2.2	7843	
E050X	BEBE050N	BEBE055N	47		45.5													49.0			Hal Scott - flooding not a pro
E055X	BEBE055N	BEBE060N	43.1			44.6	1.5	2813	47.4	47.2	4.1	5700	48.1	47.9	4.8	6883	49.2		5.9	8642	Hal Scott - flooding not a pro
EOSX	BEBE05LK	BEBE255N	49.2		47.6	46.3		18	48.4	47.5	-	48	48.7	47.8		60	49.2	48.5	-	83	Hal Scott - flooding not a pro
E060X	BEBE060N	BEBE065N	37.4		44.6	44.6	7.2	2967	47.2	47.2	9.8	6150	47.9	47.9	10.5	7360	49.0	49.0	11.6	9211	Hal Scott - flooding not a pro
065C	BEBE065N	BEBE070N	44.7	Powerline Bridge Equivalent	44.6	44.5	1 · · · · · · · · · · · ·	178	47.2	47.2	2.5	186	47.9	47.9	3.2	188	49.0	49.0	4.3	159	Hal Scott - flooding not a pro
065W	BEBE065N	BEBE070N	44.7	Powerline Overflow	44.6	44.5		0	47.2	47.2	2.5	419	47.9	47.9	3.2	492	49.0	49.0	4.3	542	Hal Scott - flooding not a pro
_	BEBE065N		44.7		44.6	44.5		2779	47.2	47.2	2.5	5606	47.9	47.9	3.2	6766	49.0	49.0	4.3	8661	Hal Scott - flooding not a pro
E065X	and the second se				44.5	44.4	1	2900	47.2	47.0	2.2	6086	47.9	47.8	3.0	7302	49.0	48.8	4.0	9145	
2070X	BEBE070N		44.8																		Hal Scott - flooding not a pro
E075X	BEBE075N		43.4		44.4	44.1	0.7	3025	47.0	46.6	3.2	6435	47.8	47.3	3.9	7783	48.8	48.4	5.0	9697	Floodplain of Big Econ
E080X	BEBE080N	BEBE085N	42.9		44.1	43.9	1.0	2957	46.6	46.4	3.5	6390	47.3	47.1	4.2	7736	48.4	48.2	5.3	9579	Floodplain of Big Econ
E085X	BEBE085N	BEBE090N	42.8		43.9	43.6	0.8	2904	46.4	46.1	3.3	6358	47.1	46.8	4.0	7719	48.2	47.9	5.1	9566	Floodplain of Big Econ
090X	BEBE090N		40.6		43.6	43.3	2.7	2862	46.1	45.6	5.0	6437	46.8	46.3	5.7	7852	47.9	47.4	6.8	9855	Floodplain of Blg Econ
095X	BEBE095N	the second se	40.7		43.3	41.1	0.4	2824	45.6	43.7	3.0	6355	46.3	44.6	3.9	7724	47.4	46.1	5.3	9761	Floodplain of Blg Econ
			38.4		41.1	40.5	2.1	2852	43.7	43.1	4.7	6497	44.6	43.9	5.5	7943	46.1	45.5	7.1	10316	Floodplain of Big Econ
100X	BEBE100N	the second se			40.5	39.6	0.3	2879	43.1	43.1	2.9	6567	43.9	43.2	3.9	8029	45.5	44.9	5.6	10462	
105X	BEBE105N	the second s	39.3												9.9				5.0		Floodplain of Big Econ
E10X	BEBE10LK		41.7		45.3	39.7		35	46.3	40.5		93	46.6	40.8		118	47.1	41.6		173	
E110X	BEBE110N	BEBE115N	37.8		39.6	39.1	1.3	2866	42.2	41.7	3.9	6510	43.2	42.8	5.0	7969	44.9	44.6	6.8	10388	Floodplain of Big Econ
115X	BEBE115N	BEBE120N	38		39.1	37.9	1.000	2855	41.7	41.1	3.1	6453	42.8	42.2	4.2	7909	44.6	44.2	6.2	10322	Floodplain of Big Econ
E120X	BEBE120N	BEBE125N	37.9		37.9	37.7	······	2832	41.1	40.9	3.0	6379	42.2	42.0	4.1	7840	44.2	44.0	6.1	10295	Floodplain of Big Econ
E125X	BEBE125N		35.1		37.7	36.6	1.5	2812	40.9	40.3	5.2	6312	42.0	41.5	6.4	7792	44.0	43.6	8.5	10364	Floodplain of Big Econ
	BEBE130N	the second se	61.8		72.4	51.9		117	72.7	53.8	-	233	72.8	54.2		277	72.9	55.2	-	360	i loopian or big Loon
E130X				Suchanas Trail Estantian	51.9	51.5		109	53.8	53.0	0.4	207	54.2	53.8	0.8	209	55.2	55.2	1.8	208	Dephier Area 12 Double
E135C	BEBE135N		53.4	Sunflower Trail Extension			1														Problem Area 12 - Sunflower
E135W	BEBE135N		53.4	Sunflower Trail - Overflow	51.9	51.5	1.0000	0	53.8	53.0	0.4	59	54.2	53.8	0.8	154	55.2	55.2	1.8	301	Problem Area 12 - Sunflower
E145C	BEBE145N	BEBE150N	55.8	Sunflower Trail	51.5	50.5		140	53.0	51.2	-	284	53.8	51,3	· · · · · ·	343	\$5.2	51.5		420	
E145W	BEBE145N	BEBE150N	55.8	Sunflower Trail - Overflow	51.5	50.5		0	53.0	51.2	· · ·	0	53.8	51.3	1. The second	0	55.2	51.5	1.00	0	the second second second
E150X	BEBE150N	BEBE125N	37.9		50.5	37.7	1	139	51.2	40.9	3.0	283	51.3	42.0	4.1	342	51.5	44.0	6.1	420	Floodplain of Big Econ
E152C			62	State Road 50	59.6	57.4		84	60.6	58.3		200	61.1	58.4	•	200	61.9	58.6	-	201	
E152W		BEBE153N	62	State Road 50 - Overllow	59,6	57.4		0	60.6	58.3		0	61.1	58.4		0	61.9	58.6		0	1
		BEBE154N	52	Cidia (1040 00 Orelino)	57.4	50.8	1.1.1.1.1.1	128	58.3	53.6	1.6	171	58.4	53.7	1.7	180	58.6	53.7	1.7	200	Floodplain of Big Econ Tribe
			and the second	Old Chappy Highway	50.8	36.6		84	53.6	40.3	1.0	152	53.7	41.5		153	53.7	43.6		154	Plooplain of Big Econ Triba
		BEBE155N	54	Old Cheney Highway																	
E154W	the second se	BEBE155N	54	Old Cheney - Overflow	50.8	36.6		0	53.6	40.3		19	53.7	41.5		27	53.7	43.6		45	
E155X	BEBE155N	BEBE160N	32.7		36.6	36.5	3.8	2780	40.3	40.1	7.4	6250	41.5	41.3	8.6	7742	43.6	43.3	10.6	10366	Floodplain of Big Econ
E160X	BEBE160N	BEBE165N	44.7	SR 50 Bridge Equivalent	36.5	36,4	1.0	2763	40.1	40.1		6220	41.3	41.3		7716	43.3	43.3	1	10360	
E160W	BEBE160N	BEBE165N	44.6	SR 50 Bridge - Overflow	36.5	36.4	11 · · · · · · · · · · · · · · · · · ·	0	40.1	40.1		0	41.3	41.3	- · · · · · · · · · · · · · · · · · · ·	0	43.3	43.3		0	
E165X	BEBE165N	and the second se	36.5	A CONTRACTOR OF	36.4	35.7	in the second	2752	40.1	39.6	3.1	6194	41.3	40.8	4.3	7693	43.3	42.9	6.4	10356	Floodplain of Big Econ
E169C	BEBE169N		41.3	South Tanner Road	35.7	35.7	1	167	40.3	39.6		291	41.6	40.8	0.3	266	42.9	42.9	1.6	171	Overtopping due largely to tailwa
			41.3	South Tanner - Overflow	35.7	35.7		0	40.3	39.6		0	41.6	40.8	0.3	49	42.9	42.9	1.6	299	
E169W	BEBE169N			Bouth Family - Overnow			11														Overtopping due largely to tailwa
E170X	BEBE170N		31.7		35.7	35.4	3.7	2711	39.6	39,3	7.6	6121	40.8	40.5	8.8	7620	42.9	42.7	11.0	10338	Floodplain of Big Econ
A-4B	4A	4B	65.4	Waterford Chase Parkway - d/s of pond 4A	64.9	64,9		4	65.5	65.3	0.1	9	65.7	65.4	0.3	12	66.1	65.5	0.7	17	Problem Area 10 - Maple Cree
-4-2	48	4-2	66.5	Control structure out of pond 4-B	64.9	63.6	1.0.0	0	65.3	64.3		11	65.4	64.7	· · · · · ·	16	65.5	65.4	· · · · ·	24	
-4-2	4-1	4-2	66.5	Waterford Chase Parkway - d/s wetland 4-2	63.6	63.6		0	64.3	64.3		0	64.6	64.7	•	0	65.2	65.4		0	
1.3	4-1	3	66	Drop structure - Maple Creek Drive	63.6	63.6	1	2	64.3	64.1		8	64.6	64.3		10	65.2	64.6		12	
3-2	3	2	66.5	Oak Chase Drive	63.6	63.6		20	64.1	64.0		42	64.3	64.2		61	64.6	64.4		96	
					63.6	59.4		10	64.0	59.9		16	64.2	60.1		17	64.4	60.4		19	
-99	2	BEBE190N	66	Waterford Chase outfall																	
99A	2	BEBE190N		Waterford Chase outfall	63.6	59.4		2	64.0	59.9		27	64.2	60.1		38	64.4	60.4		48	
99B	2	BEBE190N		Waterford Chase outfall	63.6	59.4		0	64.0	59.9	1.1.4.1.1.1	0	64.2	60.1	-	7	64.4	60.4	100 100 100	30	and the second sec
E190X	BEBE190N	BEBE195N			59.4	54.6	2.1	108	59.9	54.7	2.2	252	60.1	54.8	2.3	311	60.4	54.8	2.3	419	Floodplain of Big Econ Tribu
E195X	BEBE195N	BEBE200N	47.8		54.6	46.5	1 × 1	169	54.7	47.8	0.0	301	54.8	48.3	0.5	370	54.8	49.3	1.5	496	Floodplain of Big Econ Tribu
		BEBE205N		Old Cheney Highway Bridge Equivalent	46.5	44.7		258	47.8	45.2		513	48.3	45.7		621	49.3	47.5		817	
				Old Cheney - Overflow	46.5	44.7		0	47.8	45.2		0	48.3	45.7		0	49.3	47.5		0	
	BEBE200N																				
		BEBE215N		SR 50	44.7	44.6		353	45.2	45.0		512	45.7	45.4		621	47.5	47.1		807	
E210W	BEBE205N	BEBE215N		SR 50 - Overflow	44.7	44.6		0	45.2	45.0		0	45.7	45.4		0	47.5	47.1		0	
E215X	BEBE215N	BEBE170N	36.5		44.6	35.7	11 N 19	403	45.0	39.6	3.1	512	45.4	40.8	4.3	621	47.1	42.9	6.4	805	Floodplain of Big Econ Tribu
E220X		BEBE222N			35.4	34.8	0.2	2676	39.3	38.9	4.3	6051	40.5	40.1	5.5	7568	42.7	42.3	7.7	10318	Floodplain of Big Econ
		BEBE225N		Lake Pickett Bridge Equivalent	34.8	34.8		2724	38.9	38.9	-	6137	40.1	40.1	-	7792	42.3	42.3		10408	interapidin of big 2001
BE222X	DEDEZZZN	I DEDE220N				the second s									-	0	42.3		0.9		Elevelate - Chinese
E222W		BEBE225N		Lake Pickett - Overflow	34.8	34.8	15.00	0	38.9	38.9	1 N. 1	0	40.1	40.1	-			42,3		194	Floodplain of Big Econ
	I DECEMBER	BEBE230N	38.3	the second	34.8	32.5	1	2723	38.9	35.9	· · · · · · · · · · · · · · · · · · ·	6135	40.1	37.6		7700	42.3	40.5	2.2	10601	Floodplain of Big Econ
E225X		BEBE235N			32.5	32.2	1 - 1 - 1	2719	35.9	35.6		6129	37.6	37.3		7696	40.5	40.3		10600	

Notes: 1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels. 2) Flow taken from Link Maximum Conditions Report (cfs) 3) Stages taken from Node Maximum Conditions Report (It NGVD)

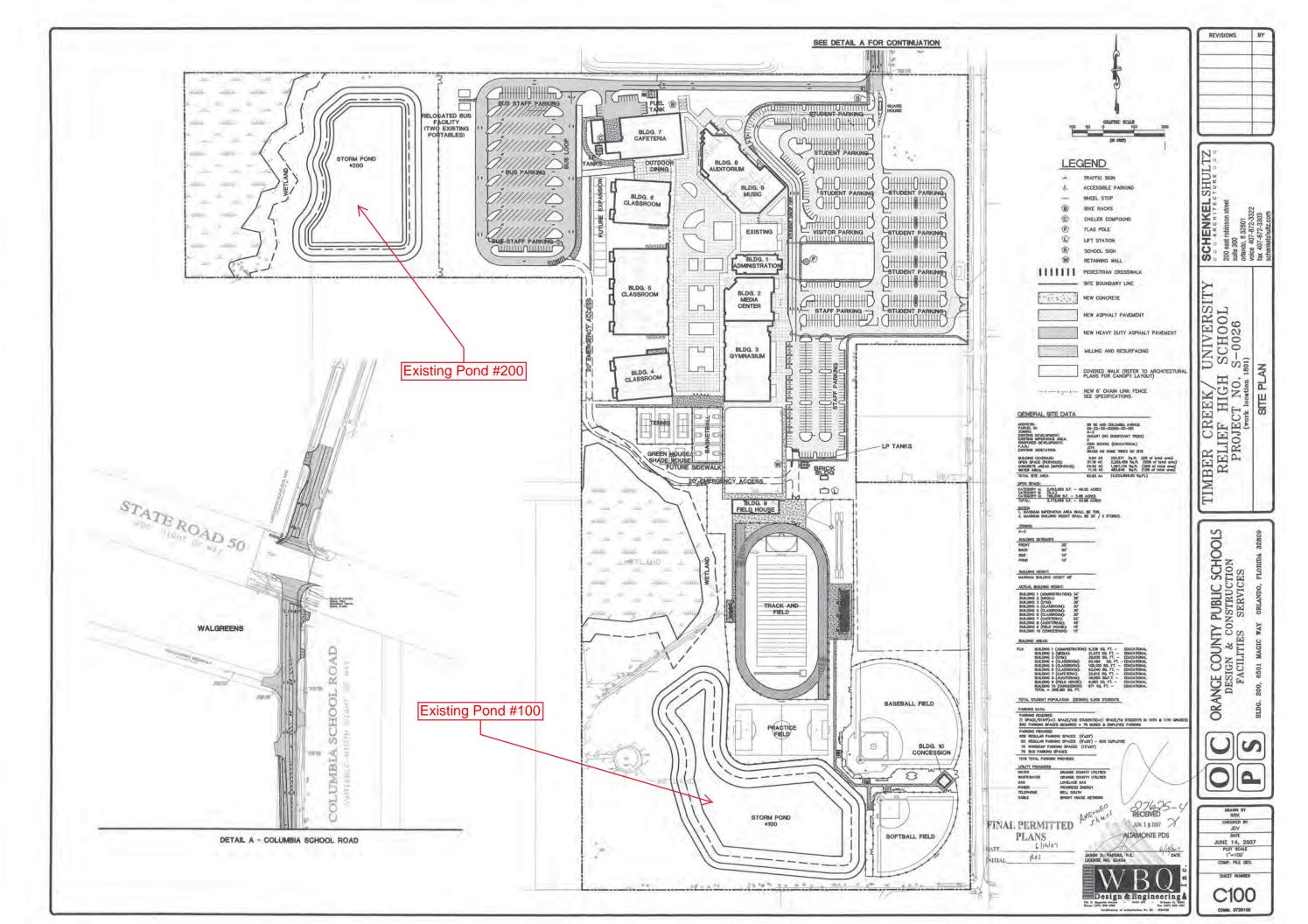
Table 5-1 Big Econ Stormwater Management Master Plan Orange County, Florida Existing Conditions Results

	1.000	A STATE OF THE				Mean Ann	ual		1	10 Year - 24 Hour			1.000	25 Year - 24	Hour	1.10		100 Year - 24	Hour		
lodel ID	U/S Node	D/S Node	Critical Elevation	Location	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage	Flooding	Flow ²	U/S Stage ⁴	D/S Stage	Flooding	Flow ²	U/S Stage	D/S Stage ³	Flooding	Flow ²	Comments
CH-4B	CH-4A	CH-4B	51		47.7	47.0	100 B 11	816	49.0	48.2	100.000	1769	49.9	49.3	12.12.101	2117	50.0	49.1		2778	From Avalon Park FEMA floodplain st
CH-4C	CH-4B	CH-5	49		47.0	46.0	1	815	48.2	47.1	1.20-01	1768	49.3	48.8	1.1.2.4.2.1	2116	49.1	48.8	-	2779	From Avalon Park FEMA floodplain st
CH-5	CH-5	CH-6	50		46.0	44.4	-	820	47.1	47.0	1.00	1775	48.8	47.8		2114	48.8	48.8		2791	From Avalon Park FEMA floodplain st
CH-6	CH-6	CH-7	50		44.4	44.4		816	47.0	47.0	1 2 4 4 4 1	1736	47.8	47.8		2047	48.8	48.8		2671	From Avalon Park FEMA floodplain st
CH-7	CH-7	BEBE075N	44.8		44.4	44.4		784	47.0	47.0	2.2	1617	47.8	47.8	3.0	1886	48.8	48.8	4.0	2429	From Avalon Park FEMA floodplain stu
CONS5-W	BESB050N	C1	78	Weir flow to Alafaya Trail Culverts	76.2	74.7		82	76.4	75.4	-	196	76.5	75.7	0.0	243	76.6	76.1	4.0	326	FIOR AVAION FAIR FEMA ROOUDIAIN ST
	and the second second second	BETCO20N	55.4	Wein now to Malaya Than Barrons	55.6	53.9		498	56.2	55.9	0.5	989	56.7	56.5	1.1	1161	57.1	57.1			Photoble (T. L. On L
BETC005X	BETCOOSN				73.0	64.8		_	73.6	65.6			73.8						1.7	1866	Floodplain of Turkey Creek
BETCO10X	BETC010N	BETC015N	62.6				2.2	1828			3.0	2762		65.9	3.3	3132	74.1	66.4	3.8	3864	Floodplain of Turkey Creek
BETC015X	BETC015N	BETC020N	48.8		64.8	53.9	5.1	802	65.6	55.9	7.1	1546	65.9	56.5	7.7	1816	66.4	57.1	8.3	2339	Floodplain of Turkey Creek
BETC020X	BETC020N	BEBE035N	57.4		53.9	53.6		1047	55.9	55.7		2018	56.5	56.3	-	2335	57.1	57.0		2505	
BEWF005X	BEWF005N	BEWF010N	65.1	the first state of the state of	65.5	65.4	0.3	448	66.7	66.6	1.5	771	67.0	66.8	1.7	912	67.4	67.2	2.1	1160	Floodplain of Wedgefield Canal
BEWF010P	BEWF010N	BEWF015N	65.3	Culvert Riser in Wedgefield Canal	65.4	61.0	0.1	408	66.6	63.5	1.3	431	66.8	63.7	1.5	433	67.2	64.1	1.9	435	Floodplain of Wedgefield Canal
EWF010W	BEWF010N	BEWF015N	65.3		65.4	61.0	0.1	13	66.6	63.5	1.3	461	66.8	63.7	1.5	603	67.2	64.1	1.9	851	Floodplain of Wedgefield Canal
BEWF015X	BEWF015N	BEWF020N	61,1		61.0	61.0	1990 - 19900 - 19900 - 19900 - 19900 - 1990 - 1990 - 1990 - 1990 - 1990 - 1990	667	63.5	63,5	2.4	771	63.7	63.7	2.6	912	64.1	64.1	3.0	1160	Floodplain of Wedgefield Canal
EWF020P	BEWF020N	BEWF025N	62.3	Culvert Riser in Wedgefield Canal	61.0	57.4	C 4 1	401	63.5	59.0	1,2	482	63.7	59.2	1.4	488	64.1	59.6	1.8	494	Floodplain of Wedgefield Canal
EWF020W	BEWF020N	BEWF025N	62.3	The second second second second second	61.0	57.4		0	63.5	59.0	1.2	397	63.7	59.2	1.4	539	64.1	59.6	1.8	784	Floodplain of Wedgefield Canal
BEWF025X	BEWF025N	BEWF030N	57.8		57.4	57.4		379	59.0	59.0	1.2	764	59.2	59.2	1.4	909	59.6	59.6	1.8	1155	Floodplain of Wedgefield Canal
BEWF030P	BEWF030N	BEWF035N	57.5	Culvert Riser in Wedgefield Canal	57.4	54.6		348	59.0	57.9	1.5	413	59.2	58.1	1.7	421	59.6	58.6	2.1	430	Floodplain of Wedgefield Canal
	BEWF030N	BEWF035N	57.5	Carter Theor in Trougenois Cartai	57.4	54.6		0	59.0	57.9	1.5	571	59.2	58.1	1.7	720	59.6	58.6	2.1	974	
EWF030W		BEWF040N	54.8	the second s	54.6	54.6		348	57.9	57.9	3.1	761	58.1	58.1	3.3	906	58.6	58.6	3.8		Floodplain of Wedgefield Canal
EWF035X	BEWF035N	the second se	the second se	Culvert Riser in Wedgefield Canal	54.6	52.1		340	57.9	54.2	1.1	465	58.1	54.8	1.3	482	58.6			1153	Floodplain of Wedgefield Canal
BEWF040P		BEWF045N	56.8	ouvert meet in wedgeneid oanal	the second s				57.9									55.5	1.8	501	Floodplain of Wedgefield Canal
EWF040W	BEWF040N	BEWF045N	56.8		54.6	52.1		0		54.2	1.1	324	58.1	54.8	1.3	477	58.6	55.5	1.8	747	Floodplain of Wedgefield Canal
BEWF045X	BEWF045N	BEBE045N	54.6		52.1	52.1		322	54.2	54.2		717	54.8	54.8	0.2	858	55.5	55.5	0.9	1098	Floodplain of Wedgefield Canal
BEWF050X	BEWF050N	BEWF055N	55		65.3	51.9	-	414	66.7	52,7		809	67.1	52.8		1010	67.5	52.7	· · · · ·	1501	
EWF055X	BEWF055N	BEBE050N	48.3		51.9	45.5	· · · · · · · · · · · ·	668	52.7	48.1		1387	52.8	48.8	0.5	1624	52.7	49.8	1.5	2022	Floodplain of Wedgefield Canal
EWF060X	BEWF060N	BEWF065N	63.7		60.9	60.3		379	63.4	63.1	6	510	64.2	64.0	0.3	546	65.5	65.3	1.6	651	Floodplain of Wedgefield Canal
EWF065P	BEWF065N	BEWF070N	64.9	Culvert Riser in Wedgefield Canal	60.3	58.0		379	63.1	59.7	- 1 (A. 1	505	64.0	60.3	1-1-1	536	65.3	61.1	0.4	569	Floodplain of Wedgefield Canal
EWF065W	and the second data was not second data	BEWF070N	64.9		60.3	58.0		0	63.1	59.7	*	0	64.0	60.3		0	65.3	61.1	0.4	78	Floodplain of Wedgefield Canal
EWF070X	BEWF070N	BEWF075N	60.3	the second se	58.0	58.0	-	727	59.7	59.7		711	60.3	60.3	1	729	61.1	61.1	0.8	713	Floodplain of Wedgefield Canal
EWF075P	BEWF075N	BEWF080N	60.7	Culvert Riser in Wedgefield Canal	58.0	56.2		378	59.7	56.5		502	60.3	56.6		533	61.1	56.9	0.4	570	
			60.7	Convert miser in treageneric Canal	58.0	56.2		0	59.7	56.5		0	60.3	56.6		0	61.1				Floodplain of Wedgefield Canal
EWF075W	BEWF075N	BEWFOBON									-				0.5			56.9	0.4	74	Floodplain of Wedgefield Canal
BEWF080X	BEWF080N	BEWF085N	56		56.2	56.1	0.1	378	56.5	56.4	0,4	502	56.6	56.5	0.5	532	56.9	56.7	0.7	643	Floodplain of Wedgefield Canal
BEWF085P	the second se	BEWF090N	55.4	Culvert Riser in Wedgefield Canal	56.1	49.2	0.7	210	56.4	50.7	1.0	215	56.5	51.8	1.1	216	56.7	53.5	1.3	216	Floodplain of Wedgefield Canal
BEWF085W	BEWF085N	BEWF090N	55.4		56.1	49.2	0.7	168	56.4	50.7	1.0	286	56.5	51.8	1.1	332	56.7	53.5	1.3	480	Floodplain of Wedgefield Canal
BEWF090X	BEWF090N	BEWF095N	52.6		49.2	48.6		378	50,7	50.3		500	51.8	51.5	a to define the	530	53.5	53.4	0.8	643	Floodplain of Wedgefield Canal
BEWF095P	BEWF095N	BEWF100N	53	Culvert Riser in Wedgefield Canal	48.6	44.6		378	50.3	47.2		497	51.5	47.9		528	53.4	49.0	0.4	591	Floodplain of Wedgefield Canal
BEWF095W	BEWF095N	BEWF100N	53		48.6	44.6	1. 1.	0	50.3	47.2		0	51.5	47,9	1	0	53.4	49.0	0.4	60	Floodplain of Wedgefield Canal
BEWF100X	BEWF100N	BEBE060N	43.1		44,6	44.6	1.5	378	47.2	47.2	4.1	497	47.9	47.9	4.8	528	49.0	49.0	5.9	642	Floodplain of Wedgefield Canal
BEWF105X	BEWF105N	BEWF110N	69.3	and the second sec	63.3	61.7		53	64.1	62.2		155	64.4	62.3		167	65.0	62.4		194	ricoopiant of theogeneia canal
BEWF110P		BEWF115N	64.6	Culvert Riser in Wedgefield Canal	61,7	58.4	-	53	62.2	59.1	-	155	62.3	59.2		167	62.4	59.3		194	
	BEWF110N	BEWF115N	64.6	Barron moor in thoughing band	61.7	58.4		0	62.2	59.1		0	62.3	59.2		0	62.4	59.3	-	0	
BEWF110W					58.4	58.4		53	59.1	58.9			59.2	58.9							
BEWF115X	BEWF115N	BEWF120N	61.5					_				155				167	59.3	59.0	7	194	
BEWF120P	BEWF120N	BEWF125N	60.5	Culvert Riser in Wedgefield Canal	58.4	53.8		53	58.9	54.4		155	58.9	54.4		167	59.0	54.6		194	
BEWF120W	BEWF120N	BEWF125N	60.5	and the second se	58.4	53.8		0	58.9	54.4	- <u>-</u>	0	58.9	54.4	- 21	0	59.0	54.6	1	0	
BEWF125X	BEWF125N	BEWF130N	56.4		53.8	53.8		221	54.4	54.3		246	54.4	54.4		249	54.6	54.5	•	250	
BEWF130P	BEWF130N	BEWF135N	54.9	Culvert Riser in Wedgefield Canal	53.8	50.0	-	53	54.3	50.6	1 - A - 1	155	54.4	50.7		167	54.5	52,4	· · ·	194	
BEWF130W	BEWF130N	BEWF135N	54.9		53.8	50.0		0	54.3	50.6	10.001	0	54.4	50.7	1. In Taylor 1	0	54.5	52.4	÷	0	
BEWF135X	BEWF135N	BEWF140N	57		50.0	50.0		53	50.6	50.6	•	405	50.7	50,7		426	52.4	52.4		421	
BEWF140P			53.7	Culvert Riser in Wedgefield Canal	50.0	46.5		52	50.6	48.3	11-2	155	50.7	48.8		166	52.4	50.2		194	
	BEWF140N		53.7	the second se	50.0	46.5		0	50.6	48.3		0	50.7	48.8	1	0	52.4	50.2		0	
	BEWF145N		53.3		46.5	46.4	-	52	48.3	48.3		808	48.8	48.8		808	50.2	50.2		799	
	BEWF145N		50.2	Culvert Riser in Wedgefield Canal	46.4	43.8		52	48.3	46.9		153	48.8	47.1		165	50.2	48.0		199	
		the second se	50.2	Ourent hister in Wougenoid Callal	46.4	43.8		0	48.3	46.9			48.8	47.1				48.0			
	V BEWF150N							_				0				0	50.2			0	
	BEWF155N		49		43,8	43.8		52	46.9	46.9	-	153	47.1	47.1		164	48.0	47.9	1	191	A state of the second state of the second
	BEWF160N	BEWF165N	46.6	Culvert Riser in Wedgefield Canal	43.8	43.6	1	52	46.9	46.1	0.3	149	47.1	46.8	0.5	149	47.9	47.9	1.3	129	Floodplain of Wedgefield Canal
BEWF160W	BEWF160N	BEWF165N	46.6	and the second	43.8	43.6		0	46.9	46.1	0.3	37	47.1	46,8	0.5	92	47.9	47.9	1.3	172	Floodplain of Wedgefield Canal
BEWF165X	BEWF165N	BEBE090N	48.9		43.6	43.6	· · ·	52	46.1	46.1	1.11.1	153	46.8	46.8		164	47.9	47.9	1. 1.	190	Floodplain of Wedgefield Canal
CULV-2	81X	82	74	Woodbury Road	69.9	69.3		170	71.2	69.9	1 - A.C.	350	71.6	70.1		416	72.6	70.6		526	general output
CHANL-5		24	65	the second se	69.3	62.8		171	69.9	63.6		352	70.1	63.8		416	70.6	63.9		526	
CHANL-6		26	65		62.8	59.7		200	63.6	61.2	1	414	63.8	61.6		467	63.9	62.3		545	
			60		59.7	55.4		268	61.2	55.7	1.2	560	61.6	55.9	1.6						Eleadalsia et bio e
CULV-10		13A						_								656	62.3	56.2	2.3	795	Floodplain of Big Econ Tributary
13A-13B		13B	55		55.4	53.7	0.4	63	55.7	55.0	0.7	72	55.9	55.3	0.9	74	56.2	55.8	1.2	76	Floodplain of Big Econ Tributary
B13A-13B		13B	55		55.4	53.7	0.5	240	55.7	55.0	0.5	570	55.9	55.3	0.5	675	56.2	55.8	0.5	834	Floodplain of Big Econ Tributary
CHN-12-0	13B	STA-9700	57		53.7	52.0	1 - A	342	55.0	53.2	1	873	55.3	53.3	1	1007	55.8	53.7		1312	
BEWL015X	(STA-9700	BEWL020N	49	and the second second second	52.0	50.1	1.1	339	53.2	50.4	1.4	873	53.3	51.1	2.1	1013	53.7	52.1	3.1	1322	Floodolain of Big Econ Tributary
	BEWL020N			Bridgeway Blvd - Bridge Equivalent	50.1	50.1		531		50.3	and the second	1136		51.0		1325		52.0	-	1690	The second of the court inditially
				Bridgeway Blvd Overflow	50.1	50.1		0		50.3	in the last t			51.0							
	V BEWL020N			Bridgeway bive Overnow								0	51.1			0	52.1	52.0	-	0	P1 11
	K BEWL025N				50.1	46.4		531	50.3	49.5	1.7	1136	51.0	50.2	2.4	1324	52.0	51.3	3.5	1695	Floodplain of Big Econ Tributary
		BEWL035N	54.4	SR 50	46 4	144	1	612	40.5	45.0		1954	50.2	45.1		1 1549	513	45.4		2000	

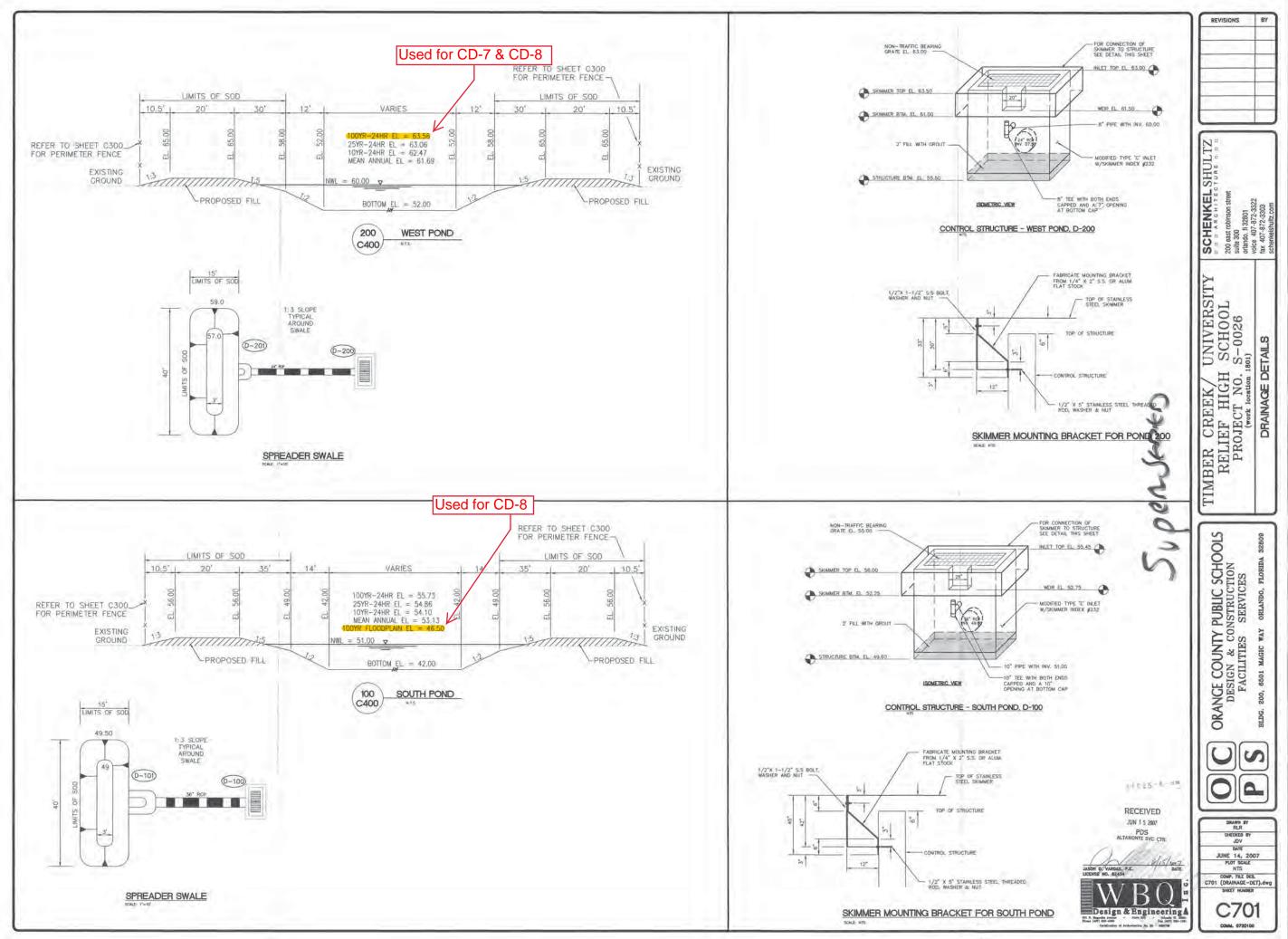
Notes: 1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels. 2) Flow taken from Link Maximum Conditions Report (cfs) 3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Appendix: L

Excerpt from Orange County Public Schools Timber Creek High School Construction Plans



