CENTRAL FLORIDA EXPRESSWAY AUTHORITY

Final Location Hydraulics Report March 2018



SR 408 Eastern Extension PD&E Study



PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with Metric Engineering, Inc. and I have reviewed or approved the evaluation, findings, opinions and conclusions as reported for:

3 , 1	
PROJECT:	SR-408 Eastern Extension PD&E Study
FINANCIAL PROJECT NUMBER:	CFX-Project No. 408-254
LOCATION:	Orange County
CLIENT:	Central Florida Expressway Authority
collection efforts, and limited calculation evaluations prepared for the conceptual Environment Study for SR-408 Easter procedures and references used to destandard to the professional practice of h	LHR) provides the results of a summary of data of for the proposed cross drains and floodplain all analyses for the Project Development and on Extension project. I acknowledge that the evelop the results contained in this report are hydrologic analysis and hydraulic engineering as and experience. This document is for planning effort required for the final design.
Florida Registered Engineer:	
Name: Chandra S Raman, P.E.	
Registration Number: FL # 58740	
Signature:	
Date:	



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ACRONYMS

PD&E – Project Development and Environment

LHR - Location Hydraulics Report

BHR - Bridge Hydraulics Report

PSR – Pond Siting Report

CFX – Central Florida Expressway Authority

SJRWMD – St. Johns River Water Management District

IDF – Intensity-Duration-Frequency

BMP – Best Management Practices

MSSW – Management and Storage of Surface Waters

FIRM - Flood Insurance Rate Map

FPL – Florida Power & Light Company

SR - State Road



EXECUTIVE SUMMARY

The purpose of the SR-408 Eastern Extension Project Development and Environment (PD&E) study is to develop a proposed improvement strategy that is technically sound, environmentally sensitive and publicly acceptable. As with every PD&E Study, emphasis has been placed on the development, evaluation and documentation of detailed engineering and environmental studies including data collection, conceptual design, environmental analyses, project documentation and the preparation of a Location Hydraulics Report (LHR). The project is located in Orange County, Florida.

The Central Florida Expressway Authority (CFX) is presently evaluating the potential to expand SR-408 from its current eastern terminus at SR-50, locally known as East Colonial Drive, to SR-520 in northeast Orange County. This new seven-mile eastern extension of SR-408 would constitute the first stage towards providing a west-east high-speed corridor with future connectivity to I-95; enhancing safety, capacity and mobility for the region and CFX's customers. After a comprehensive evaluation process of various typical sections, horizontal alignment combinations, and public involvement efforts, a recommended alignment was selected.

The proposed SR-408 Eastern Extension project is divided into three segments based on the land use characteristics. Segment 1 is more urban in nature and exhibits a higher traffic demand than Segments 2 and 3. Segment 1 is from the beginning of the SR-50/SR-408 interchange to Avalon Park Boulevard. Segments 2 and 3, beginning east of Avalon Park Boulevard to SR-520 at the east end of the study area, exhibit more of a rural tendency.

The purpose of this LHR is to identify and discuss the proposed cross drains throughout the project corridor. There are fourteen new cross drains identified for this project. The cross drains were sized appropriately using HY-8 program to minimize the impacts to flood elevations and limits of the floodplain. The cross drain analysis indicates the proposed structures will be able maintain hydraulic connectivity within the tributaries, wetlands or floodplains that the project crosses without significant increase in the existing flood elevation. Thus, the project will not affect existing flood heights or floodplain limits. This project will not cause significant change in the potential for interruption or termination of emergency service or emergency evacuation routes in the surrounding areas. Therefore, it has been determined that the encroachment due to the proposed roadway is not significant.

1.0 INTRODUCTION

The vision of this enhanced west-east corridor has been documented in prior concept studies prepared by CFX, including the SR-408 Eastern Extension Concept Development and Evaluation Study completed in 2008. The limits of this study generally extend from the current terminus of SR-408 at SR-50 to the vicinity of the SR-50/SR-520 intersection. The project location and vicinity are shown in **Appendix-A**. The proposed Typical Sections



for Segment 1 and Segment 2/3 are provided in **Appendix-D**. The SR-408 Eastern Extension is one piece of Florida's Strategic transportation investments to support future growth and create connections between global trade activities, from the Orlando International Airport and the University of Central Florida to Cape Canaveral.

SR-50 is located within the project vicinity and is classified as a major arterial facility. SR-50 provides an important connectivity function between the east Orlando area to the west, and I-95 just south of Titusville to the east. As traffic continues to grow within the study area due to the projected development, it is essential to maintain adequate mobility for the region. A new expressway facility will not only improve mobility but significantly reduce the existing exposure to at-grade conflict points associated with traffic signals and local access issues. In summary, the proposed SR-408 Eastern Extension will greatly enhance Central Florida's regional expressway needs and provide the initial phase of the ultimate vision of an expressway connection from Orlando to I-95.

This report discusses and analyzes proposed cross drains throughout the project corridor. The proposed corridor impacts wetlands and floodplains, therefore the placement of cross drains is crucial to maintain the natural flow. A description of each proposed cross drain is located in Section 4.1 of this report. Exhibits showing proposed cross drains within wetlands and floodplains are in **Appendix-E**. Based on an assumed profile, the proposed culverts are shown along the existing ground based on a 1' contour tin file (**Appendix-F**).

2.0 CROSS DRAIN ANALYSIS METHODOLOGY AND DESIGN CRITERIA

The proposed project alignment is a new corridor. There are no existing cross drains along the proposed project corridor; therefore, the project will consist of all new cross drains. Cross drains were located strategically along the proposed SR-408 Eastern Extension corridor to maintain flow connectivity within the impacted wetlands, floodplains, and Econ River tributaries. There are a total of fourteen cross drains proposed along this new corridor. The flow rates for cross drains 1 through 4 were obtained from the Big Econ River Basin Stormwater Management Master Plan (**Appendix-I**). In accordance with the FDOT Drainage Design Guide for designing culverts, the Rational Method was used to conduct hydrologic analysis for cross drains 5 through 9. The Rational Method was used because the delineated drainage areas for each cross drain were less than 600 acres. Drainage areas were delineated by using a one foot Lidar contour map (St. Johns River Water Management District), existing drainage maps from SR-50 projects, and drainage maps from land development projects along the project corridor. The flow rates for cross drains 10 through 13 were obtained from the Bithlo Area Stormwater Management Master Plan (**Appendix-J**).



2.1 Contributing Flow Determination

Rational Method

- The Rational Method procedures require calculating a peak basin flow rate from the basin characteristics.
- The composite runoff coefficient was calculated based on the percentage of land use for residential, commercial, flat lawns, and woods/wetland areas per the FDOT Hydrology Handbook.
- Time of concentration was calculated using the TR-55 Method.
- The intensity for each storm event was calculated from the FDOT Intensity-Duration-Frequency (IDF) curve for Zone 7.
- The composite coefficient is only designed for a storm period of 10 years. Storm frequency factors were used to adjust the composite runoff coefficient for 25, 50, and 100 year storm events (**Appendix-H**, **Table B-5**).
- Frequency Factor for Return Period 500 year runoff coefficient is not provided in the FDOT Hydrology Handbook; therefore, a log-log graph was created in order to interpolate the peak discharge.
- The Rational Method should only be used for areas up to 600 acres.

2.2 Floodplains/Floodways Criteria

- The proposed project may not cause a net reduction in flood storage within the 10-year floodplain.
- Structures shall cause no more than a one-tenth (0.1) of a flood increase in the 100-year flood elevation 500-feet upstream.
- Proposed construction shall not cause a reduction in flood conveyance capabilities.
- Best Management Practices (BMP's) shall be employed to minimize velocity to avoid undue erosion.
- The design of encroachments shall be consistent with standards established by FEMA.

2.3 Culvert Design Criteria

The following criteria was drawn from the 2018 FDOT Drainage Manual. The following table provides the required storm events to be analyzed for each cross drain per the FDOT Drainage Manual and the FDOT Drainage Design Guide.

Table-1 S	torm Freat	uency Criteria
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Storm Event Frequency	Definitions
50-Year	Design Flood Event
100-Year	Base Flood Event
500-Year	Greatest Flood Event

- All cross drains, if applicable, shall be designed to have sufficient hydraulic capacity to convey the 50-year (Design Frequency) storm event. In accordance with the FDOT Drainage Manual, mainline interstate culverts should be designed for a frequency of 50 years (Appendix-H). All culverts shall be analyzed for the base flood (100 year).
- Backwater shall not significantly change land use values unless flood rights are purchased.
- The headwater for design frequency conditions shall be kept at or below the travel lanes
- The highest tailwater elevation, which can reasonably be expected to occur coincident with the design storm event, shall be used (typically, crown of pipe is used at the outlet).
- The minimum culvert size is 18" or its equivalent size.
- The design of all cross culverts shall comply with the guidelines set forth in the FDOT Drainage Manual, Chapter 4.
- The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.

The criteria listed above was collected from the following applicable sources:

- FDOT Drainage Design Guide Culvert Design (January 2018)
- FDOT Drainage Manual (January 2018)
- FHWA Code of Federal Regulation 23 CFR 650A
- SJRWMD Management and Storage of Surface Waters (MSSW) Permit Information Manual (October 2013)

2.4 Culvert Sizing

All cross drains were sized for a 100-year storm event even though the FDOT design criteria specifies a 50-year Design Frequency. The Big Econ River Basin Stormwater Management Master Plan and Bithlo Area Stormwater Management Master Plan only provided flows and stages for 5-year, 10-year, 25-year, and 100-year. The 50-year and 500-year flows were interpolated by a log-log graph. Since stages were not provided for the 50-year storm event, the 100-year flows and stages were used instead. The calculated 100-year backwater stage elevation from the HY-8 analysis was compared with the existing 100-year flood stage. Culvert trial sizes were determined by using the Manning's Equation. The trial sizes were used to perform HY-8 analysis. While performing the overtopping analysis, the cross drains were appropriately sized to conform with the floodplain criteria in Section 2.2 of this report.



Manning's Equation

- The pipe length was measured from R/W to R/W for each cross drain.
- The change in flow line elevation from upstream to downstream was assumed to be 0.50 ft.
- Manning's "n" value of 0.012 was used.
- The 100-year flow rate for each cross drain was used.