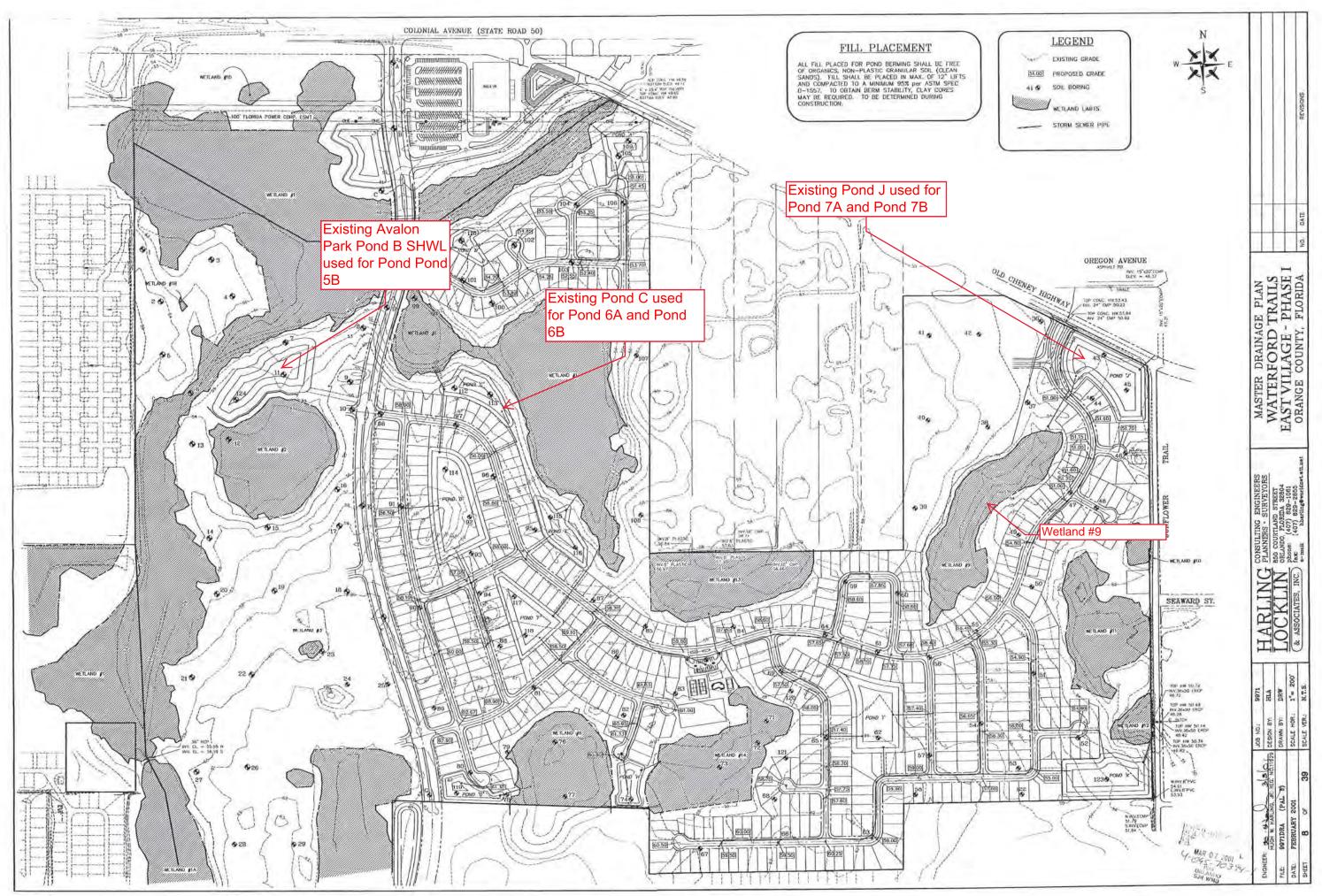
L-1

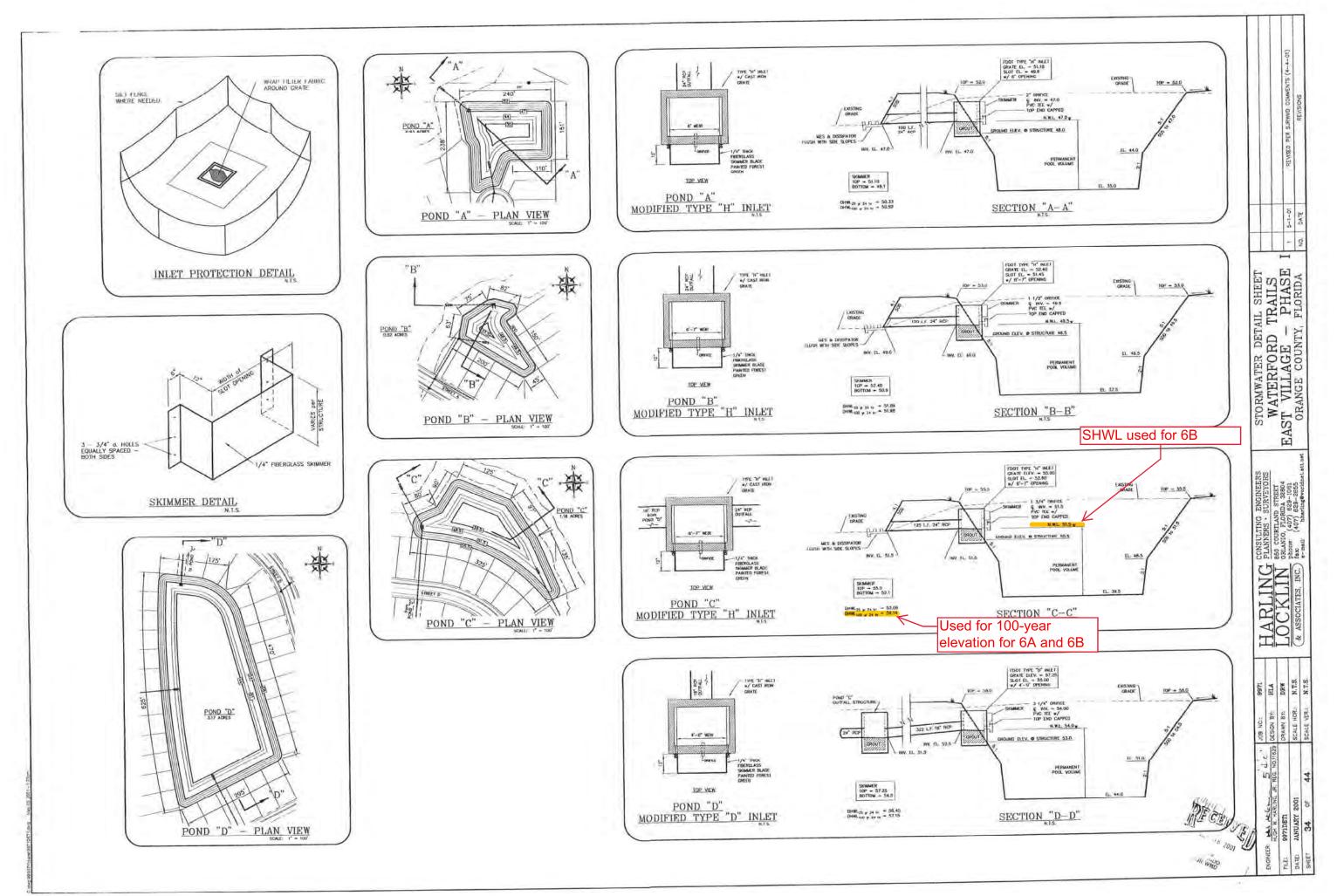


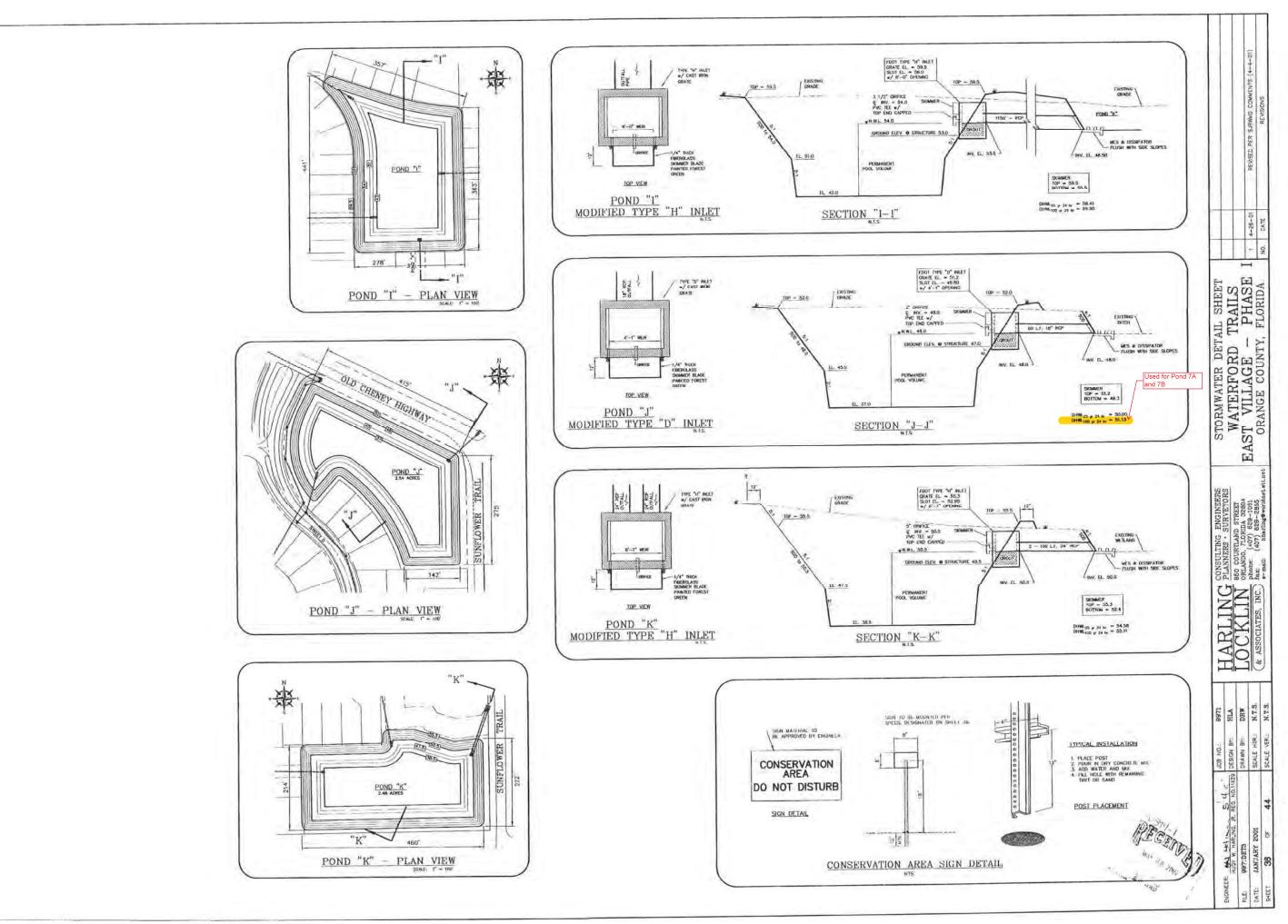
L-2

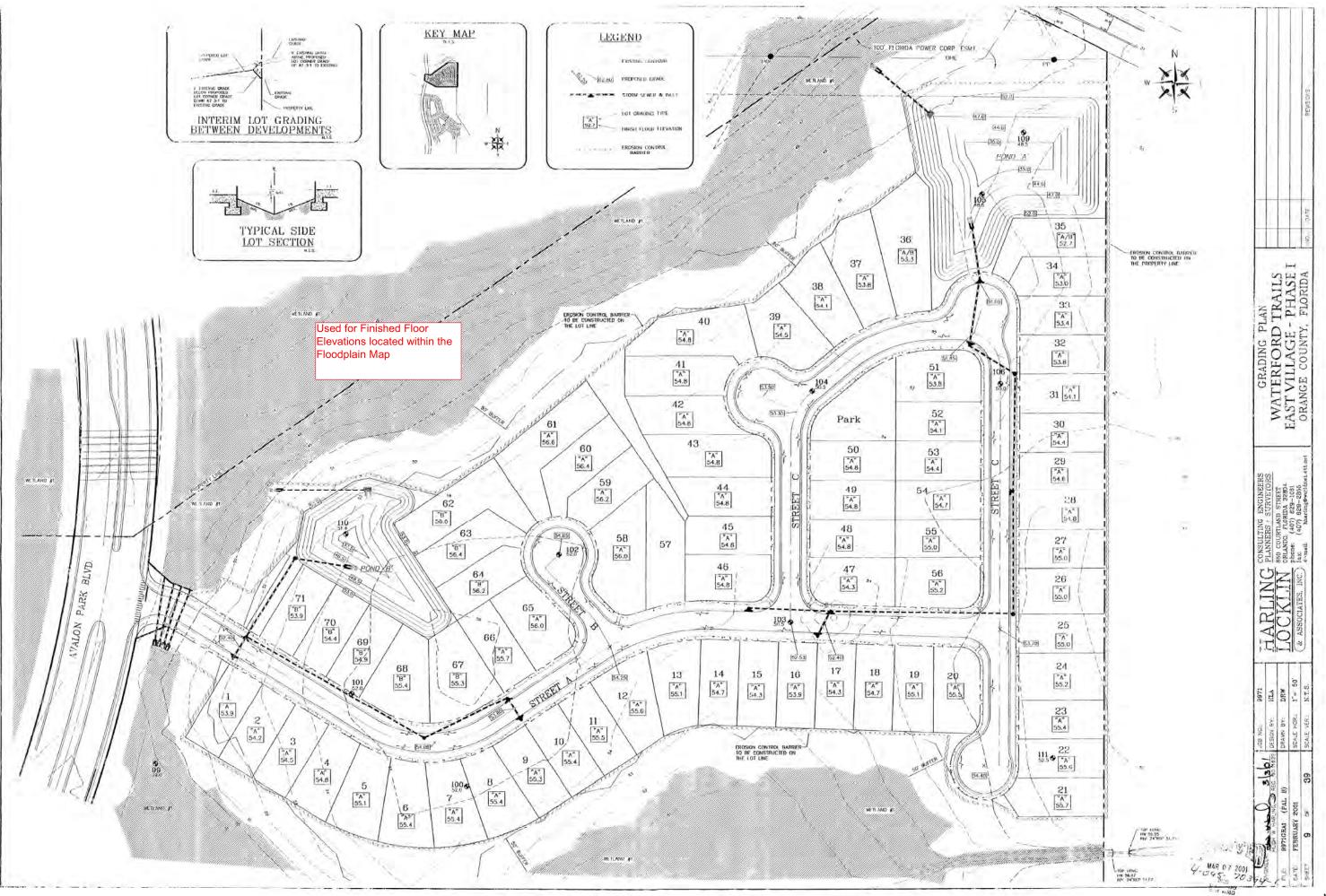
Appendix: M

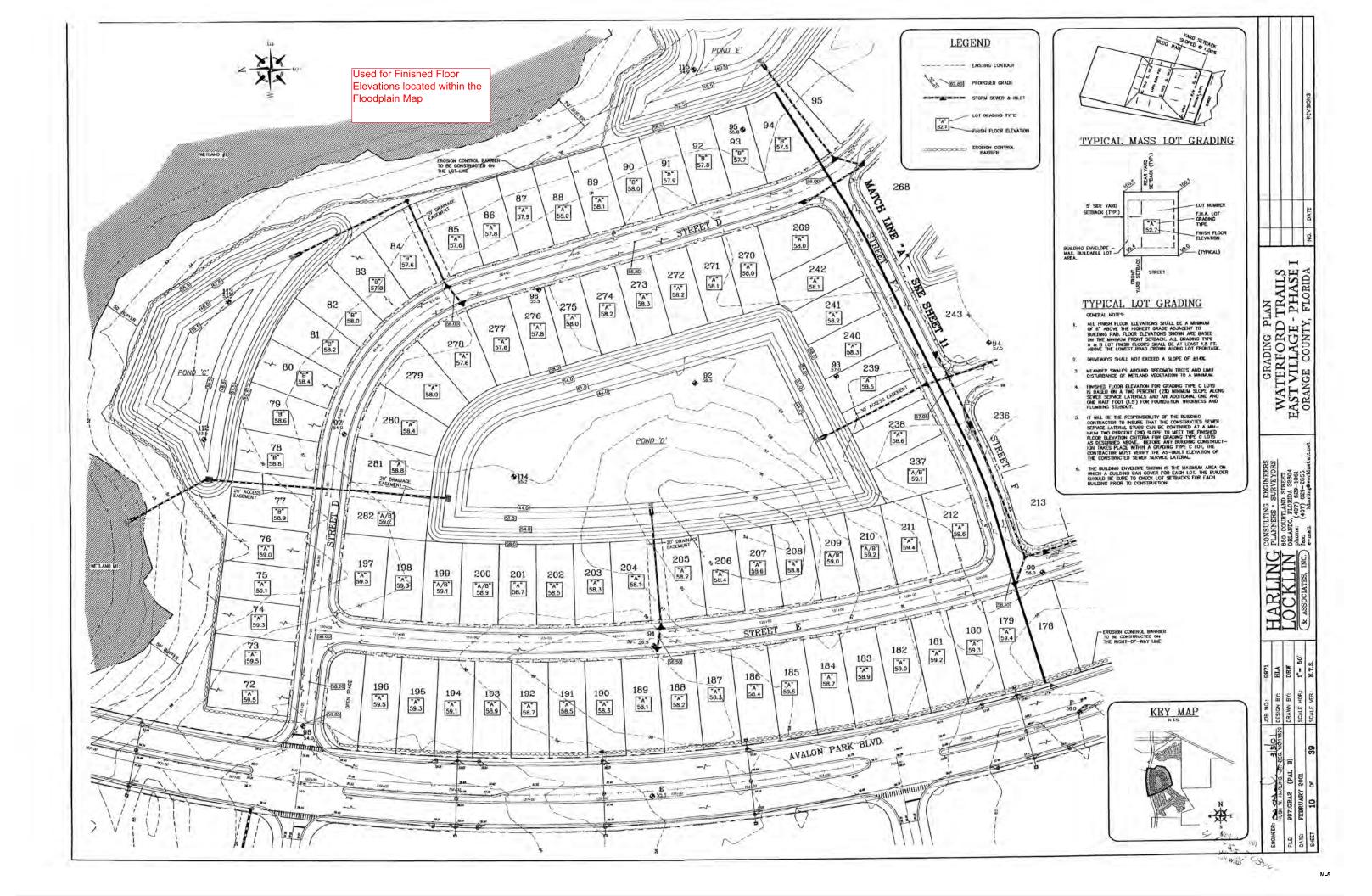
Excerpt from Harling Locklin & Associates, Inc. Waterford Trails Plans and Avalon Park Boulevard Plans

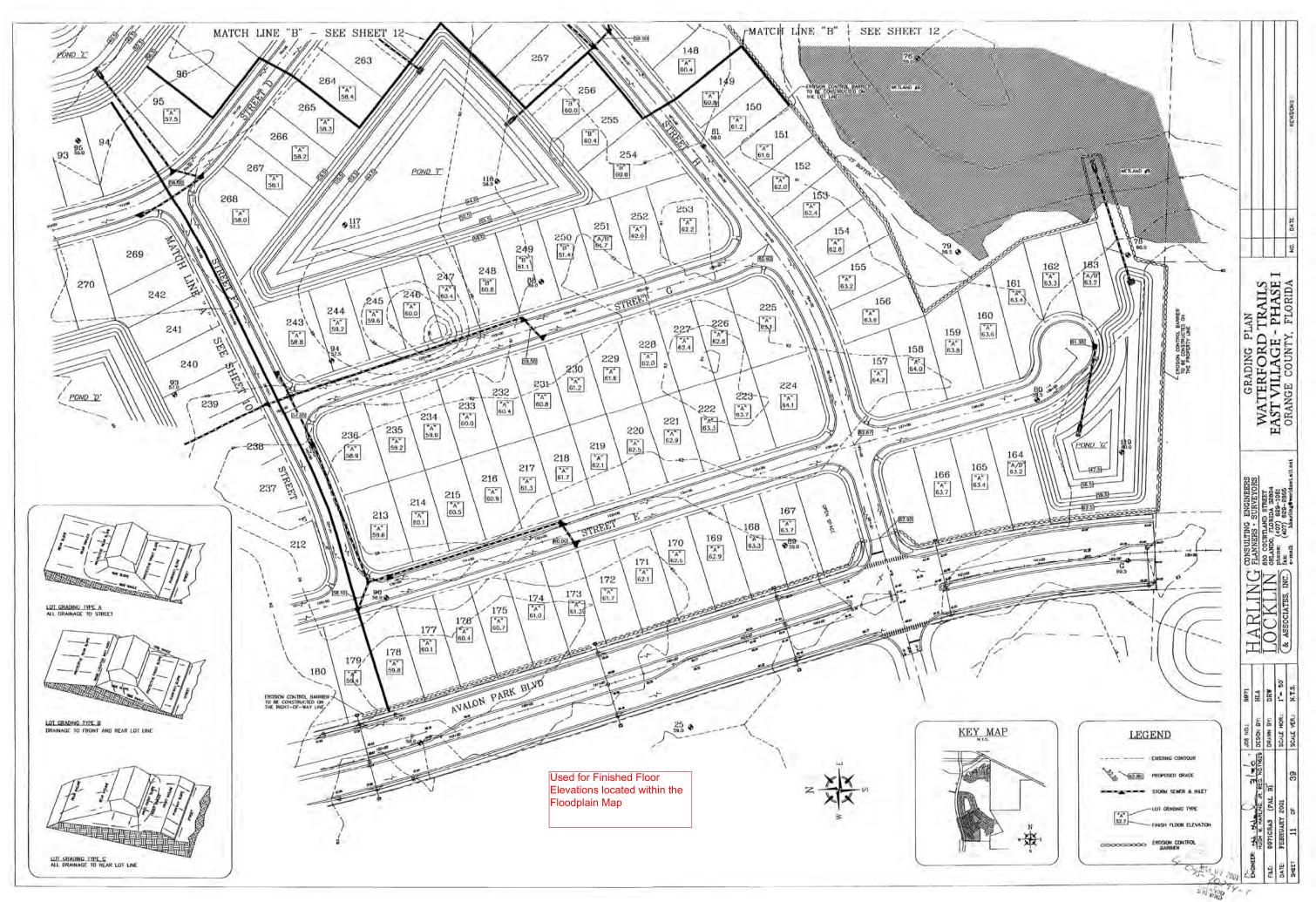


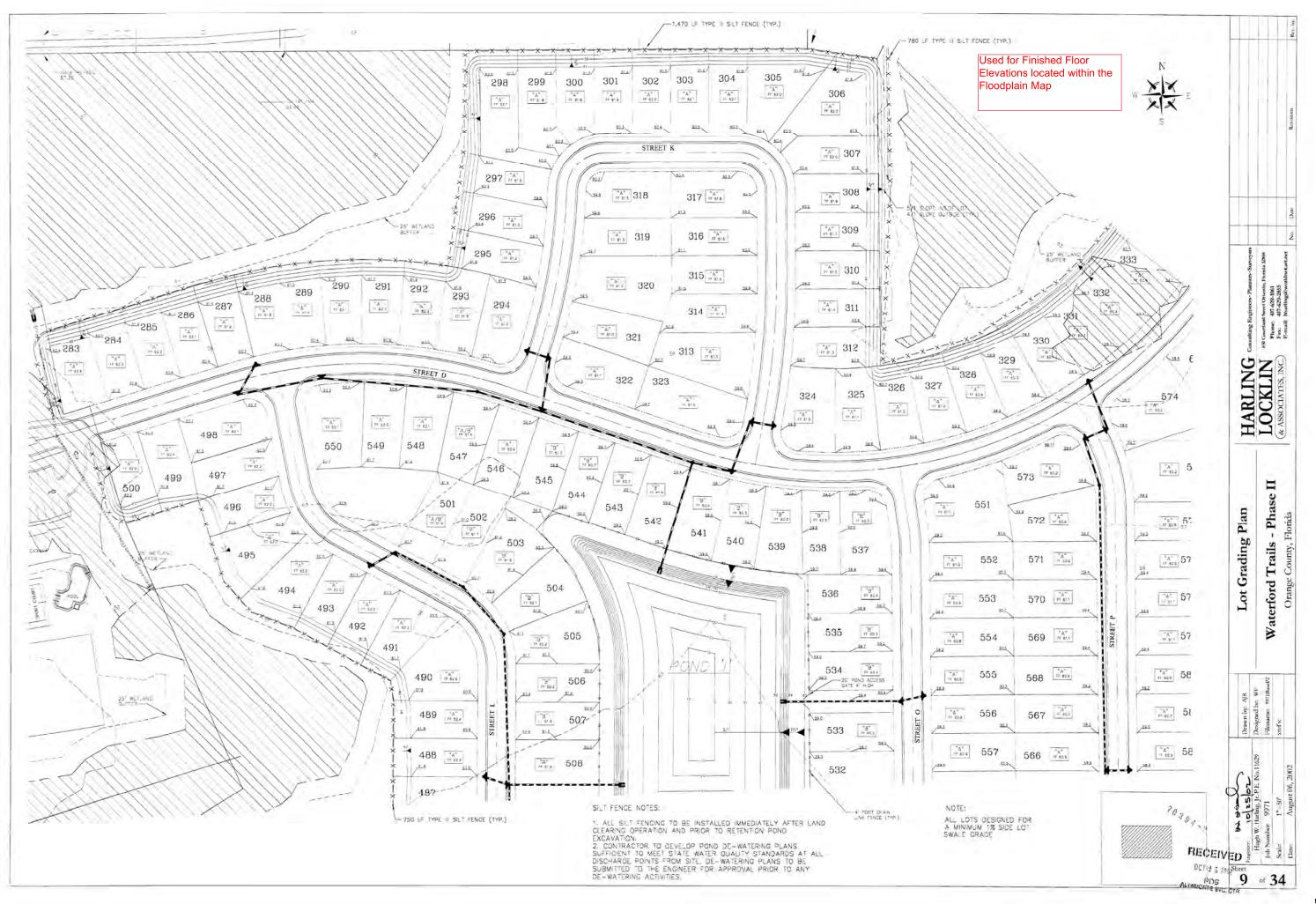


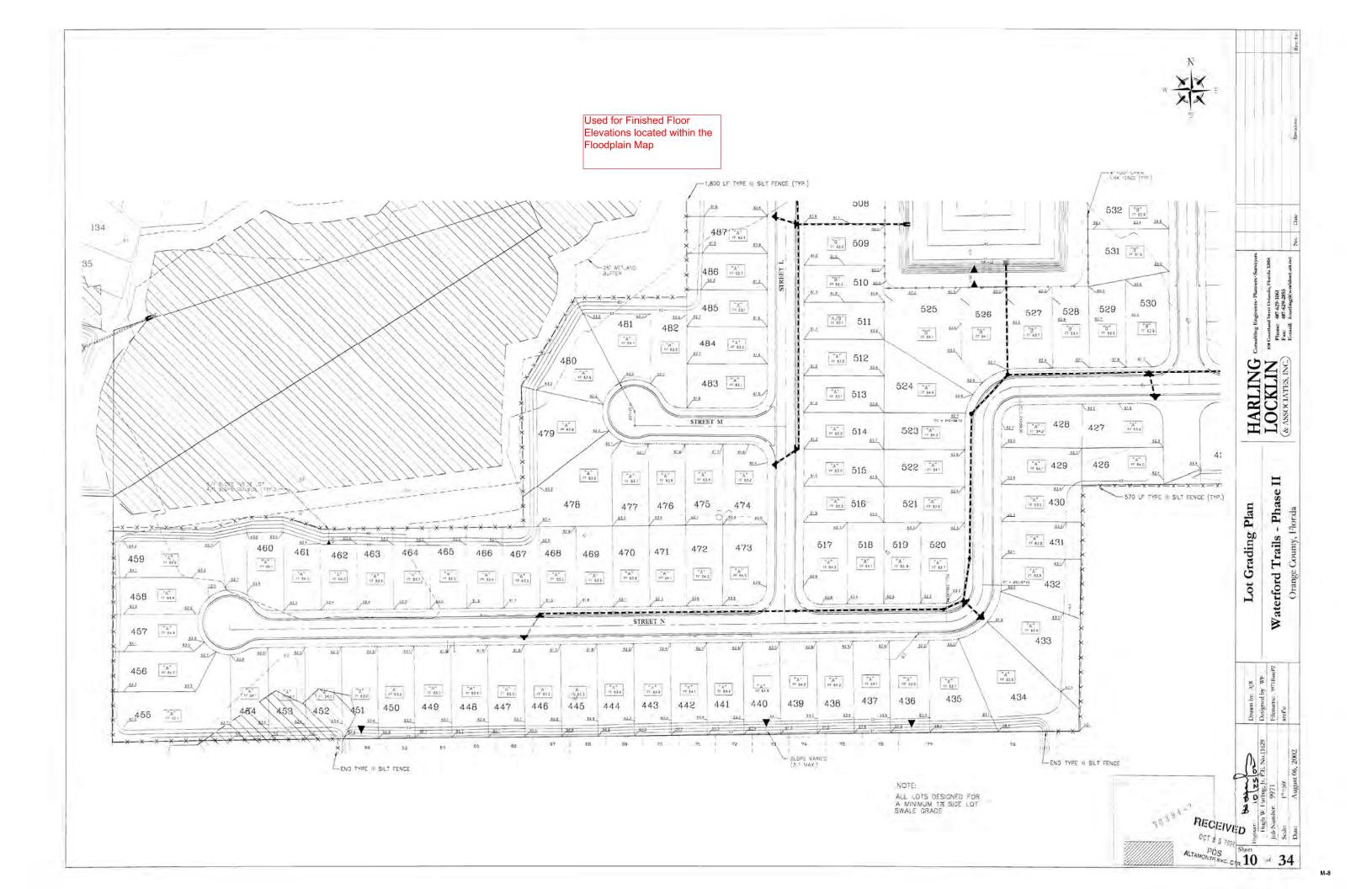


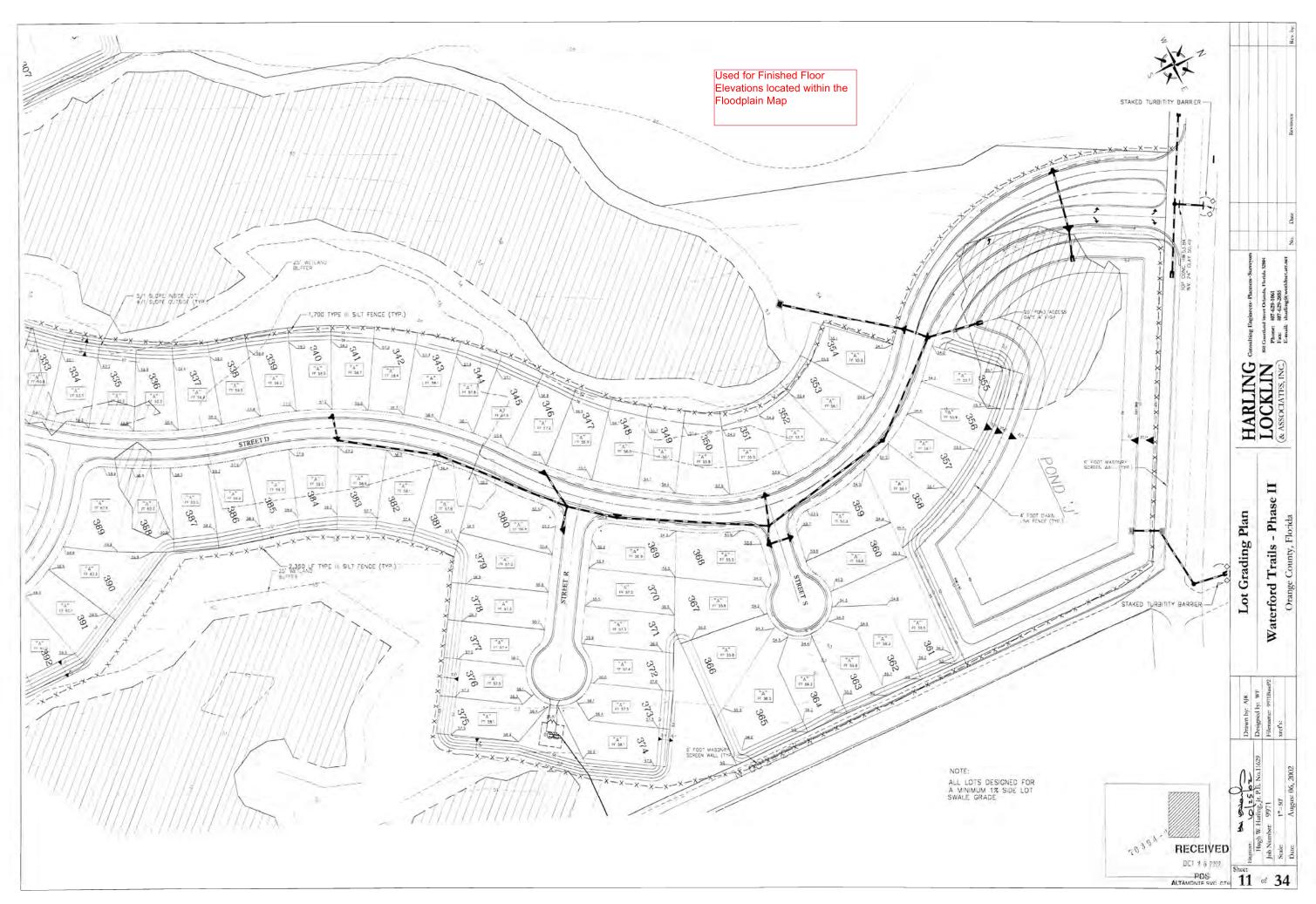


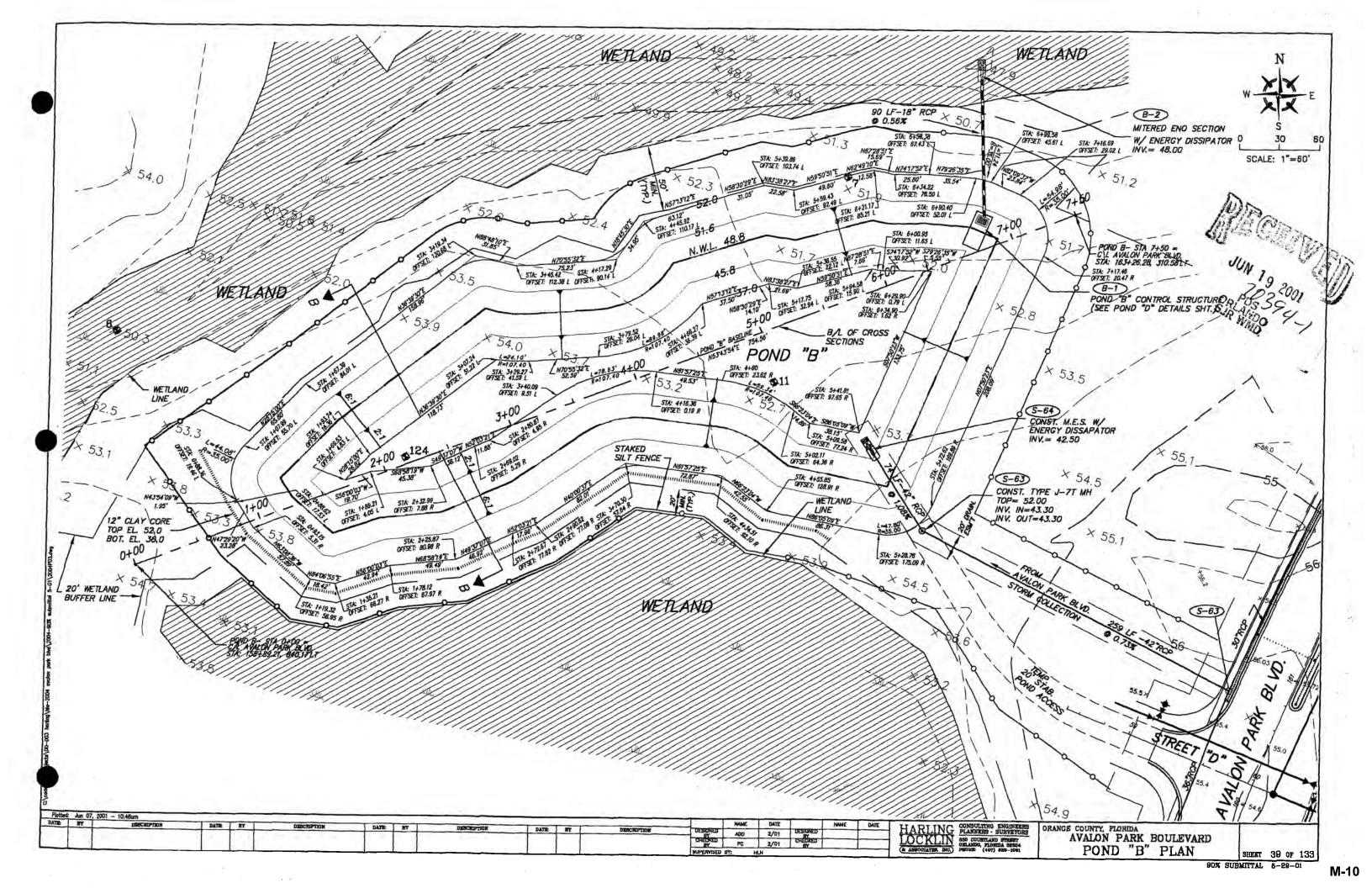


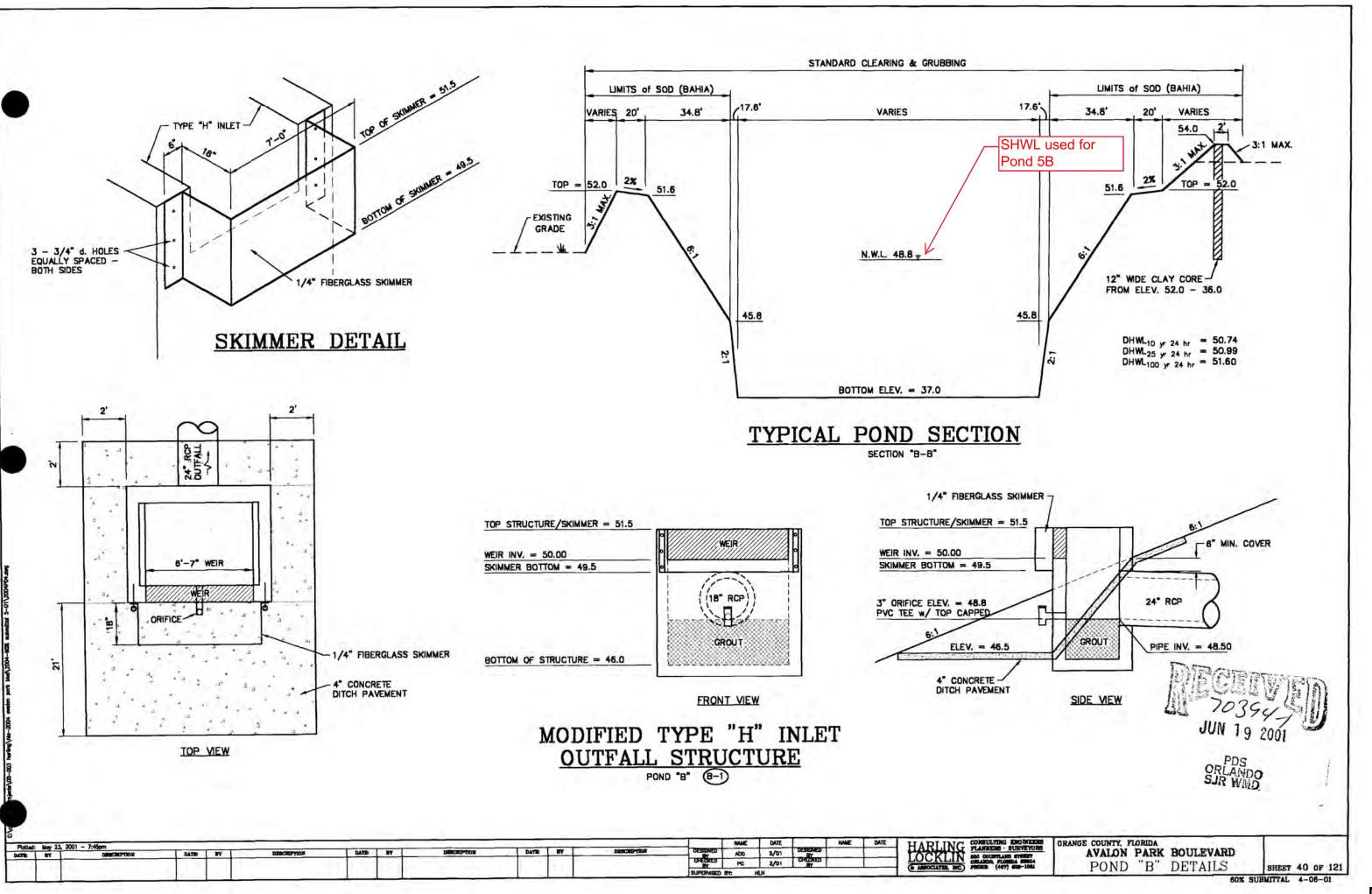










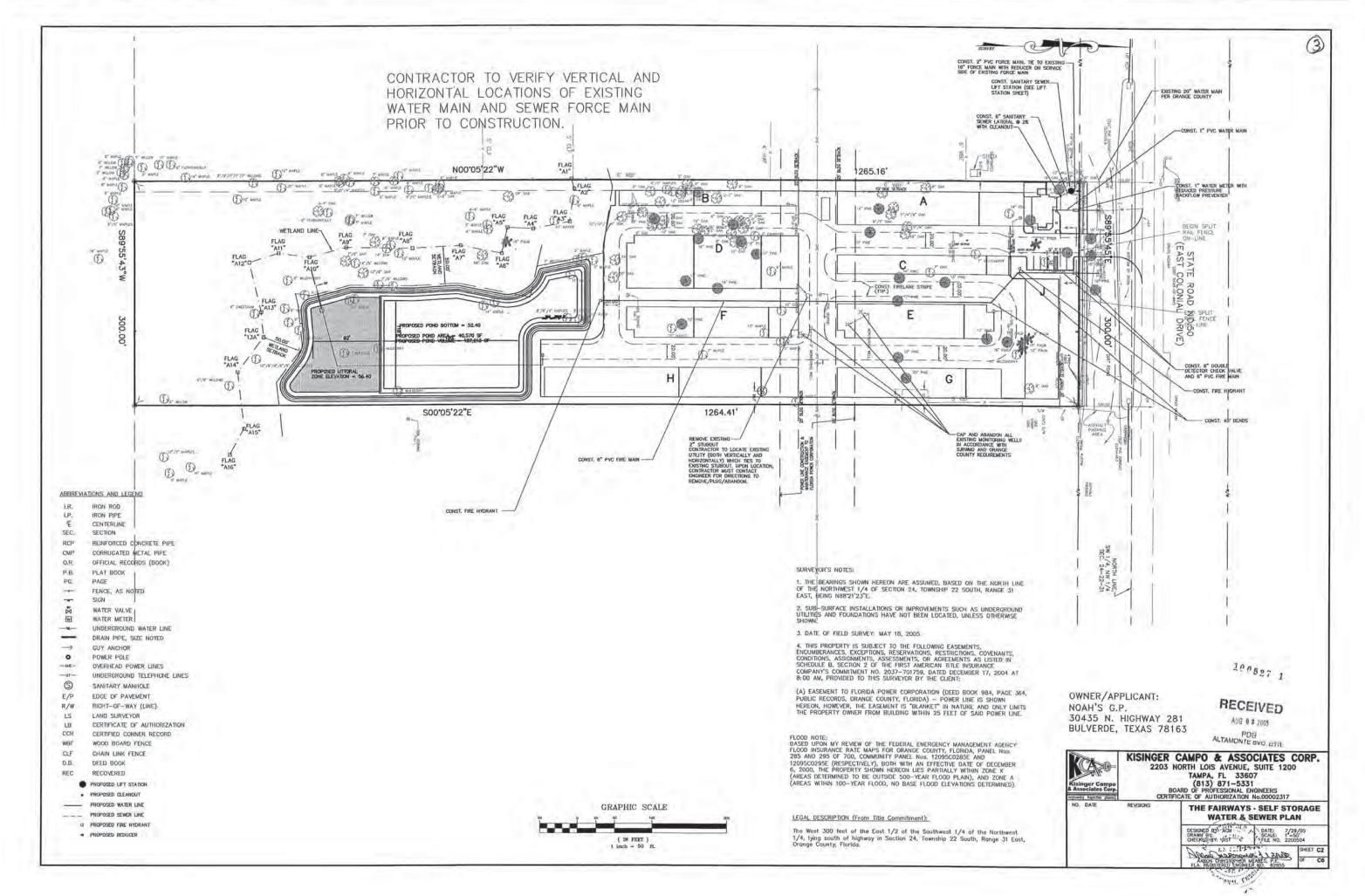


M-11

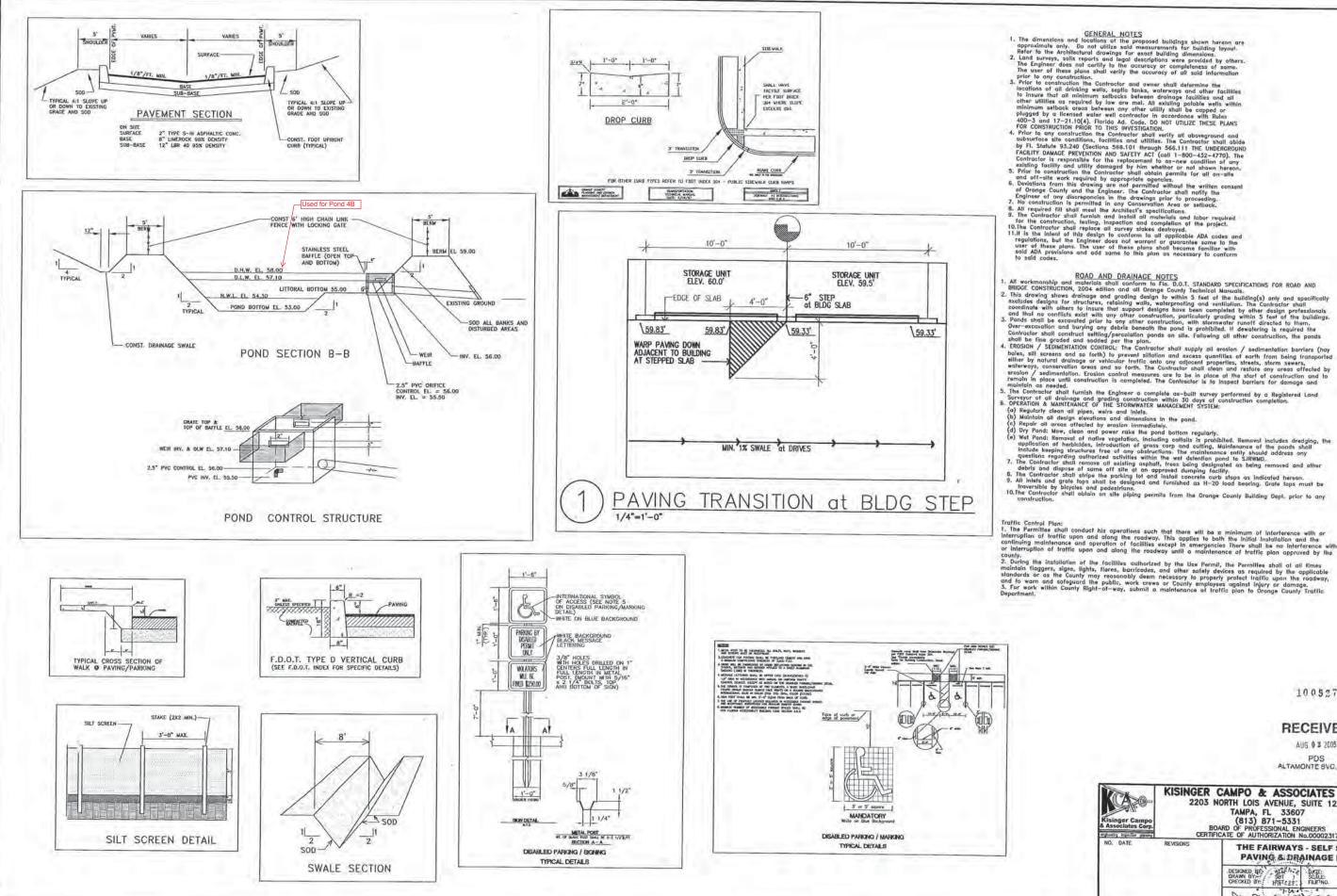


Appendix: N

Excerpt from Kisinger Campo & Associates Corp. The Fairways – Self Storage



N-1



BOAD AND DRAINAGE NOTES
 All workmanship and materials shall conform to file. D.O.I. STANDARD SPECIFICATIONS FOR ROAD AND
 BRIDGE CONSTRUCTION, 2004 edition and all Orange County Technicol Manuals.
 This drawing shows drainage and grading design to within 5 feet of the building(a) only and specifically
 accludes designs for structures, reliaining walls, woleproofing and veniloiding. The Confractor shall
 coordinate with others to insure that support designs have been completed by other design professionals
 and that no conflicts exist with any other construction, particularly gradient to design professionals
 ord that no conflicts exist with any other construction, with sformwater runoff directed to them.
 Order-excavelion and burying any defits beneating the prohibited. If develoring is required the
 contractor shall be accounted prior to any other construction, particularly gradient to be and added per the plan.
 Ponds shall be accounted and added per the plan.
 Contractor shall access and a solded per the plan.
 Contractor shall access and so forth, for prevent silicition and access quantities of earth from being fransported
 siliner by natural drainage or vehicular traffic onto any adjacent properties, strest, storm savers,
 welleway, conservation areas and so forth, for breadulated by it reconstruction and restore any areas atflected by
 eraction i place unit construction is completed. The Contractor shall earth and restore any areas atflected by
 eraction in place unit construction control measures are to be in place at the stort of construction and
 maintain the store shall turnish the Engineer accutator is to inspect barriers for damage and
 maintain a store and grading construction within 30 days of construction completion.
 So the Contractor shall turnish the Engineer accomplete ac-built survey performed by a Registered Land
 Surveyor of all drainage and grading construction within 30 days of construction completion.
 So the Contracto

Traffic Control Plan: 1. The Permittee shall conduct his operations such that there will be a minimum of interference with or interruption of traffic upon and along the roadway. This applies to both the initial installation and the confinuing maintenance and operation of facilities except in emergencies. There shall be no interference with or interruption of traffic upon and along the roadway until a maintenance of traffic plan approved by the county.

County. 2. During the installation of the facilities authorized by the Use Permit, the Permittee shall of all times maintain flaggers, signs, lights, flares, barricades, and other safety devices as required by the applicable standards or as the Gounty may reasonably deem necessory to properly protect inditio upon the readway, and to warn and scaunty may reasonably deem necessory to properly protect indition upon the readway. 3. For work within County Right-of-way, submit a maintenance of traffic plan to Grange County Traffic Department.

100527 1

(4)

RECEIVED

AUG 0 # 2005 PDS ALTAMONTE BVC. OTR.

Kisinger Campo 8 Associates Corp.	2203	R CAMPO & ASSOCIATES CORP. NORTH LOIS AVENUE, SUITE 1200 TAMPA, FL 33607 (813) 871-5331 BOARD OF PROFESSIONAL ENGINEERS TIFCATE OF AUTHORIZATION No.00002317
NO. DATE	REVISIONS	THE FAIRWAYS - SELF STORAGE PAVING & DRAINAGE DETAILS
		DESIGNED BY:
1		Man Charge with Start C3
		Sbuilt Elin

Appendix: O

Correspondence

FDOT Drainage Coordination Meeting Minutes SR408 Extension PD&E (SR408 to SR520 along SR50) Project No. 408-254 Contract No. 001064

Wednesday, November 18, 2015 1:30 pm to 3:00pm

Attendees:	Todd Alexander (FDOT)
	Annette Brennan (FDOT)
	Gene Howerton (Arcadis)
	Walter Nemecek (Arcadis)
	Matt Gibbs (CES)
	Chris Wence (CES)
	Eric Arp (CES)
	Ferrell Hickson (FDOT)
	Will Sloup (Metric)
	Gabriela Garcia (Metric)
	Chandra Raman (Metric)
	Lance Decuir (Atkins)

- Mr. Sloup introduced the team and explained the project history, background, current scope and status.
- The FDOT team (CES) explained that for the first project segment from Avalon Park to Chuluota Road, most of the drainage is being handled by the eastern project segment (from Chuluota Road to SR 520). FDOT owns a parcel at Corner School Drive which currently has a Park and Ride facility on the northern edge. A portion of that land will be used to construct a new pond for attenuation. The remnants of the land will be deeded over to the School Board who plans on developing the land for a new bus loops facility. This segment discharges to existing cross drains and to the Econlockhatchee River. Permit application is anticipated for April 2016.
- The FDOT project segment from Avalon Park to Chuluota Road has Phase II due January 15, 2016 and final due in August 2016. Survey is completed but required modification due to ongoing construction.
- The eastern project segment (Arcadis) will be modifying existing county ponds A1, M1, M2 and M2 East which will be transferred to the FDOT for maintenance. The existing ditches in this segment have severe contamination and are not proposed to be modified. The proposed typical section will consist of curb and gutter with curb flume to drain the roadway runoff into the swales. The swale will drain into Econ River without treatment. Instead of treating SR 50, this segment will modify pond A1 and treat the runoff from the Bithlo community. That pond currently serves as overflow and is not treating the runoff. The county and SJRWMD have approved this method as that community has major contamination issues.
- Phase II for the eastern project segment is due in February 2016. Survey is underway.

FDOT Drainage Coordination Meeting Minutes SR408 Extension PD&E (SR408 to SR520 along SR50) Project No. 408-254 Contract No. 001064

- The FDOT team described the following features in the project area:
 - There are many pristine wetlands and the area residents are very protective of them.
 - There are large elevation differences throughout the area
 - There should be available capacity in the existing ponds for treatment. For additional attenuation the existing ponds can likely be modified.
 - There is an existing ICPR model for the area that is owned by the County. The Model was done by Streamline Technologies Inc.
 - The owner of the exiting borrow pits on the northwest of the SR 520 intersection has stated he is willing to sell some borrow pits to the FDOT for use for drainage.
- Econ River is critical for OFW, RFPZ and contaminations.
- Mr. Tim McKinney from United Global Outreach (Florida Hospital Affiliate) is a Bithlo resident that is very involved. The FDOT team recommended that CFX team reach out to him. Mr. Sloup explained that he has been invited to our PAG.
- Frank O'Dea traveled to Tallahassee to discuss funding for the SR 50 widening. The results of the meeting is not known. Both of these projects are top priorities for the district.



Scott Gamit

From:	Grace.ChuaCorn@ocfl.net
Sent:	Monday, April 4, 2016 4:14 PM
То:	Chandra Raman; William Sloup
Cc:	Mike.Drozeck@ocfl.net
Subject:	OC Response to Bithlo SWMMP data request - SR 408 Ext PD&E

Please find Bithlo Area Stormwater Management Master Plan Final Reports in the provided link below: <u>ftp://ftp.orangecountyfl.net/divisions/Public_Works/pub/Stormwater%20Mgmt%20Div/Data%20Request/Metric/</u>

Regarding your County easement inquiries, I found the following details below: Red outline - Environmentally Sensitive Land / Green Place Project Pink outline - Vacant Lands / Bithlo Ranches Foreclosure Blue outline – Retention Ponds / Waterford Lakes Property donated in 2006, this is only easement that I'm sure controlled under Public Works Dept.



Regards,

Grace L. Chua Corn, El, CFM, GISP Stormwater Management Division Orange County Public Works 4200 South John Young Parkway Orlando, Florida 32839 407.836.7965 <u>Grace.ChuaCorn@ocfl.net</u>

PLEASE NOTE: Florida has a very broad public records law (F. S. 119). All e-mails to and from County Officials are kept as a public record. Your e-mail communications, including your e-mail address may be disclosed to the public and media at any time.

Scott Gamit

From:	Grace.ChuaCorn@ocfl.net
Sent:	Wednesday, June 1, 2016 12:28 PM
То:	Chandra Raman
Cc:	Mike.Drozeck@ocfl.net; Jeff.Charles@ocfl.net
Subject:	RE: OC Response to Bithlo SWMMP data request - SR 408 Ext PD&E

For more information regarding the parcel below, please contact Engineering Division.



Point of contact:

Raymond Williams Chief Engineer Engineering Division Orange Co Public Works <u>Raymond.Williams@ocfl.net</u> (407) 836-7900

Regards,

Grace L. Chua Corn, El, CFM, GISP

Stormwater Management Division Orange County Public Works 407.836.7965 Grace.ChuaCorn@ocfl.net

From: Chandra Raman [mailto:chandra.raman@metriceng.com]
Sent: Friday, April 08, 2016 10:12 AM
To: Chua Corn, Grace L
Subject: RE: OC Response to Bithlo SWMMP data request - SR 408 Ext PD&E

Grace,

Thank you for your prompt response. Need further clarification, is that mean the red and pink outline parcels are not owned by County? What are the blue outline ponds are being used for now.

Thank You

CHANDRA RAMAN, P.E. Senior Drainage Engineer



11760 Marco Beach Dr, Jacksonville, Florida 32224 Office: (904)-260-1567 Cell: (561)-713-8977 Fax: (904)-260-1613 chandra.raman@metriceng.com www.metriceng.com

From: Grace.ChuaCorn@ocfl.net [mailto:Grace.ChuaCorn@ocfl.net]
Sent: Monday, April 04, 2016 4:14 PM
To: Chandra Raman <<u>chandra.raman@metriceng.com</u>>; William Sloup <<u>william.sloup@metriceng.com</u>>
Cc: <u>Mike.Drozeck@ocfl.net</u>
Subject: OC Response to Bithlo SWMMP data request - SR 408 Ext PD&E

Please find Bithlo Area Stormwater Management Master Plan Final Reports in the provided link below: <u>ftp://ftp.orangecountyfl.net/divisions/Public_Works/pub/Stormwater%20Mgmt%20Div/Data%20Request/Metric/</u>

Regarding your County easement inquiries, I found the following details below: Red outline - Environmentally Sensitive Land / Green Place Project Pink outline - Vacant Lands / Bithlo Ranches Foreclosure Blue outline – Retention Ponds / Waterford Lakes Property donated in 2006, this is only easement that I'm sure controlled under Public Works Dept.



Regards,

Grace L. Chua Corn, El, CFM, GISP Stormwater Management Division Orange County Public Works 4200 South John Young Parkway Orlando, Florida 32839 407.836.7965 Grace.ChuaCorn@ocfl.net

PLEASE NOTE: Florida has a very broad public records law (F. S. 119). All e-mails to and from County Officials are kept as a public record. Your e-mail communications, including your e-mail address may be disclosed to the public and media at any time.

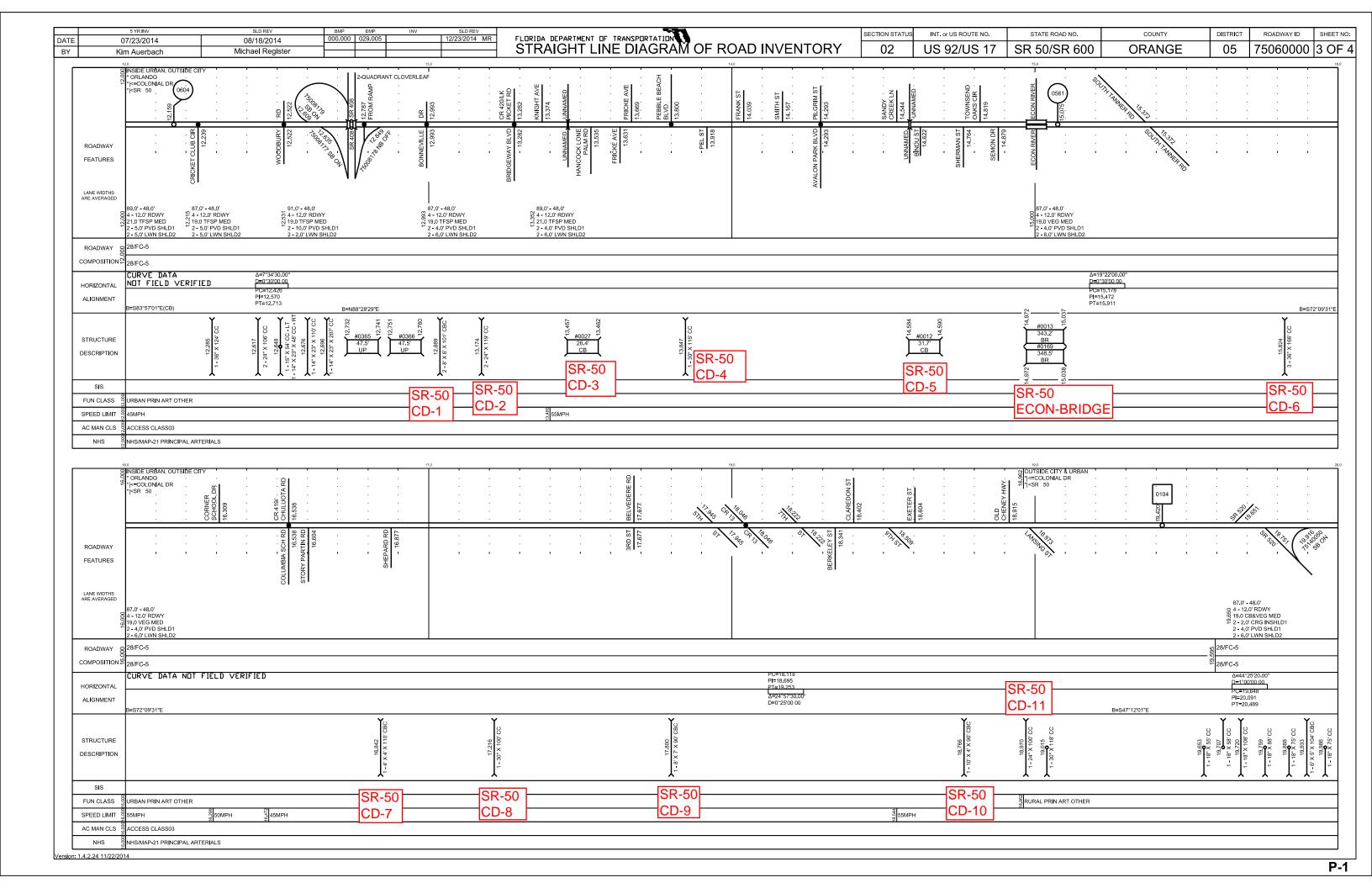
Attention: The information contained in this E-mail message is privileged and confidential information intended only for the use of the individual(s) named above. If the reader of this message is not the intended recipient, you are hereby notified that any dissemination, distribution or copy of this communication is strictly prohibited. If you have received this communication in error, please contact the sender by reply E-mail and destroy all copies of the original message. Thank you.

PLEASE NOTE: Florida has a very broad public records law (F. S. 119). All e-mails to and from County Officials are kept as a public record.

Your e-mail communications, including your e-mail address may be disclosed to the public and media at any time.

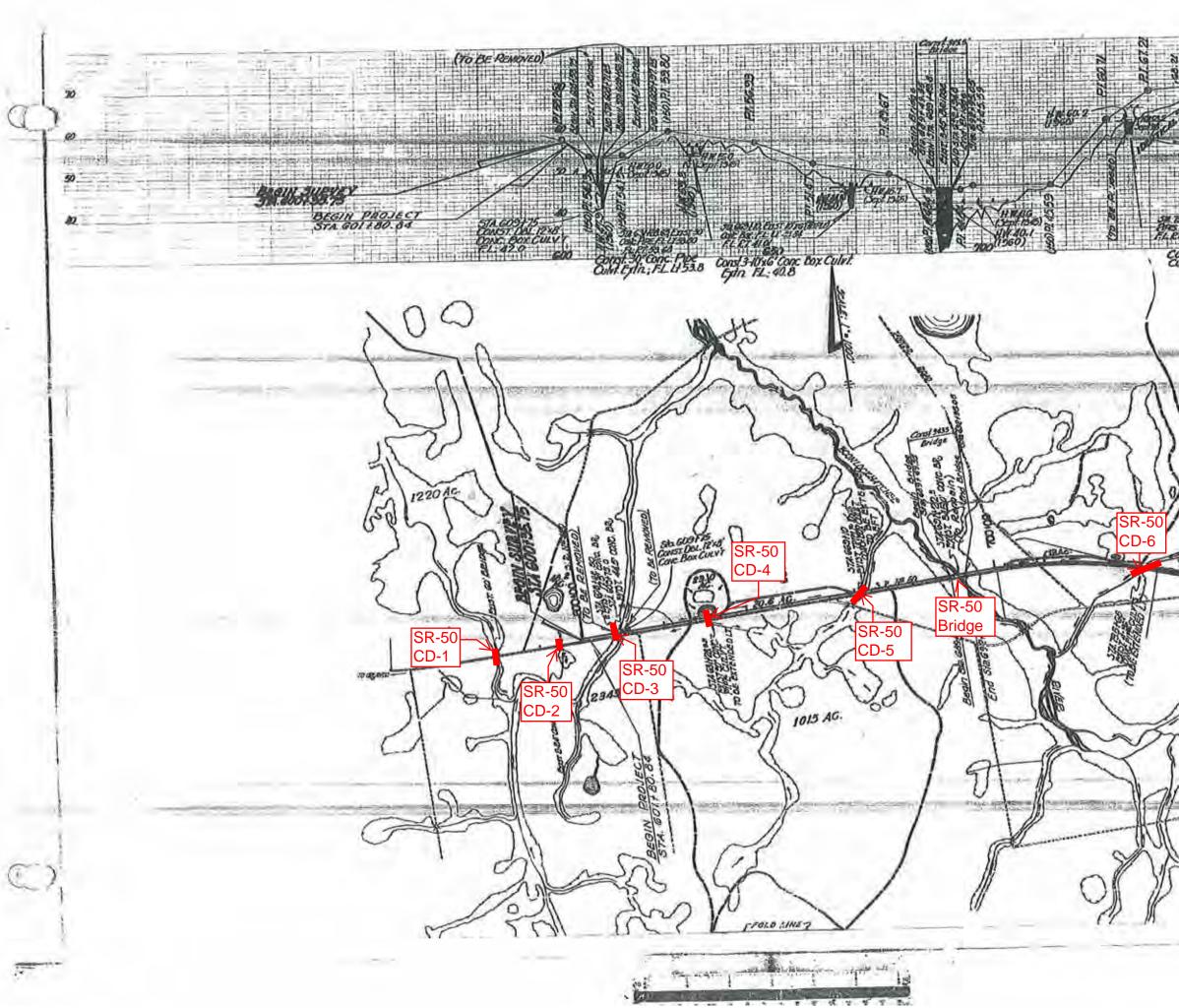
Appendix: P

SR.50 Straight Line Diagram

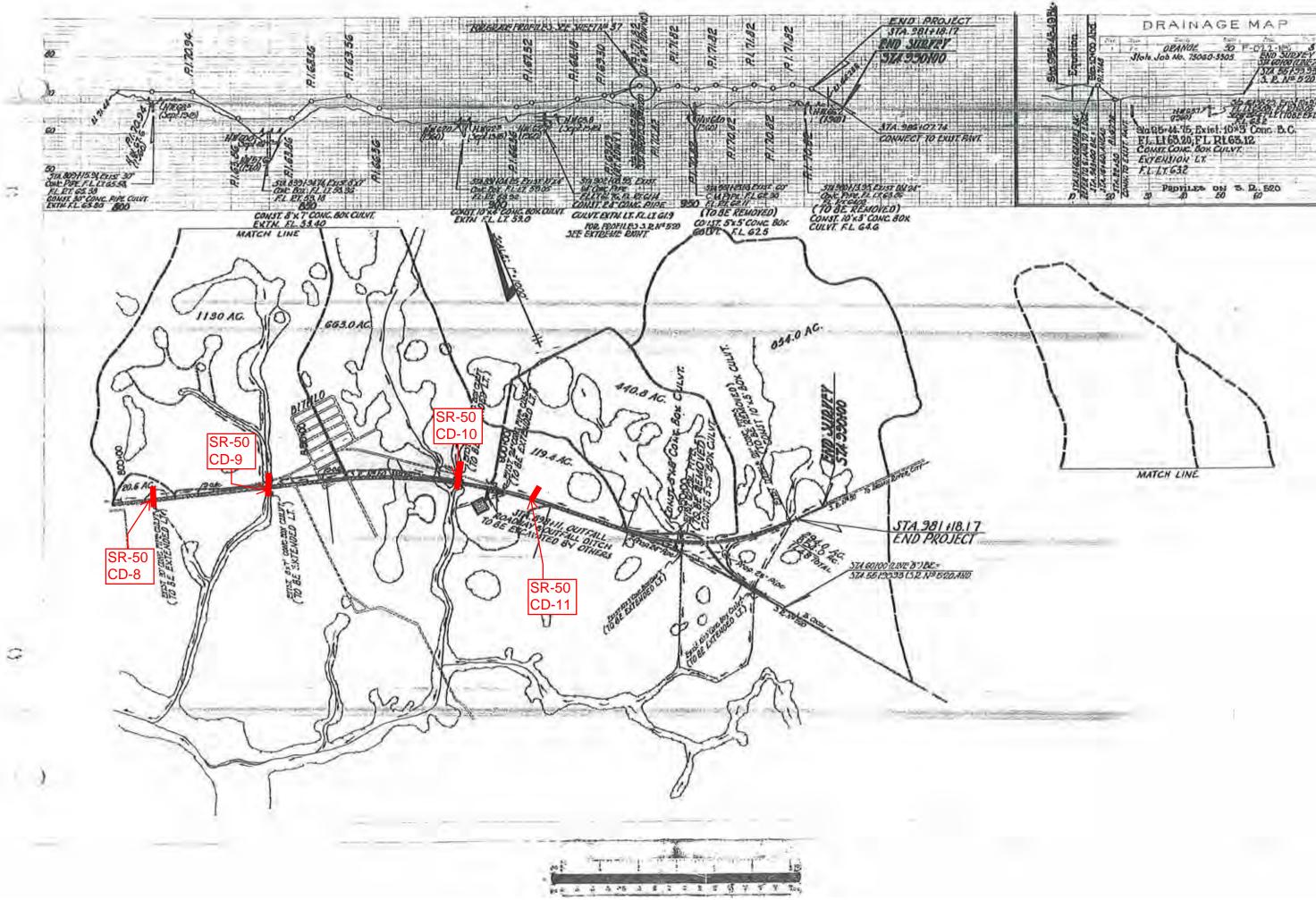


Appendix: Q

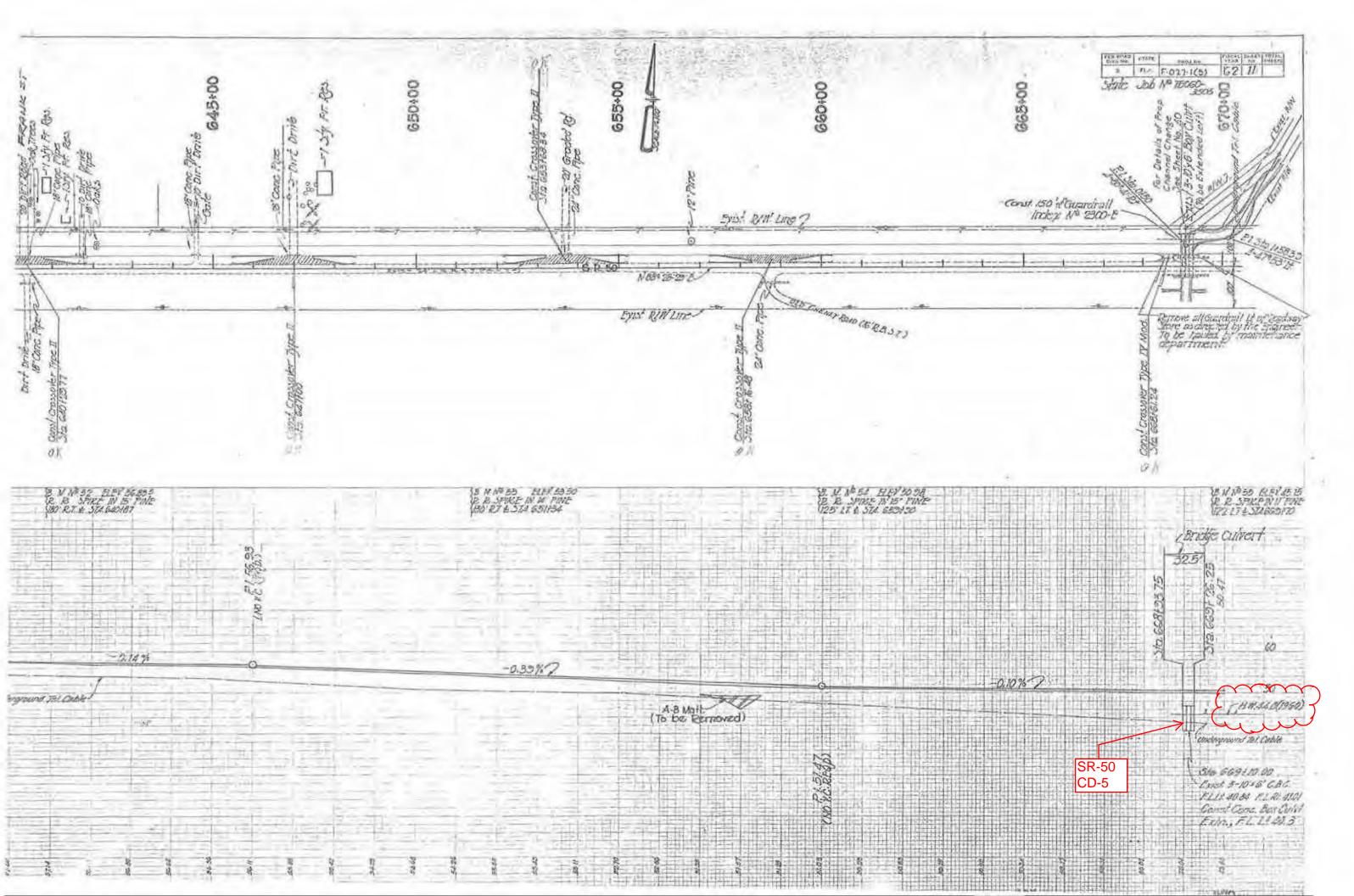
Excerpt from SR 50 Original Construction Plans

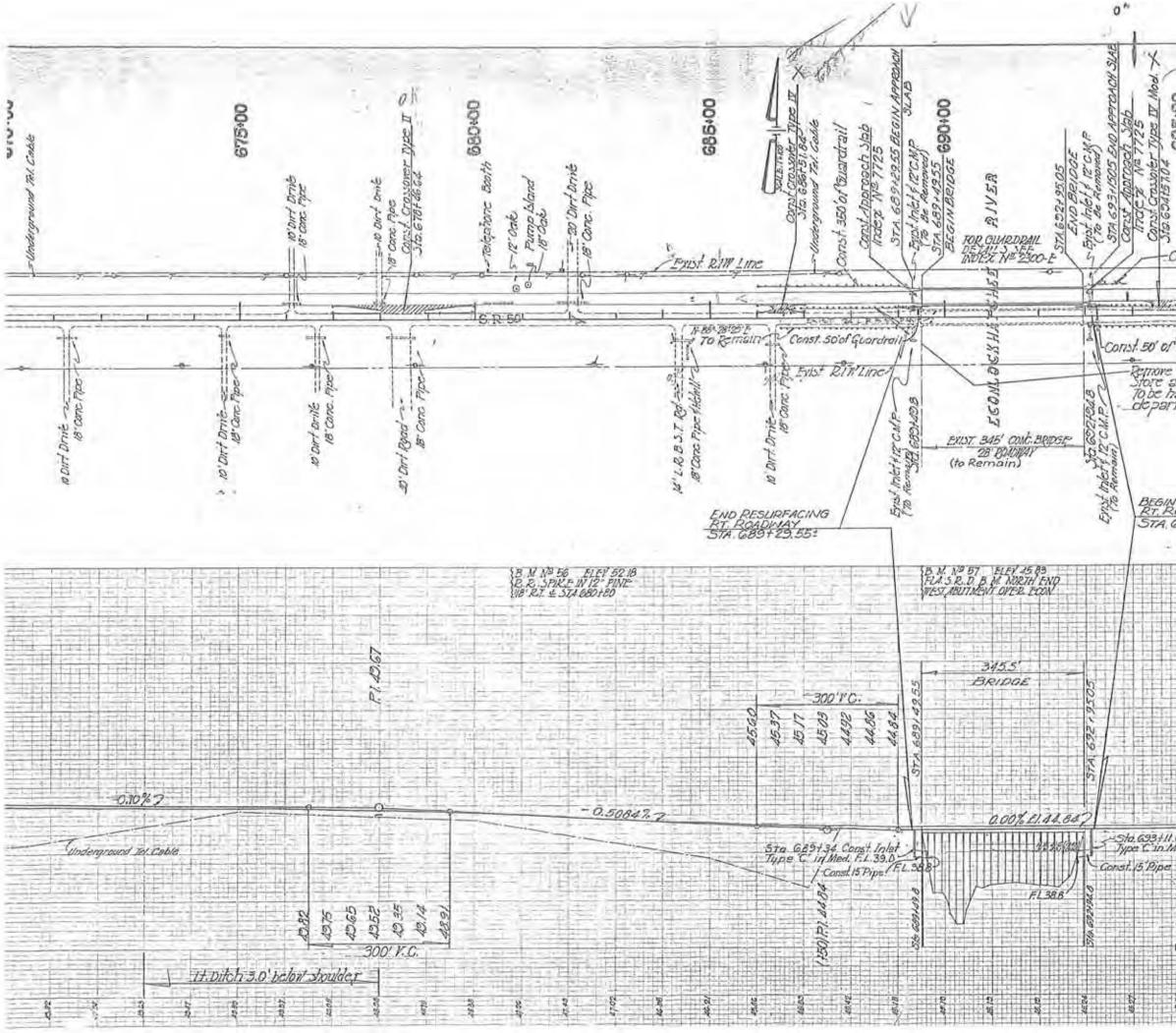


DRAINAGE MAP OPANEE STATE JOAND PISCED ST 1891445 FUST 424 ONE BOX ALL 19943 AL FT 53 30 CONST 4X4 CONC. BOX CUNT. EXTIN.; FL. 59 40 NOTE: 1945 H.W. ARE ESTIMATED AS A BOYR FREQUENCY STORM. 3 00514-35 Can Const 3-36 Corre Pipe Curvi Exta (Skew) FL Lt 58.4 N CR82 211.2 16 17.1 -----SR-50 CD-7 212 SQ. MILES

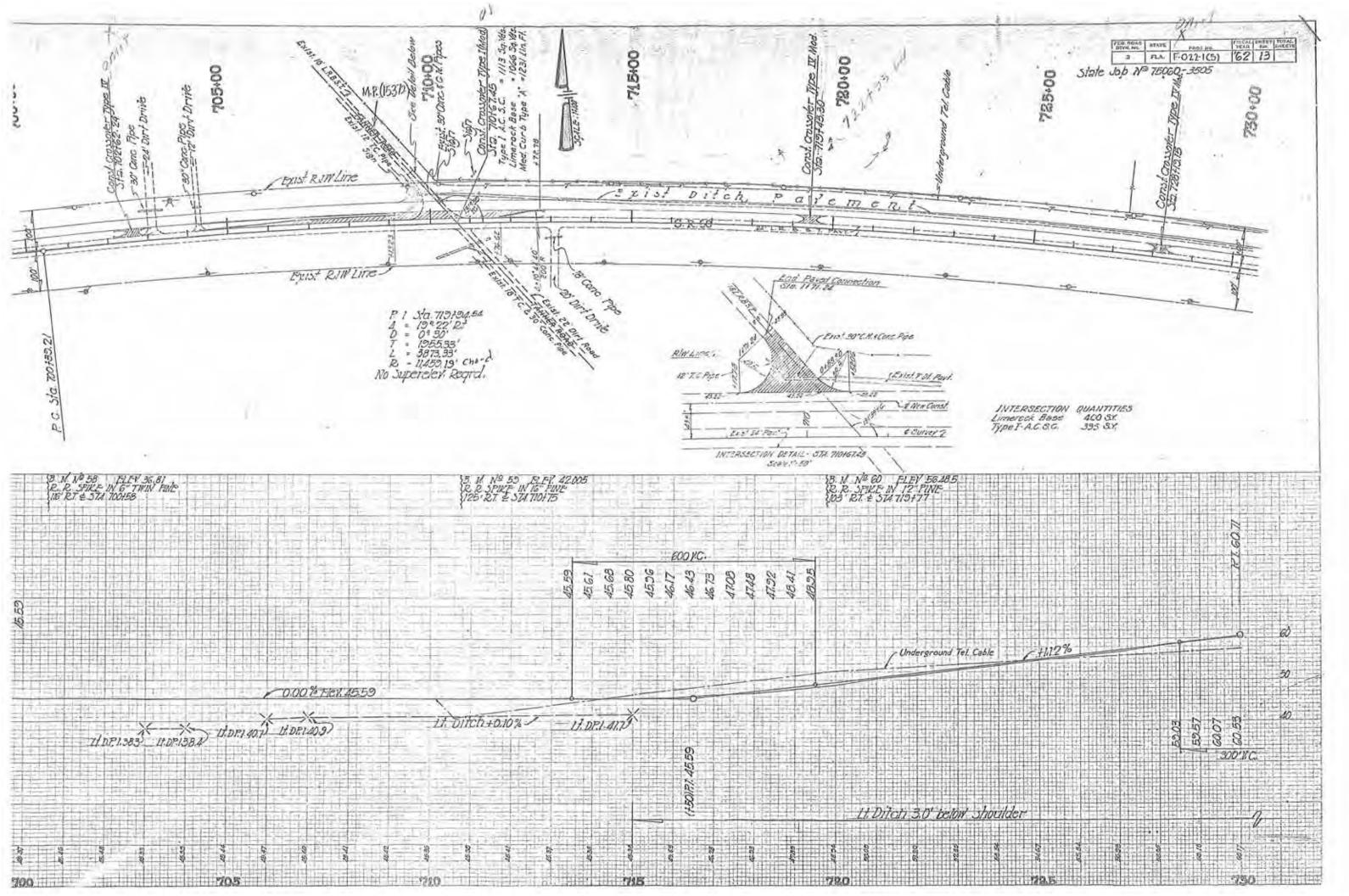


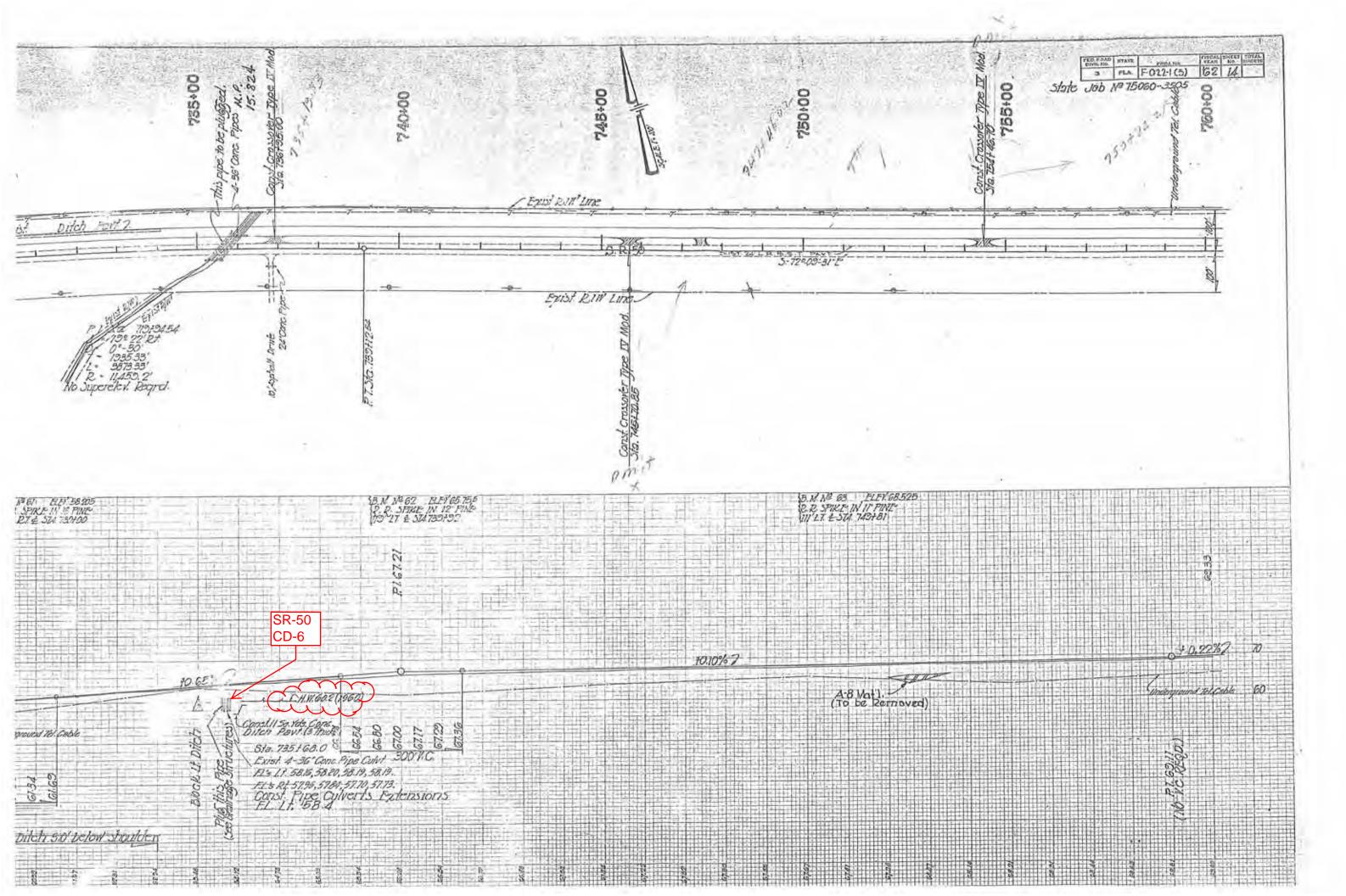
DRANGE 50 F-022-15 S OPANOE 50 F-022-15 S END SUBJEY Sta GHORING FINE Job No. 75050-5505 JIA 551579-53 JIA 551579-53 JIA 551579-53 JIA 551579-53 JIA 520 AUR B 1296.80 LECTOBEET LT) 60