HY-8

- The trial culvert size from the Manning's equation was used for the HY-8 analysis.
- The culvert size was adjusted to maintain backwater stage elevations below the 100-year stage elevation.
- The 10-year flow was the minimum flow, 50-year flow was the design flow, and 100-year flow was the maximum flow.
- The crown of the pipe/top of box culvert or existing SR-50 cross drain DHW elevations were used as the constant tailwater elevations.

3.0 EXISTING CONDITIONS

3.1 Soil Data

The NRCS Soil Survey of Orange County published by United States Department of Agriculture (USDA) has been reviewed for the project. The soil survey map and soil types found throughout the proposed corridor are shown in the complete NRCS USDA Soil Survey located in **Appendix-C**. In general, the superficial soils consist of fine sands, muck and poorly drained soil. The groundwater is at a depth of 0'-3.5' below the existing ground. Refer to **Table-2** below for the most occurring soils within the project area.

Table-2 USDA NRCS Soil Survey Information

Soil No.	Orange County USDA Soil Name	Depth to Water Table	Hydrologic
		(inches)	Soil Group
3	Basinger Fine Sand	0	A/D
15	Felda Fine Sand	0 to 6	A/D
20	Immokalee Fine Sand	6 to 12	B/D
34	Pomello Fine Sand	24 to 42	Α
37	St. Johns Fine Sand	6 to 12	B/D
42	Sanibel Muck	0	A/D
44	Smyrna-Smyrna, Wet, Fine Sand	6 to 18	A/D
51	Wabasso Fine Sand	6 to 18	B/D
53	Wauberg Fine Sand	0 to 6	D
54	Zolfo Fine Sand	24 to 42	Α



3.2 Land Use

The existing land use along the proposed SR-408 Eastern Extension corridor consists mostly of residential developments, commercial properties, and undeveloped areas. The residential areas consist of both multi-family and single-family residences. There are a few commercial properties along the proposed corridor as well. The undeveloped areas are mostly wetlands and upland forests with conservation easements. Please refer to **Appendix-A** for a Land Use map.

3.3 Existing Cross Drains

Considering this is a new alignment, there are not any existing cross drains or bridge structures for review. However, existing cross drains upstream and downstream of the proposed alignment were taken into consideration to maintain functionality and to verify the recommended improvements do not adversely impact the overall drainage function. Refer to **Table-3** for existing SR-50 cross drain information. The SR-50 Straight Line Diagram is in **Appendix-N** and identifies each SR-50 cross drain. The culvert size and 50-Year DHW elevations were obtained from the construction plans in **Appendix-P**, **Appendix-Q**, and **Appendix-R**. There is no evidence of scour or sedimentation of any existing cross drains along SR-50. Refer to **Appendix-S** for photos of the existing SR-50 cross drains.

Table-3 Existing SR-50 Cross Drain General Information

Cross Drain ID	Pipe Description	50-Year DHW EL (ft)	Date of Construction
SR-50 CD-1	2-8'x6' CBC	58.57	2012
SR-50 CD-2	2-24" RCP	53.53	2012
SR-50 CD-3	2-12.95'x8.5' CBC	50.04	2012
SR-50 CD-4	1-30" RCP	54.68	2012
SR-50 CD-5	3-10'x6' CBC	43.70	1960
SR-50 CD-6	3-36" RCP	59.10	1960
SR-50 CD-7	1-4'x4' CBC & 1- 54" RCP Jointed	59.10	1960
SR-50 CD-8	1-30" RCP	66.50	1960
SR-50 CD-9	1-8'x7' CBC	54.80	1960
SR-50 CD-10	1-10'x4' CBC	60.80	1960
SR-50 CD-11	1-24" RCP	61.60	1960



4.0 PROPOSED CONDITIONS

The project corridor will cross through residential homes, commercial businesses, wetlands, wooded areas, and Econ River tributaries. Most tributaries west of the Econ River which cross the proposed SR-408 Eastern Extension corridor flow north and eventually into the Econ River. There is one slough, where UCF is located north of SR-50, which flows south into one of the Econ River tributaries and ultimately flows north to the Econ River. All tributaries east of the Econ River, which cross the proposed SR-408 Eastern Extension corridor, flow south and ultimately flow into the Econ River. Refer to the Drainage Basin Map located on **Page-17**.

4.1 Proposed Cross Drains

The roadway geometry is limited in order to minimize impacts and meet the requirements for the proposed design speed. Different interchange layouts and considerations were made to provide alternative conceptual designs. Fourteen cross drain locations were selected once the alignment and the most effective interchange layouts were identified. The proposed cross drain locations were also chosen based on the natural flow of the land from the surrounding floodplains and wetlands. The proposed SR-408 Eastern Extension corridor will have floodplain impacts along most of the corridor. These floodplain impacts will be mitigated by routing this volume to the project's proposed storm water management facilities, and roadside swales. Refer to **Table-4** for calculated culvert size, flow direction, and floodplain status. Refer to **Table-5** for flood data and **Table-6** for 100-year flows, 100-year stage elevations, tailwater elevations, and backwater stage elevations. Refer to **Appendix-G** for proposed cross drain calculations and HY-8 analyses.



Table-4 Proposed SR-408 Cross Drain General Information

Cross Drain ID	Pipe Description	Flow Direction	Receiving Water Body	Within Floodplain (Yes/No)
05.4			Unnamed	(-
CD-1	3-11'x5' CBC	North	Tributary(1)	Yes (Zone A)
_			Unnamed	
CD-2	4-10'x5' CBC	South	Tributary(1)	Yes (Zone A)
			Unnamed	
CD-3	3-11'x7' CBC	North	Tributary(1)	Yes (Zone A)
			Unnamed	
CD-3A	1-30" RCP	South	Tributary(2)	Yes (Zone A)
			Unnamed	
CD-4	2-8'x4' CBC	North	Tributary(2)	Yes (Zone A)
CD-5	2-72" RCP	North	Floodplain	Yes (Zone A)
CD-6	2-72" RCP	North	Floodplain	Yes (Zone A)
CD-7	2-48" RCP	South	Wetland	Yes (Zone X)
CD-8	1-10'x5' CBC	South	Wetland	Yes (Zone X)
CD-9	1-72" RCP	South	Floodplain	Yes (Zone AE)
CD-10	2-6'x4' CBC	South	Channel E	Yes (Zone AE)
CD-11	2-24" RCP	South	Channel K	Yes (Zone A)
CD-12	2-8'x4' CBC	South	Channel KE	Yes (Zone A)
CD-13	1-48" RCP	South	Channel M	Yes (Zone X)



Table-5 Flood Data Summary Table

Structure	Proposed	Size	Design F 50-Yr Storr		Base Fl 100-Yr S Ever	Storm	Overtopping Flood		=lood	Overtopping
Number	Size	Length (ft)	Discharge (cfs)	Stage (ft)	Discharge (cfs)	Stage (ft)	Discharge (cfs)	Stage (ft)	Storm Frequency	EL (ft)
CD-1	3-11'x5' CBC	485	1160.00	51.97	1322.00	52.45	4902.10	88.87	>500 Yr	88.87
CD-2	4-10'x5' CBC	302	1499.00	51.91	1690.00	52.41	5709.63	85.27	>500 Yr	85.27
CD-3	3-11'x7' CBC	400	1770.00	52.05	2000.00	52.51	6240.70	80.88	>500 Yr	80.88
CD-3A	1-30" RCP	303	5.76	57.88	7.69	57.95	84.31	75.41	>500 Yr	75.41
CD-4	2-8'x4' CBC	456	427.00	52.03	496.00	52.95	1727.16	82.31	>500 Yr	82.31
CD-5	2-72" RCP	374	226.00	51.51	312.00	52.46	1603.28	84.25	>500 Yr	84.25
CD-6	2-72" RCP	427	190.00	52.10	259.00	52.91	1588.91	84.64	>500 Yr	84.64
CD-7	2-48" RCP	129	165.00	61.86	231.00	63.17	384.40	68.47	<500 Yr	68.47
CD-8	1-10'x5' CBC	447	223.00	54.27	309.00	54.96	1356.63	84.68	>500 Yr	84.68
CD-9	1-72" RCP	300	153.00	43.51	212.00	44.45	532.70	54.79	>500 Yr	54.79
CD-10	2-6'x4' CBC	310	353.00	44.11	398.00	44.69	896.98	55.97	>500 Yr	55.97
CD-11	2-24" RCP	395	21.00	58.98	24.00	59.28	107.98	83.94	>500 Yr	83.94
CD-12	2-8'x4' CBC	522	373.00	54.57	409.00	54.89	1405.58	75.36	>500 Yr	75.36
CD-13	1-48" RCP	325	42.00	56.50	51.00	56.73	173.94	64.50	>500 Yr	64.50

^{**} The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.



Table-6 Summary of Proposed SR-408 Cross Drains (HY-8 Analysis)

Cross Drain	HY-8 Cross Drain Size	100-Year Flow (cfs)	Existing Ground EL (ft)	Tailwater EL (ft)	Existing 100- Year EL (ft)*	Backwater Stage Based on HY-8 (ft)
CD-1	3-11'x5' CBC	1322	51.00	50.04	52.70 ¹	52.45
CD-2	4-10'x5' CBC	1690	49.38	50.04	52.70 ¹	52.41
CD-3	3-11'x7' CBC	2000	45.00	50.04	52.70 ¹	52.51
CD-3A	1-30" RCP	7.69	57.71	57.80	58.00	57.95
CD-4	2-8'x4' CBC	496	49.00	50.40	53.70 ¹	52.95
CD-5	2-72" RCP	312	49.00	49.73	53.04 ³	52.46
CD-6	2-72" RCP	259	51.00	49.73	53.04 ³	52.91
CD-7	2-48" RCP	231	57.40	60.50	63.56	63.17
CD-8	1-10'x5' CBC	309	48.51	53.51	55.03	54.96
CD-9	1-72" RCP	212	37.50	42.50	45.00	44.45
CD-10	2-6'x4' CBC	398	38.00	42.00	45.40 ²	44.69
CD-11	2-24" RCP	24	58.00	58.00	59.50 ²	59.28
CD-12	2-8'x4' CBC	409	51.00	53.00	55.50 ²	54.89
CD-13	1-48" RCP	51	55.00	56.00	57.10 ²	56.73

^{*} The existing 100-year elevations from the sources listed below were converted from NGVD to NAVD by subtracting 1.1 ft.