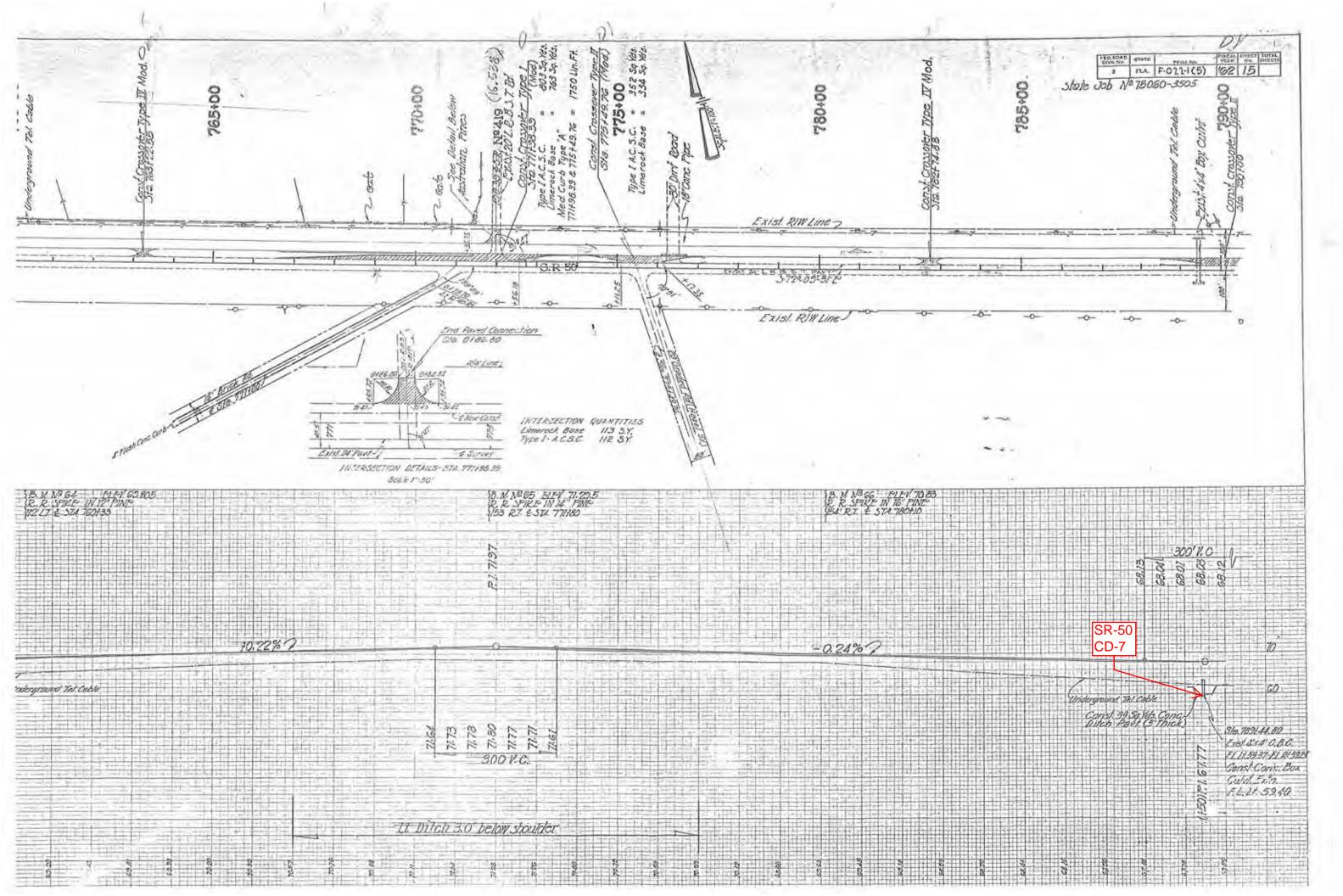


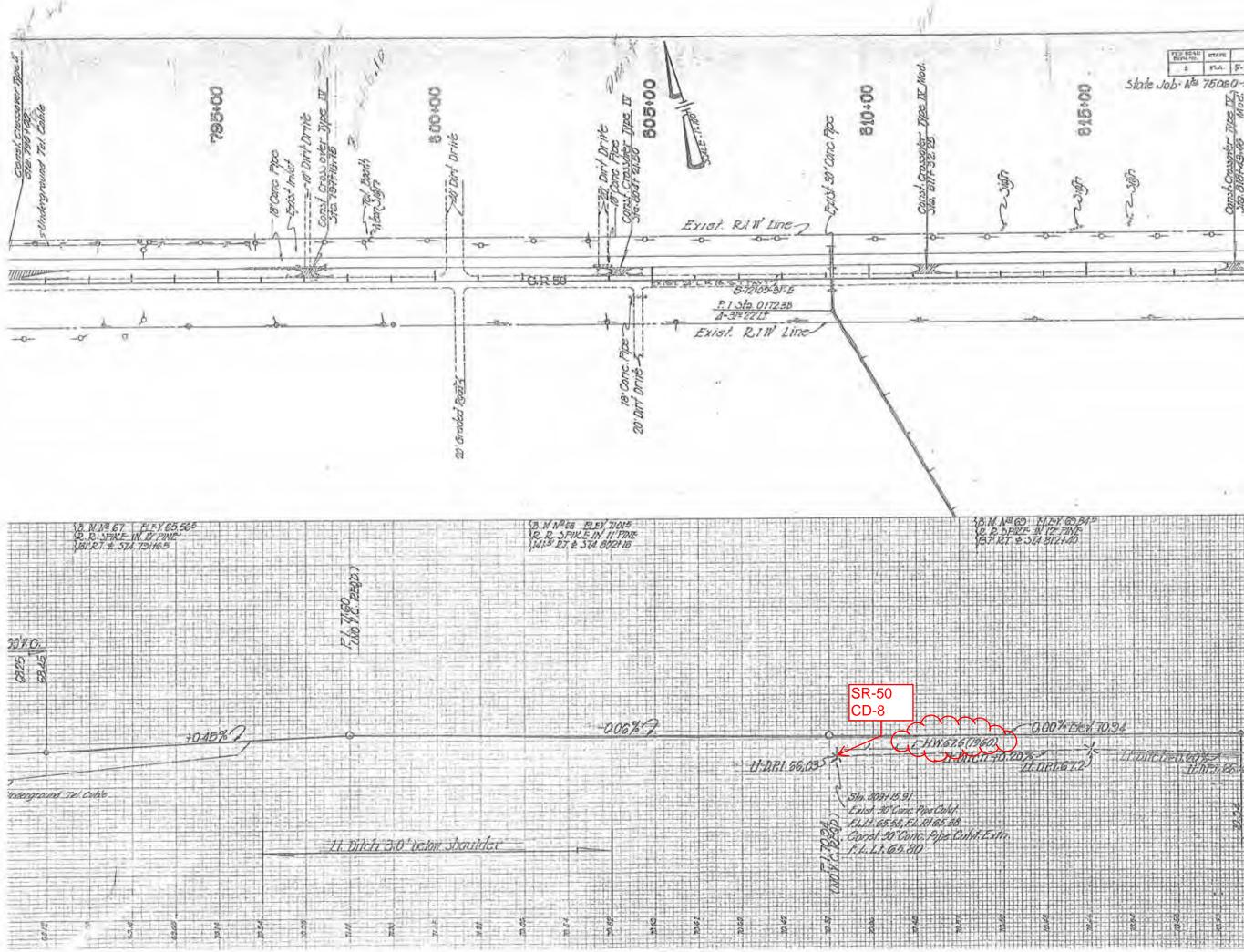


100 100, 100, 100111. 100, 100, 0412711 102 12 FED FOAD DWIE HO BLATE FIATE FROIT NE State Job Nº 15060-3505 695+00 39' -Const. 100 a Guardrail and an a second second a second second second Const 50' of Quardrail -Remove all Guardrail Lt. of Rdwy. Store as directed by the Engineer. To be hauled by maintenance de partiment. 11 BEGIN RESURFACING RT. ROADWAY STA, 693+15.051 60 1.10 60 50 +0.25% 7 0.00% 7 -Sto 693+11 Const Inlet Type C in Med. FL 39.0

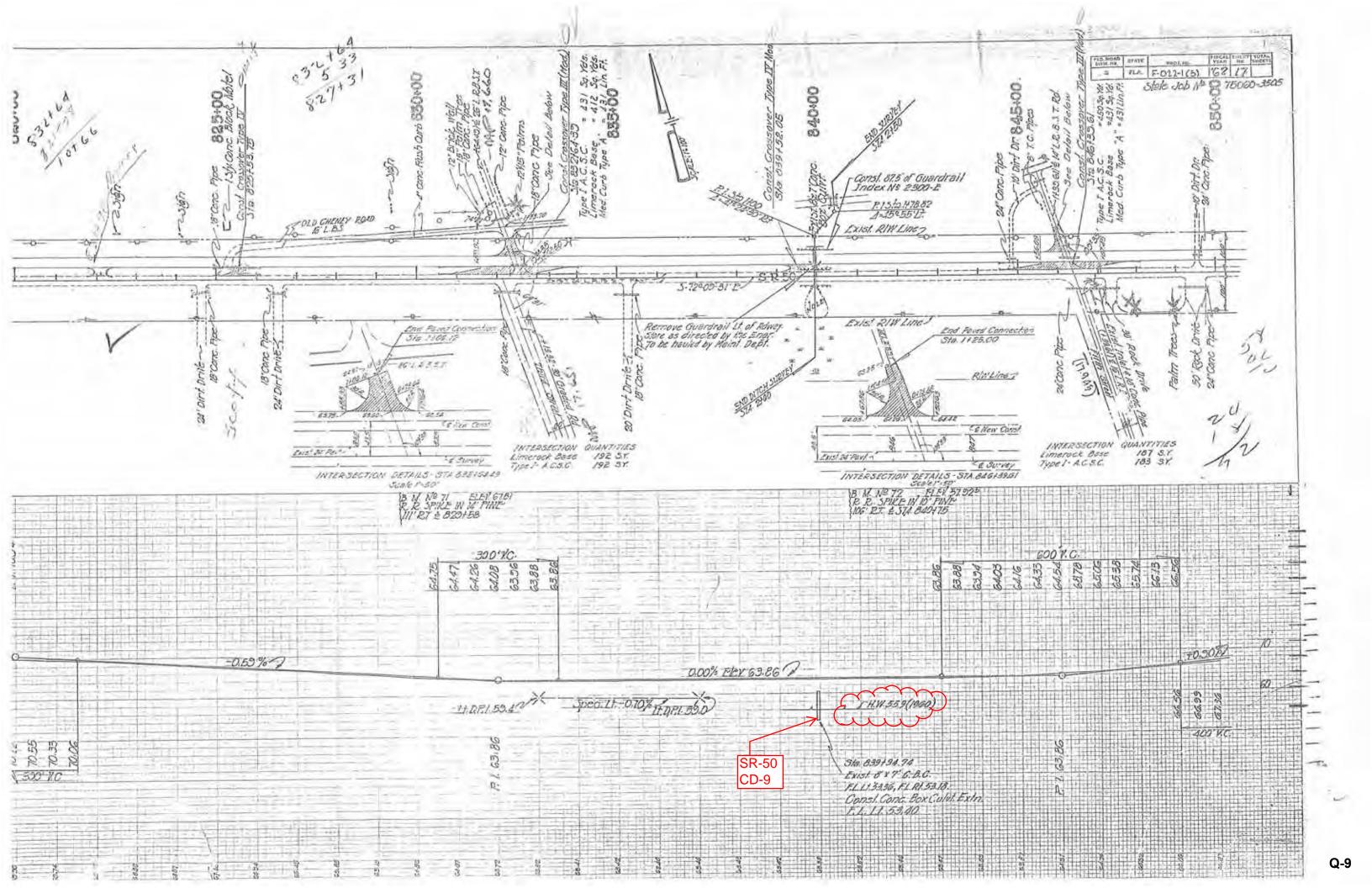


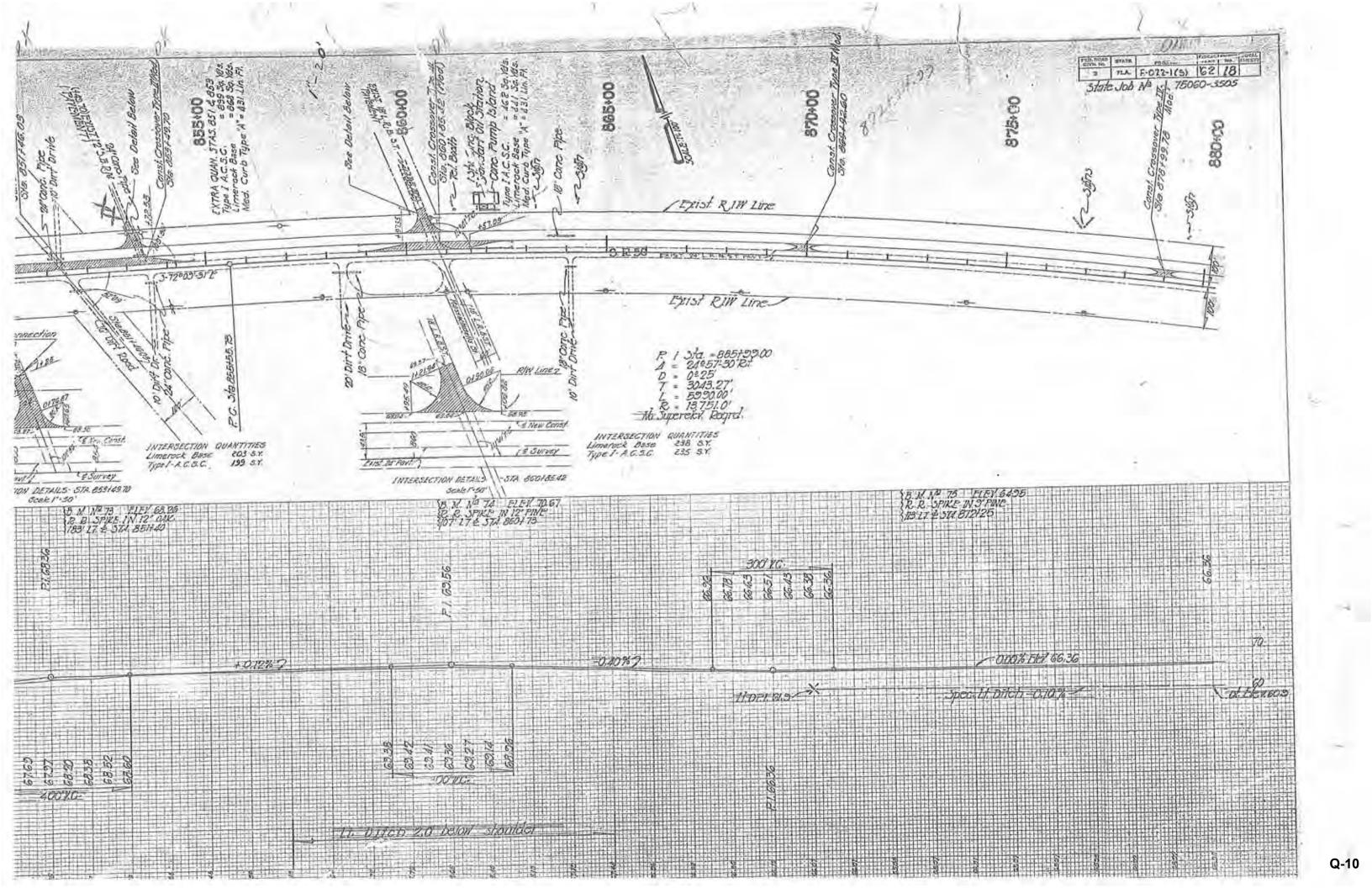


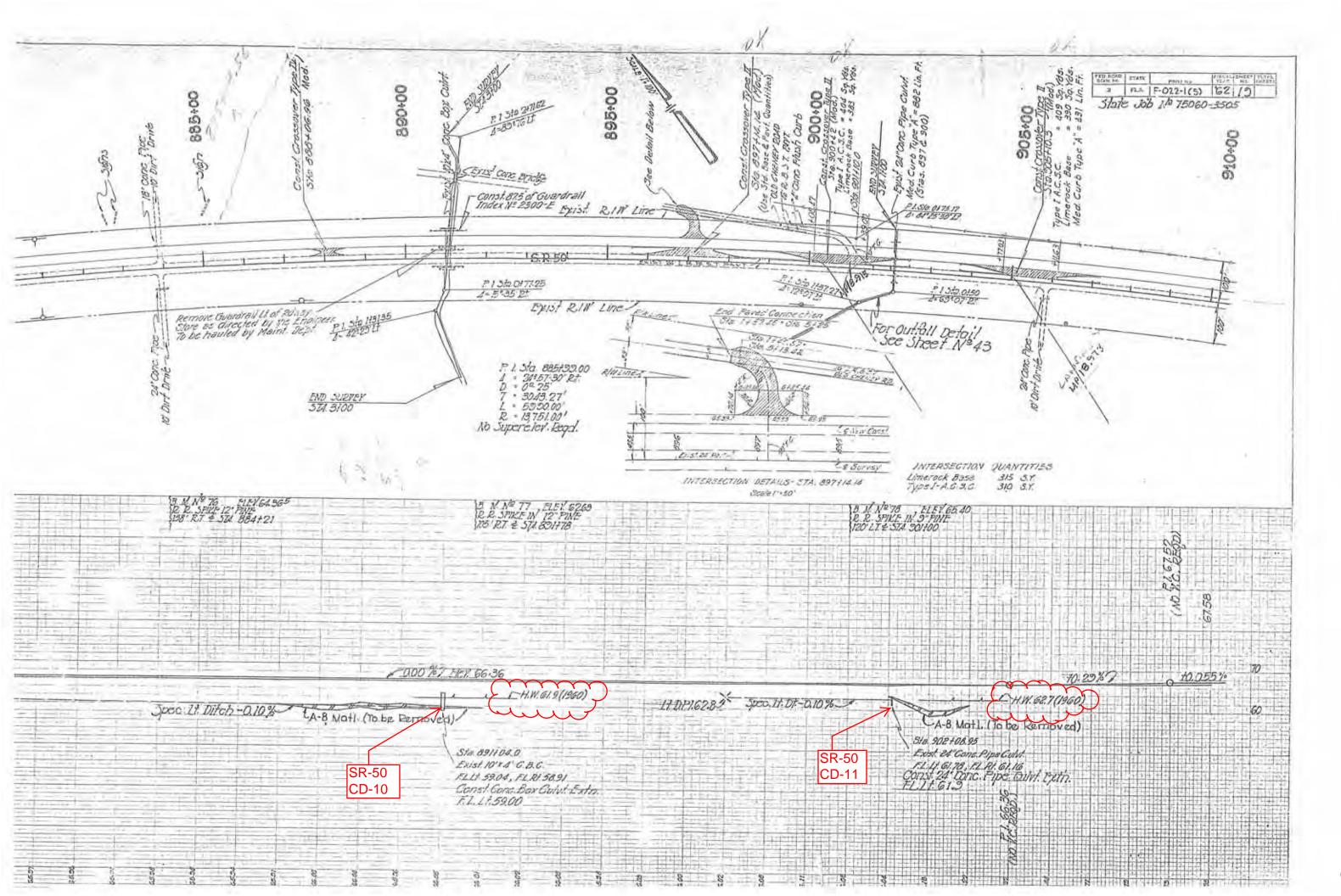


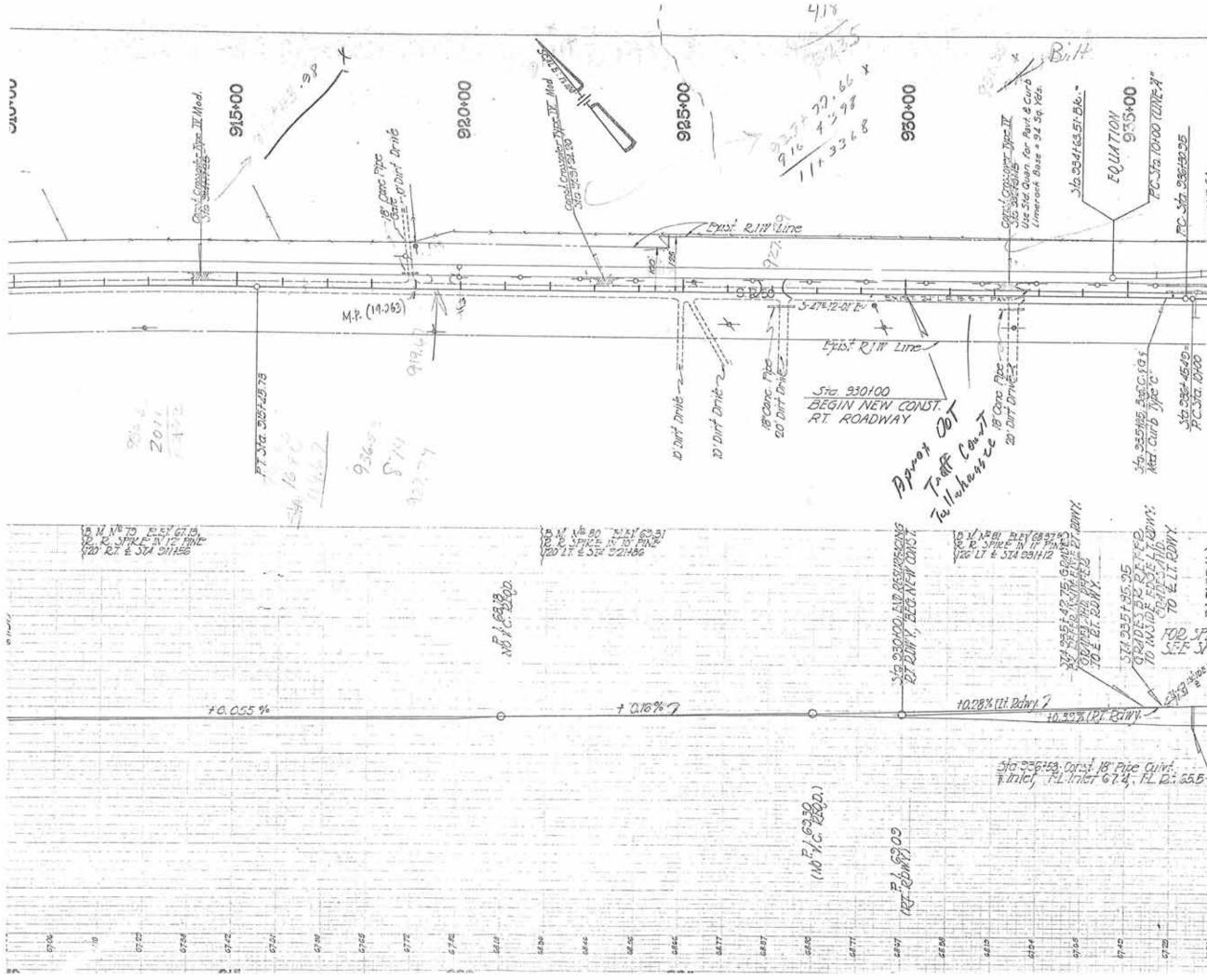


520+00 State Job. No 75080-3505 NDS IV 34000 BIOT 1 MAR 70 FLEX 597 R B. SPIKE IN 8 FIME 14 ET ± 574 810155 80 10020 Q-8

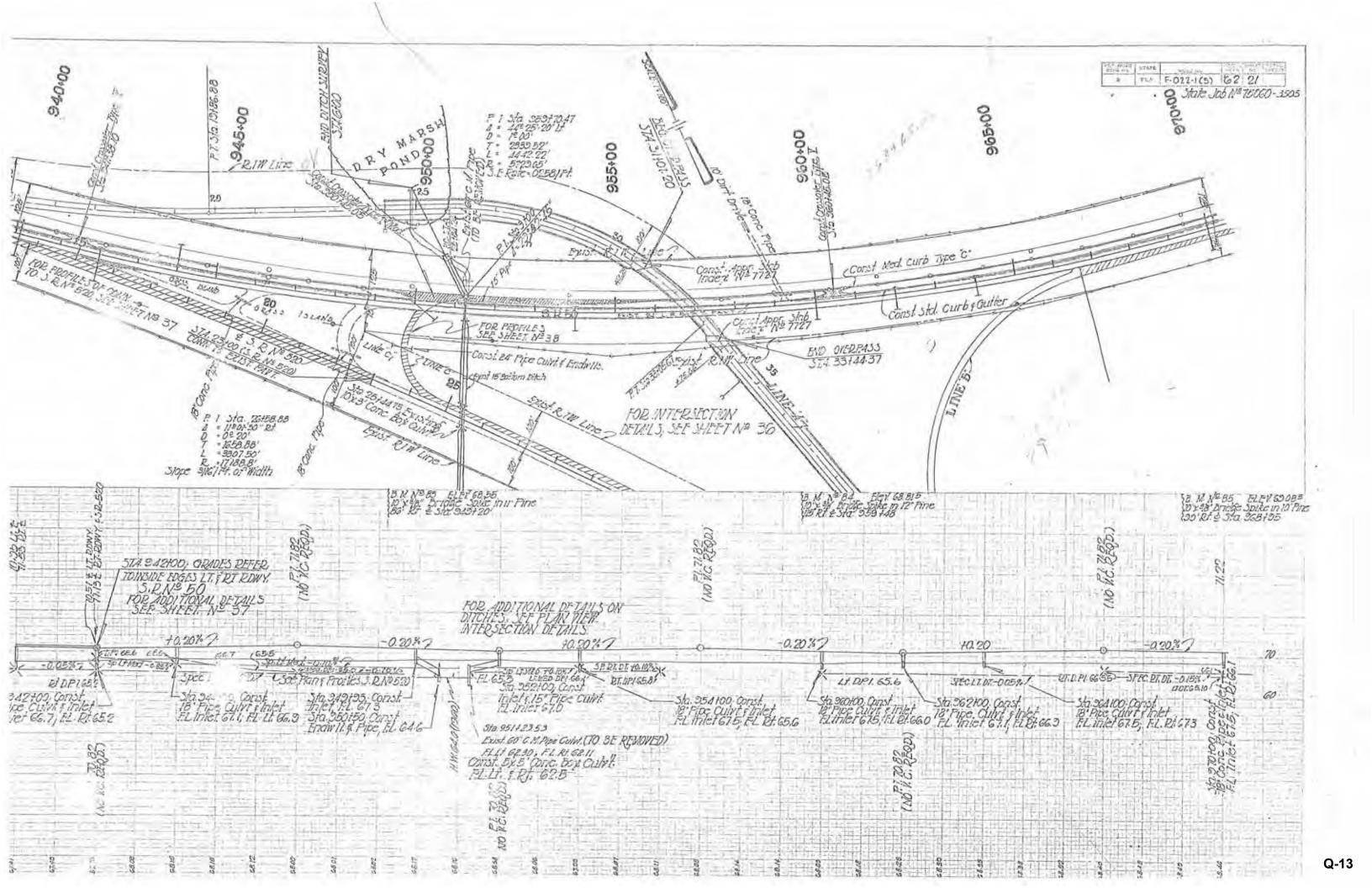








TED READ FRATE PROVING PRESENT TO THE PROVING THE PROVING PRESENT FRATE PROVING PRESENT FOR THE PROVING PRESENT FRATE PROVING PR FQUATION 935400. Sta. 10400 (UNE 7 Sta. 236420.95 93 [12:00 Linc 132.33 0---------Sta 3364 4540-PC Sta. 10400 10. 335405 300.050 4 N Nº 82 FLEY 46.9: R. SPRF IN 12 PINE R. STA 938104 £5.250 71:33(£) RD 70.354 Lt 7103-354 RWN 7103-354 _Rt 0.91.653 Sto 340100 Cons 18 Pice Curvi e Inie. FL Inier LE 67 2 FL Inier LE 67 3 FL RE 65 3 Q-12



Appendix: R

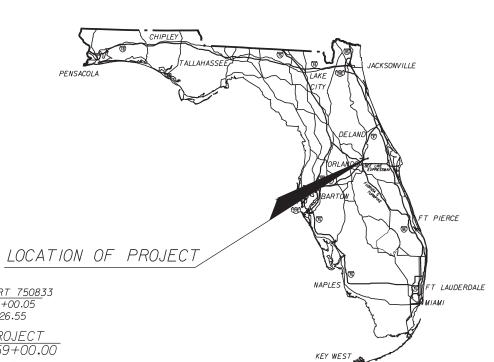
Excerpt from Lochner SR-50 Widening Construction Plans

COMPONENTS OF CONTRACT PLANS SET

A DETAILED INDEX APPEARS ON THE KEY SHEET OF EACH COMPONENT

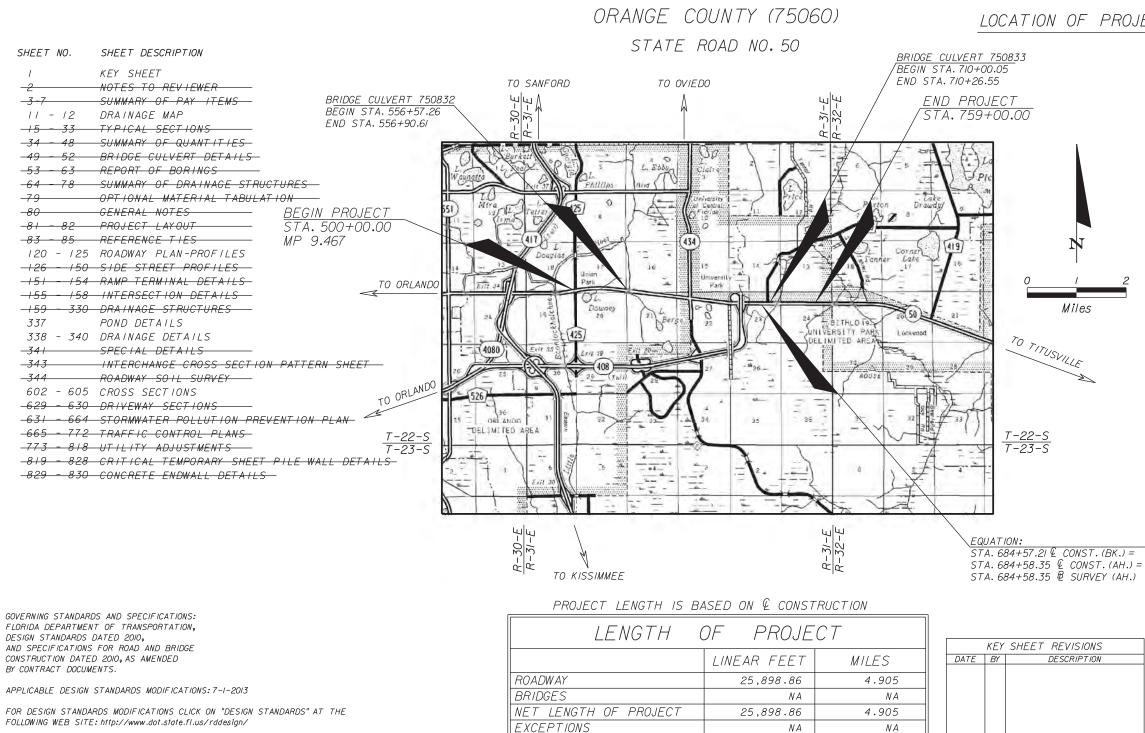
ROADWAY PLANS SIGNING AND PAVEMENT MARKING PLANS SIGNALIZATION PLANS ITS PLANS

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION



CONTRACT PLANS

FINANCIAL PROJECT ID 239203-4-52-01



REVISIONS

FDOT PROJECT MANAGER: CHRISTOPHER L. DABSON, P.E.

25,898.86

4.905

GROSS LENGTH OF PROJECT

ROADWAY SHOP DRAWINGS TO BE SUBMITTED TO: JOHN N. BOX P.E. NO. 41832 H.W. LOCHNER INC. 13577 FEATHER SOUND DR., SUITE 600 CLEARWATER, FLORIDA 33762

PLANS PREPARED BY:

LOCHNER

H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 15577 FEATHER SOUND DR., SUITE 600 CLEARWATER, FLORIDA 33762 VENDOR NO. 36-2338811 CONTRACT NO. C-7461 C.A. 894

NOTE: THE SCALE OF THESE PLANS MAY HAVE CHANGED DUE TO REPRODUCTION.

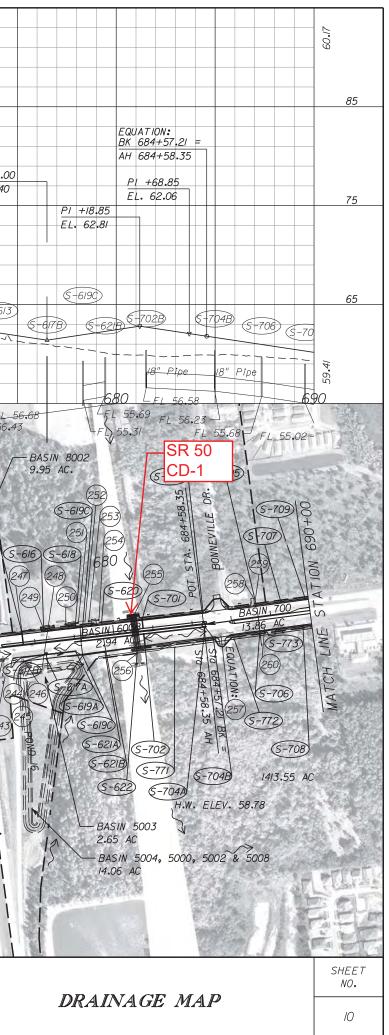
PLANS UPDATE PERMIT SUBMITTAL SEPTEMBER 2012

 ROADWAY PLANS ENGINEER OF RE

Y PLANS ER OF RECORD (E.O.R.): .					
P.E. NO	41832				
		F ISCAL YEAR	SHEET NO.		
		14	/		

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	S-536 S-542 S-546 FL 75.86	(S-552) S-554 S-556 (S-558)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
(S-506) (S-500)	Feet 5-539 (5-543) (5-539) (5-543) (5-534) (5-544) (5-534) (5-544) (5-547) (5-534) (5-544) (5-547) (5-534) (5-544) (5-547) (5-534) (5-544) (5-547) (5-534) (5-544) (5-547) (5-546) (5-546) (5-547) (5-546) (5-546) (5-547) (5-546) (5-547) (5-547) (5-547) (5-546) (5-547) (5-547) (5-547) (5-546) (5-547) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) (5-57) ($\begin{array}{c ccccccccccccccccccccccccccccccccccc$	SECTION 23 1223 10 STA, 660+57.60 POND 19 S-589 S-589 S-604 S-600 S-614 S-612 T
CONSTRUCTION PURPOSES. THIS SHEET FOR DOCUMENTATION AND TO ASSIST CO PERSONNEL WITH DRAWAGE CONCERNS. REVISIONS DATE BY DESCRIPTION DATE BY	IS IN THE PLANS	LOCHNER C.A. 894 H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 13577 FEATHER SOUND DRIVE, SUITE. 600 CLEARWATER, FLORIDA 33762 THERESA D. ELLISON, P.E. NO. 53918	2159.46 AC BASIN 5005 5.88 AC. BASIN 5005 5.88 AC. BASIN 5005 5.88 AC. COUNTY FINANCIAL PROJECT ID S.R. 50 ORANGE 239203-4-52-01

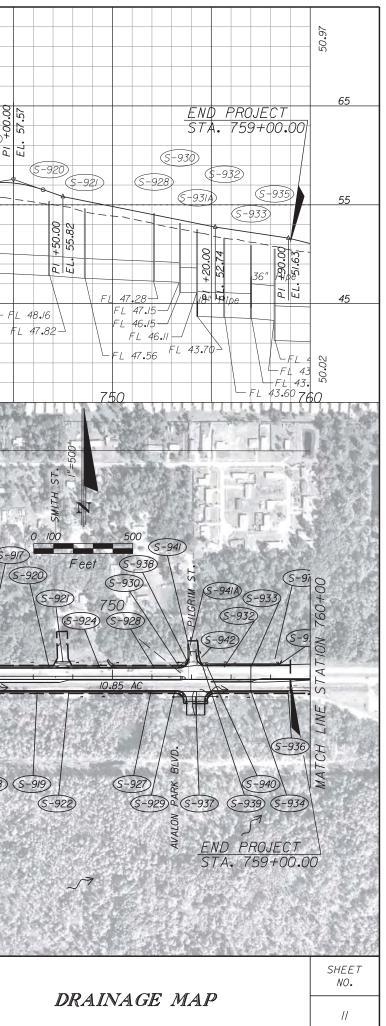
9/6/2012

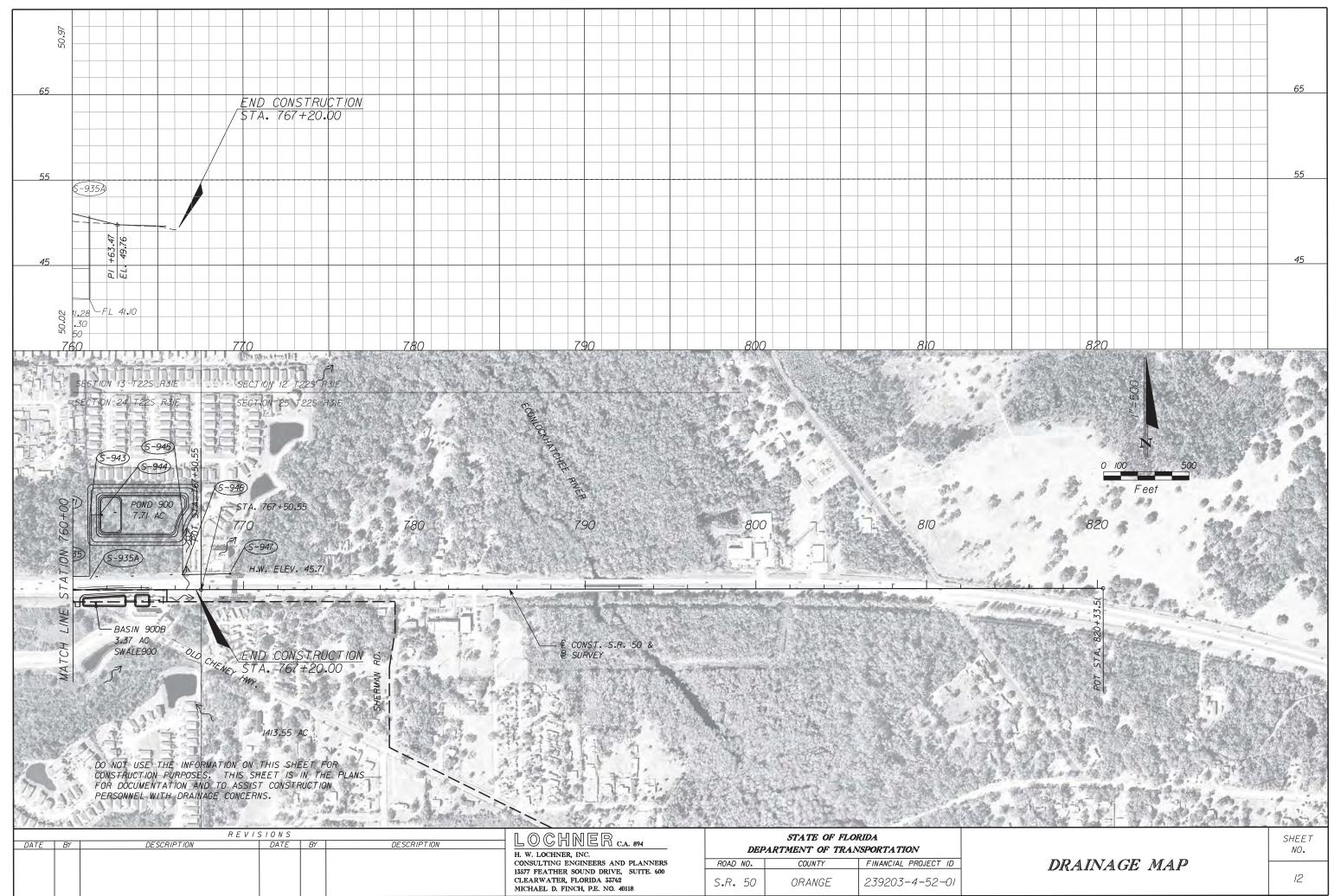


^{\\}nasclr0l\design\design\d5\42l0_sr50\2392034520l\drainage\drmprd03.dgn

2/				
60.17	00.021 BEGIN_BRIDGE G_+ STA. 710+00.92	CULVERT END BRIDGE	CULVERT	
65	PI ELL	22-0-000		2975 2975 EEFT
	\$-713B \$-717B \$-711B \$-715B \$-719B \$-722B	23.52 <i>EL</i> . + <i>F</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i> <i>B</i>	(S-825)	R S-901 S-905 S-909 S-917 -8270 S-833 S-903 S-907 S-917
-			(5-8/2)	S-912 S-912 S-915
55		S-73) (S-807)		
- - -	54.13			0: - FL 54.23 0: - FL 53.86
-	L 53.58- FL 53.46 FL 53.25- C 00 S 0 S 0 S 0 C 0 S 0 C 0 C 0 C 0 C 0 C 0 C 0 C 0 C		-FL 51.70 FL 52.91-	FL 53.68 FL 53.68 FL 53.10 FL 53.10
45	FL 52.87	FL 49.3 5 5 FL 450 FL 49.00 FL 48.9	7.00 IL JZ. TI	FL 53.70 FL 53.55 FL 53.65
-	FL 47.95 - FL 47.68 FL 47.20 - FL 47.20 - FL 47.00 - FL	FL 48.4 D FL 48.2 FL 47.78	FL 49.80 FL 45.66 FL 46.06	FL 53.27 FL 48.80 ////////////////////////////////////
9 59.4I		FL 47.56	FL 46.87 FL 46.87 FL 46.87	7.30 7.40
	SR 50	The average of the second seco	SECTION 13 T225 RUE SECTION 24 T225 RUE	
	CD-2 742 742 743		(S-814) (S-836) (S-840)	
	41.78 AC (S-738) (S-723) (S-712) (S-714) (S-718) (S-712) (S-714) (S-718)	S-730 S-734 S-8 POND 700 3.45 AC J	337) (S-838) (S-816) (S-839) (S-84)	S-913A S-913A S-913B
	S-712 S-714 S-718 a S-727 S-710 S-716 HAV	-744		3 5 -829 5 -901 5 -913C 5 3 5 -829 5 -903 5 -909 5 5 -913C 5 3 5 -832 5 -903 5 -909 5 5 -915 -915 5 -915 5 -915
690+00	700-	0 (S-803)	POND 800 5.08 ACT 20	<u>5-843</u> 12 730 740
ON 65	S-720	5-80		9.05 AQ
STATI	BASIN 700 ; 13.86 AC		AASIN 800 7 10.52 AC	
LINE S	G-774			
ATCH L	5-719	5-804		ber 23
MAT	(S-71) (S-715) (S-72) (S-725) (S-7	29 (S-733)	5-812 (5-825) (5-	-828 S-830 S-834 S-903A S-906 S-910 S-914 S-918
	(S-713) 2159.46 AC	5-73) (5-735) (5-802) (5-807) (5-837)	└── € CONST. S.R.	50 & (\$-933) (\$-902) (\$-908) (\$-911) (\$-916) 413.55 AC
14		H.W. ELEV. 51.38 2000	₿ SURVEY	SR 50 CD-4
	DO NOT USE THE INFORMATION ON THIS SHEET FOR CONSTRUCTION PURPOSES. THIS SHEET IS IN THE	PLANS	STA. 714+07.07	
	FOR DOCUMENTATION AND TO ASSIST CONSTRUCTION PERSONNEL WITH DRAINAGE CONCERNS.	SR 50 CD-3		Partition Brotha
DATE BY	REVISIONS DESCRIPTION DATE BY	DESCRIPTION	LOCHNER C.A. 894	STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION
	4 50		H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 13577 FEATHER SOUND DRIVE, SUITE. 600 CLEARWATER, FLORIDA 33762	ROAD NO. COUNTY FINANCIAL PROJECT ID
			MICHAEL D. FINCH, P.E. NO. 40118	S.R. 50 ORANGE 239203-4-52-01