¹ Big Econ Stormwater Management Master Plan (Appendix-I)

² Bithlo Area Stormwater Management Master Plan (**Appendix-J**)

³ Waterford Trails Construction Plans from Harling Locklin & Associates, Inc. (Appendix-L)

^{**} The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.



The proposed alignment will impact wetlands; therefore, CD-1 was strategically placed to maintain the flow connectivity between wetlands and the Econ River tributary that flows south through proposed CD-2 and then north through proposed CD-3. The culvert will convey runoff from one side of the road to the other while replicating the natural flow of the tributary. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 1322 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL015X, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.45 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 3-11'x5' concrete box culverts.

CD-2

CD-2 was proposed in order to maintain flow connectivity of the existing slough, which drains from the north to the south into a tributary. The tributary flows north through proposed CD-3 and drains into the Econ River. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 1690 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL020C, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.41 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 4-10'x5' concrete box culverts.

CD-3

CD-3 maintains flow connectivity to a tributary, which flows north into the Econ River. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 2000 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL030C, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.51 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 3-11'x7' concrete box culverts.

CD-3A

The basin area is approximately 2.35 acres. A time of concentration of 10 minutes was assumed. The crown of the pipe was used as the tailwater. The DHW elevation of 58.00 ft was obtained from SJRWMD Permit 100527 (**Appendix-X**). The calculated backwater stage elevation of 57.95 ft from HY-8 analysis is less than the existing 100-year flood elevation of 58.00 ft; therefore. The 100-year flow of 7.69 cfs was calculated using the Rational Method. The proposed culvert size from the HY-8 analysis are 1-30" RCP. The culvert will convey runoff from the wetlands that are severed by the proposed corridor, which flows southeast to the tributary that flows north and drains into the Econ River.



The culverts will maintain flow connectivity to a tributary, which flows north into the Econ River. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.70 ft and the 100-year flow of 496 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEBE195X, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.95 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.70 ft. The proposed culvert sizes from the HY-8 analysis are 2-8'x4' concrete box culverts.

CD-5

The basin area is approximately 109.03 acres. A time of concentration of 1.39 hours was calculated for this basin area using the TR-55 method. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.04 ft was obtained from SJRWMD Permit 70394-1 (Appendix-L). The calculated backwater stage elevation of 52.46 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.04 ft. The 100-year flow of 312 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-72" pipes. The culvert will convey runoff from the wetlands to the tributary which flows north and drains into the Econ River. There is forty-six feet of space from the edge of the proposed ramp to the right-of-way line; therefore, a by-pass swale can be constructed in order to provide flow connectivity from CD-5 to CD-6 (Appendix-E, Page-E3). In addition to the one foot contour map, two drainage maps (Appendix-O and Appendix-R) were used to determine the basin area.

CD-6

CD-6 will maintain flow connectivity between the wetlands that will be severed by the proposed SR-408 Eastern Extension alignment. The runoff from the wetlands flows north and drains into the Econ River. The basin area is approximately 119.01 acres. The time of concentration was calculated for this basin area using the TR-55 method. The total time of concentration for this basin area is 1.44 hours. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.04 ft was obtained from SJRWMD Permit 70394-1 (**Appendix-L**). The calculated backwater stage elevation of 52.91 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.04 ft. The 100-Year flow of 259 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-72" pipes. There is forty-six feet of space from the edge of the proposed ramp to the right-of-way line; therefore, a by-pass swale can be constructed in order to provide flow connectivity from CD-5 to CD-6 (**Appendix-E, Page-E3**). In addition to the one foot contour map, a regional drainage map (**Appendix-O**) was used to determine to the basin area.



CD-7 will provide flow connectivity between wetlands that will be severed by the proposed CR 419 (Chuluota Road) corridor. The runoff flows south through proposed CD-8 and drains into the Econ River. The basin area is approximately 77.95 acres. A time of concentration of 1.54 hours was calculated for this basin area using the TR-55 method. The crown of pipe was used as the tailwater. The 100-year elevation of 63.56 ft was obtained from SJRWMD Permit #27625-4 (Appendix-M). The calculated backwater stage elevation of 63.17 ft from HY-8 analysis is less than the existing 100-year flood elevation of 63.56 ft. The 100-year flow of 231 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-48" RCP. A one foot contour map was used to delineate the basin area for this cross drain. This basin area consists of single-family residential homes, several commercial businesses located on SR-50, several ponds, and woodland areas.

CD-8

The culvert will convey runoff from the severed wetlands to the tributary which flows south and drains into the Econ River. The total basin area for CD-8 is 121.44 acres and consists of two basin areas, which includes the basin area for CD-7. The time of concentration was calculated for this basin area using the TR-55 method. The total time of concentration calculated for this basin area is 1.68 hours. The elevation from the top of the box culvert used as the tailwater. The 100-year elevation of 55.03 ft was averaged from two 100-year elevations of 63.56 ft from existing Pond 200 and 46.50 ft from existing Pond 100 (SJRWMD Permit #27625-4, **Appendix-M**). CD-8 is located between existing Pond 200 and existing Pond 100. The calculated backwater stage elevation of 54.96 ft from HY-8 analysis is less than the existing 100-year flood elevation of 55.03 ft. The 100-year flow of 309 cfs was calculated using the Rational Method. The proposed culvert size from the HY-8 analysis is a single 10'x5' concrete box culvert. A one foot contour map was used to delineate the basin area for this cross drain. This basin area consists of single-family residential homes, several commercial businesses located on SR-50, several ponds, and woodland areas.

CD-9

The basin area is approximately 75.82 acres. A time of concentration of 1.66 hours was calculated for this basin area using the TR-55 method. The calculated flow rate for a 100-year storm event is 212 cfs. The 100-year flood elevation of 45.00 ft was obtained from the FEMA Flood Map (**Appendix-B**). The top of the box culvert was used as the tailwater for this culvert. The calculated backwater stage elevation of 44.45 ft from HY-8 analysis is less than the existing 100-year flood elevation of 45.00 ft. The proposed culvert size from the HY-8 analysis is a single 72" RCP. The culvert will convey runoff from the wetlands to the tributary which flows south and drains into the Econ River. A one foot contour map was used to delineate the basin area for this cross drain.



CD-10 will maintain flow connectivity from Channel E that flows south into the Econ River. The proposed alignment interrupts the natural flow of Channel E; therefore, culverts will be strategically placed where the proposed corridor and the channel intersect. The elevation from the top of the box culvert was used as the tailwater. The 100-year stage elevation of 45.40 ft and 100-Year flow of 398 cfs for Channel E (Node ID: NE-020, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 44.69 ft from HY-8 analysis is less than the existing 100-year flood elevation of 45.40 ft. The proposed culvert sizes from the HY-8 analysis are 2-6'x4' concrete box culverts.

CD-11

CD-11 will provide flow connectivity between a wetland and Channel K that will be severed by the proposed SR-408 Eastern Extension corridor. The proposed cross drain location is on an existing wetland that is east of CR13. The crown of pipe was used as the tailwater. The proposed location of CD-11 lies directly on a Wetland East of CR13 (Node ID: NK-130, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan. The wetland has a 100-year stage elevation of 59.50 ft and a 100-year flow of 24 cfs, which were used to size this cross drain. The calculated backwater stage elevation of 59.28 ft from HY-8 analysis is less than the existing 100-year flood elevation of 59.50 ft. The proposed culvert sizes from the HY-8 analysis are 2-24" pipes.

CD-12

The new alignment interrupts the natural flow of Channel KE. To maintain the natural flow connectivity of Channel KE, concrete box culverts will be strategically placed where the proposed roadway and channel intersect. The culverts will convey runoff from one side of the road to the other as it flows south towards the Econ River. The elevation from the top of the box culvert was used as the tailwater. The 100-year stage elevation of 55.50 ft and 100-Year flow of 409 cfs for Channel KE (Node ID: NKE-080, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 54.89 ft from HY-8 analysis is less than the existing 100-year flood elevation of 55.50 ft. The proposed culvert sizes from the HY-8 analysis are 2-8'x4' concrete box culverts. The existing upstream pipe size is a single 10'x4' concrete box culvert, therefore, the calculated culvert sizes of 2-8'x4' CBC are larger than the existing upstream culvert and will not restrict flow.

CD-13

The new alignment interrupts the natural flow of Channel M. To maintain the natural flow of Channel M, CD-13 will be strategically placed where the proposed roadway and channel intersect. This pipe will convey runoff from Channel M to the existing pond M-1. The crown of pipe was used as the tailwater. The 100-year stage elevation of 57.10 ft and 100-Year flow of 51 cfs for Channel M (Node ID: NM-070, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 56.73 ft from HY-8 analysis is less than the



existing 100-year flood elevation of 57.10 ft. The proposed culvert size from HY-8 is a single 48" pipe. Pond M-1 will also be modified due to the proposed alignment. Please refer to **Appendix-K** for oversized drawings of pond M-1.

4.2 Floodplain Impacts

The project will impact the 100-year floodplain in three different ways:

- 1) Longitudinal roadway widening impacts resulting from filling the floodplain areas associated with Econ River and its tributaries.
- 2) Impact due to proposed pond locations in floodplain.
- 3) Impact due to proposed cross drains in floodplain.

The longitudinal impact due to the recommended SR-408 Eastern Extension alignment cannot be avoided. During the final design phase of the project, every effort should be taken to minimize floodplain impacts. During the design phase, floodplain impacts should be mitigated by routing to proposed stormwater management facilities and roadside swales. Also, a Bridge Hydraulics Report (BHR) will be prepared during the design phase to document the hydraulic impacts of the recommended SR-408 Eastern Extension alignment.

The FEMA's Flood Insurance Rate Map (FIRM) for Orange County shows that a portion of the project lies within the 100-year floodplain areas Zone AE (100 year Base flood elevations are provided) and Zone A (100 year base flood elevations are not provided, areas with 1% change of flooding). Most of the project lies within flood Zone X (Areas of minimal flood hazard and above the 500-year flood zone). FEMA Map No. 12095C0280F, 129095C0285F, 12095C0295F and 12095C0315F, provide flood information for the project. Floodplain impact will occur throughout the project corridor and includes the Econ River and its tributaries. Please refer to **Appendix-A** for a FEMA exhibit and **Appendix-B** for a FEMA Flood Insurance Rate Map.

The total floodplain impact due to roadway fill for the entire proposed project corridor is 100.28 ac-ft. Available compensation in the proposed stormwater ponds and floodplain compensation ponds are 107.47 ac-ft. Please refer to Table-7 in the PSR for a summary of floodplain impacts and compensation. The dredge and fill volume are based on limited information available during the PD&E study. A detail evaluation has to be done during the final design. Based on the preliminary evaluation the project will provide more floodplain compensation than the impact. Therefore, a cup for cup compensation is provided by the project.

Two floodplain compensation pond sites were identified for this project in Basin 11C. The pond sites are Pond 11C3 and Pond 11C4. Both Pond 11C3 and Pond 11C4 are selected as the recommended floodplain compensation ponds. Beside this two floodplain compensation ponds, several stormwater ponds located adjacent to floodplains will also provide floodplain compensation. Please refer to Table-7 in the PSR. At certain segments of the project, for example at Basin 11C, the roadway profile is low enough to provide



floodplain compensation in the swales; this option should be evaluated during the design phase.

Runoff from within the corridor will be collected and conveyed to stormwater management facilities; therefore, reducing the overall impact to the remaining floodplains. The preliminary hydraulic evaluation indicates the flood elevation and limits will not change significantly; therefore, it is assumed that the project will not have a significant impact and the encroachment will be minimal.

4.3 Project Classification

The floodplain is in a medium density, semi-urbanized area and the encroachments are classified as "minimal". Minimal encroachment of a floodplain occurs when there is floodplain involvement, but the impacts on human life, transportation facilities, and natural and beneficial floodplain values are not significant and can be resolved with minimal efforts. Normally, these minimal efforts to address the impacts will consist of applying the FDOT drainage design standards and following the Water Management procedures to achieve results that will not increase or significantly change the flood elevation and the floodplain limits.

4.4 Flooding History and Maintenance Concern

In a phone interview with FDOT maintenance staff at the Oviedo Operations Center on 7/8/2016; there are no areas of flooding concern along the SR-50 corridor. The staff member Mike Danos mentioned that there have been no reports of flooding or overtopping within the SR-50 corridor. The proposed SR-408 Eastern Extension alignment is located just south of SR-50. Due to the close proximity of the proposed SR-408 Eastern Extension project to existing SR-50, flooding history of SR-50 will be used as a comparison for this project. Future investigation regarding flooding concerns at the proposed SR-408 Eastern Extension project corridor should be conducted during the final design.

5.0 BRIDGE HYDRAULICS EVALUATION

Bridges are proposed at the Econ River and at a major Econ River Tributary (Channel A) just east of the FPL Transmission Line (Sta. 660+00). Both proposed bridges will maintain flow conveyance in the Econ River and its major tributary. Bridge Hydraulic Reports for these proposed bridges shall be prepared during the design phase. The proposed Econ River Bridge will span over the river without impacting the floodplain or wetland. Please refer to the Bridge Analysis Report for the determination of bridge length, span and the pier locations. There is minimal impact to the floodplain due to the bridge piers. Refer to the Drainage Basin Map on Page-17, Econ River Basin Map on Page-18, Floodplain and Wetland Exhibits in Appendix-E, and Bridge Profiles in Appendix-F. The flows and stages in Table-7 for the Econ River Bridge were obtained from the Big Econ River Stormwater Management Master Plan (Model ID: BEBE160X, Appendix-I). The flows and stages in Table-7 for the Econ River Tributary Bridge were obtained from the Bithlo



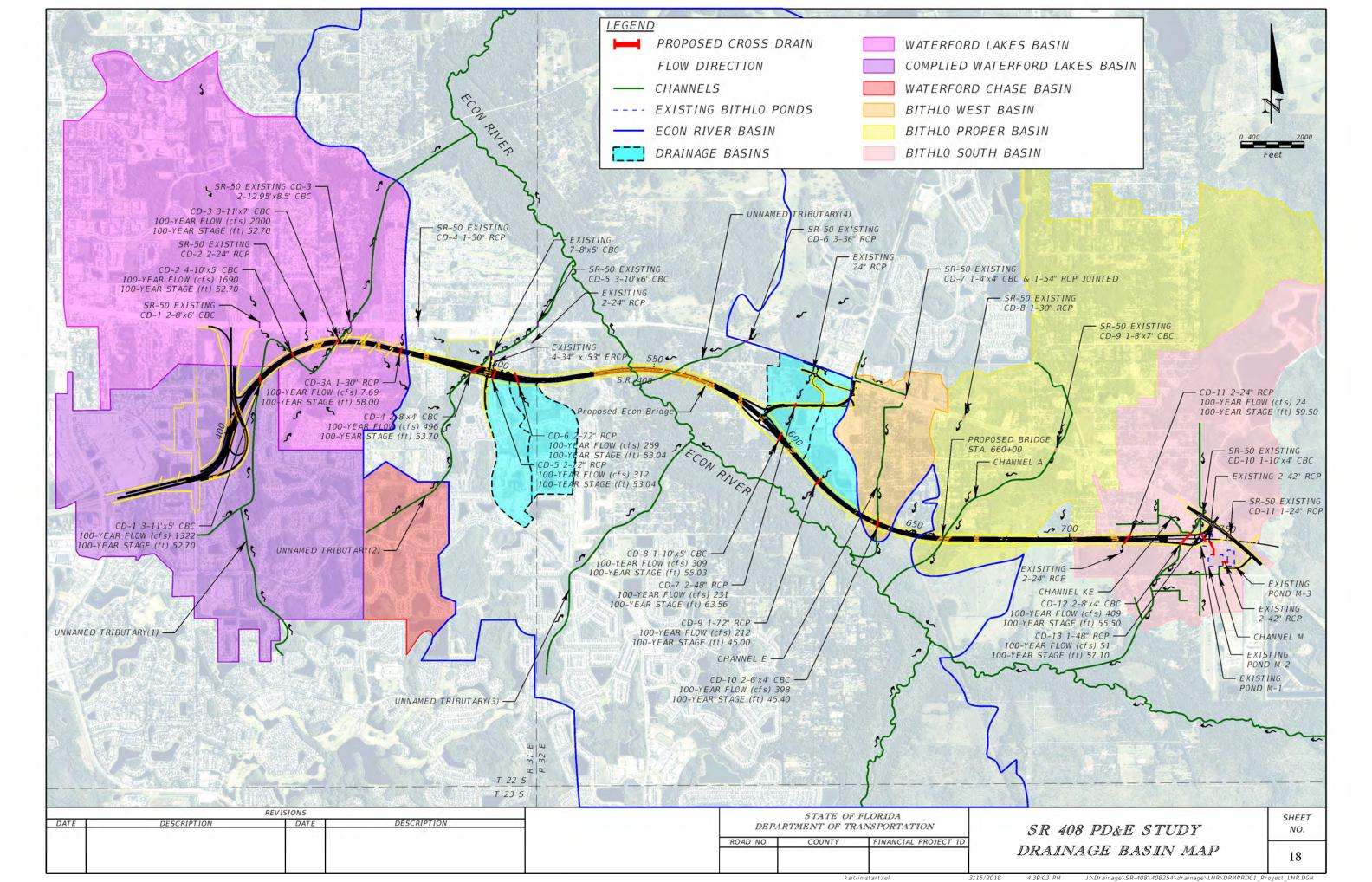
Area Stormwater Management Master Plan (Node ID: NA-060, **Appendix-J**). The Econ River Tributary Bridge will need to account for additional runoff from a small area between Station 649+50 to 651+00. It is assumed that the proposed bridge over the Econ River will not increase the flood stage or the flood limits. Minor floodplain impacts are anticipated due to the bridge pier placement. Overall, insignificant impacts are anticipated at the Econ River. During the design phase, a FEMA No-Rise Certification should be assessed.

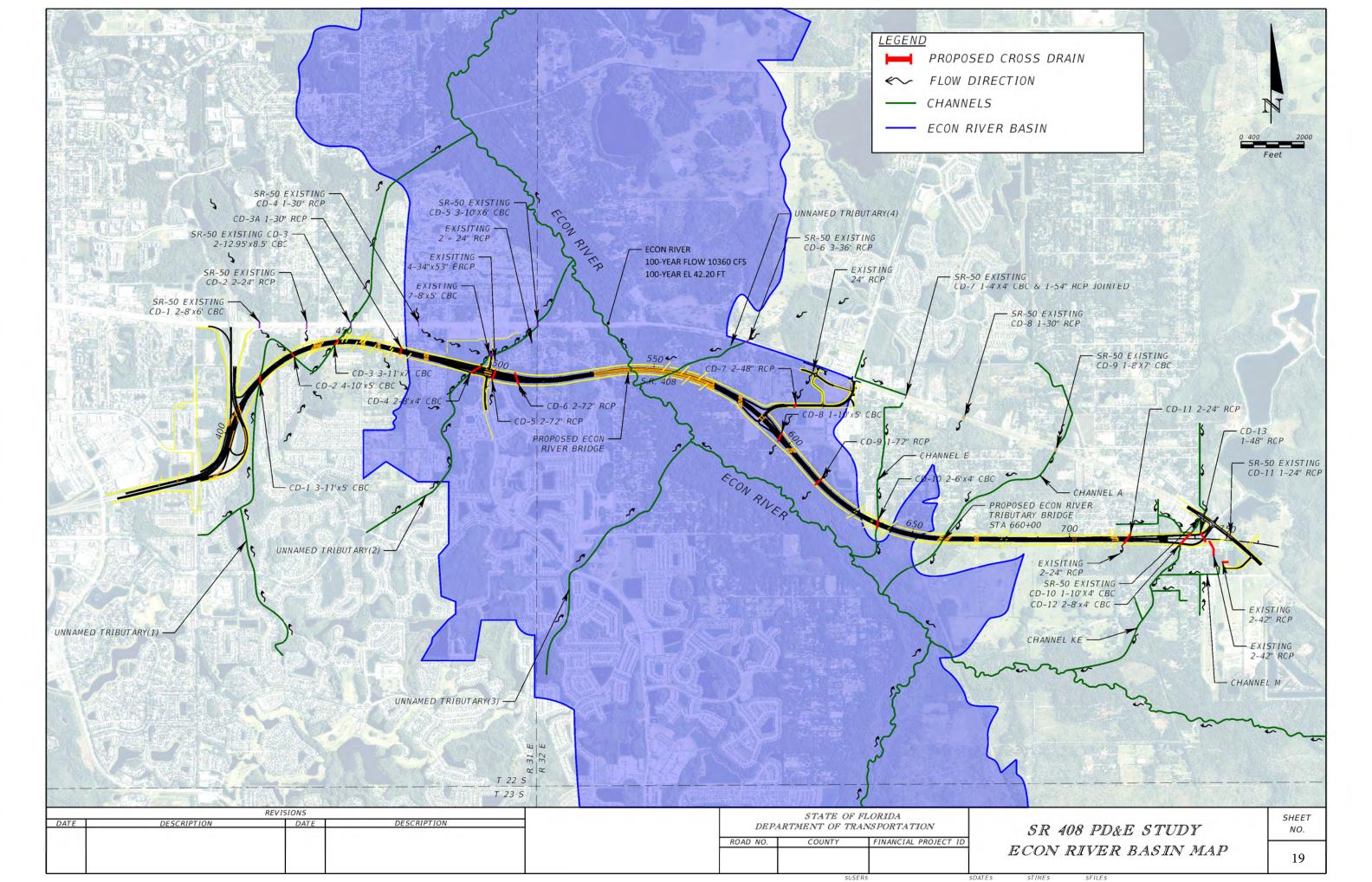
Bridge 100-Year 100-Year **Bridge Low** Bridge Existing Bridge Flow Clearance Length Structure EL Member EL Ground EL (ft) (cfs) (ft) (ft) (ft) (ft) 31.00 42.20 Econ River 10360 42.20 74.41 3820 **Econ River** Tributary Channel A) 697 48.30 63.41 40.00 16.87 300