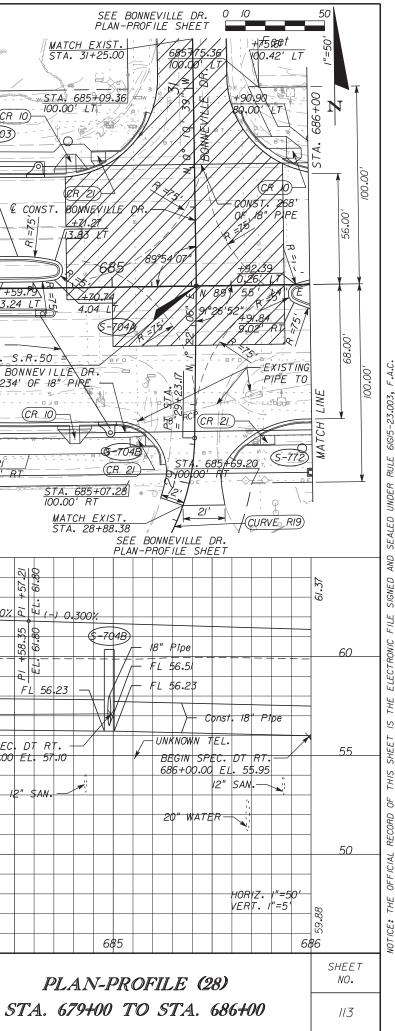
dholden

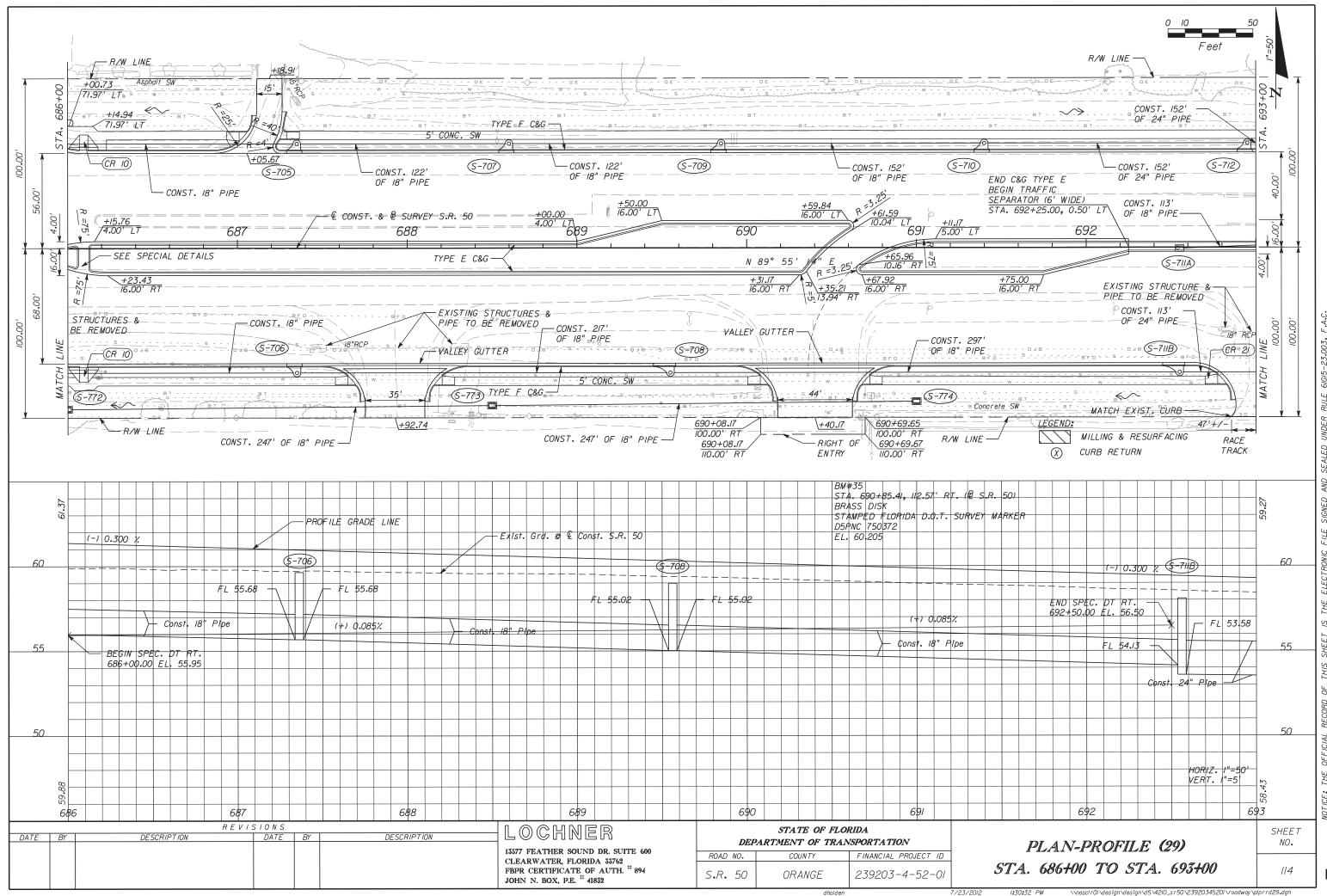




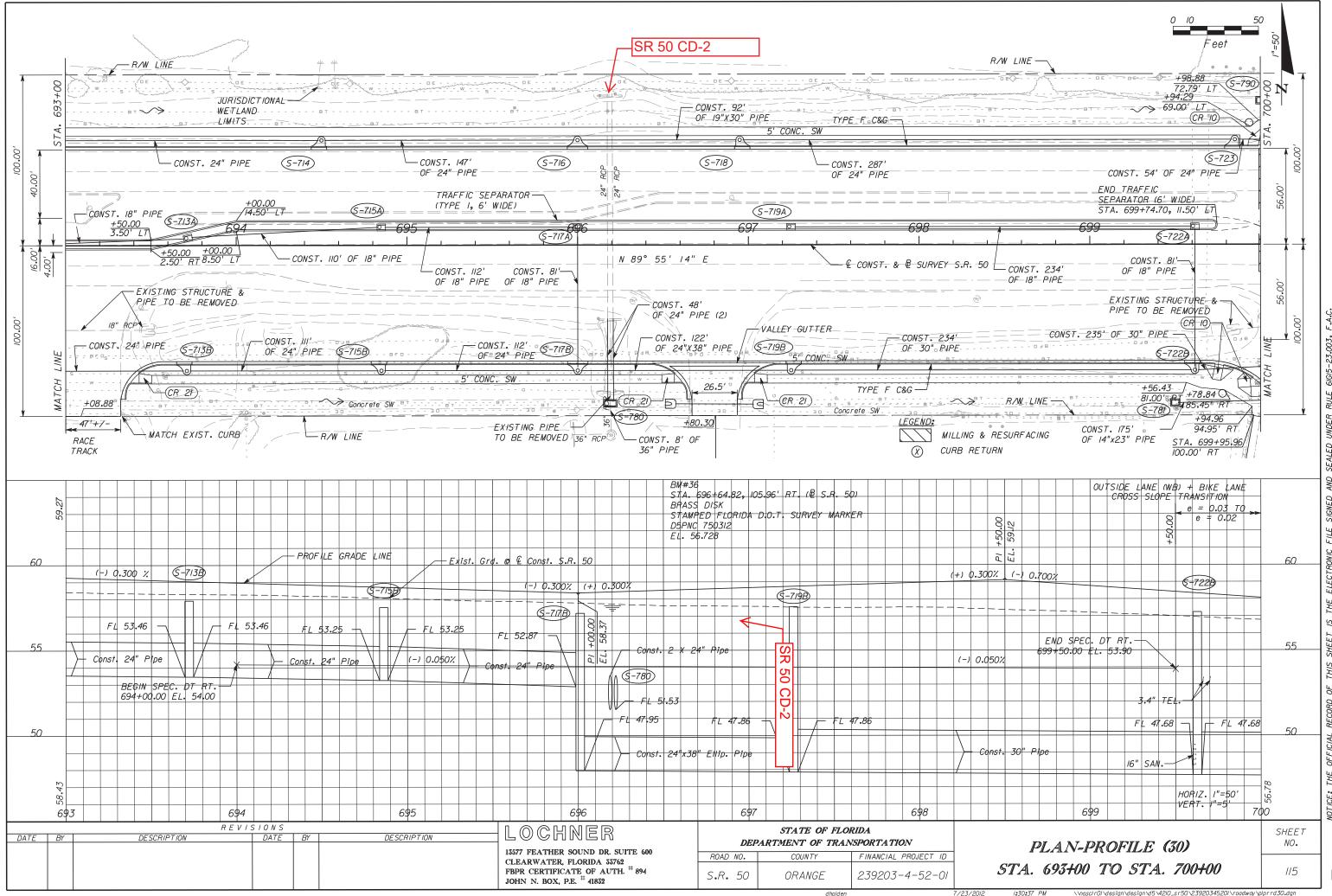
dholden

	SR 50 CD-1]		
+06.21 	END STEEL HANDRAIL/ WING WALL STA. 681+39.68, 80.83'_L1	: 	JURISDICTIONAL — WETLAND LIMITS	R/W LINE
Asphalt SW Brown 24 TO BE REMOVED		<u>у ліс</u> У Т	PAR	D. GUARDRAIL W/ <(RALLEL END ANCHORAGE (\$-7) A. 684+28.22, 57,50' LT
	(s-70) — 5' CONC.	SW		
	ST. 158' OF 84" PIPES = = = = = =	<i>C0/</i> 	NST307'-0F-19"-X-30" F 	PIPE
	682		683	684
CONST. 18" PIPE 680 5 89° 04' 46" E 687 2 4		TYPEEC&G	<u> 683 </u>	
	\$-702.			<u> </u>
EXISTING BOX CULVERT	RISDICTIONAL TLAND MITS CONST.61'_OF 8"_PIPE	TRAFFIC S — — — — — — — — — — — — — — — — — — —		CONST. 67' OF 18" PIPE STA. 685+42.53 € CONST STA. 30±00.00 € CONST.
EEGIN STEEL PICKET RAILING/	END GUARDRAIL TYPE-II END-AI STA. 681+71.22,	W/	OF JOTAL STREET	CONST.
ВЕGIN 8' SW EXIST. FENCE 5TA. 679+10.38, 108.56' - RT вт. (ТО. REMAIN). вт. , 8', CONC. SW Asphalt SW , , , , , , , , , , , , , , , , , ,	€_702B CONST. 16 18" PIPE	B' OF TYPE F C&C	5-771 +00.91 84.00' RT	<u>+57.2</u> <u></u>
L/A R/W LINE 3" DITCH PAVEMENT	, ND'STÉEL PICKET `RAILING 'ING WALL TA. 681+43.49, 87.41' RT	+17.31 103.20' RT	L/A R/W LINE CONST. 25	99' OF 18" PIPE
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	702B			
STAL 601719.50, 100.95 RT. 12 S.R. 301 END SPEC. DT 17. BRASS DISK STAMPED FLORIDA D.O.T. SURVEY MARKER D5PNC 750371, EL. 60.448 (+) 50.000% LT-		E GRADE LINE (+) O.	300% (-) 0.300% N	(-) 0.30
(+) 0.300%	Exist. Grd. @	€ Const. S.R. 50		
60	F_{-} FL 56.58 (+)	1.640%		╌╡═╪╼╞╼╡═╪╼╞╼╡═╪═╞
$DP_{I} LT. \qquad \frac{680+80.67}{57.57} = 0.H.W. = 58.57$				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	FL 56.58		Const. 19"x; EIITp.	. Pipe (+) 0.050%
55 Const. 18" Aipe			BEGIN SPEC	C. DT RT. END SP
DP/ UT. (-) 2.900;	DPI RT. 681+40.19		683+00.00 L C. DT RT.	
	EL. 57.73	682+50.00	EL. 59.53	
(-) 15.935% LT.	(+) 50.000% RT. DPI RT.			
50 DPY LT.	681+25.85 EL. 50.56			
EL 50.96 DPI RT. (+) 0.000%				
680+93.59 LT. AND RT. EL. 50.56 DPI LT.				
681+23.7 681+23.7 681-23.7				
679 680 681 681	682		683	684
R E V I S I O N S DATE BY DESCRIPTION DATE BY DESCRIPTION	LOCHNER	}	STATE OF FL DEPARTMENT OF TRA	
	13577 FEATHER SOUND DR. CLEARWATER, FLORIDA 3 FBPR CERTIFICATE OF AU JOHN N. BOX, P.E. [#] 41832	SUITE 600 5762 TH. [#] 894	NO NO. COUNTY R. 50 ORANGE	FINANCIAL PROJECT ID 239203-4-52-01
	JOHN N. BOX, P.E. ⁺⁺ 41832		dholde	



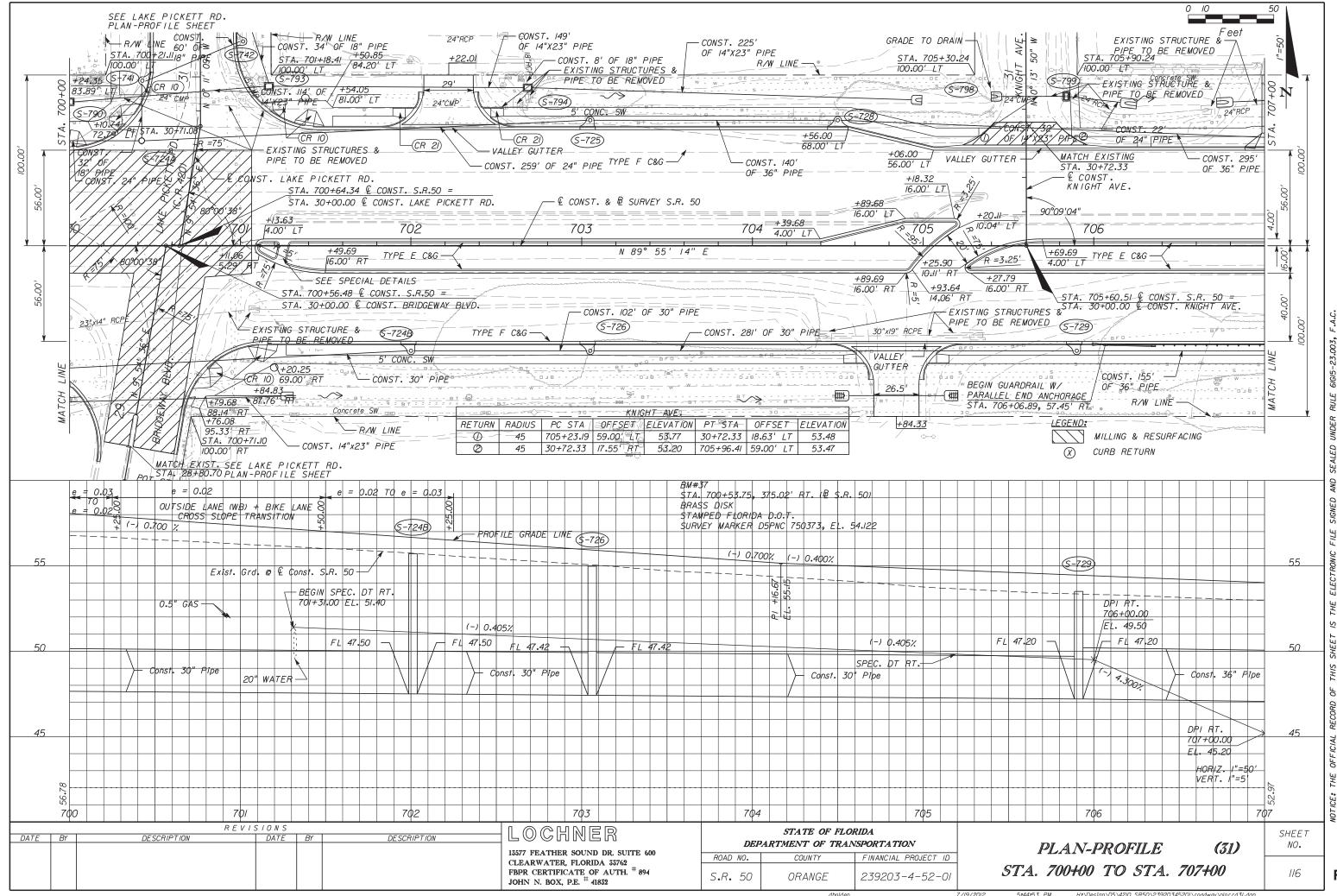


R-6



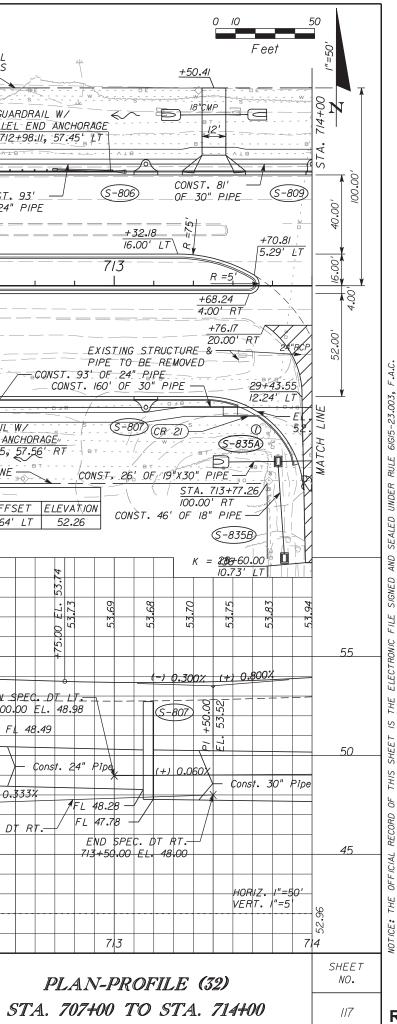
R-7

^{\\}nasclr0l\design\design\d5\42I0_sr50\2392034520l\roadway\plprrd30.dgn

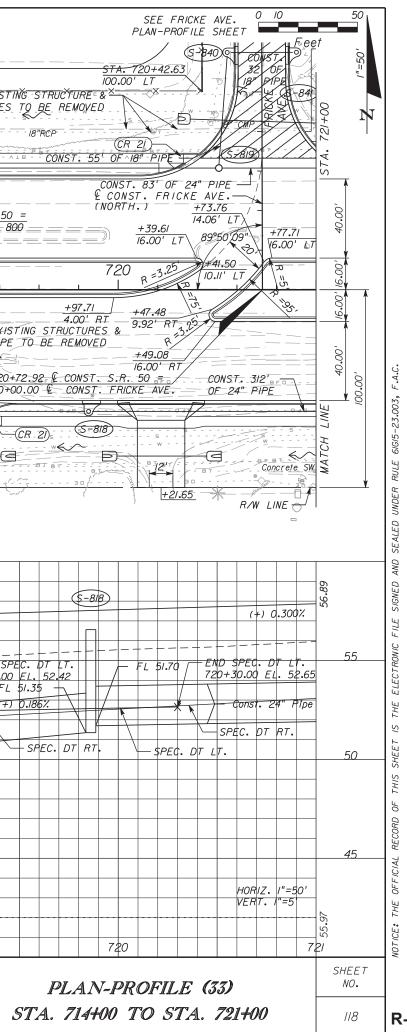


R-8

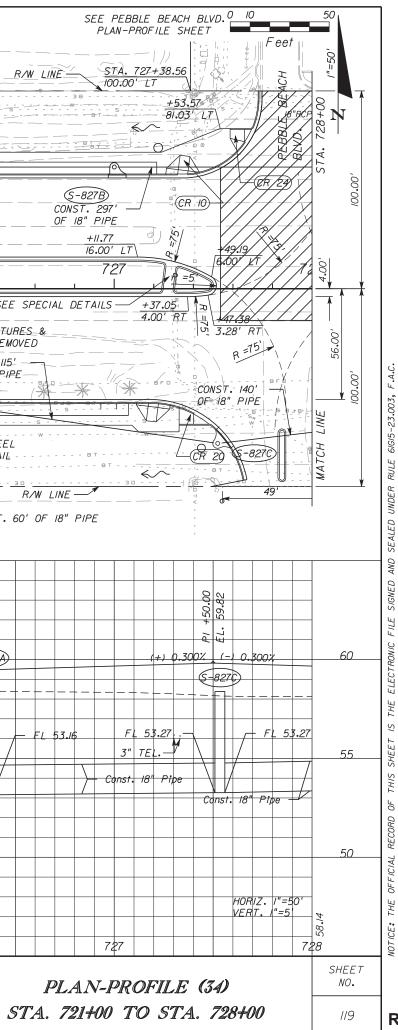
						_	I :-					х		PERI	PETUA	L DRA	INAGE	EASEMEN		T114 ·	004.00					
		l	R/W LINE 707+39,96	ROND TOO		×	- <u>+43.2</u>	<u>2/</u> × 16'DBLSW	<u> </u>	B E 120.00 ATE	209+65.62, 	STA		65.62		·			PERPE	TUAL	DRAIN.	AGE EAS	_	JURIS WETLA R		IMIT
		707+00	+10.52 R/W LINE 24' 24"RCP	IRCP		127 PIPF		WING WA	TEEL	PICKET RAILI, 00, 83.00' LT	NG/	2 PA	学习社会				RUBBLE DIT <u>CH</u> END	100:0' x RIP RAI <u>LINING</u> (11 STEEL P1	IDER 28 CKET R	AILING			W	- <u>S</u>	7	END C
		STA.								DNC. SW				BT			WING -	WALL 710+50.00	вт				T - ^ 18 -		 	\$7A.
			<u>S-730</u>	-		CONST. 142 OF 18" PIF	E	(5-/34)	TYPE	GUARDRAIL W 11 END ANCHC 708+78.75, 57	RAGE			/2.95 W	TYPE F	- C&G	<u> </u>	S-80		CONST	. 107' PIPE			(S-80.	<u>▲</u> <u>}</u>	CONS
	56.00'		└── CONST. 36"		KISTING ST PE-TO-BE		0 E	2 CONST. POND 700 +69.6	<u>BEG</u> 59 STA	N BRIDGE CU	VERT.75	0833		x 8.50	/		T. 151' 2' x 8	OF CBC								
		4.00'		=	708	89°48'25	# / 	4.00'	LT ZO	+/9.69		1-		т В ох Ох				7/	T = 7	<u> </u>	CONS	ST. & Ø	SURVEY	s.r. 5 712	50	
	16.00'				NST. 118' 36" PIPE	*				16.00' TYP	LT E E C&G -			CULVER				89°55'	14"	<u> </u>				<u> </u>		<u> </u>
		(C(DNST. JACK BORE PIPE							+92.18				4.00'	<u>RT</u>									
	40.00'					<u>ST. 142'</u>	-BFO	STA. 100	+00.00	6 € CONST. 4	S.R50⊫ POND 700			BFD	\	END STA.	3RIDGE 710 + 20	6.55	.75002		CONST			BFD		
			S-731			· · · · · · · · · · · · · · · · · · ·		<u> </u>	35)— -	EXISTING WALL TO	BE REMO	VED						<u>(\$-80;</u>	2	(OF 18'	" <i>PIPE</i>		(5-80-	∮ →	
		LINE						T- RAILING		DNC: SW	E F C&G -		//			- sy	5		s,	s		0 J 8	<u>s</u>		ID _s GUA	RDRA
		MATCH	- CONST:	-~~~~~~~ <u>\</u>	JUR ISDIC		00.00, 79	.58' <u>R</u> T								Q WI	IG WAL	EL PICKE L≪∽ +50.00, 7			BT	· · · · · · ·	BT	\ <u>77</u> <u>57</u> ₈	<u>PE 11-</u> A. 712	<u>END</u> 2+01,2 2/W LI
	¥		LEGEND:		WET_LAN_D					<u> </u>		1795	<u>7937</u>	S-7	36		<u>***</u>				HA	NCOCK L	ONE PALI	 		
			×××	MILLING & R CURB RETUR	N.		SR	R 50 CD	9-3	//	ONST. 150 RUBBLE RI DITCH LINI	IP RAF))		3 M/#3 9					70 56	•00' RT	ELEVAT IC 52.76		7 57A 3+96.67	
				HEADWA	0+42.91, 88	3.02' LT. ED FLORID	(B S.R. 5) A D.O.T.	50) SURVEY N	IARKER	, , , , , , , , , , , , , , , , , , , ,			8	24	2 2	57A . 4x4 VITH	710+68 CONC. BRASS		RT.	(BS.F FLORI	R. 50) DA			+		
				D5PNC 8. EL. 50. 5.	750374 .752						DEILE GRA	DE LI	00.00+ /	-i	L E	D.D.T. EL. 4:	SURV 5.036	2, & CD-3) <i>BM#</i>	70 EI	LEV 4	6.39				
	55					– Exist. G	rd. @ 4	Const. S.R	50 (5-75				۵.	(-) 0.300)				ω	-802)					+	5-804	
			(-) 0.400%	(+) 0.300%																						BEGIN
			5-731	FL	-49.00		FL 4	49.34					<u> </u>	736 = Cons	it. 2 X	12'	 к в' С	BC's		\overline{F}	49.	32	 FL 48.99	,+		713+
	50)	<u> </u>			- Const	. 18" Pîpe	e		<u>BEGIN BRIDGE</u> STA. 710+00.9		1508.				<u>v</u> _0	. <i>H.</i> W.	= 50.04) - Con	nst. 18" 1	Pipe		\square
			FL 47.00	Const.	36" Pipe			DPV RT. 709+00.0		BEGIN SPEC. 709+50.00 E	DT LT.	7					RIDGE 10+25.	CULVERT 92	750833				.00			(+)
						SF	PEC. DT	EL. 45.10 RT.	<u>, </u>								I RT.		PEC. D .00 EI.	T <u>LT.</u> 47.13	3.000	EL. 47.)%.	50			SPEC.
-	45		DPI RT.	(-) 0.0	050%				+			709	LT. +99.54 40.82	DP1 LT. 710+26.0 EL. 40.8	4 /	o //()+48.4 . 44.2				PI RT 11+00.0					
			707+00.00 EL. 45.20					(-) 25.00>	;	\mathbf{A}	J. J	-500				-	DPI R 710+31	7.00			L. 44.			+		
		52.97						DPI R 709+15	5.00	×	(+) 0.0						EL. 4									
E		70			708 REVIS	SIONS		EL. 41	.35709			\square		0+) 0.006%]ER	:		_	7		TATE	OF F	LORIDA		712	—	
	DATE	BY		SCRIPTION		DATE	BY		DESCRIF	PTION	1357	7 FEAT	HER SOU	JND DR. SUI	TE 600			DE ROAD NO.			OF TR	ANSPOR	TATION		ID	
											FBF	R CER	TER, FLC FIFICATE OX, P.E.	ORIDA 33762 2 OF AUTH. [#] 41832	# 894			S.R. 50		ORAN			9203-4-			
																					dhol	den			7/19	/2012



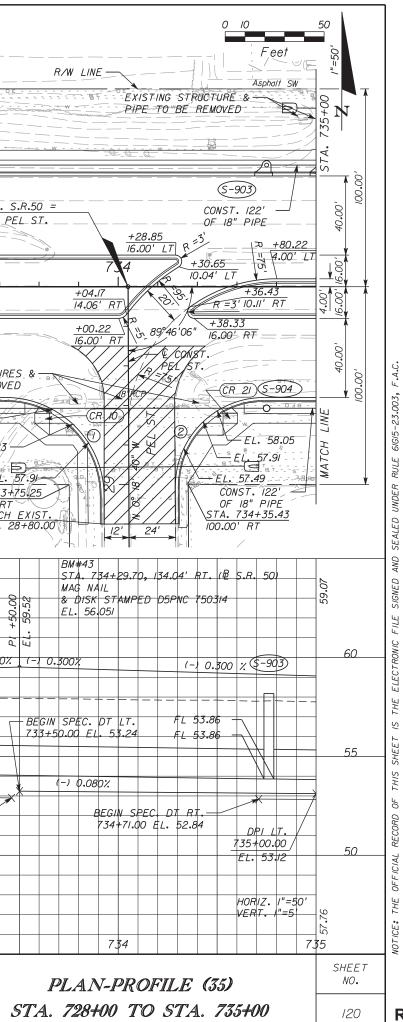
			CONS t. 369		I F	+75.68	POND 800
	+40.00	R/W LINE	OF 24"-PIF				
			TYPE B FENCE	., ., ., .,	×××	<u> </u>	×
Î		24		RAP	w	<u>—</u> 🛛 сол\$т. ғ	POND 800 PIPE
			DITCH_LINING	CONST. 99'		<u></u>	-8
				С			m.B.J.J
			5' - CONC .^ -\$\$\$\$*				
00.00	(9-809) CONST. 266'					— CONST. 227'	
100	DF 30" PIPE VALLEY GUTTL	ER/	<u>(S-814)</u>	OF36"PIPES	-816 ≥	OF_24"PIPE	€ CONST. S.R. 5
56.00'	STA. 714+07.06 & CONST. S.R.50 =	NF PAM RD					B CONST. POND
56.	- +82.21				2.21 90°00'00"	<u> </u>	
4.00	$\frac{1}{2} + \frac{1}{43.57} - \frac{1}$	— — — — — 716— ¹	€ CONST. & ₽ SURVEY S.	$\frac{R.}{2} \frac{50}{2} - \frac{+72.21}{4.00' LT} - \frac{16.0}{24}$			719 — — — —
							<u> </u>
l î î	$\frac{1}{R} = 5'$ TYPE E C&G	N 89° 55′ 14″ E	+50.00	CONST. JACK			
	89°53'08" + 26.24 + 46.15 _	+00.00	4.00' RT	AND BORE PIPE	STRUCTURES &		FX
56.00'	-X/// 20.00' RT - 16.00' RT		PIPE TO BE REMOV		BE REMOVED		EX P#
26	2 CONST. HANCOCK LONE PALM RL 29+64.37 EXISTING STRUCTURE 10/11/9T TO BE REMOVED		CONST	. 750'		CONST 161' -	18"RCP
	8 1 10.41/ RT 10 BE REMOVED	- BFO				LLEY GUTTER	STA. 72
<u>∗</u>	29+33.89						31A. 30
		5' CONC. SW					
	CONST. 30" PIPE	TYPE F C&G			s	(CR 21)	
	CONST. 64 ¹ 0F 19 ¹ × 30 ¹¹ PIPE		BT -				24
			443.00 	+72.48	<u> </u>	BT 	
	STA. TI4+37.26	RESURFACING		K LONE PALM RD.			<i>↓ <i>+II</i>.<u>33</u></i>
	TOO.OO' RT (X) CURB RET	TIE TO			ET ELEVATION		1
	28+60.00						
	12.27' RT MATCH EXIST.	BN#40					
	STA. 28+60.00	STA. 720+59.53, 255.	-71' LT (B S.R. 50)	56.85			
		BRASS DISK STAMPED FLORIDA DU	0.7.		(5-817)		
		SURVEY MARKER D5PN	VC 750375, EL 55.510 \$-812	(+) 0.800% (+) 0.300%			
	PROFILE	GRADE LINE		xist. Grd. @ & Const. S.R. 50		DPI RT. 719+00.00	
55	S-BID					7/9+00.00 EL.52.00	
							719+06
	BEGIN SPEC. DT RT. +						
						9.80	
	BEGIN SPEC. DT RT. 714+50.00 EL. 50.90		50.00	(+) 0.244%	FL 4		*
		+) 0.244%.	50.00			526%	t. 24" Pipe
		+) 0.244%.	50.00 49.19 (+) 3.300 ⁷ /	(+) 0.244%. 		526%	t. 24" Pipe
50			50.00			526%	t. 24" Pipe
50		+) 0.244% EL. ·	50.00 49.19 (+) 3.300 ⁷ /		(+) ().526% - Cons	:t. 24" Pipe
50	Const. 30" Pipe	+) 0.244%.	50.00 49.19 (+) 3.300 ⁷ /		(+) (526%	:t. 24" Pipe
50		+) 0.244% EL. ·	50.00 49.19 (+) 3.300 ¹ FL 46.37		(+) ().526% - Cons	:t. 24" Pipe
50 45	Const. 30" Pipe	+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe	50.00 49.19 (+) 3.300 ¹ FL 46.37		(+) ().526% - Cons	:t. 24" Pipe
	Const. 30" Pipe	+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe	50.00 49.19 (+) 3.300 ¹ FL 46.37		(+) ().526% - Cons	:t. 24" Pipe
	Const. 30" Pipe	+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe	50.00 49.19 (+) 3.300 ¹ FL 46.37		(+) ().526% - Cons	:t. 24" Pipe
45	Canst. 30" Pipe	+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe	50.00 49.19 (+) 3.300 ¹ FL 46.37		(+) ().526% - Cons	:t. 24" Pipe
45	6 6 <td>+) 0.244% EL. ·</td> <td>50.00 49.19 (+) 3.300^{1/} FL 46.37 .87 .87 .87</td> <td> END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 Const. 42" Pipe D</td> <td>(+) C</td> <td>1.526% - Cons 42" Pipe</td> <td></td>	+) 0.244% EL. ·	50.00 49.19 (+) 3.300 ^{1/} FL 46.37 .87 .87 .87	END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 Const. 42" Pipe D	(+) C	1.526% - Cons 42" Pipe	
45	96 7 </td <td>+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe</td> <td>50.00 49.19 (+) 3.300^{1/} FL 46.37 .87 .717</td> <td> END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 Const. 42" Pipe L 45.90</td> <td>(+) C</td> <td>42" Pipe</td> <td>7/9</td>	+) 0.244%. EL. · (+) 0.060%. Const. 36" Pipe	50.00 49.19 (+) 3.300 ^{1/} FL 46.37 .87 .717	END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 Const. 42" Pipe L 45.90	(+) C	42" Pipe	7/9
45	6 6 <td>+) 0.244% EL. 4 (+) 0.060% EL. 4 Const. 36" Pipe FL 46.</td> <td>50.00 49.19 (+) 3.300^{1/} FL 46.37 .87 .87 .87</td> <td> END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 FL 45-90 Const. 42" Pipe I I I I I I I I I I I I I I I I I I I</td> <td>Const. A</td> <td>0.526% Cons 42" Pipe</td> <td>7/9</td>	+) 0.244% EL. 4 (+) 0.060% EL. 4 Const. 36" Pipe FL 46.	50.00 49.19 (+) 3.300 ^{1/} FL 46.37 .87 .87 .87	END SPEC. DT LT. 717+00-00 EI. 50-84 FL 46-06 FL 45-90 Const. 42" Pipe I I I I I I I I I I I I I I I I I I I	Const. A	0.526% Cons 42" Pipe	7/9
45	96 7 </td <td>+) 0.244% EL. 4</td> <td>50.00 49.19 (+) 3.300^{1/}× FL 46.37 .87 .87 .87 .87 .87 .87 .87 .8</td> <td></td> <td>Const. 4 Const. 4 Con</td> <td>A2" Pipe</td> <td>7/9</td>	+) 0.244% EL. 4	50.00 49.19 (+) 3.300 ^{1/} × FL 46.37 .87 .87 .87 .87 .87 .87 .87 .8		Const. 4 Const. 4 Con	A2" Pipe	7/9
45	96 7 </td <td>+) 0.244% EL. 4</td> <td>50.00 49.09 (+) 3.300^{1/} FL 46.37 .87 .87 .87 .87 .87 .87 .87 .8</td> <td> END SPEC. DT LT. 7/7+00.00 EI. 50.84 FL 46.06 FL 45.90 Const. 42" Pipe FL 45.90 7/ R. SUITE 600 R. SUITE 600 ROAD NO.</td> <td>COUNTY</td> <td>0.526% Cons 42" Pipe</td> <td>7/9</td>	+) 0.244% EL. 4	50.00 49.09 (+) 3.300 ^{1/} FL 46.37 .87 .87 .87 .87 .87 .87 .87 .8	END SPEC. DT LT. 7/7+00.00 EI. 50.84 FL 46.06 FL 45.90 Const. 42" Pipe FL 45.90 7/ R. SUITE 600 R. SUITE 600 ROAD NO.	COUNTY	0.526% Cons 42" Pipe	7/9



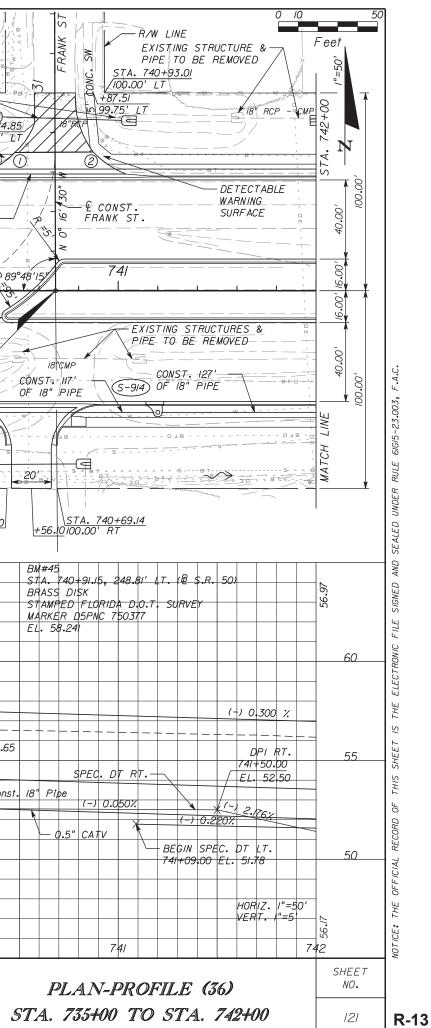
	8 8 8 8 8 8 8 8 8 8 8 8 8 8	RTW LINE	s	30 	38 38 5
	18 CMP CR-10 +27.62 83.99' LT	OVED BT TYPE_F_C&G		87 87	
	2 Z Z	5' CONC. SW			
100.00	<u>S-820</u> <u>CONST-24"</u> PIPE	CONST. 159' (S-822) DF 24" PIPE	CONST. 132' (S-824) OF 24" PIPE	CONST. 142'	(S-826) CONST. 117' OF 18" PIPE
		TYPE F CRG 723	€ CONST. & ₽ SURVEY S.R. 50	725	
16.00'		TYPE E C&G	<u>/ </u>	725	
16.0		+07.25 +57.25	<u>N 89° 55′ 14″ E</u>		
40.00'	IB" RCP	16.00' RT 4.00' RT 16.00' RT 4.00' RT G STRUCTURE & BE REMOVED	Plu IB"CMP		EXISTING STRUC PIPES TO BE R IB"RCP CONST. OF IB"
100.00	W VALLEY GUTTER		OF 24" PIPE	5-825 - BFD - CONST. 182'BFD OF 18" PIPE	C-827)
	HOLE MARKET CONCRETE SW 27'	5' CONC. SW. TYPE F C&G	S - 24'		A/L
¥	LEGEND: WILLING & RESURFACING CURB RETURN	R/W LINE	$\frac{1}{1} = \frac{1}{1} = \frac{1}$		
	29:30				
60			Exist. Grd. @ & Const. S.R.	50	
		FILE GRADE LINE			
55		(+) 1.000% FL 52.28	FL 52.28 FL 52.41	FL 52.91	FL 53.16
	Const. 24" Pipe ⁽⁺⁾ 0.526%		Const. 24" Pipe	Const.	. 18" Pipe
50	6.5" WATER		END SPEC. DT RT. 723+50.00 EL. 54.45		
	25.97				
	721 722 REVISIO		LOCHNER	5725 STATE OF FL	lorida 726
DATE	BY DESCRIPTION D.	ATE BY DESCRIPTION	13577 FEATHER SOUND DR. SUITE 600	DEPARTMENT OF TRA ROAD NO. COUNTY	
			CLEARWATER, FLORIDA 33762 FBPR CERTIFICATE OF AUTH. [#] 894 JOHN N. BOX, P.E. [#] 41832	S.R. 50 ORANGE	239203-4-52-01



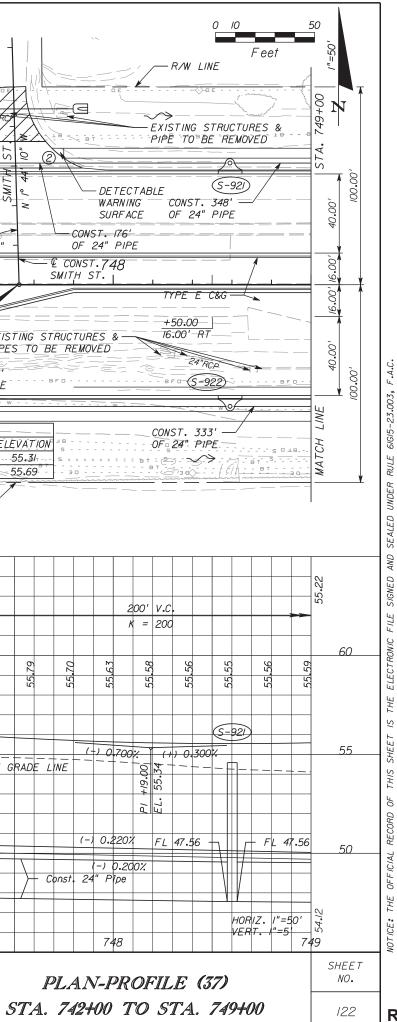
SEE PLA	PEBBLE BEACH AN-PROFILE SH	BLVD. EET	_							,												SR	50 C	<u>-</u>	1		1			
<u>.</u>			728+38.56 0' LT	5		1	R/W LI				/		<u> </u>	0									and a second s							
	A. 128+00 A. 128+00		+62.48 81.93 L +70.1	19	EXIST TO BE	ING STR	JCTURF	B-T-	"LAND	ONAL				<u> </u>	&G —		8 7				- w			w					Instantion B	
		20-7-7-		(0D 10)						<u>م</u>				7'															CONS	ST. 247'
00,001	20°00',00"/	& CONST FEBPLE + 35.58 V.09 LT	реасну ві	(<u>CR 10</u> VD.		-18"-P1P	E		-829			0	JNS1.9 - <u>18"</u> P	" IPE	5-83	2								-901	• 			(734+0	0F 18 04.93 0.00	8" PIPE © CONST © CONST. 0.00
4.00'		R =75'	SEE SF +56.27 /4.00' LT	72:		LS			7	30	 	<u>/</u>	€ CONS	ST. &	₽ si	JRVEY 731				30"RCP		732	2	<u>+50</u> 4.00	.00 '' LT\			13.	/ 16.0	00' <u>LT</u>
16.00'		R 5	·			3+02 . 54 +00 . 00 _4				EACH	BLVD+			TYPE	E C	&G —	*	N 89	° 55	5' 4" E										
00.00' 56.00'		+34.74 œ 8.20' RT NST 18"	PIPE_CON	EXIS RT TO	TING S BE REN	STRUCTUI MOVED				EXISTI	ING ST TO E	BE RE	URES E MOVED ONST S F 18" F			-833					т С	O BE	NG STR REMOV 42' PIPE	ΈD	B7	F 0		EXIS PIPE	TING TO	G STRUCTU D BE REMO
-		VZ-		205	828)		<u> </u>			5	5' -CON	IC SV		J			Z.,	S S S	;[s	Z			_ s † -		3	S		• ^{\$} 58.43
	ES 7 - CR-24	CR AW LINE	Ю 10 в т	(C	\sim		GUTTL 26' CONST.	58' (-856 &				(PE F -860	C&G -	- /) 3(- BT -		K.	(-&	л - w -	~> D		BT			1		ST. 247 18" PIPL		вт В-Т-	EL. 58.2
<u>¥</u> -			& RESURI	FACING	<u> (S-8</u> 5	<i>∠</i>	<u>18"'-PIF</u> 4.52	<u>S</u>			CC 18 ONST. 8" PIP	0NST. " PIP 8'0)F 		88.59			CONST 8" PII	. 18" . 46'		<u>(S-870</u>	Deres -	- 30 - 7	R⁄N	V LINE					<u>STA. 73</u> 100.24 <u>MAT</u> STA
	BM#41 STA. 729+ BRASS DIS STAMPED D5PNC 750 EL. \$8.278	к - LOR IDA - 376																				S M 8	1AG NA	IL STAN			:9' <i>RT (</i> C 75031:		_ 	
										PROF	ILE G	RADE	LINE			+00.00)		_		— Exis	t. Gra	1. @ É	Cons	t. S.R	. 50				
60				\$-828	-, 0	.300 %			6	-830)				(-)	0.30	àù		300%					\$	-901)				<u> </u>	(+) 0.30
																			/											
	- BEC 72E	+50.00	DT RT. <u>EL. 55.25</u> 53.55		F	FL 53,55	FL	53.70			F	L 53.		PI RT 30+50			S-83 DF 73	3) 11 RT. 1+50.0		\$-870)" Pipe			FL 54	4 <u>.2</u> 3			
55					4	(-) 0.30		=					L. 54	.65	=	EL	. 53./				\$7. 50						Const.	-18"	Pipe
	Consi	. 18" Pig	be	NK			— Cons.	t. 18"	Pipe \		$\succ c$	`onst.	18" Pip		+	\mathbb{H}	(-) /	650%	+				(-)	0.05	50%		/	+++	—	
			- 12" WATE	R										53.85				FI	L 52.1	18		F					END 733+46	SPEC. 5.00 EL	DT 1	RT
50																			_				+	\mathbf{r}				+	_	
				+											-				+					SR				+	+	
.	4																							50						
	28.14																					770	<u> </u>	CD-4						_
	728			729 REV	15101					30			<u> </u>	\square	<u> </u>	7\$1 N)				732	: 	- 1		FLORI	 DA	733	ע	
DATE E	BY	DESCRI	PTION		DA	<u>TE BY</u>			DESC	RIPT IOI	V		13	577 FE	ATHE	R SOUN R, FLOR ICATE (, P.E. [#]	ND DR.	SUITE 762		-	ROAD	NO.	PARTM		ΟΓ ΤΙ ΓΥ		PORTAT FINANCIAL 239203	L PROJE		_
													JO	OHN N	. BOX,	, P.E. ⁺⁺	41832				J •/ 1 •	50								7/19/2012

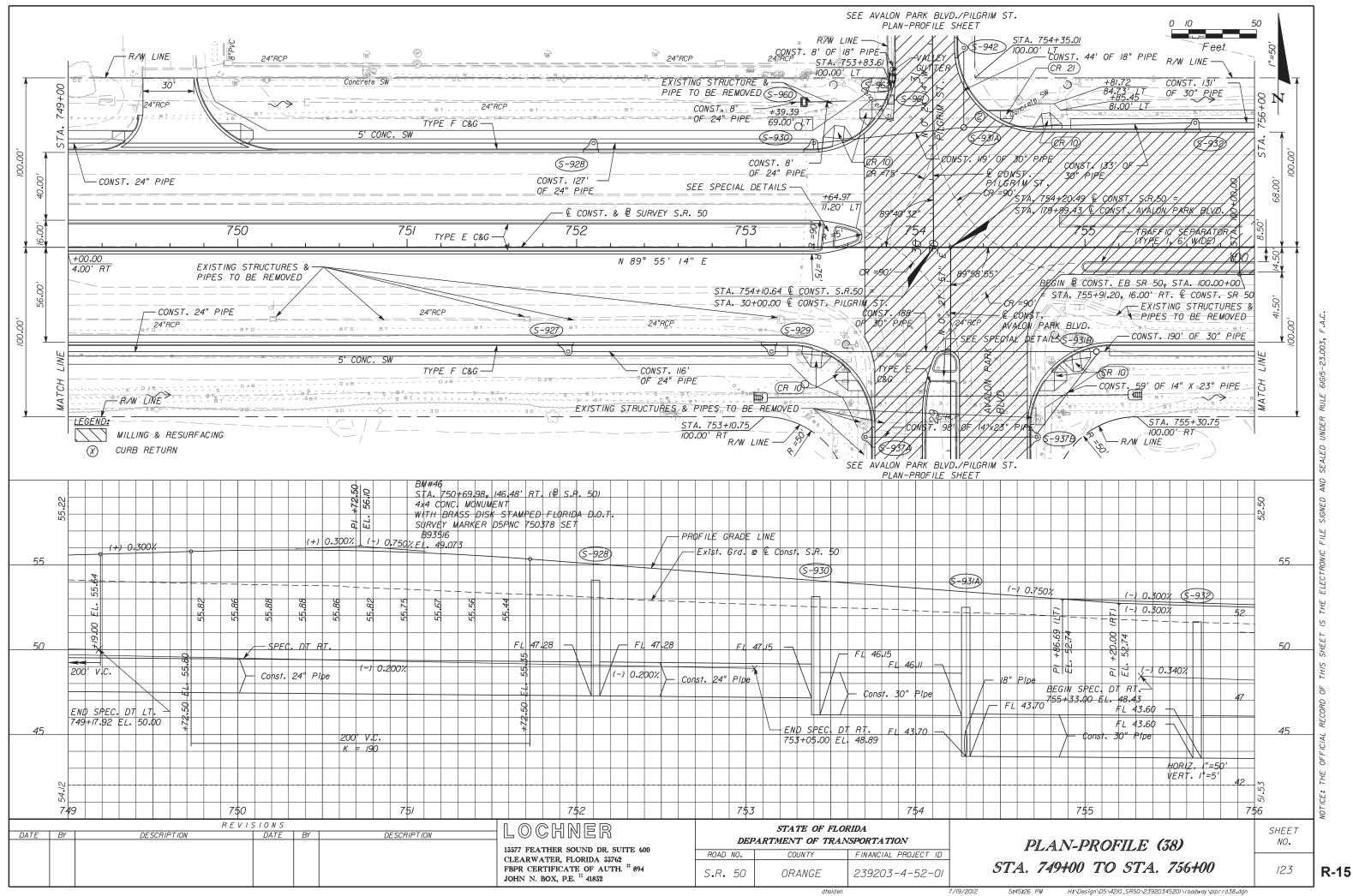


,00,001	52.00'	STA. 735+00	15" RCP +18.92 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Sphall SW		Exist Pipes		EMOVÉD		PE F CONC.	SW 907 CC			478.7, 24 18"CMP	AF	PIPES	ING STRU TO BE		S & ED 					CO	INE STING E TO E DETE WARN SURF SURF NST. 2 I8" P	BE RE CTABL ING ACE 247' -	MOVE	D 30+84 10.30'
			=			736	-€ CONST.	& & SUI		50 737				7	38					739)					74	10	R=3 R
	16.00' 4.00'						TYPE E	C&G -									89° 55	<u> </u>	Ē				<u> </u>				R =7	R=3'
,00°00/	40.00'	MATCH LINE	CONST18	R/W LINE	OF	NST. 127' - 18" PIPE -906 5' CONC. TYPE F 	C&G →		.35 59.00	SET D'LT		30+7	70.00	S B T -	24' 24' ELEV T 56				ED CONS	57. 137 8"							R/W	
		59.07																		E S C	3M#44 STA. 74(BRASS [STAMPE] SONTROL SONTROL	DISK D ORA L-60						
	60		(-) 0.30 		53.68	(5-905) 			FILE GRAD		<u>5</u> -907		— Ex — — — 53.48	ist. Grd.		Const. 53.10_	<u> </u>							FL 52		6-	912	
	55			- Const. 18) 0.080%					nst. 18" P	ipe					st. 18"	Pipe						Const.	. 18" F	Pipe	-) 0.05	50%		- Cor
	_50		(-) 0.05 DPI LT 735+00 EL 53									0.2237				SPEC.	SPEC.	DT RT.							END : 740+34	SPEC. 1.00 E	DT EL- 51	LT
		~ 27 . 76	35			7 3 6 <i>REVISI</i> 0				737					38					739		ATE	OF FL	OPID	4	74	10	
	DATE	BY		DESCRIF	°T ION		DATE BY		DES	CRIPTIO	DN		13577 F	EATHER SO WATER, FI WATER,	OUND D	R. SUI	TE 600 [#] 894		ROAD	NO.	PARTME		OF TR / Y	1NSPC		PROJL		

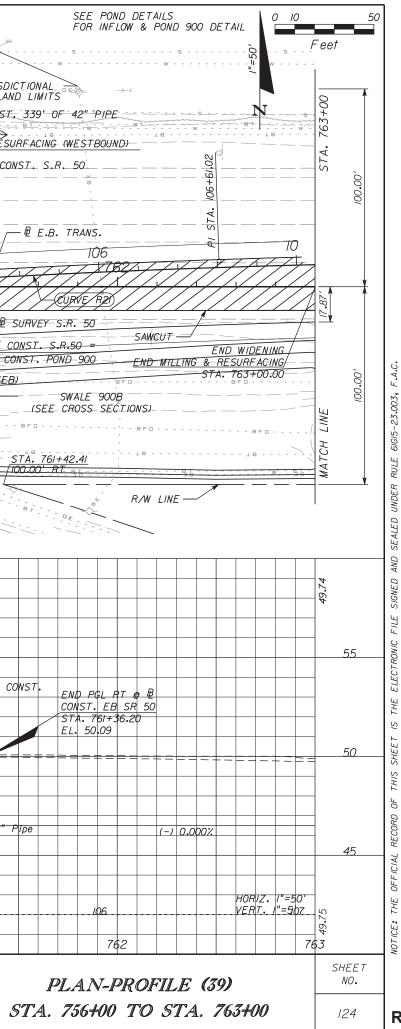


•	00 18" RdP - OMP 15' VISTING STRUCTURE & PIPE TO BE REMOVED	+79.16 EXISTING S PIPE TO BU 15' 15' E E E E E E E E E E E E E		RAW LINE DE H H BT BT BT	
40.00'	S-915 CONST. 92' S-917 OF 18" PIPE 	CONST. 332' TYPE F OF 24" PIPE		€ CONST. & ₽ SURVEY S.R. 50	S-920 DE TECTABLE WARNING SURFACE 88°20'35
16.00' 16.00'		744 TYPE E	C&G 745	746	
100.00' 40.00'	HOLENNE <i>CONST IB" - PIPE</i> <i>S-916</i> <i>OF IB"</i> <i>PIPE</i> <i>S-918</i> <i>OF IB"</i> <i>PIPE</i> <i>S-918</i> <i>OF IB"</i> <i>PIPE</i> <i>S-918</i> <i>OF IB</i> <i>S-918</i> <i>OF IB</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i> <i>S-918</i>	BT S DT TYPE F C	8F0 ₩ 8F0 QF 18" PIPE 8G 8G S S S S S S S S S S S S S	BF (5-919) SMITH RADIUS PC STA OFFSET ELE 45 747+12.92 59.00' LT	ONST. SMITH STREET PI
60			0.00% (-) 0.700%	Exist. Grd. @ Const. S.R. 5	
55	FL 51.89 - Grief Const. 18" Pipe Pipe Const. 18" Pipe Pipe Pipe Pipe Pipe Pi	SPEC. DT RT.		255 ¹ 95 50% 50% 50% 50% 50% 50% 50% 50	FL 47,82
DATE	DPI RT. Image: Constraint of the second se	- FL 48.16	$\frac{1}{745}$	746 STATE OF FLO DEPARTMENT OF TRAN	NSPORTATION
			13577 FEATHER SOUND DR. SUITE 600 CLEARWATER, FLORIDA 33762 FBPR CERTIFICATE OF AUTH. [#] 894 JOHN N. BOX, P.E. [#] 41832	ROAD NO. COUNTY S.R. 50 ORANGE dholden	FINANCIAL PROJECT ID 239203-4-52-01

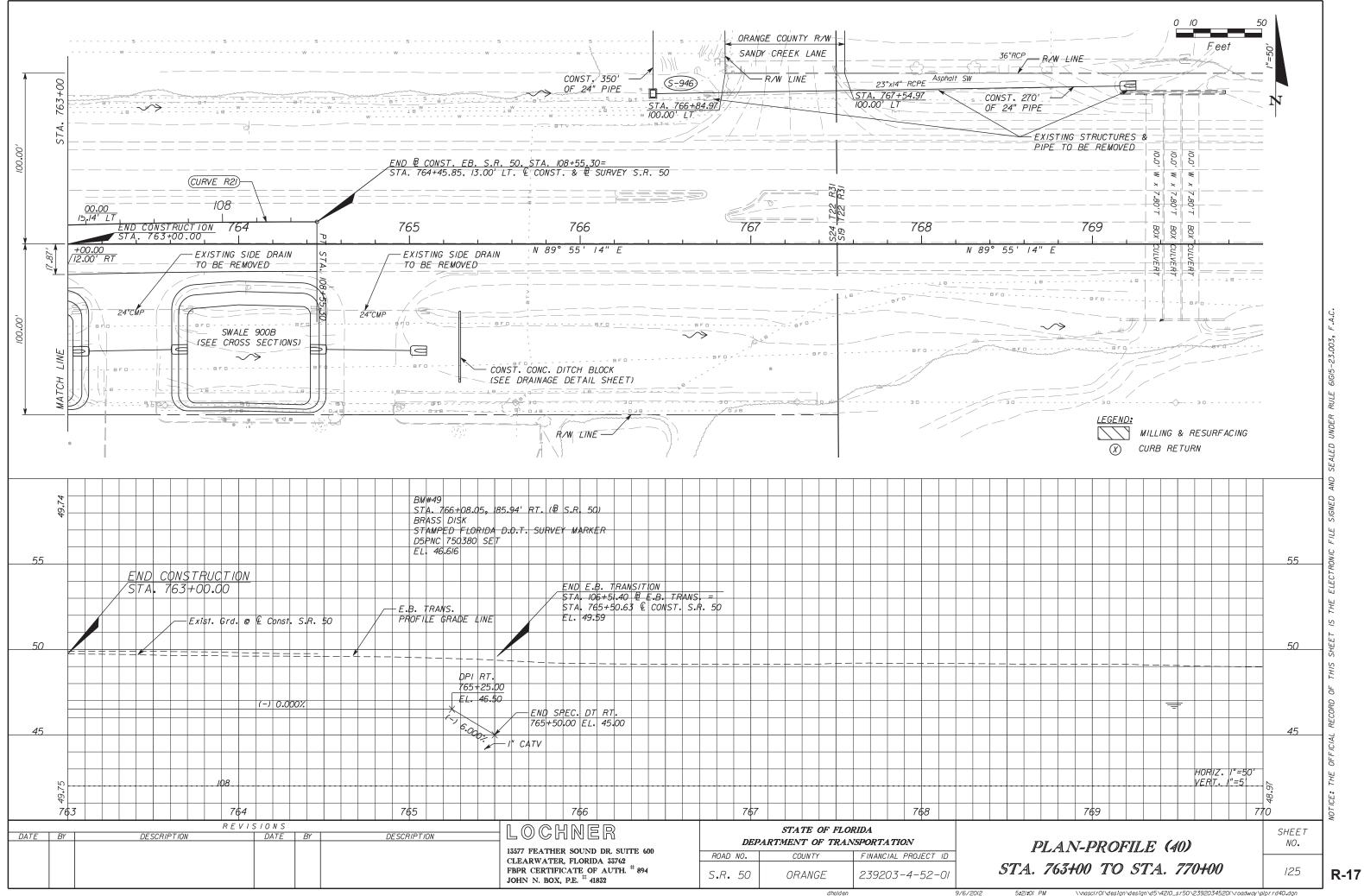




100.00'	56.00'	CONST. 30" PIPE	JURISDICTIONAL WETLAND LIMITS CONST. 8' OF 19"x30" PIPE 5' CONC. SW 5' CONC. SW 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	+56.67 99.37' LT	+06.00 100.00' LT +40.00 76.68' LT * +40.00 60.00' LT +40.00 60.00' LT END PROJECT STA, 759 +00,00 FREMOVE EXIST.	<u>θε</u> <u>700</u> 	A. 760+80.01 0.00' LT 8 6-9359 JURIS WETL CONS
×	NF 41.50' 41.50' 56.	409.72 409.72	102 TYPE I 102 TY	E C&G	N 89° 55' 14"	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	F5 90°00'00" 90°000
<u> </u>	52 50 MATCH 11	TYPE F C&G	$CUTVe = R22$ $P = STA = 102+33.3$ $Delta = 3^{\circ} \cdot 53^{\circ} \cdot 1$ $D^{\circ} = 1 = 233.39^{\circ} \cdot 5$ $T = 233.39^{\circ} \cdot 5$ $R = 6,878.00$ $PC \ STA \cdot 100+00.00$ $PT \ STA \cdot 104+66.59$ $E = ND \ PROJECT$	39 12.63" (LT) 58 91"		63.20 - H = 1 SHLDR. 	29 10.00' RT
	55 50	PGL LEF	LT OF & CONS	PANS P 57. 935 (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300% (-) 0.300%	2 0.600% 2 0.700% = = = = = = = = = = = = = BEGIN PGL RT @ BCONST. EB SR 50	PGL LT	
	<u>45</u> يو تو		Image: Fill 44.60 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30 Image: Fill 43.50 Image: Fill 43.30 Image: Fill 43.30	STA. 759+00 EL. 5/.73 FL 4/.28 	STA. 759+00 EL. 5/.74 SPEC. 1 Const. 42		FL 41-10 761+00.00 EL. 46.50 FL 46.50 FL 41-10 761
DAT	E B		DATE BY DESCRIPTION	LOCHNE 13577 FEATHER SOUND CLEARWATER, FLORI FBPR CERTIFICATE O JOHN N. BOX, P.E. # 4	D DR. SUITE 600		



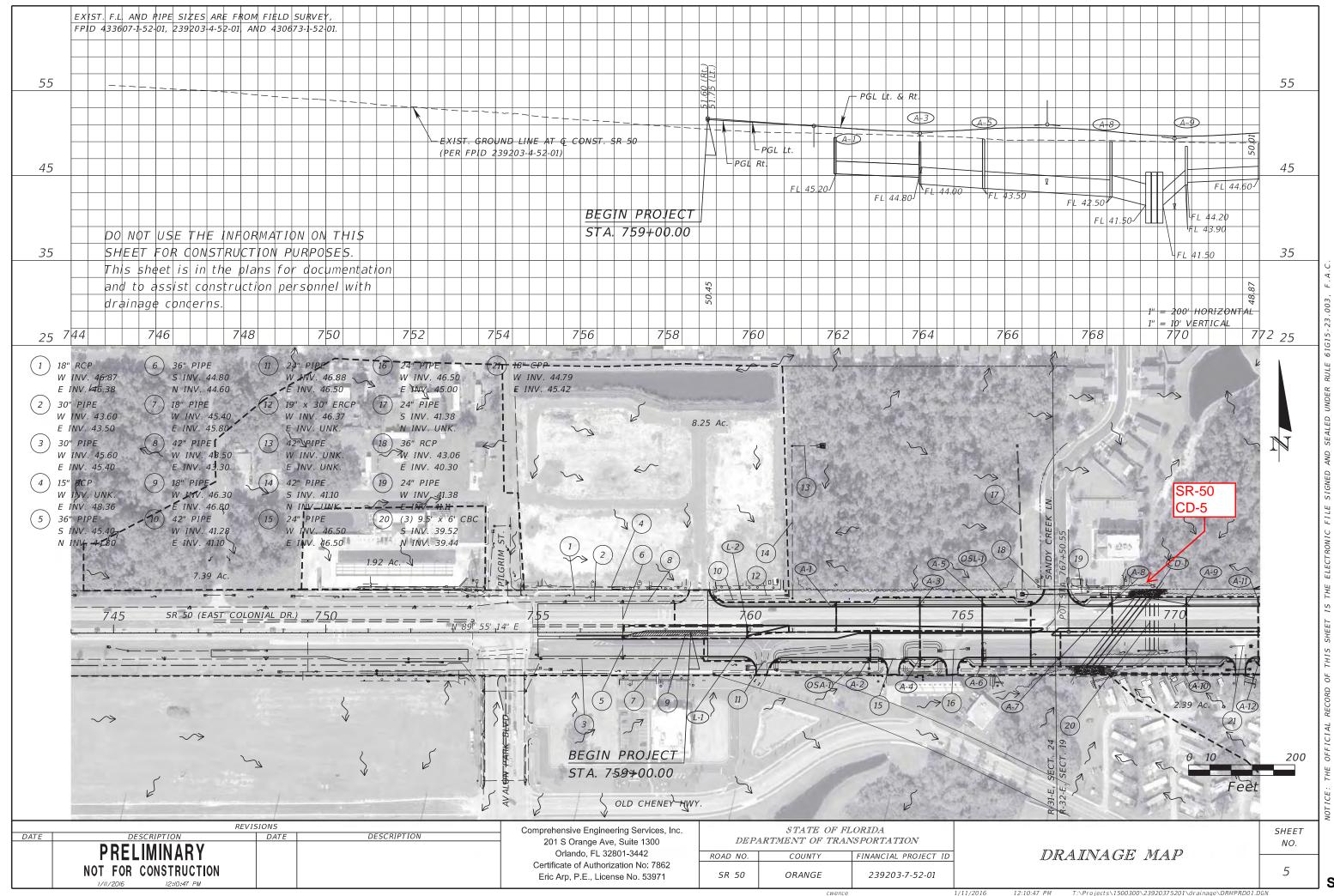
5:20:57 PM \\nascIr0I\design\design\d5\42I0_sr50\2392034520I\roadway\plprrd39.dgn



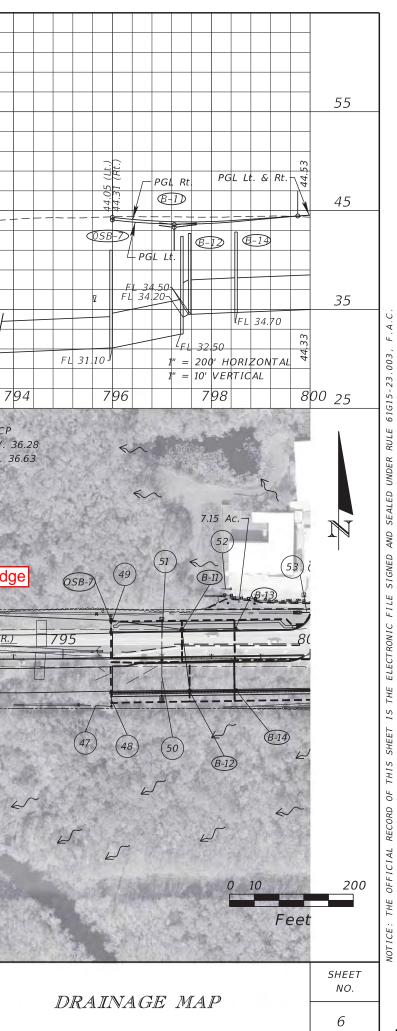
Appendix: S

Excerpt from Comprehensive Engineering Services, Inc.

SR-50 Widening Construction Plans

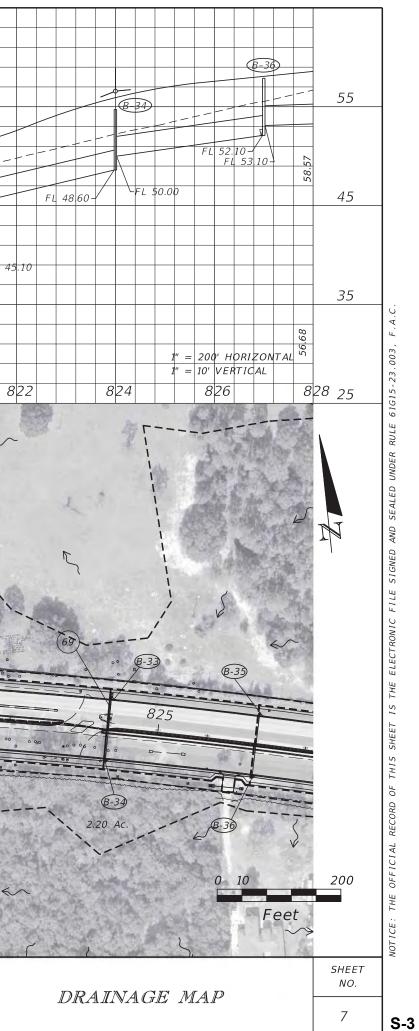


	EXIST. F.L. AND PIPE SIZES ARE FR FPID 433607-1-52-01, 239203-4-52-01,		SHEET FOR CO.	IE INFORMATION ON THIS NSTRUCTION PURPOSES. n the plans for documentation
55		EXIST. GROUND LINE AT Q CONST. SR 50	and to assist c	nstruction personnel with
	PGL Lt. & Rt.	PGL Rt.		
			144.80 (Lt.) 144.80 (Lt.)	
45		PGL Lt.		
	Σ Σ	FL 43.00	<u> </u>	
35		FL 43.50	FL 38.80	EXIST. GROUND LINE AT Q CONST. SR 50 (PER FPID 433607-1-52-01)
35		FL 41.20 F.		
	48.87			FL 30.60-1
25	772 774 75	778 780 78	32 784 786	788 790 792 7
(22 (24 (24) (25)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	W INV. 42.94 W INV. 41.64 W INV. 4 E INV. 42.29 E INV. 41.37 E INV. 40.37 B1 12" CMP 35 18" PIPE 39 18" PIPE S INV. 45.13 W INV. 41.40 S INV. 37 N INV. 37 N INV. 44.63 E INV. 41.11 N INV. 37 W INV. 44.63 E INV. 41.11 N INV. 37 W INV. 42.01 W INV. 39.50 W INV. 41.72 E INV. 41.72 E INV. 39.28 E NV. 40 W INV. 41.72 E INV. 39.28 E NV. 40	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.20 W INV. 31.00 S INV. 37.00 W INV. 5.0 E INV. 31.10 N INV. N/A E INV. 3 5.0 E INV. 31.10 N INV. N/A E INV. 3 $ERCP$ 48 18" PIPE 51 34" x 53" ERCP 3.0 N INV. 31.10 S INV. N/A S INV. N/A 2.30 N INV. 39.89 N INV. 37.00 $ERCP$ 49 18 PIPE 52 10" CPP 3.0 S INV. 34.25 W INV. UNK. 'A N INV. 33.75 E INV. 38.96
DATE	2.39 Ac.	VISIONS DATE DESCRIPTION	Comprehensive Engineering Services, Inc. 201 S Orange Ave, Suite 1300 Orlando, FL 32801-3442 Certificate of Authorization No: 7862	(44) (45) (45) (46) (46) (47)



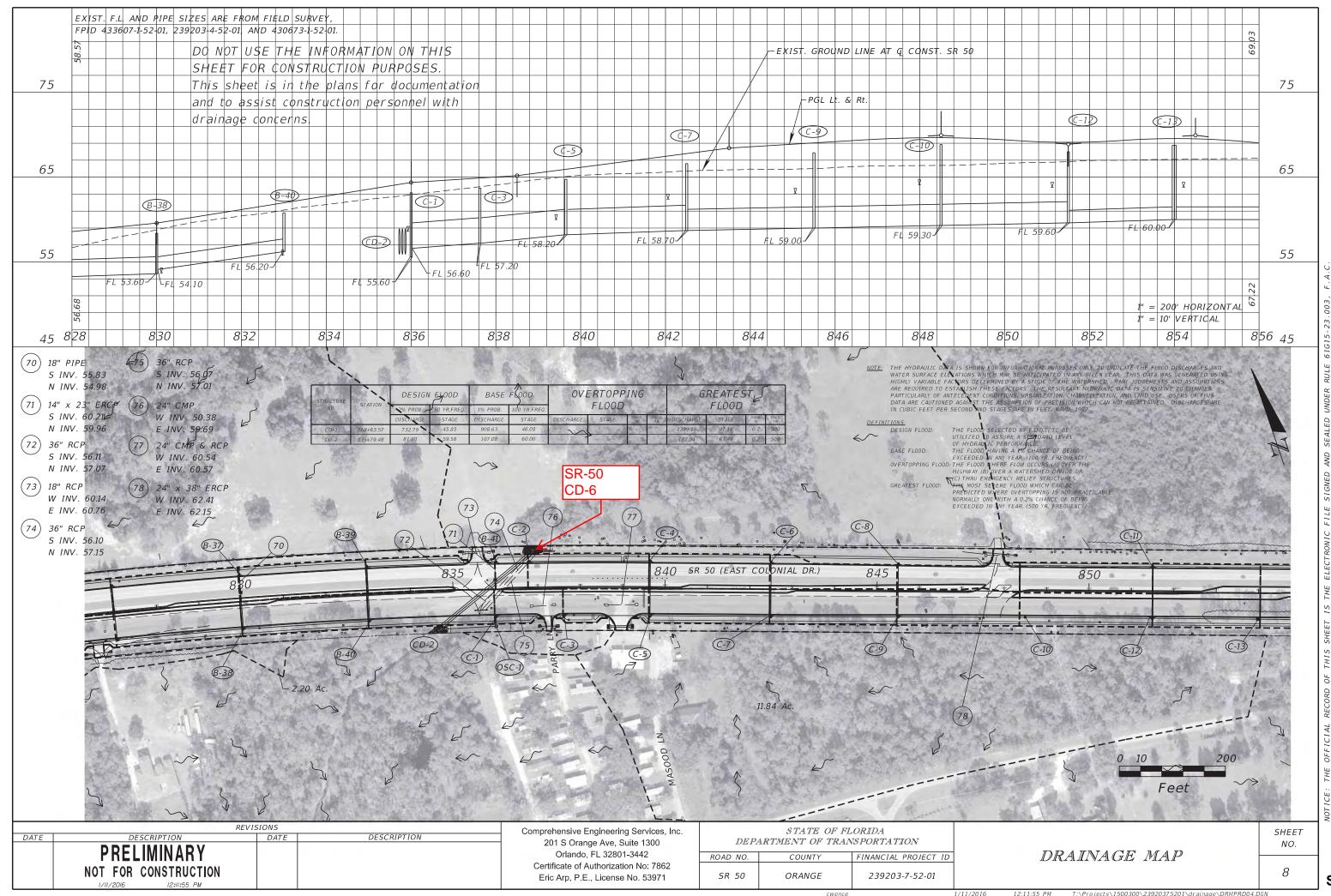
T:\Projects\1500300\23920375201\drainage\DRMPRD02.DGN