Table-7 Proposed SR-408 Bridge Structure Information

6.0 CONCLUSION

The purpose of this report was to determine potential cross drain locations along the proposed SR-408 Eastern Extension project corridor to reduce impacts to floodplains and wetlands. The proposed alignment will cross through residences, commercial businesses, wetlands, Econ River tributaries, and wooded areas. These proposed cross drain locations were chosen based on maintaining the natural flow of the land from the surrounding floodplains, wetlands, and Econ River tributaries. Fourteen potential cross drains were selected and analyzed for this project. The 100-year flow rates for cross drains 1 through 4 were obtained from the Big Econ River Basin Stormwater Management Master Plan. The 100-year flow rates for cross drains 10 through 13 were obtained from the Bithlo Area Stormwater Management Master Plan. The Rational Method was used to determine the flow for cross drains 5 through 9. Each cross drain was designed for a 100year storm event, in order to compare the 100-year backwater elevation with the 100-year existing flood elevation. Manning's Equation was used to determine trial sizes for each culvert. The trial sizes were used to perform the HY-8 analysis. The floodplains will be impacted due to longitudinal roadway widening and proposed pond locations. By following FDOT design standards and water management procedures, the proposed cross drains will have minimal impacts on the existing floodplains and wetlands. The purpose is to achieve results which do not increase or significantly change existing flood elevations or floodplain limits. The proposed cross drains located within floodplains will have minor volumetric impacts, and insignificant impact to flood stage and flood limits. The final design team should verify the proposed culvert sizes and their locations, based on the final roadway geometry and profile. BHR's for the Econ River Bridge and the Econ River Tributary Bridge should be provided during the design phase. The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.

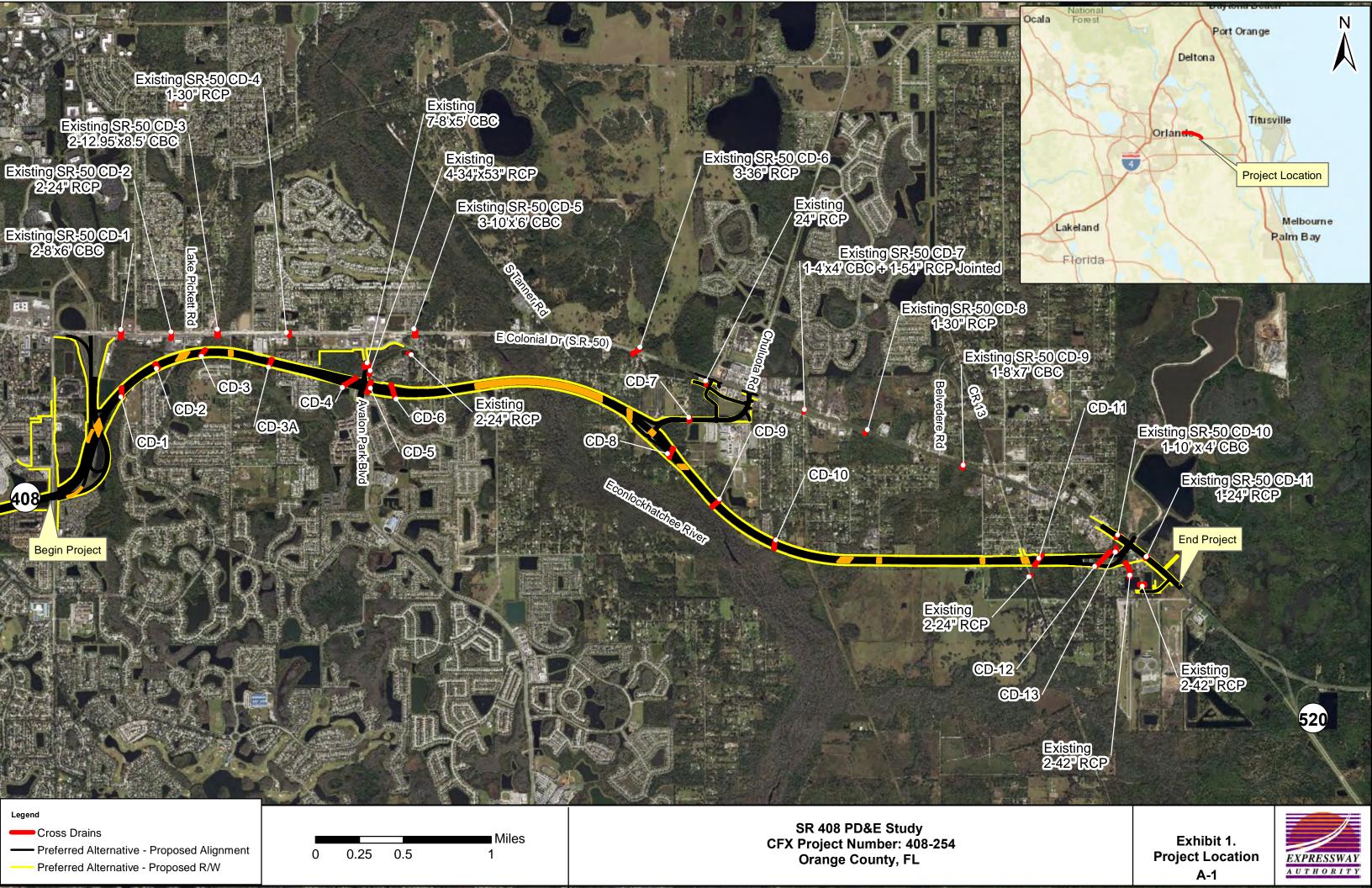


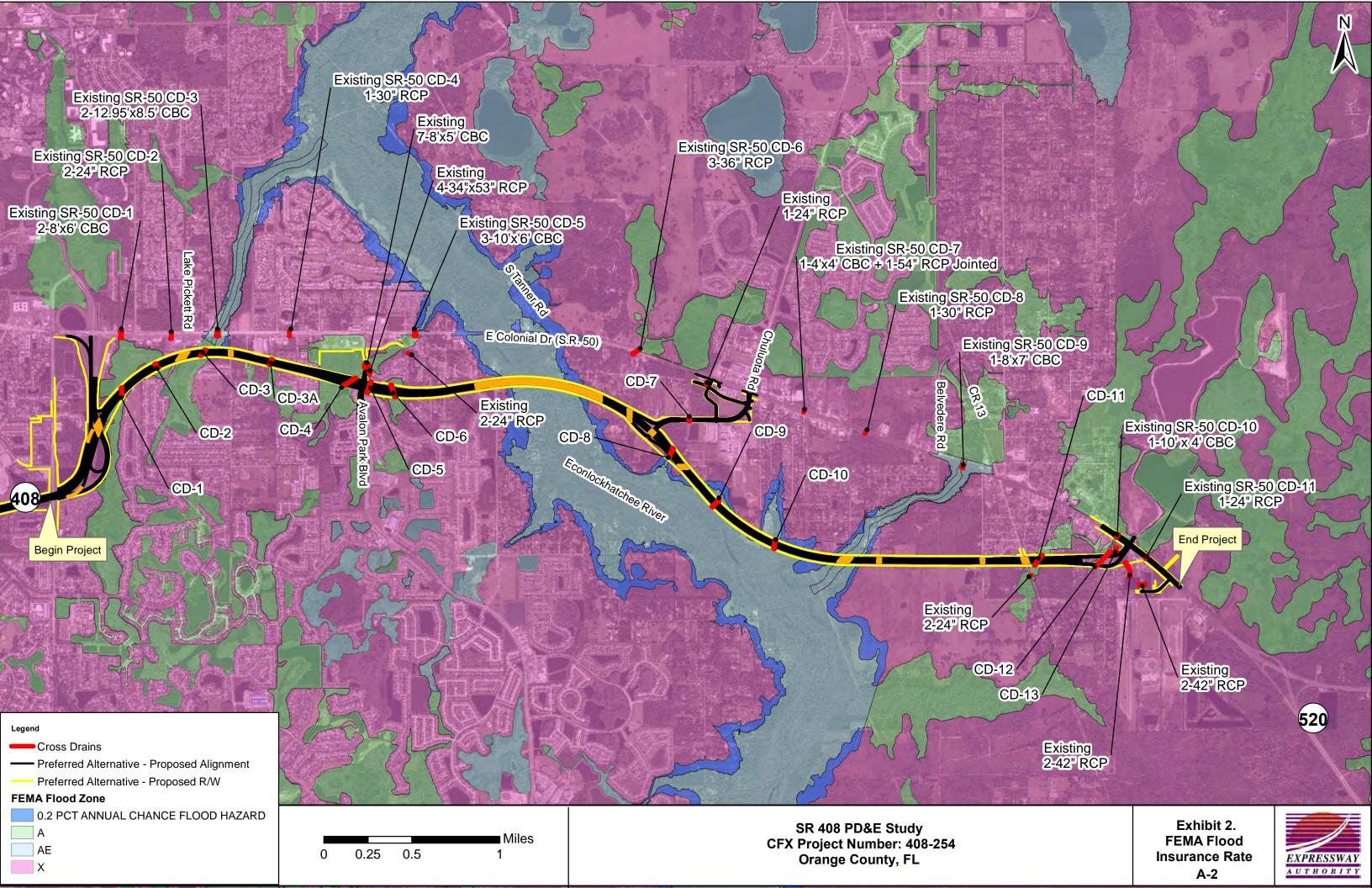


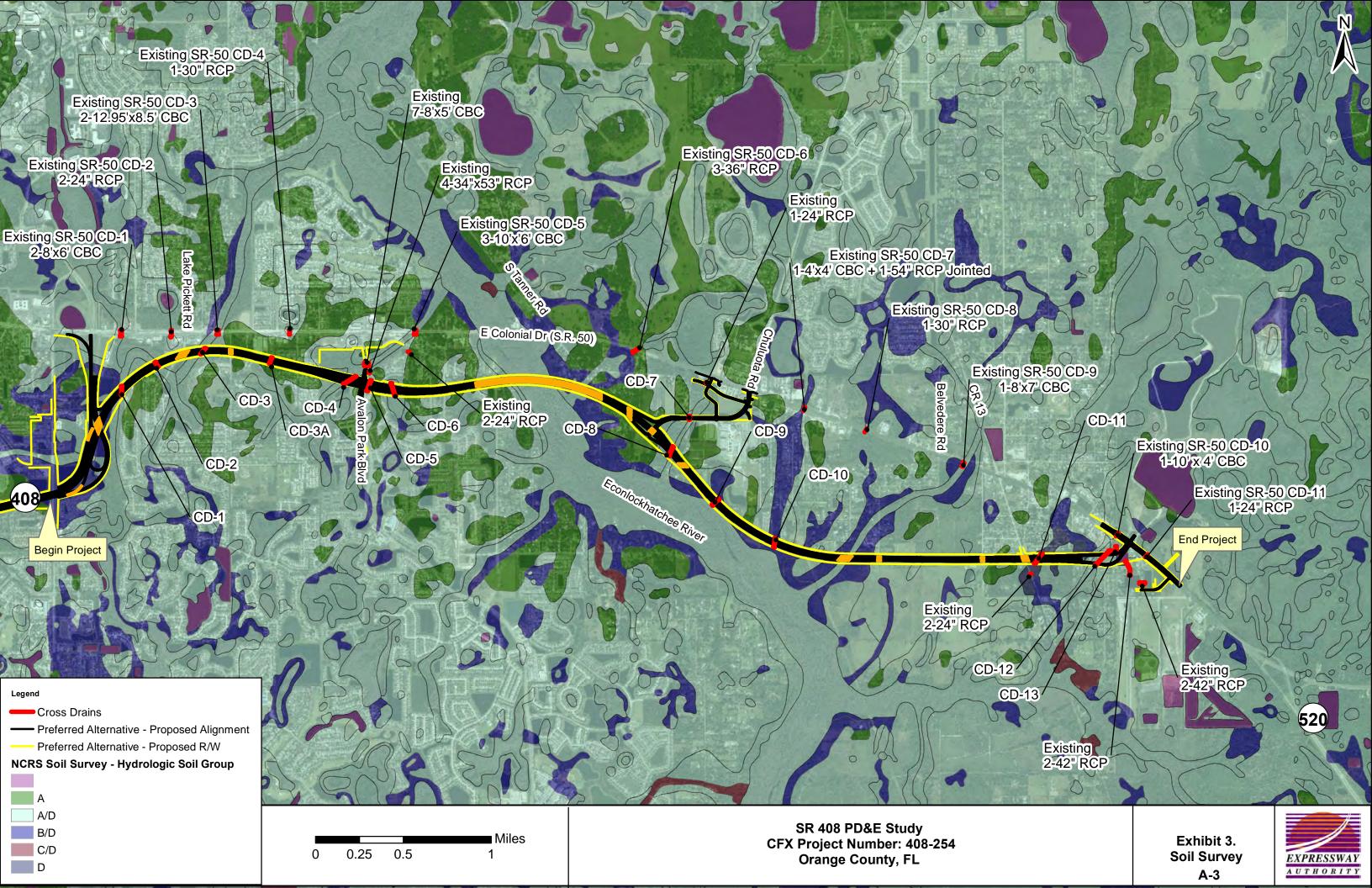
Appendix: A

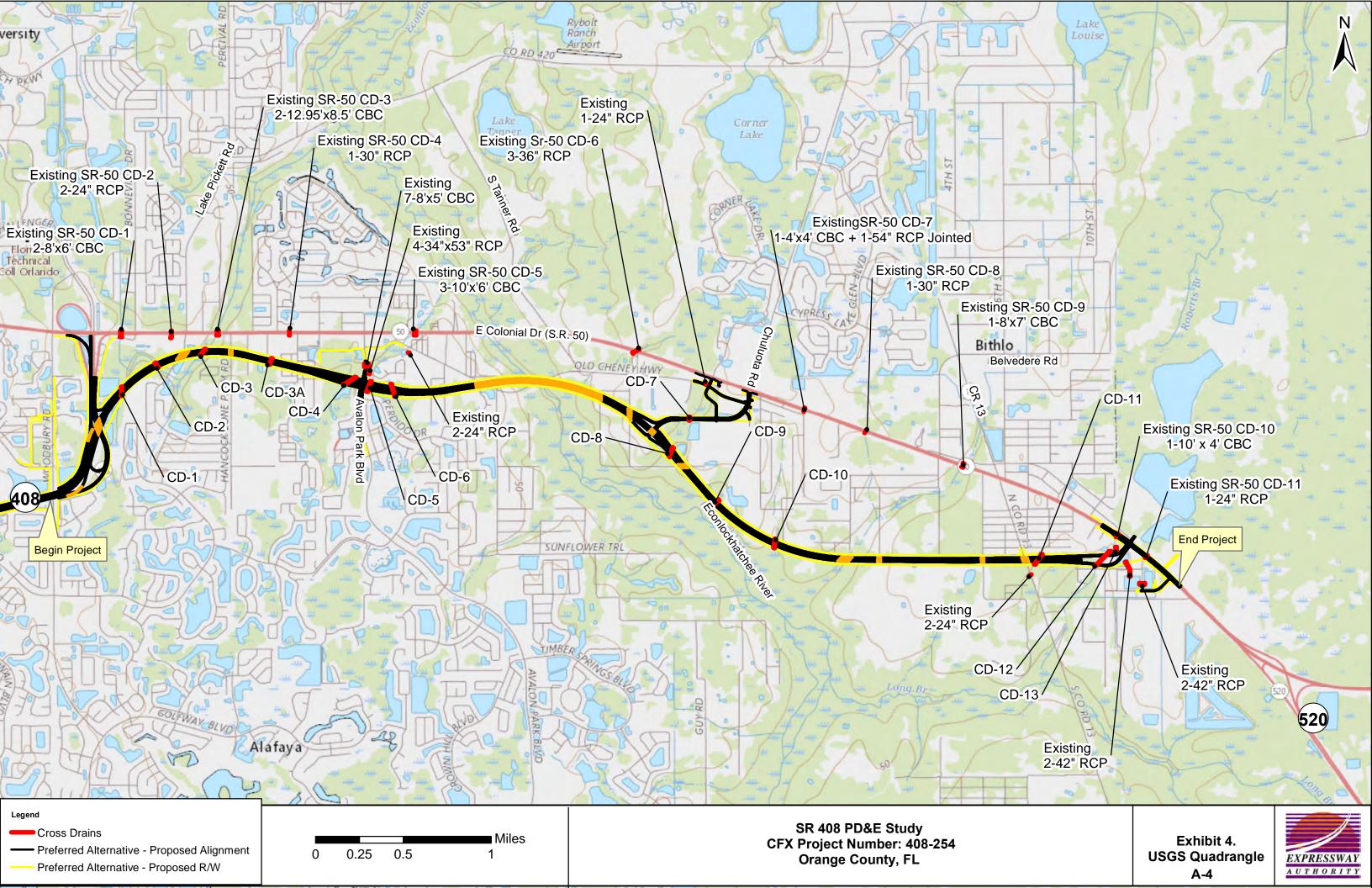
Exhibits:

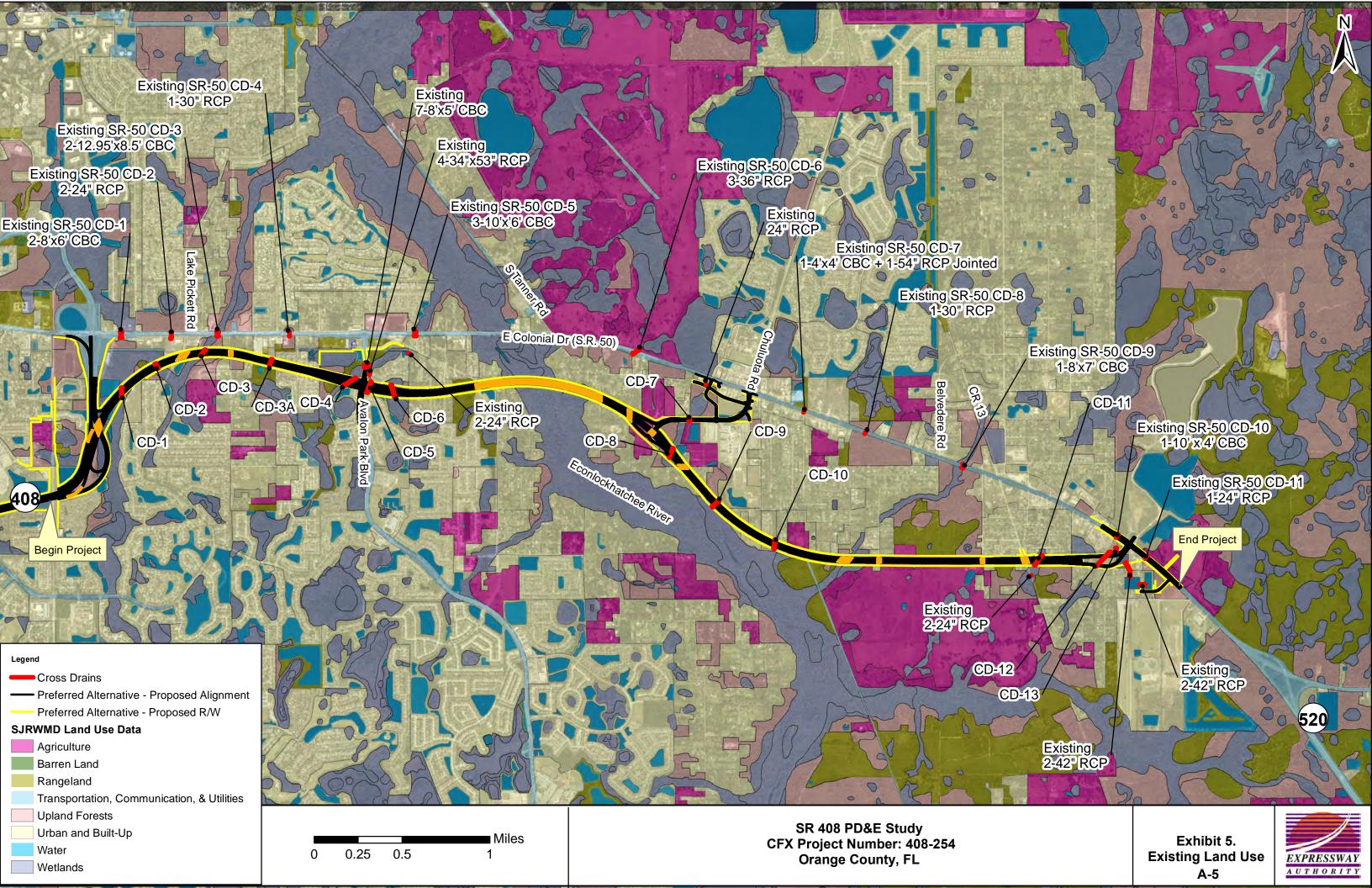
- Project Location Map
- FEMA Flood Insurance Rate Map
- Soil Survey
- USGS Quadrangle Map
- Existing Land Use Map











Appendix: B

FEMA Flood Insurance Rate Map To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations labalogy contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0′ North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or flood/plain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for the surrections.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was State Plane Florida Eas FIPS Zone 0901. The **hortzontal datum** was NAD33, GRS1960 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of PIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of Fisiod elevations on this map are referenced to the viorith American vertical Latum of 1988. These fincid elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodeloc Vertical Datum of 1923 and the North American Vertical Datum of 1988, visit the National Geodeloc Survey website at http://www.mps.mear.gov/j or contact the National Geodeloc Survey at the Following

Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.noaa.gov/.

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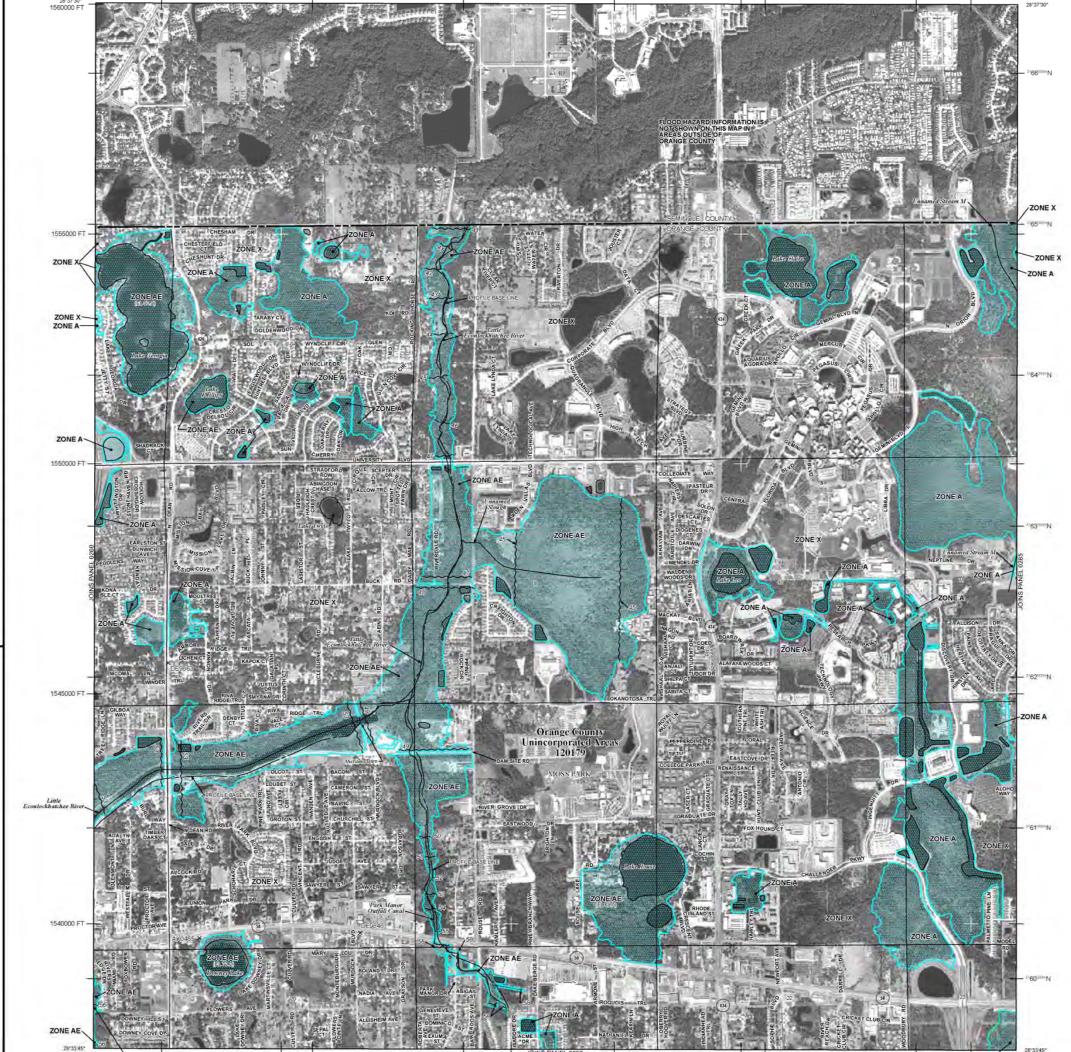
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Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

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NGVD29 to NAVD88 Vertical Datum Conversion Table (feet)

Watershed Name	Minimum	Maximum Conversion	Average Conversion	Maximum Offset
		3-3010-00100	3.01.00	
Big Econlockhalchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.69	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.88	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Miles of the land	0.00	04.00	201	0.07



area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, ASP, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance flood. No Base Flood Elevations determined. Base Flood Elevations determined. Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined. Area of special flood hazard formerly protected from the 1% annual chance flood event by a flood control system that was subsequently describled. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood. Areas to be protected from 1% annual chance flood event by a Federal flood protection system under construction; no Base Flood Elevations determined. Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations Coasta flood zone with velocity hazard (wave action); Base Flood Elevations FLOODWAY AREAS IN ZONE AE is the channel of a stream plus any adjacent floodplain areas that must be kept free so that the 1% annual chance flood can be carried without substantial increases OTHER FLOOD AREAS Areas of 0.2% annual chance flood; areas of 1% annual chance flood with everage depths of less than 1 foot or with chanage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood. OTHER AREAS Areas determined to be outside the 0.2% annual chance floodplain. Areas in which flood hazards are undetermined, but possible. COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS OTHERWISE PROTECTED AREAS (OPAs) CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas 0.2% armual chance floodplain boundary Floodway boundary Zone D boundary CBRS and OPA boundary Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities. ~~~ 513 ~~~ Base Flood Elevation line and value; elevation in feet (EL 987) Referenced to the North Am on Vertical Datum of 1988 (NAVD 88) (A)-—(A) **23-----23** Geographic coordinates referenced to the North American. Datum of 1983 (NAD 83), Western Hemisphere 97'07'30', 32'22'30' 1000-meter Universal Transverse Mercator grid ticks, zone 17 5000-foot grid values: Florida State Plane coordinate system, East Zone (FIPSZONE = 901), Transverse Mercator projection 6000000 FT Bench mark (see explanation in Notes to Users section of this FIRM panel) DX5510 • M1.5 River Mile For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction. e if flood insurance is available in this community, contact your insurance agent or call the od Insurance Program at 1-900-638-6620. MAP SCALE 1" = 1000" 569 1,600 1,500 2,000 FEET PANEL 0280F PROGRAM FIRM FLOOD INSURANCE RATE MAP ORANGE COUNTY, FLORIDA AND INCORPORATED AREAS PANEL 280 OF 750 CONTAINS COMMUNITY NUMBER PANEL SUFFIX



P

12095C0280F

B-1

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Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