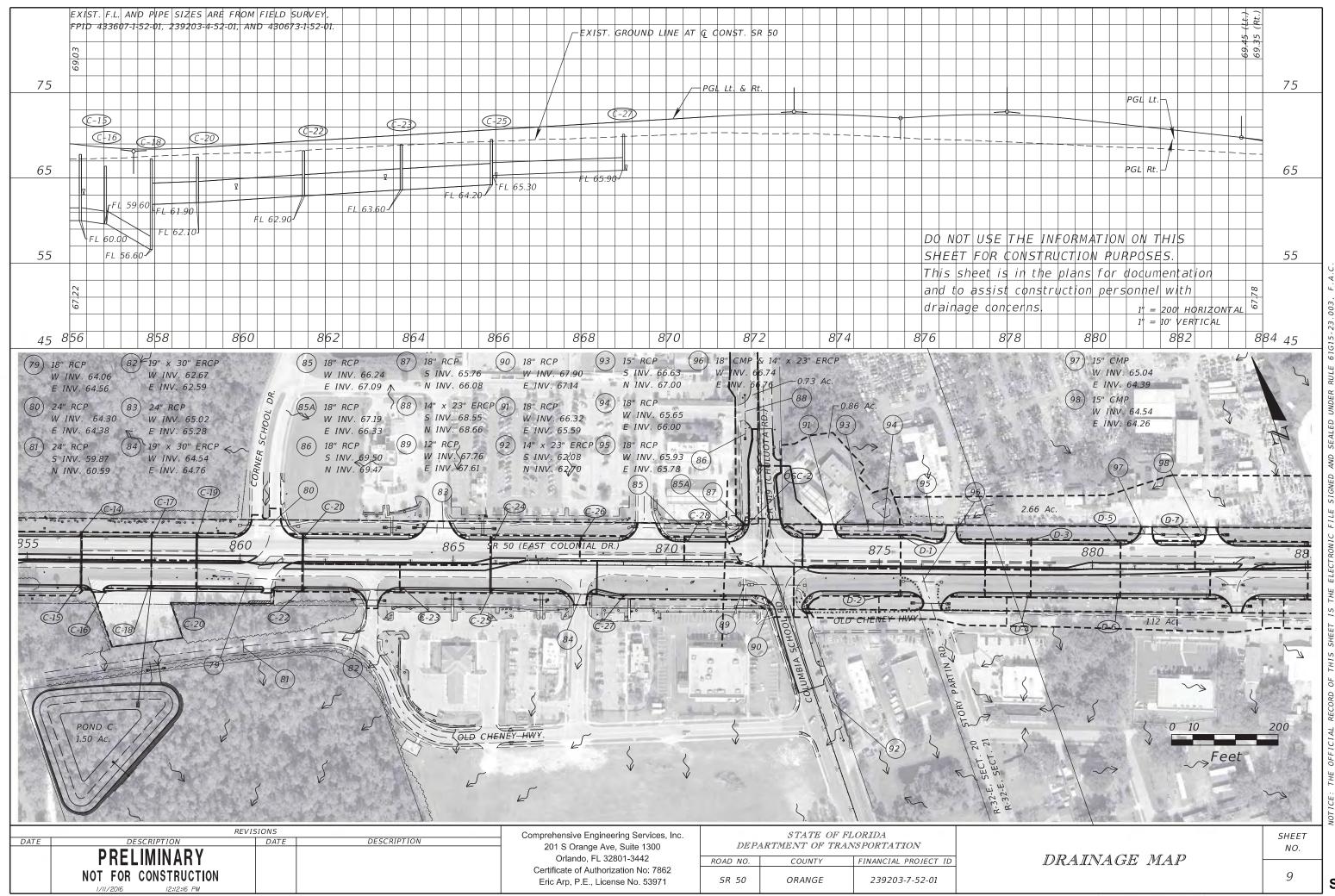
35 1	55	FPID 43360																
DD DV/ DV/ <thdv <="" th=""> DV/ <thdv <="" th=""> <thd <="" th=""> <thd <="" th=""></thd></thd></thdv></thdv>	55)7-1-52-01 239 203+4-5D-															
55 546 67 600	55																	
53 This shreet is in the plans for accomendation and to assume the plans for accomendation accom	55																	
45 and ch assist construction parsenuel with the the the the the the the the the t	55									GROUND LI	NEAIG	CONST	. SR 50					
45 1						on		/						PGL L	t. & Rt.			
45 45 45 45 45 45 45 45 45 45				ruction pe	rsonnei with			/					/	/			(B-3)	
45 45 47 47 47 47 47 47 47 47 47 47		dra	inage concerns.															_
45 45 45 45 45 45 45 45 45 45		2.3						-	B-26				ľ					
03 1												28		B	-30			
35 1	45					(B-22)	6-23											
35 1			B-18											2		- FL	44.50	
35 37 1													EI 12	50			$ \rangle$	
35 1 3 1 3 1 <th1< th=""> 1 <th1< th=""> <th1< th=""></th1<></th1<></th1<>		Z				<u> </u>		×				41.00 - 89.80	1 L 42.	.50-				-FL 4
Image: String			2		∑ □			FL 38.	.60									
1 1 <th1< th=""> <th1< th=""> <th1< th=""> <th1< th=""></th1<></th1<></th1<></th1<>	35				FL 36.00		1	, , , , , , , , , , , , , , , , , , , ,										
25 800 802 804 806 808 810 812 814 816 818 820 (a) 30' RCP (a) 30' RCP (b) (b						LFL 36.70												
25 800 802 804 806 808 810 812 814 816 818 820 (*) price		1.33	∼FL 35.20															
(8) BOT RCP (8) BOT CAP (8) PP PPE (8) BOT PPE		4																
(8) BOT RCP (8) BOT CAP (8) PP PPE (8) BOT PPE																		
39 by: RCP B): B: PIPE 50 B: PIPE B: B): B: PIPE B: B: P	25	800		804	806	808	810	81	2	814		816		818		820	2	8
INV 3528 W INV 3527 W INV 4035 W INV 4035 W INV 4035 E INV 3563 E INV 4035 W INV 4035 E INV 4355 INV 3575 W INV 3724 W INV 4035 E INV 4355 INV 3563 E INV 3524 INV 4035 E INV 4355 INV 3575 W INV 3724 E INV 4035 INV 4035 INV 3570 W INV 3724 E INV 4035 E INV 4205 INV 3770 W INV 3724 E INV 4205 E INV 4205 N INV 4205 E INV 4205 E INV 4205 E INV 4205 N INV 3570 W INV 3653 F INV 4205 E INV 4205 N INV 4205 E INV 4205 E INV 4420 N INV 4205 E INV 4445 INV 4436 INV 3770 W INV 3653 F INV 4445 INV 3770 W INV 4055 E INV 4445 INV 3770 IN INV 4055 E INV 4444 INV 3770 W INV 3653 F INV 4445 INV 3770 W INV 4055 E INV 4445 INV 3770 IN INV 4455 F INV 4445 INV 3770 IN INV 4455 F INV 4445 INV 3770 IN INV 4455 <th>(54) 7</th> <th></th> <th>\sim \sim</th> <th>10" DIDE</th> <th>64) 18" PIPE</th> <th>(68) 18" PI</th> <th>PE</th> <th>-</th> <th></th> <th>6 10</th> <th>6</th> <th></th> <th></th> <th>See. 2</th> <th>i</th> <th>2</th> <th></th> <th></th>	(54) 7		\sim \sim	10" DIDE	64) 18" PIPE	(68) 18" PI	PE	-		6 10	6			See. 2	i	2		
E-INV. 36.63 E-INV. 37.24 E-INV. 40.39 N-INV. 40.85 E-INV. 43.35 E-INV. 43.35 E-INV. 43.35 N-INV. 43.45 N-INV. 44.45 N-INV	(54) 5	INV. 36.28	W INV. 37.32	W INV. 39.	.46 S INV. 41.	.15 W INV	1. 44.44			. ~		÷		些 编	1		St.	65
S INV 37.50 W INV 37.24 W INV 49.90 E INV 49.30 S INV 37.25 W INV 49.72 W INV 49.72 W INV 49.72 W INV 49.72 W INV 49.70 W INV			~	E INV. 40.3	39 N INV. 40	0.85 E INV	10.350	,		P	1.1.4	10			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
N IWV. 37.22 E INV. 47.23 N INV. 48.90 56 18" PIPE 510 18" PIPE 620 50" CMP-160 18" PIPE 57 39" CMP-160 18" PIPE 630 18" PIPE 631 18" PIPE 57 39" CMP-160 18" PIPE 631 18" PIPE 51 NV. 44.45 59 10" CMP-160 18" PIPE 51 NV. 44.45 10" VIV. 44.45 59 10" CMP-160 18" PIPE 51 NV. 44.45 10" VIV. 44.45 59 10" CMP-160 18" PIPE 51 NV. 44.45 10" VIV. 44.36 59 10" CMP-160 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.45 10" VIV. 44.36 50 18" PIPE 51 NV. 44.55 10" VIV. 44.36 50 18" PIPE 10" VIV.45 10" VIV.45 50 18" PIPE 10" VIV.45 10" VIV.45 50 18" PIPE 10" VIV.45	(55) 18	8" PIPE 5		₹-30" RCP			PE	S		- All		The second		200	Sa.	1		
56 18° PIPE 50 18° PIPE													18			1.		
S INV. 37700 N INV. 32,222 BINV. 32,222 BINV. 33,46 BINV. 32,222 BINV. 33,46 BINV. 33,46 BINV. 33,46 BINV. 33,46 BINV. 44,45 BINV. 44,45 B		and the second second	\sim \sim \sim	ALCON COMPANY OF A	\cap					.5			. ~		~		1	
(37) 30" CMP - 60 18" PIPE (53) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (52) (53) (54) (53) (53) (54) (53) (53) (54) (53) (53) (53) (53) (53) (53) (53) (54) (52) (52) (53)	S S	INV. 37.70	W INV 31991	W INV 37	76	200		0.0		F			E	W		12		
W INV. 36,44 5 / INV. 41,61 5 / INV. 44,42 E INV. 37,24 N INV. 39,00 E INV. 41,15 N INV. 44,45 100 50 (66) 58 58 60 (83) (83) (82) 7.15 Ac. (82) 62 62 62 62 62 62 62 62 62 62 62 62 62		I INV. 37.22	E INN/ 30.46			2.00		1	STR 382				Tail	12		N		
E INV. 3724 N. INV. 3900 E INV. 41.15 N. INV. 44.36 So (2) (2) (3) (6) (6) (6) (6) (6) (6) (6) (6) (6) (6	(57) 3	1.1.1.1.1.1		<i>E</i> INV. 38.6				S	的意	-			R			0+32.	ì	
57 556 58 68A 68D 62D 715 Ac. 62 63 65 66 62 67 68 63 68 68 68 68 62 62 68 62 66 68 68 68 68 68 68 68 68 68 68 68 68		CMPT	50) 18" PIPE (63	E INV. 38.6) 18" PIPE W INV 416			4	5		1	5		(1)	atilite.	<u>m</u>	l. 820+32.	1	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	с и E	INV. 36.44	50) 18" PIPE (63 5 INV. 3246) 18" PIPE W INV. 41.6	67 18" PIPE 5 INV. 44	4.44		5			Þ					STA. 820+32.		
55 G.13 (2) 800 (2)		INV. 36.44	50) 18" PIPE (63 5 INV. 3246) 18" PIPE W INV. 41.6	67 18" PIPE 5 INV. 44	4.44 4.36		£ (8-24)	63 64	65)_(66)		5		PI STA. 820+32.		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	С и Е	V INV. 36.44 INV. 37\24	50) 18" PIPE (63 5 INV. 3246 N INV. 39.00) 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 5 N INV. 44	4.44 4.36 7.15 Ac.			40	65) (66 (66	~	(B-2	5	(67)	PI STA. 820+32.		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	роблания Страна Стра Страна С С С С С С С С С С С С С С С С С С	V INV. 36.44 INV. 37\24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 5 N INV. 44	4.44 4.36 7.15 Ac.			40	65	€-2) (66)		<u>(8-2</u>	2	67	PI STA. 820+32.	· · · · · · · · · · · · · · · · · · ·	3-33) II
$\begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} $	р С С	V INV. 36.44 INV. 37\24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2	4.44 4.36 7.15 Ac.			40	65	B-20 66		<u>@-2</u>	2	67	PI 57A. 820+32.	68 E	3-3)
$\begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} $		V INV. 36.44 INV. 37\24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac.			40	65	66 8-27 8-5 		<u>8-2</u>	2	67	8 PI 5TA. 820+32.	68 (33
$\begin{bmatrix} 54 \\ 618 \\ 618 \\ 618 \\ 618 \\ 620 \\ 59 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 6$	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac.		F-2	40		B-2) 815		(F-2	2	67	100 0 PI 5TA. 820+32.	68 E	3-3)
$\begin{bmatrix} 54 \\ 618 \\ 618 \\ 618 \\ 618 \\ 620 \\ 59 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 60 \\ 6$	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac.		F-2	40		B-2) 815				67	• 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3-3)
$\begin{bmatrix} 54 \\ 618 \\ -54 \end{bmatrix} \begin{bmatrix} 618 \\ -52 \\ -54 \end{bmatrix} \begin{bmatrix} 60 \\ -59 \\ $	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac.		F-2	40		B-2) 815				67	• 18 0 0 0 0 0 0 0 0 1 5TA. 820+32.	68 E	3.3
54 GE 10 54 GE	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac.			40		B-2) 815				67			3-37 .
	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	• 1 820+32.		3-3)
	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	0 PI 57A. 820+32.		
	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	• 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		-33 -33
	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	0 0 0 0 1 57A. 820+32.		3.3
AT A REAL FUNCTION	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	10 PI 574. 820+32.		
	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67		ECT. 20	
32-1	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815					0 PI 574. 820+32.	E. SECT. 20	
K K	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815				67	10 PI 574. 820+32.	32-E, SECT. 20 2 20 2 20 2 20 2 20 2 20 2 20 2 20	
REVISIONS Comprehensive Engineering Services, Inc. STATE OF FLORIDA	Ē	V INV. 36.44 INV. 37/24	50) 18" PIPE (63 5 INV. 32,46 N INV. 39,00 57, (56) () 18" PIPE W INV. 41.6 E INV. 41.15	67 18" PIPE 5 INV. 44 N INV. 44 B-19 B-2 CD 50 (EAST COLO	4.44 4.36 7.15 Ac. ONIA DRU	\$5. 62 810 61. 62		40		B-2) 815					201 10 PI 574. 820+32.	R-32-E, SECT. 20	
DATE DESCRIPTION DATE DESCRIPTION 2015 Orange Ave Swite 1200 DEPARTMENT OF TRANSPORTATION		V INV. 36.44 INV. 37/24	50) 18" PIPE (63 S INV. 50,46 N INV. 39,00 (57) (56) (B-17) (B-17) (B-18) 18" PIPE W INV. 41.6 E INV. 41.15 58 58A 805 805 6-20	67) 18" PIPE 5 INV. 44 N INV. 44 8-19 8-19 8-19 8-2 5R 50 (EAST COLU 	4.44 4.36 7.15 Ac. 20 7.15 Ac. 0NIA DR 59 59 59 59 50 50 50 50 50 50 50 50 50 50 50 50 50			23 43-5 (6-26) (5-6-9)	- Resources to o	B-2) 815				67	Control of the state of the state st	R-32-E, SECT. 20	
	Ē	V INV. 36.44 INV. 37/24	50 18" PIPE 63 S INV. 5046 N INV. 39,00 57 (56 B-17) B-17 B-18 B-18 D DESCRIPTION) 18" PIPE W INV. 41.6 E INV. 41.19 58 58A 805 805	67) 18" PIPE 5 INV. 44 N INV. 44 8-19 8-19 8-19 8-2 5R 50 (EAST COLU 	4.44 4.36 7.15 Ac. 20 7.15 Ac. 0NIA DR 59 59 59 59 50 50 50 50 50 50 50 50 50 50 50 50 50		mprehensive E 201 S Oran	Engineering Sige Ave, Suite	65 Record 80 of Record 80 of Re	B-2) 815		• • • • • •	· · · · · · · · · · · · · · · · · · ·			R-32-E, SECT. 20 R-32-E, SECT. 20	
NOT FOR CONSTRUCTION Eric Arp. P.E., License No. 53971 SR 50 ORANGE 239203-7-52-01		PRE	50 18" PIPE 63 5 INV. 5046 N INV. 39,00 57 56 B-17 B-17 B-18 B-18 C B-18 C C C C C C C C C C C C C) 18" PIPE W INV. 41.6 E INV. 41.15 58 58A 805 805 6-20	67) 18" PIPE 5 INV. 44 N INV. 44 8-19 8-19 8-19 8-2 5R 50 (EAST COLU 	4.44 4.36 7.15 Ac. 20 7.15 Ac. 0NIA DR 59 59 59 59 50 50 50 50 50 50 50 50 50 50 50 50 50	61 058-3 2 61 059-3 2 61 059	mprehensive E 201 S Oran Orlando,	Engineering S ge Ave, Suite, FL 32801-34	65 - Resource 80 of - Resour		DEPAR	stat RTMENT (CE OF FL	SPORT.	ATION	R-32-E, SECT. 20	
In the second seco		PRE	DESCRIPTION BESCRIPTION BESCRIPTION BESCRIPTION) 18" PIPE W INV. 41.6 E INV. 41.15 58 58A 805 805 6-20	67) 18" PIPE 5 INV. 44 N INV. 44 8-19 8-19 8-19 8-2 5R 50 (EAST COLU 	4.44 4.36 7.15 Ac. 20 7.15 Ac. 0NIA DR 59 59 59 59 50 50 50 50 50 50 50 50 50 50 50 50 50	61 058-3 2 61 059-3 2 61 059	nprehensive E 201 S Oran Orlando, Certificate of A	Engineering S ge Ave, Suite, FL 32801-34 Authorization	65 Resources 80 of The revices, Inc. a 1300 142 No: 7862	B-20 B-20 B-20 C	DEPAI	stat coun	TE OF FL OF TRAN	SPORT.	ATION	d1 1 R-32-E, SECT. 20 R-32-E, SECT. 20	

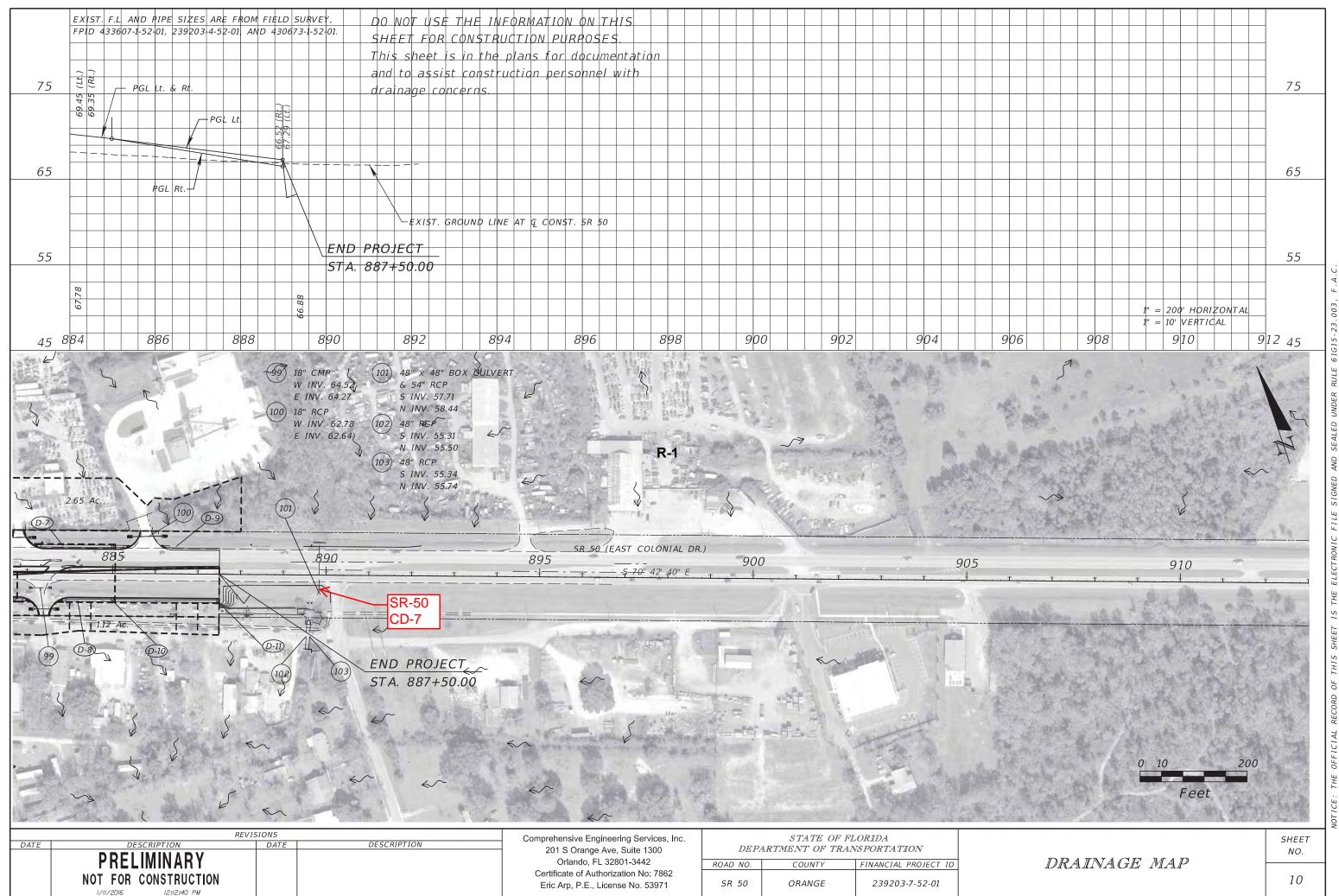


12:11:33 PM

T:\Projects\1500300\23920375201\drainage\DRMPRD03.DGN





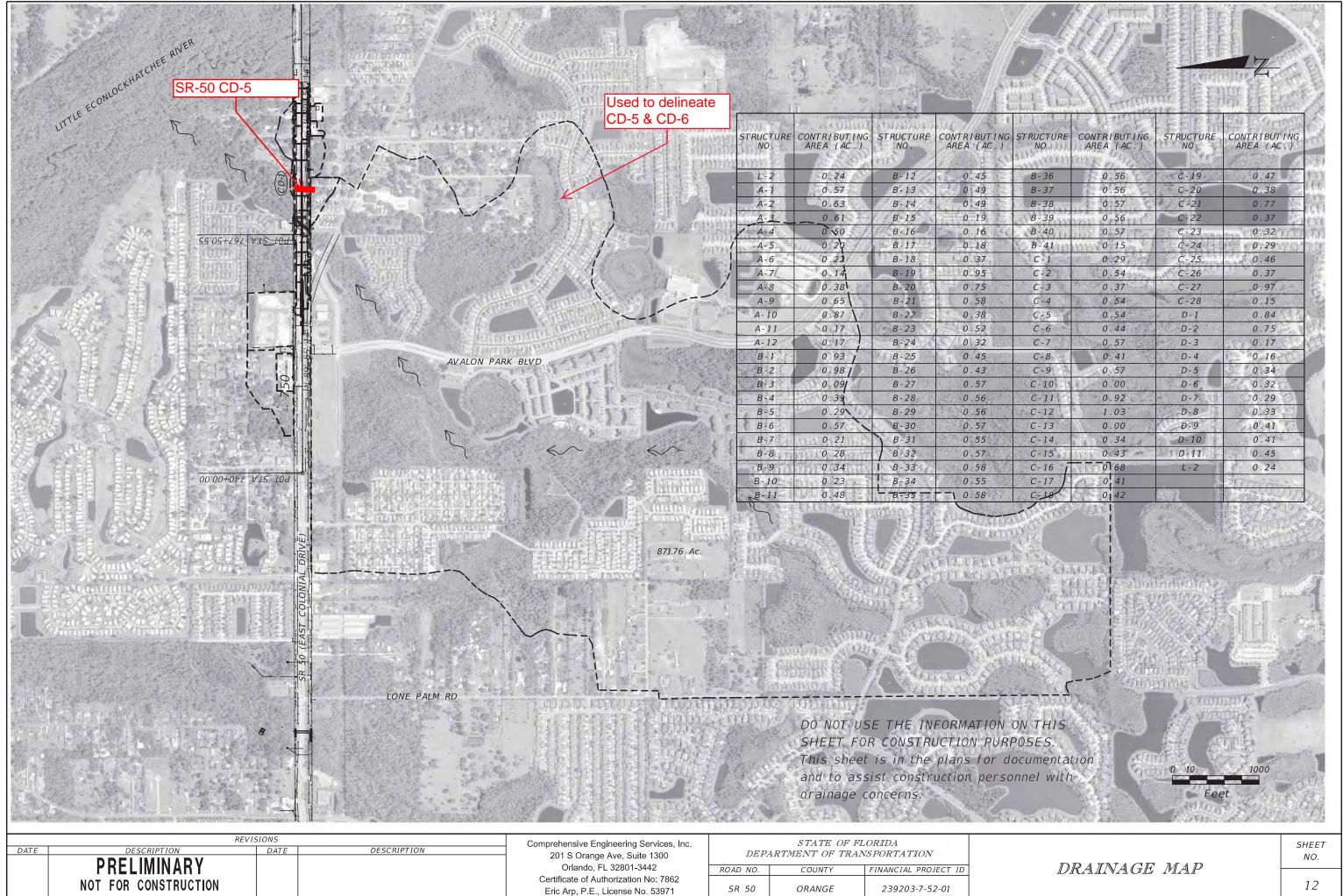


T:\Projects\1500300\23920375201\drainage\DRMPRD06.DGN

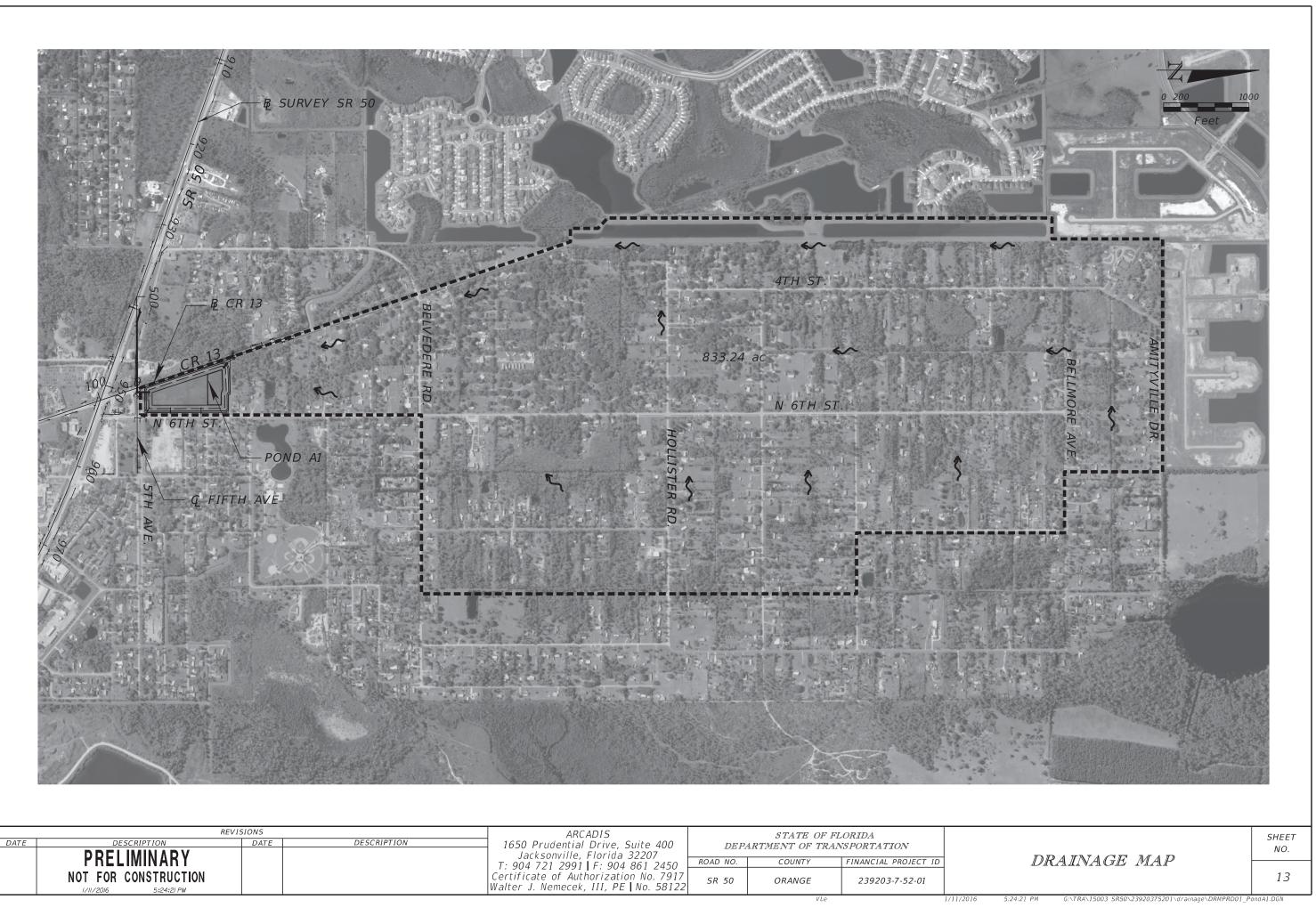


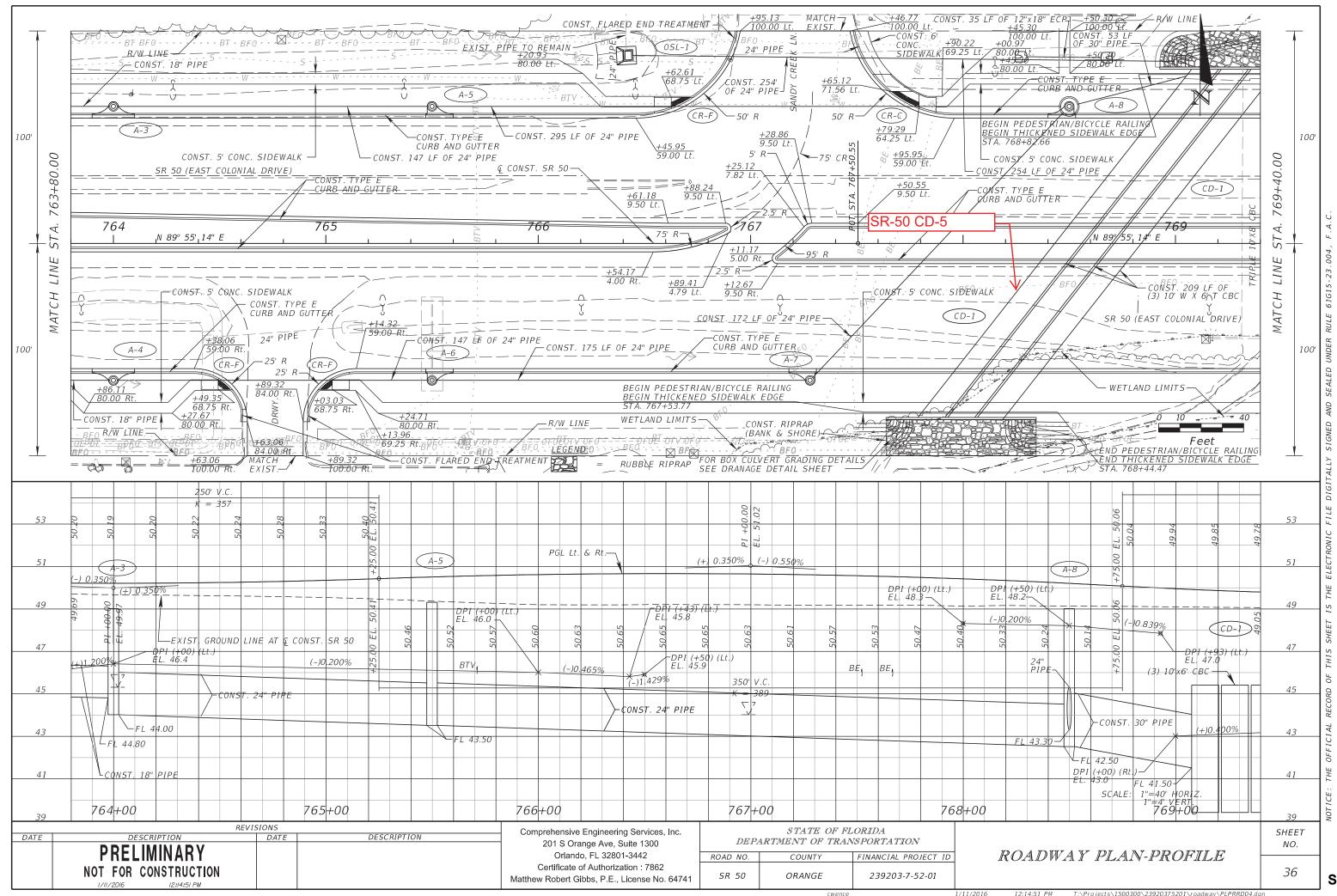
2:12:12 PM

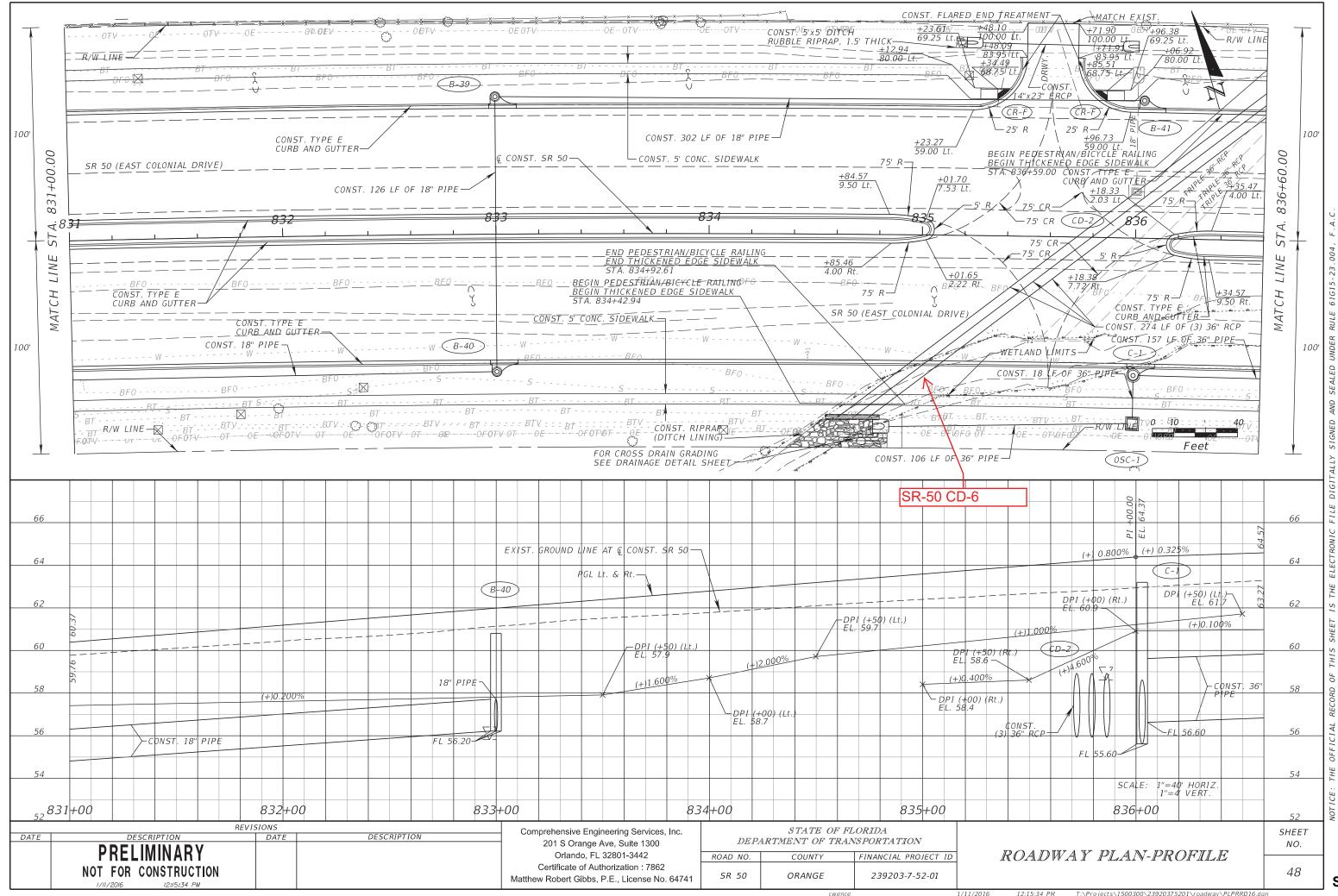
-server5\Trans\Projects\1500300\23920375201\drainage\D.



12:13:45 PI

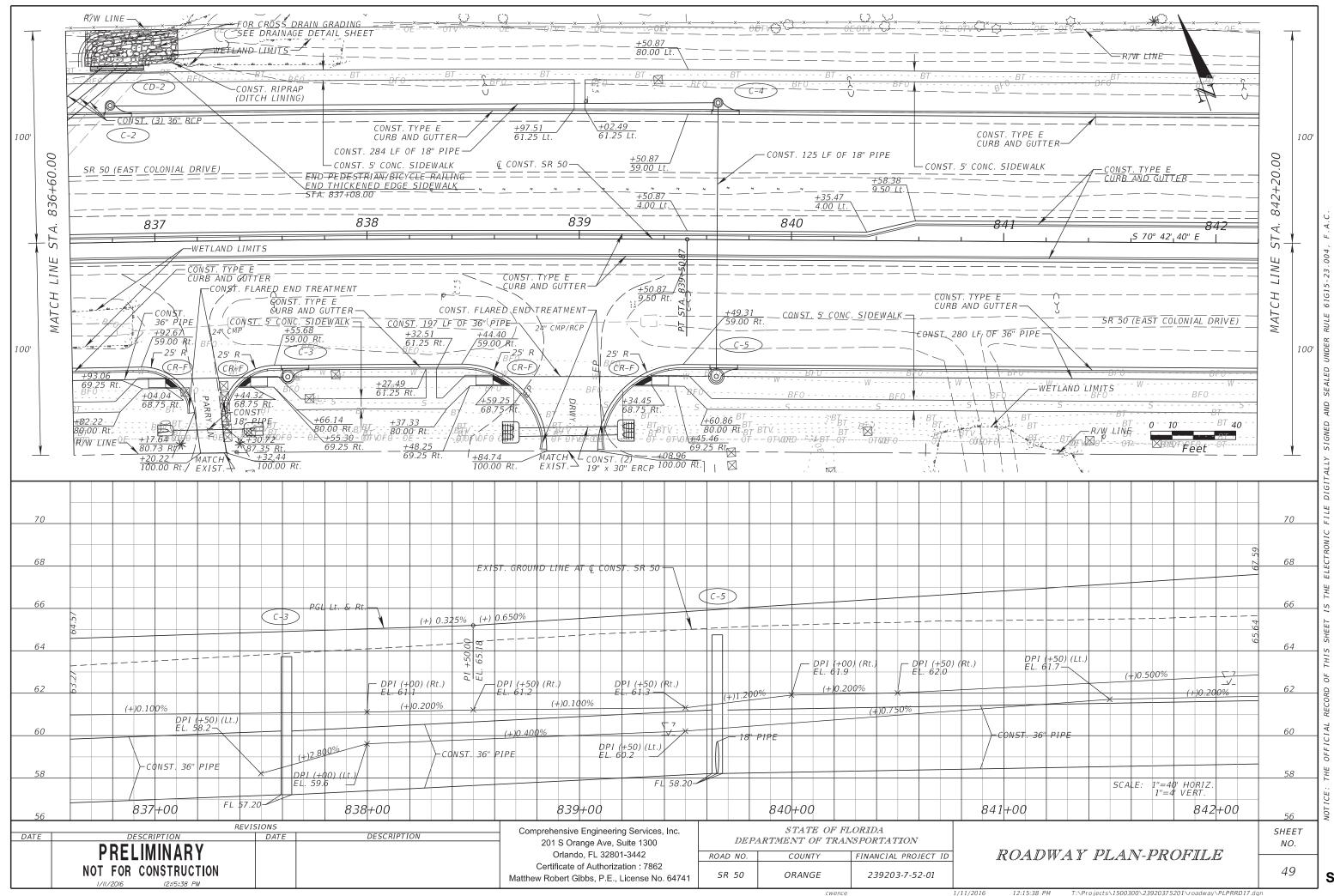


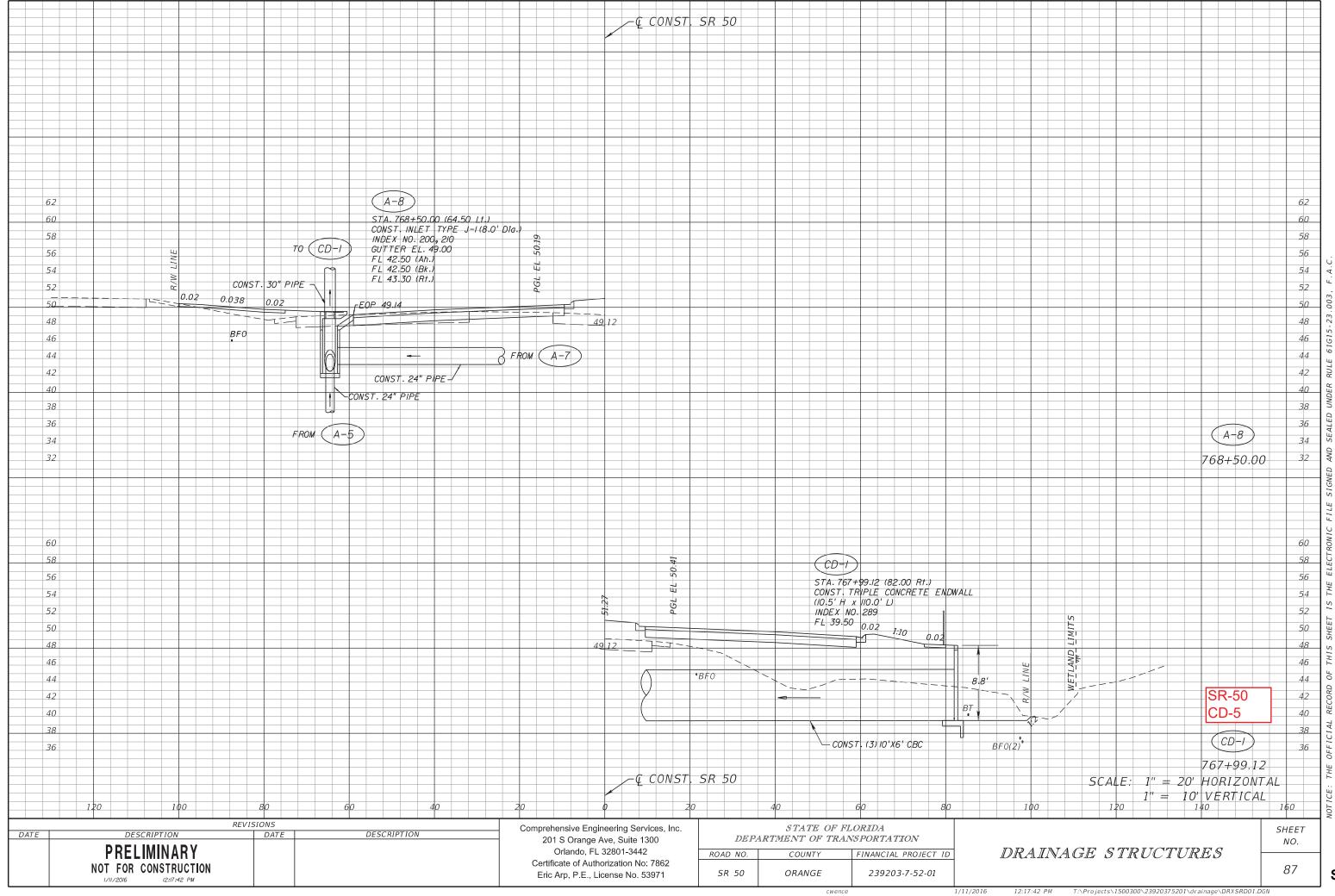


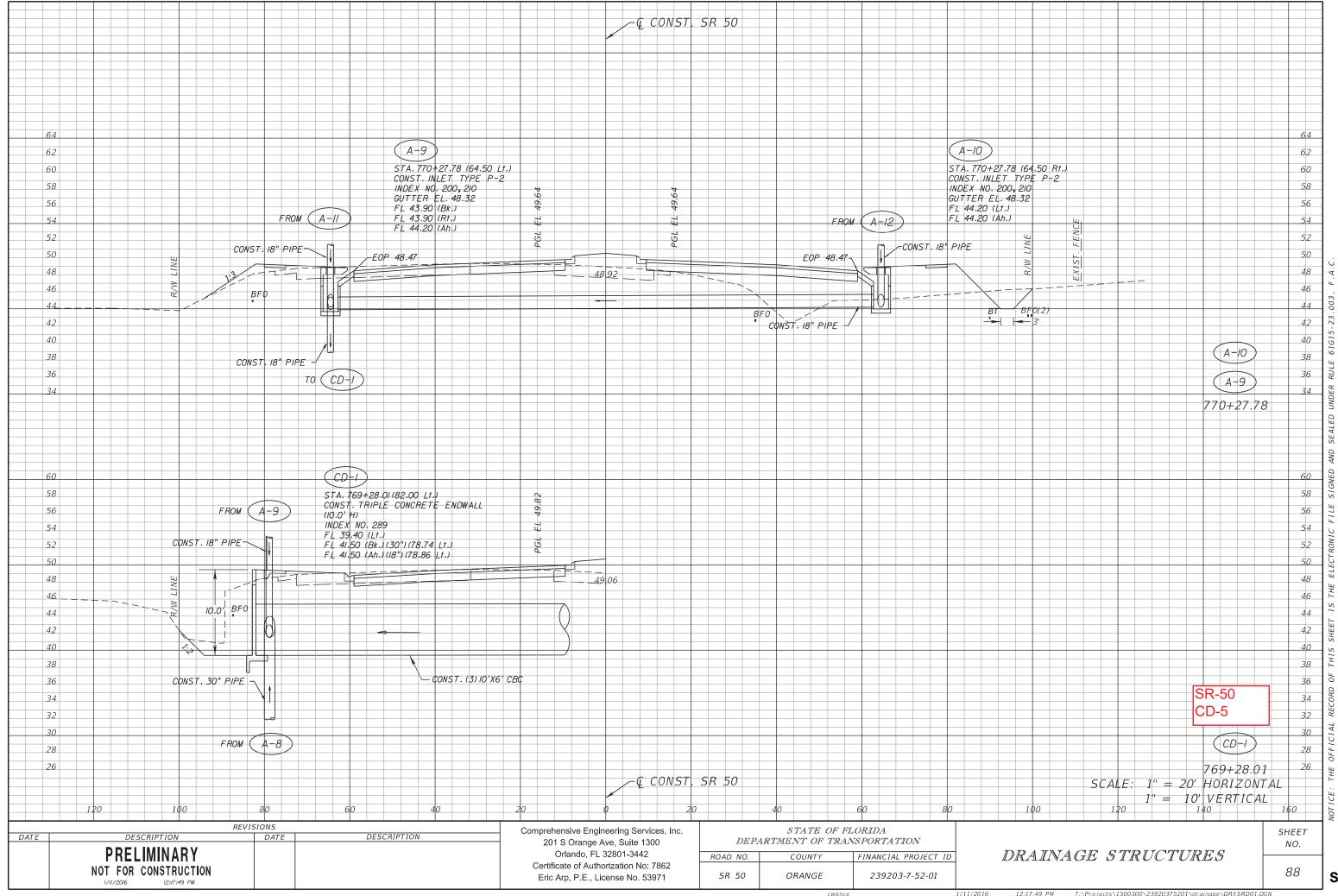


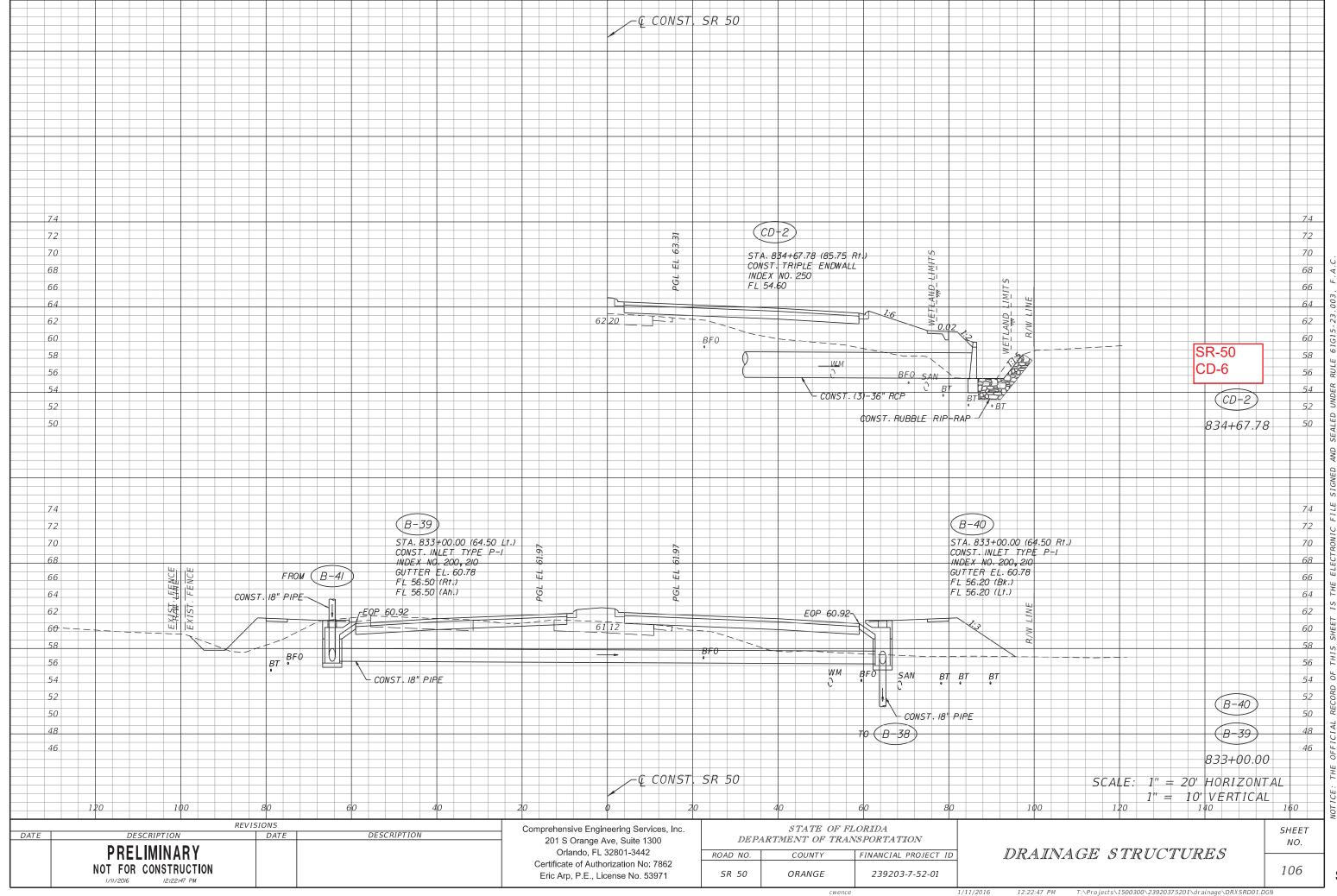
1/11/2016

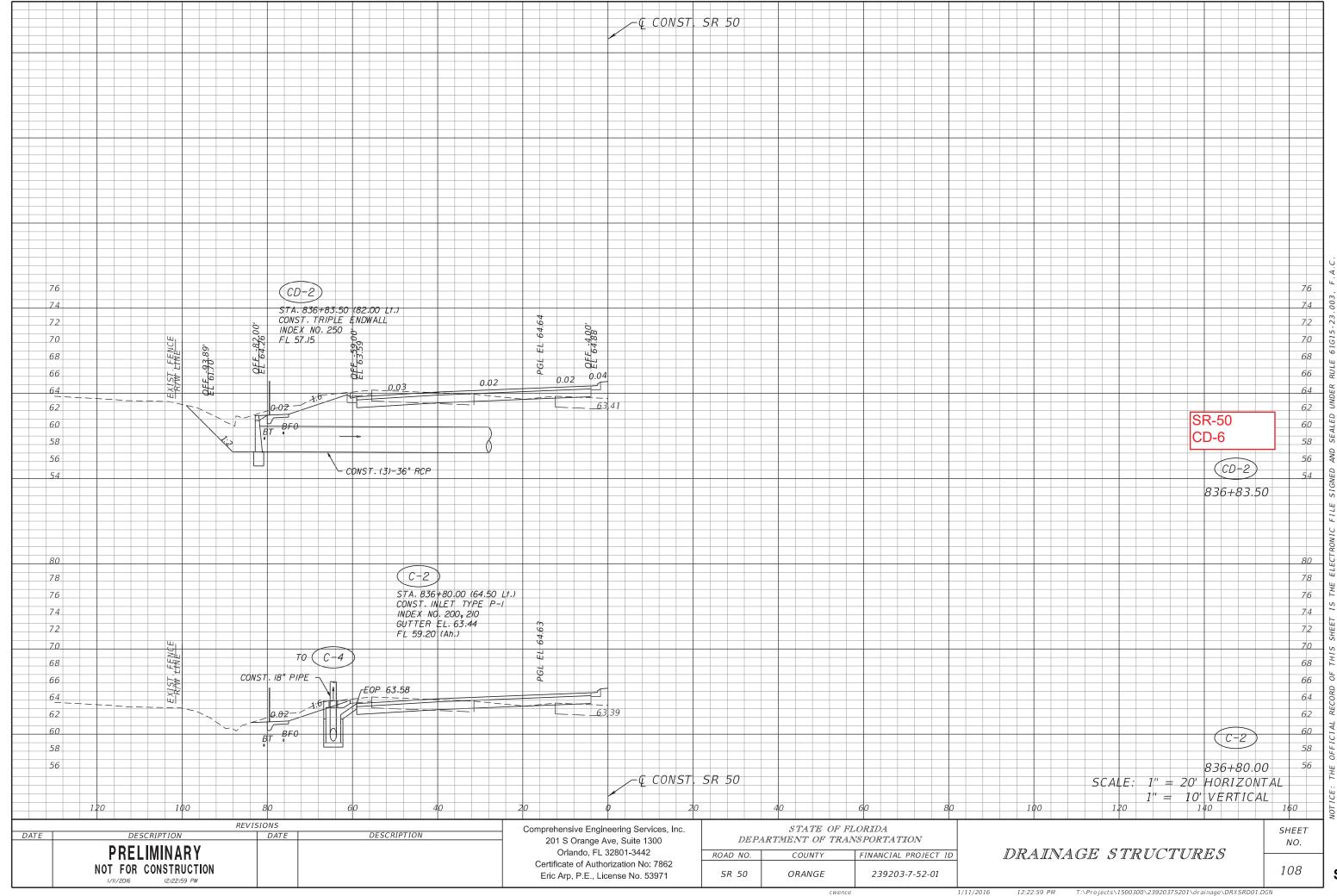
T:\Projects\1500300\23920375201\roadway\PLPRRD16.dg







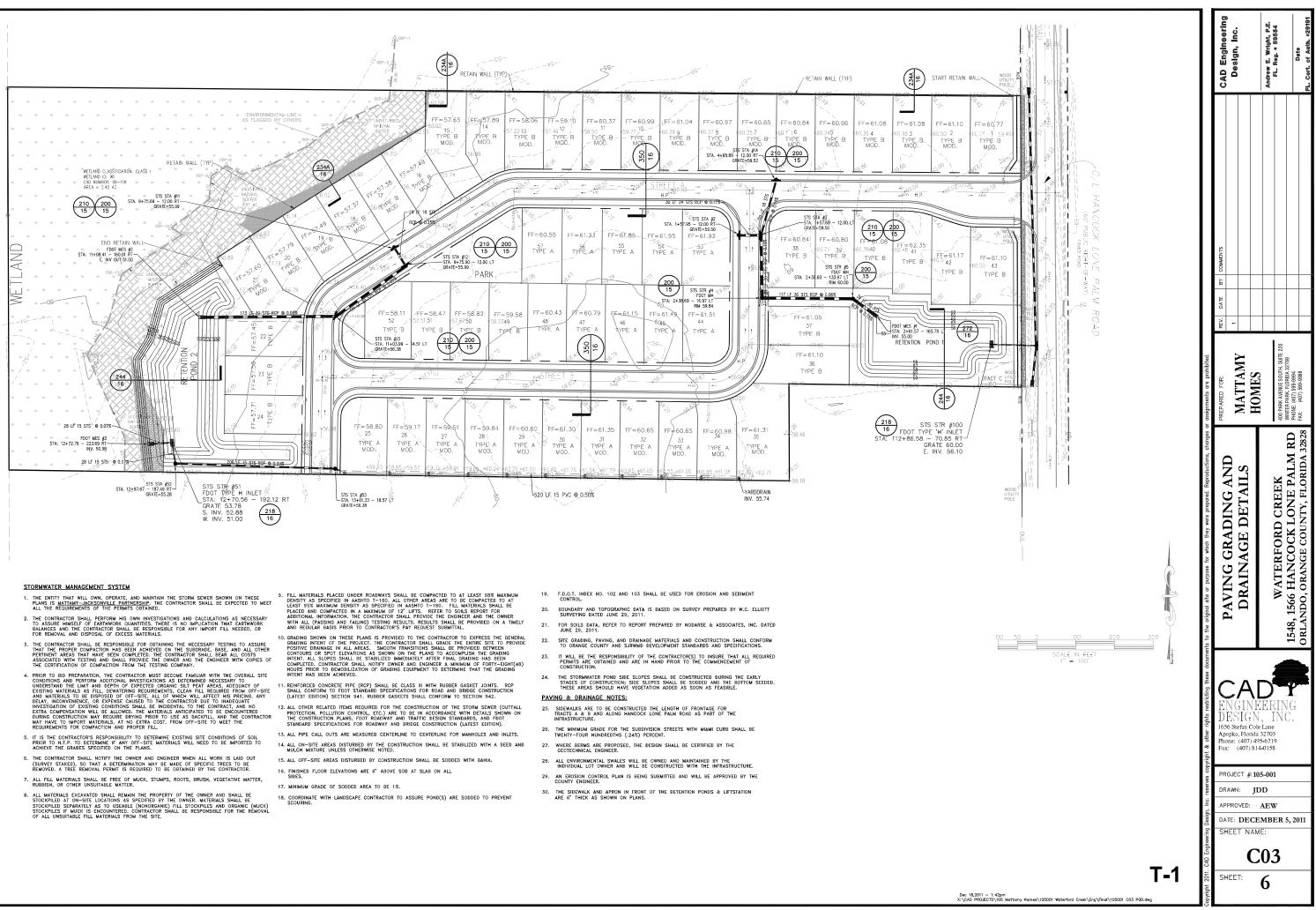


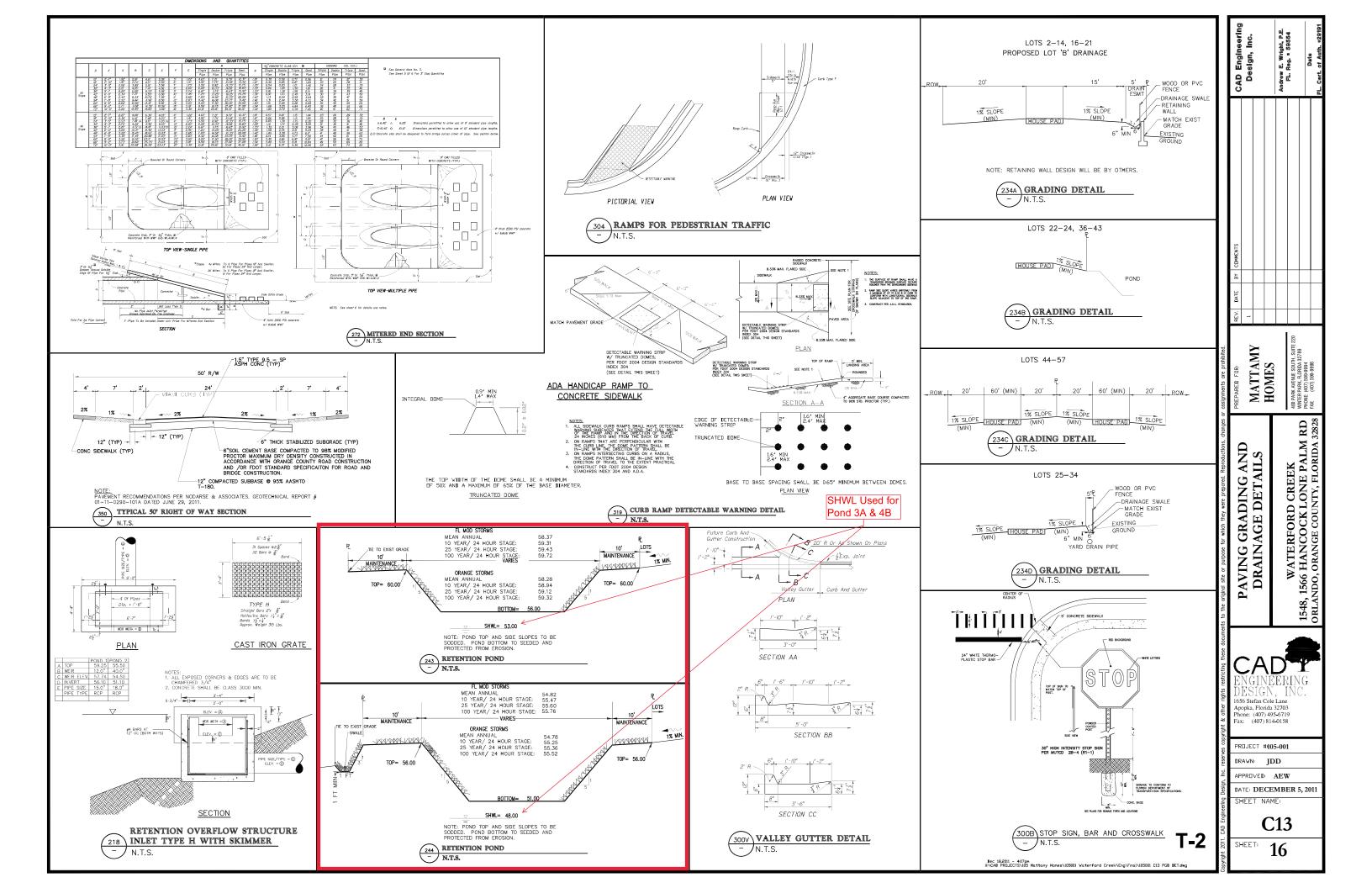


Appendix: T

Excerpt from CAD Engineering and Design, Inc

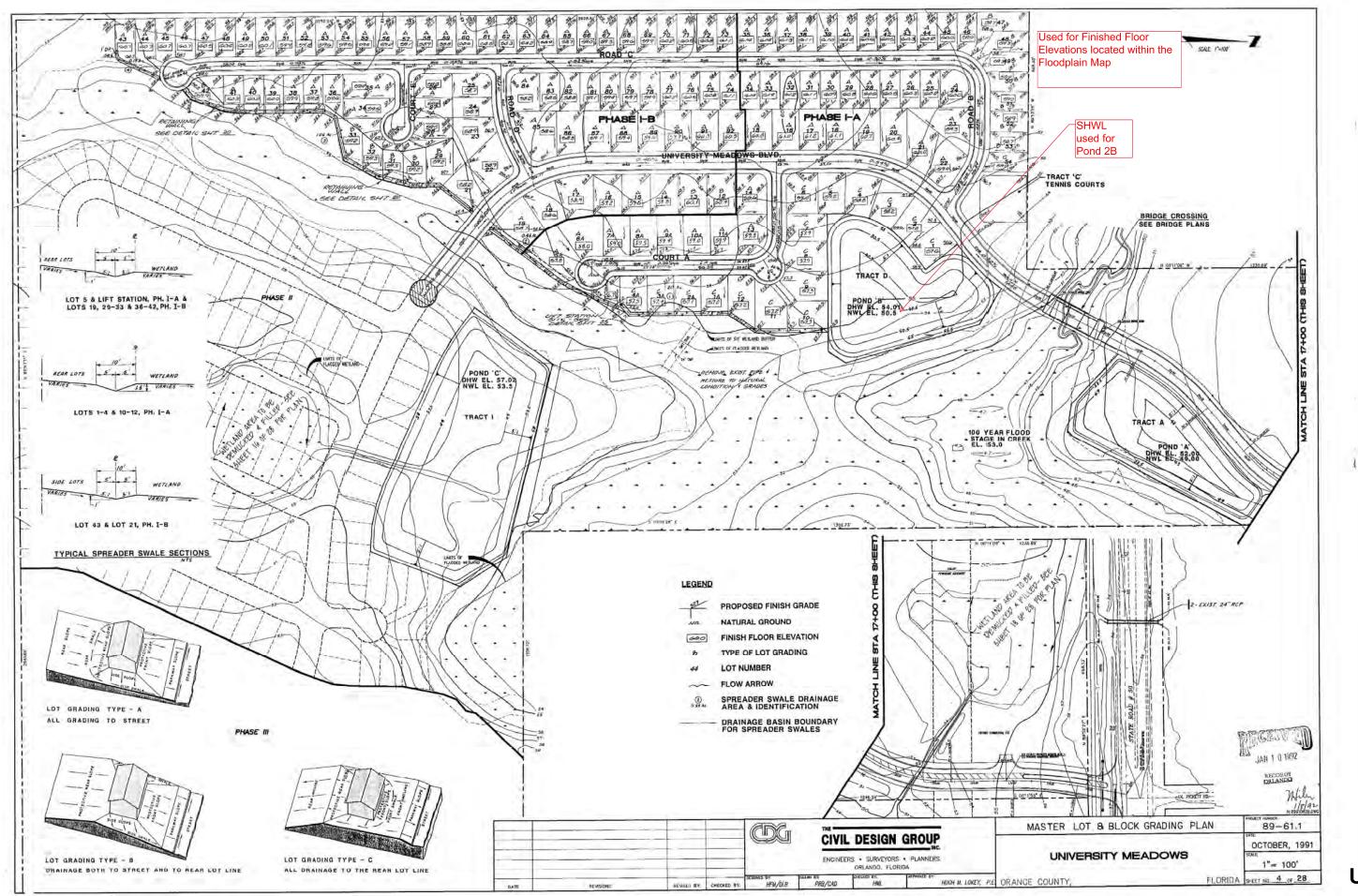
Waterford Creek



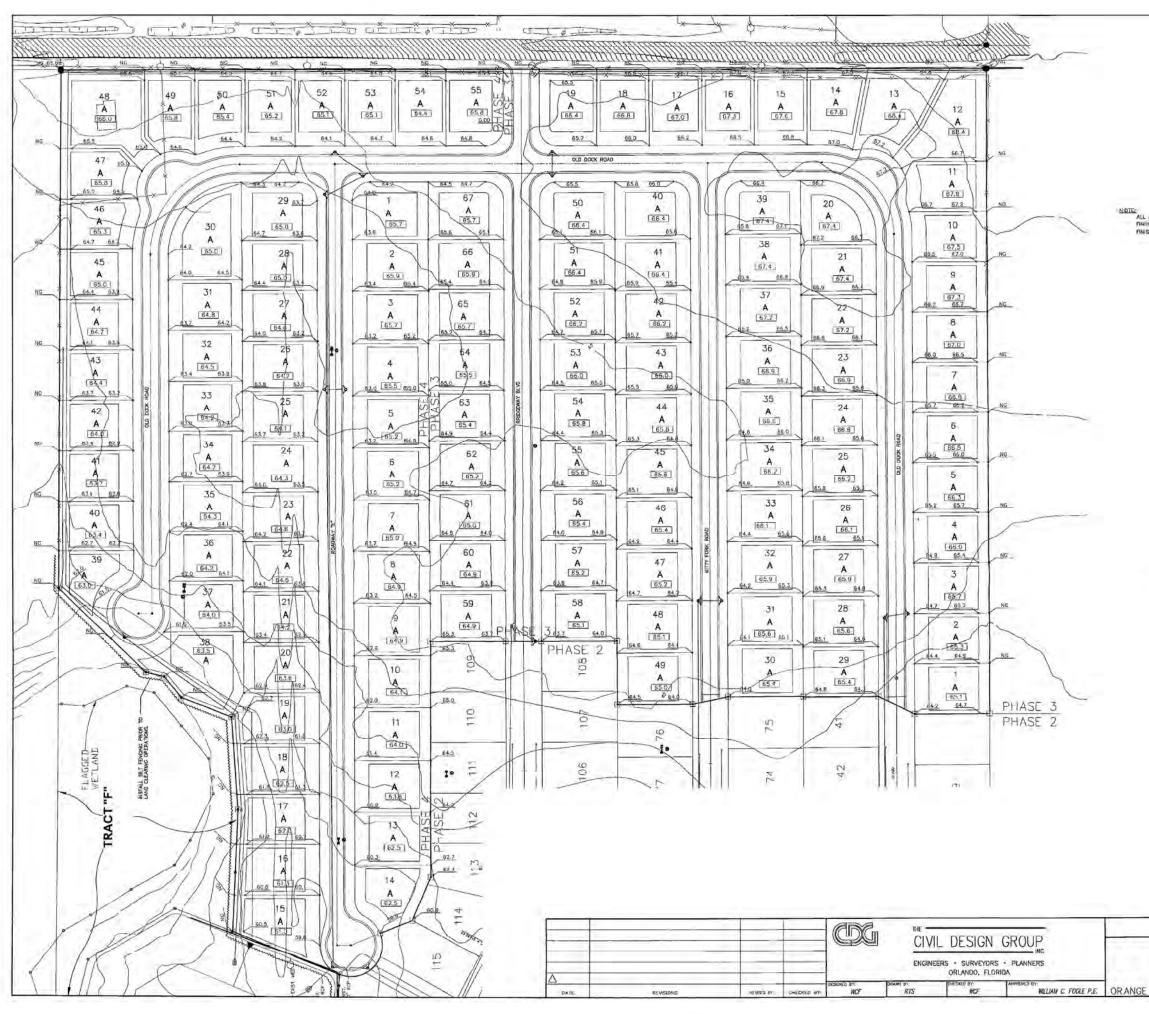


Appendix: U

Excerpt from The Civil Design Group University Meadows & Bridgewater Plans



U-1



NOTE: ALL LOTS TO BE GRADED AS SHOWN ON THIS LOT GRADING PLAN. FINIHED LOT GRADE FOR BUILDING PADS SHALL BE & BELOW THE FINISHED FLOOR ELEVATIONS SHOWN ON THE PLANS BELOW.

55402 1 + 6U

1-4-1

Used for Finished Floor Elevations located within the Floodplain Map

LEGEND:

62.4 /	FINISHED GRADE ELEVATION
84.3	FINISHED FLOOR ELEVATION
~~~	EXIST. GROUND SURFACE CONTOURS
· 62.4	GROUND SHOTS FROM ACTUAL FEILD SURVEY

	Willerson
MASTER GRADING PLAN	215700
BRIDGEWATER PHASE III RECEIVED	OCTOBER, 2001 SOLL: 1" = 60"
COUNTY NOV 07 2001	SHEET NO. 4 OF 20
ALTAMONTE SVC. C	(n.

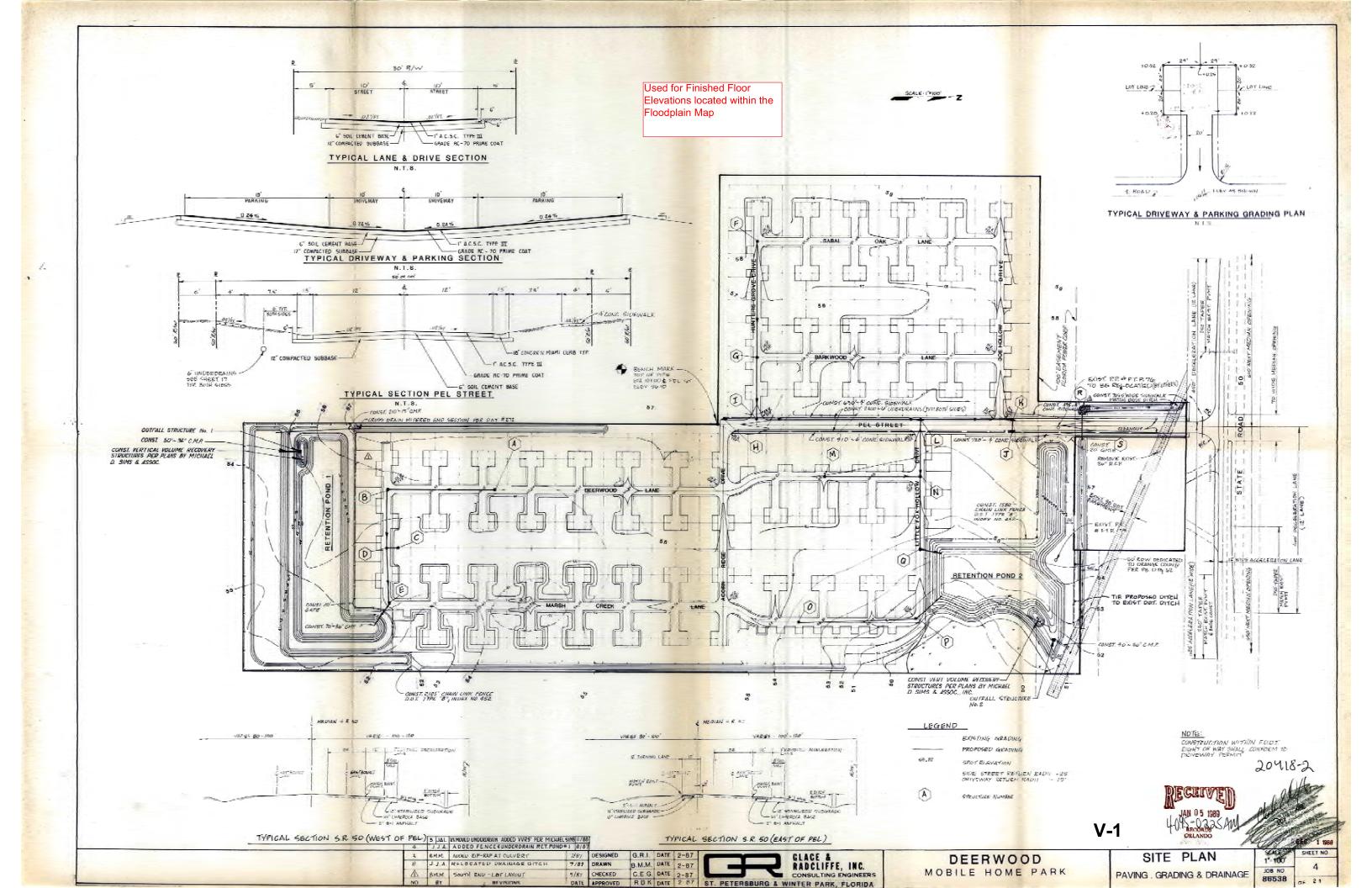
U-2

(1)

### Appendix: V

Excerpt from Glace and Radcliffe, Inc.

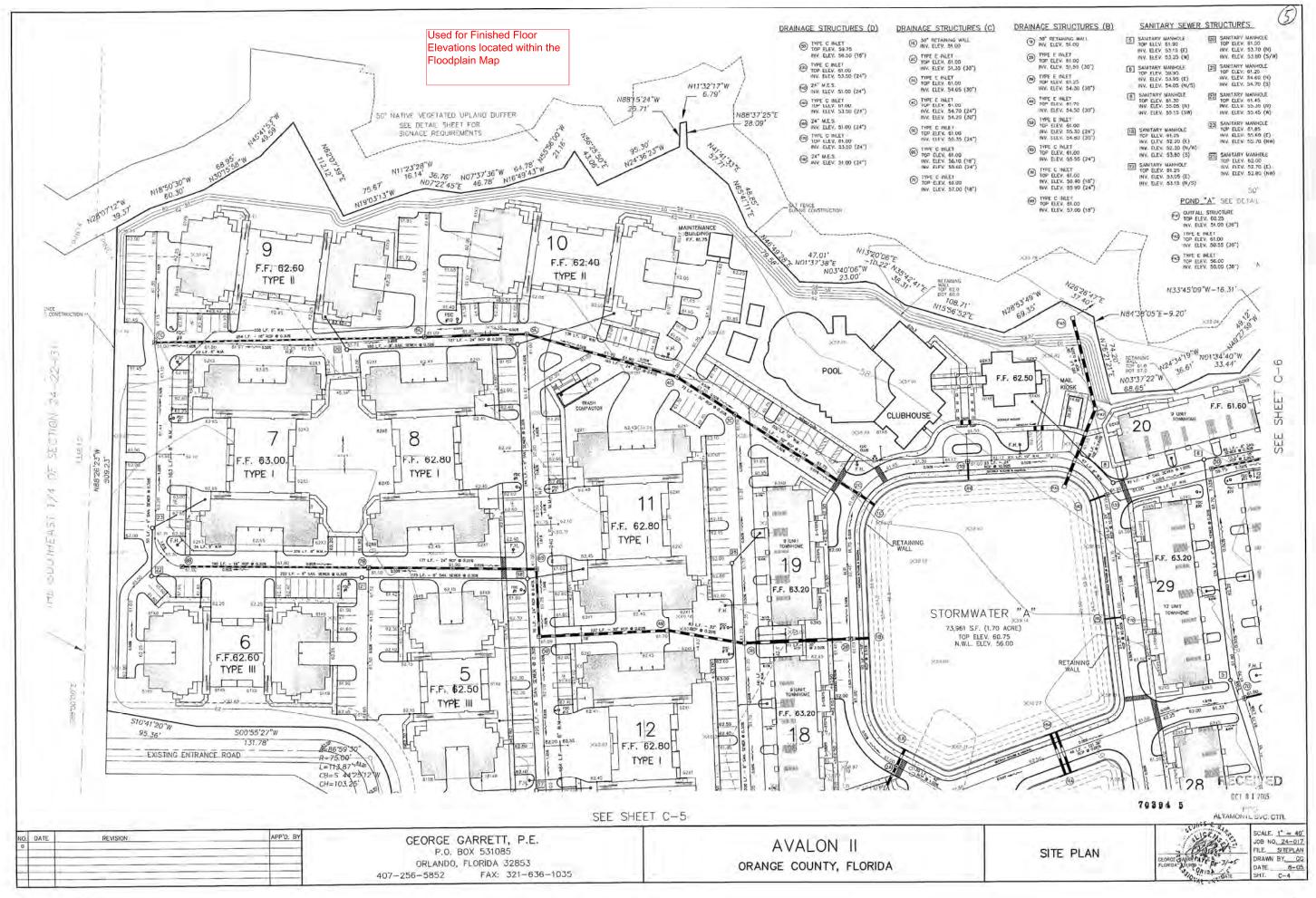
**Deerwood Plans** 



# Appendix: W

Excerpt from George Garrett, P.E.

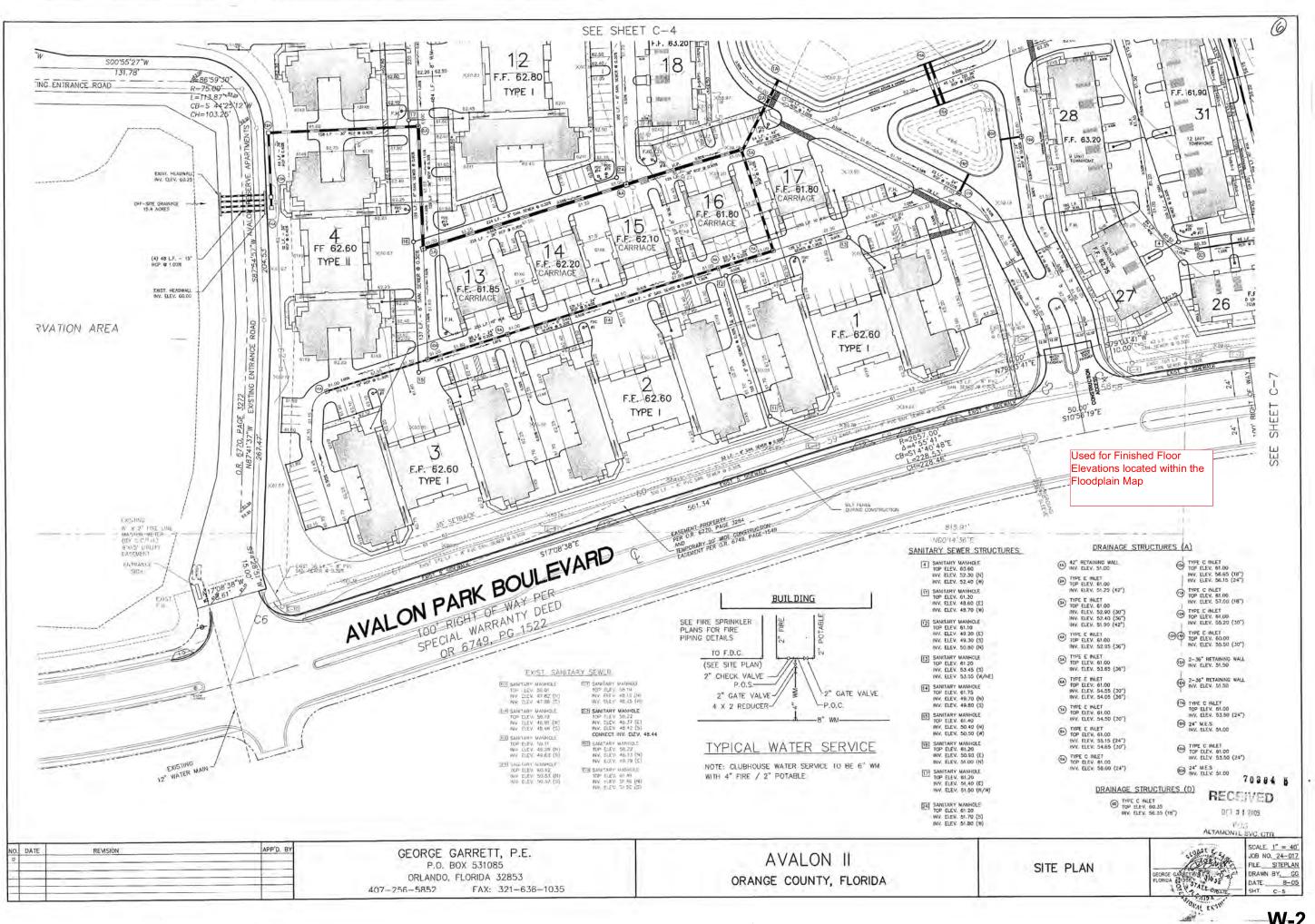
Avalon II Plans



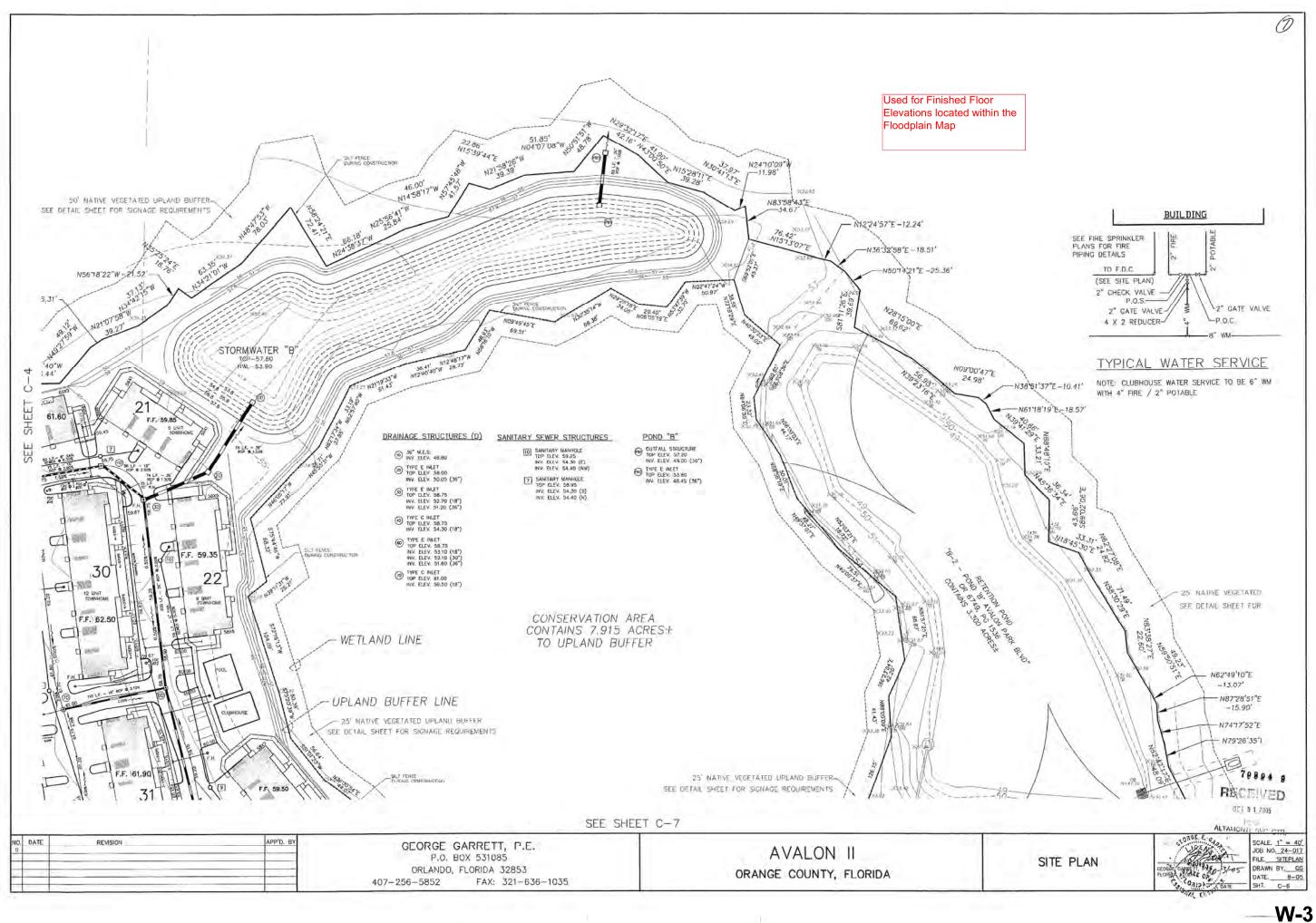
T

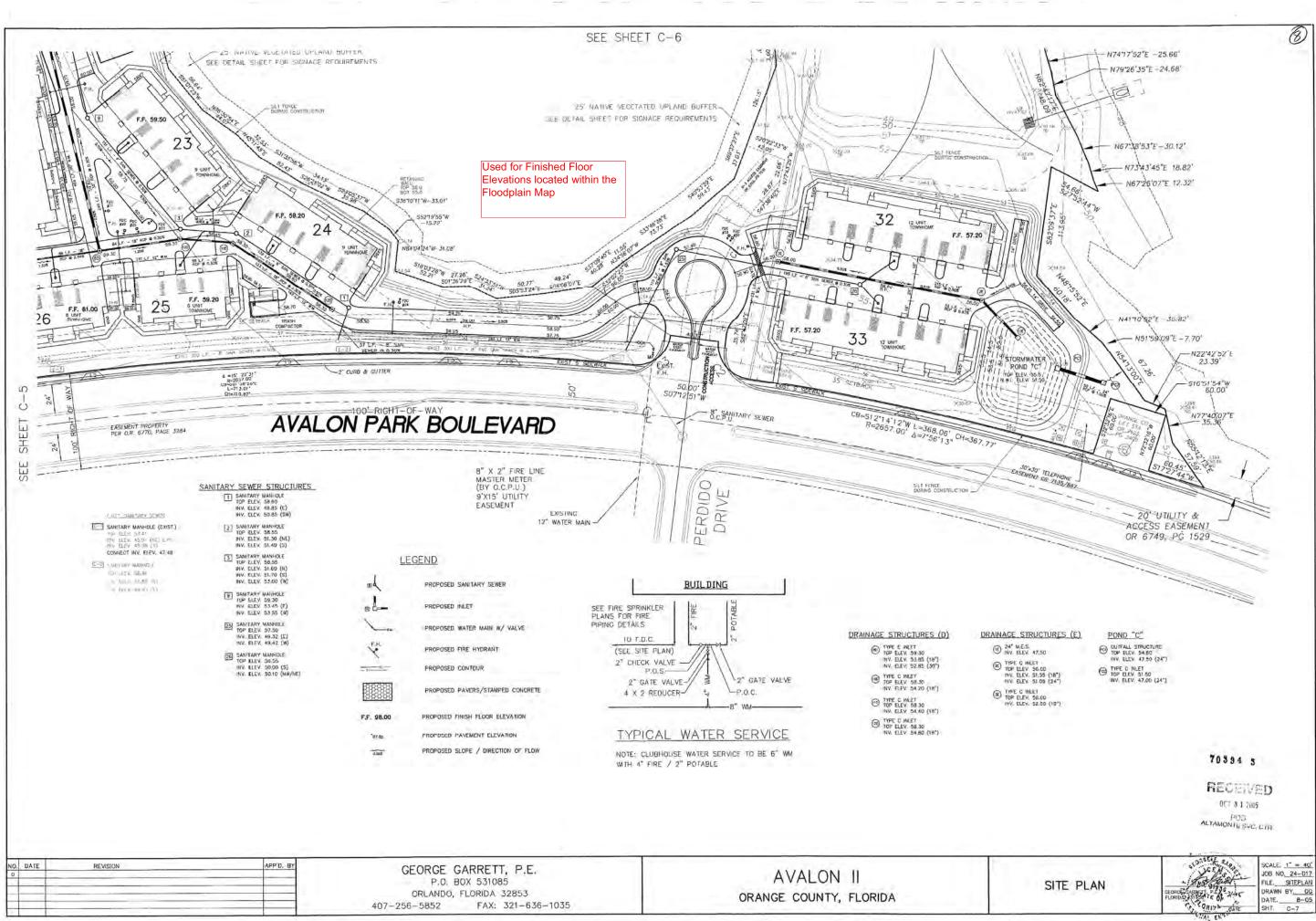
**W-1** 

W



**W-2** 





216.1

**W-4** 

## Appendix: X

SR-50 Field Visit Photos (May 2016)



### SR 50- CD1 (2-8' x 6' CBC) (Looking North Side of the Culvert)



SR 50- CD2 (2-24" RCP)

(North side of the Culvert)



### SR 50-CD3 (2-12.95' x 8.5' CBC)

(South Side of the Culvert)



SR 50-CD4 (1-30" RCP) (South Side of the Culvert)



SR 50-CD5(3-10'x6' CBC) (South Side of the Culvert)



SR 50-CD6 (3-36" RCP) (South side of the Culvert)



#### SR 50-CD7 (1-4' x 4' CBC & 1-54" RCP Jointed)

(South Side of the Culvert)



SR 50- CD8 (1-30" RCP) (South side of the culvert)



SR 50- CD9 (1-8'x7' CBC) (South Side of the Culvert)



SR 50-CD10 (1-10'x4' CBC)

(South Side of the Culvert)



SR 50-CD11 (1-24" RCP) (South Side of the Culvert)

# Appendix: Y

Waterford Lakes Town Center