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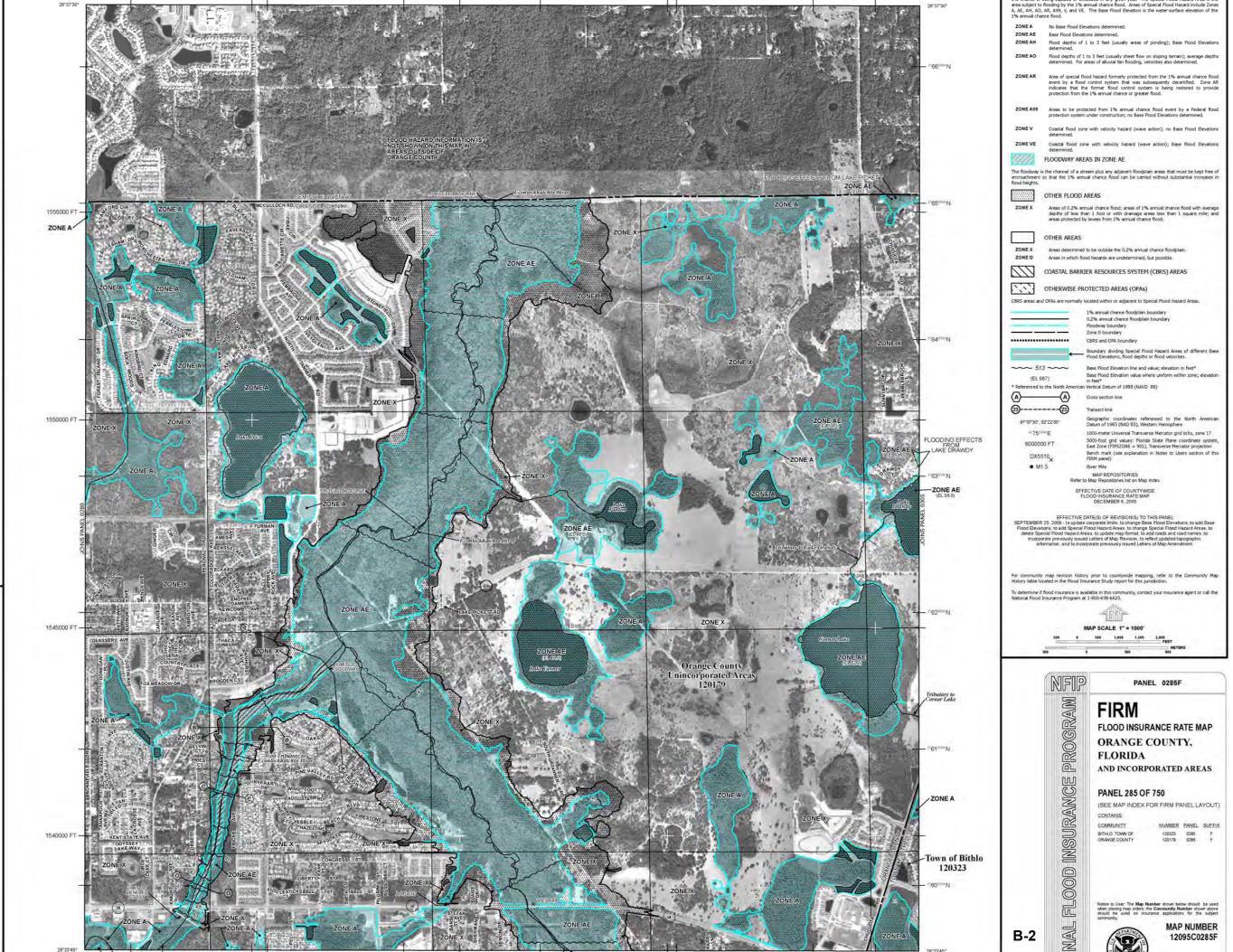
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NGVD29 to NAVD88 Vertical Datum Conversion Table (fee

NGVD25 to NAVD66 Vertical Datum Conversion Table (reet)							
Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset			
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06			
Boggy Creek	-0.91	-1.01	-0.96	0.05			
Cypress Creek	-0.87	-0.91	-0.89	0.02			
Howell Branch	-0.96	-1.05	-0.98	0.07			
Lake Apopka	-0.87	-0.97	-0.91	0.06			
Lake Hart	-0.97	-1.07	-1.02	0.05			
Little Econlockhatchee River	-0.92	-1.07	-1:01	0.09			
Little Wekiva River	-0.91	-1.02	-0.95	0.07			
Reedy Creek	-0.88	-0.89	-0.88	0.02			
Shingle Creek	-0.88	-0.95	-0.91	0.04			
St. Johns River	-1.08	-1.33	-1.19	0.14			
Weldus River	-0.88	-1.01	-0.94	0.07			



To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway. Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM Lesers should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, though every control of the FIRM represent rounded with the FIRM represent rounded with profile of the FIRM represent rounded without and the flood elevation information. Accordingly, the flood elevation data presented in the FIS report should be utilized in conjunction with

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or flood/pain management purposes when they are higher than the elevations shown on this FIRM.

the FIRM for purposes of construction and/or floodplain management.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was State Plane Florida East FIP8 Zone 0901. The **hortzontal datum** was NADS3, GRST980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of Fig. 2 everagins on this map are referenced to the viorin American vertical Latum of 1986. These fixed elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.mgs.noda.gov/ or contact the National Geodetic Survey at the following the National Geodetic Survey at the Nation

Spatial Reference System Division National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ngaa.gov/.

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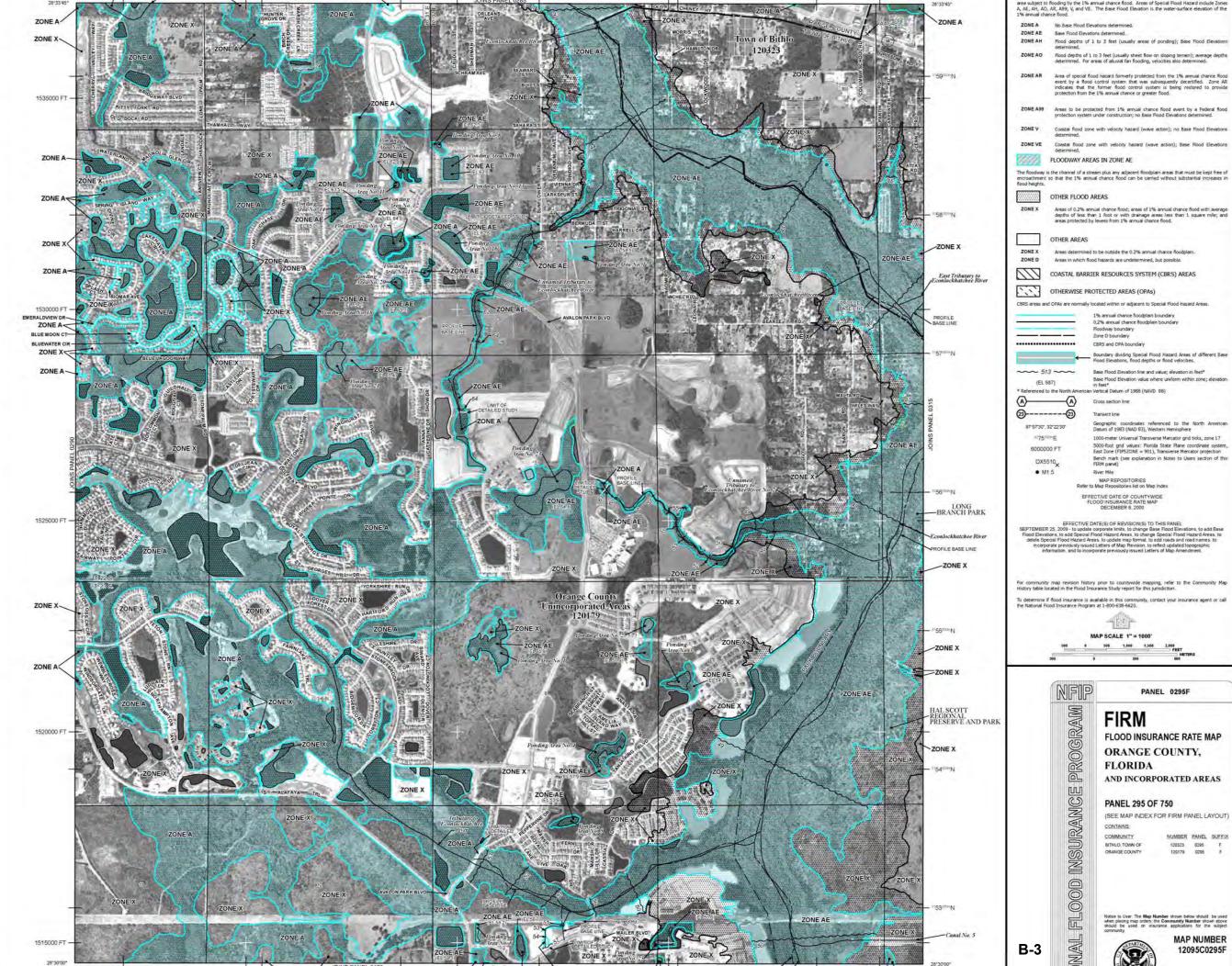
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Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously issued Letters of Map Change, a Flood Insurance Study report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by digital versions of this map. The FEMA Map Service Center may are Fax at 1-800-358-9620 and its website at http://www.msc.fema.gov/.

If you have questions about this map or questions concerning the National Flood (nsurance Program in general, please call 1-877-FBMA MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip/

NGVD29 to NAVD88 Vertical Datum Conversion Table (feet)

Watershed Name	Minimum	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.89	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	-1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1:01	0.09
Little Welova River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Maria and Maria	0.44	11.00	0.04	0.07



area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AC, AH, AO, AS, ASY, V, and VE. The Base Flood Elevation is the water-surface elevation of the 1% armual chance flood.

Flood depths of 1 to 3 feet (usually areas of ponding); Base Flood Elevations

Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined.

Area of special flood hazard formerly protected from the 1% annual chance flood event by a flood control system that was subsequently desertified. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance or greater flood.

Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations

Coastal flood zone with velocity hazard (wave action); Base Flood Elevations

Areas of 0.2% annual chance flood; areas of 1% annual driance flood with average depths of less than 1 foot or with dramage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

Areas determined to be outside the 0.2% annual chance floodolain.

OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

0.2% annual chance floodplain boundary

CBRS and OPA boundary Boundary dividing Special Flood Hazard Areas of different Base Flood Elevations, flood depths or flood velocities.

Base Flood Bevation line and value: elevation in feet*

Vertical Datum of 1988 (NAVD 88)

1000-meter Universal Transverse Mercator grid ticks, zone 17 5000-foot grid values: Florida State Plane coordinate system, East Zone (FIPSZONE = 901), Transverse Mercator projection Bench mark (see explanation in Notes to Users section of this FIRM panel)

For community map revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this jurisdiction.

mine if flood insurance is available in this community, contact your insurance agent or call

MAP SCALE 1" = 1000" 508 1,800 1,506 2,800 FEE

NUMBER PANEL SUFFIX

PANEL 0295F



12095C0295F

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This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Date tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

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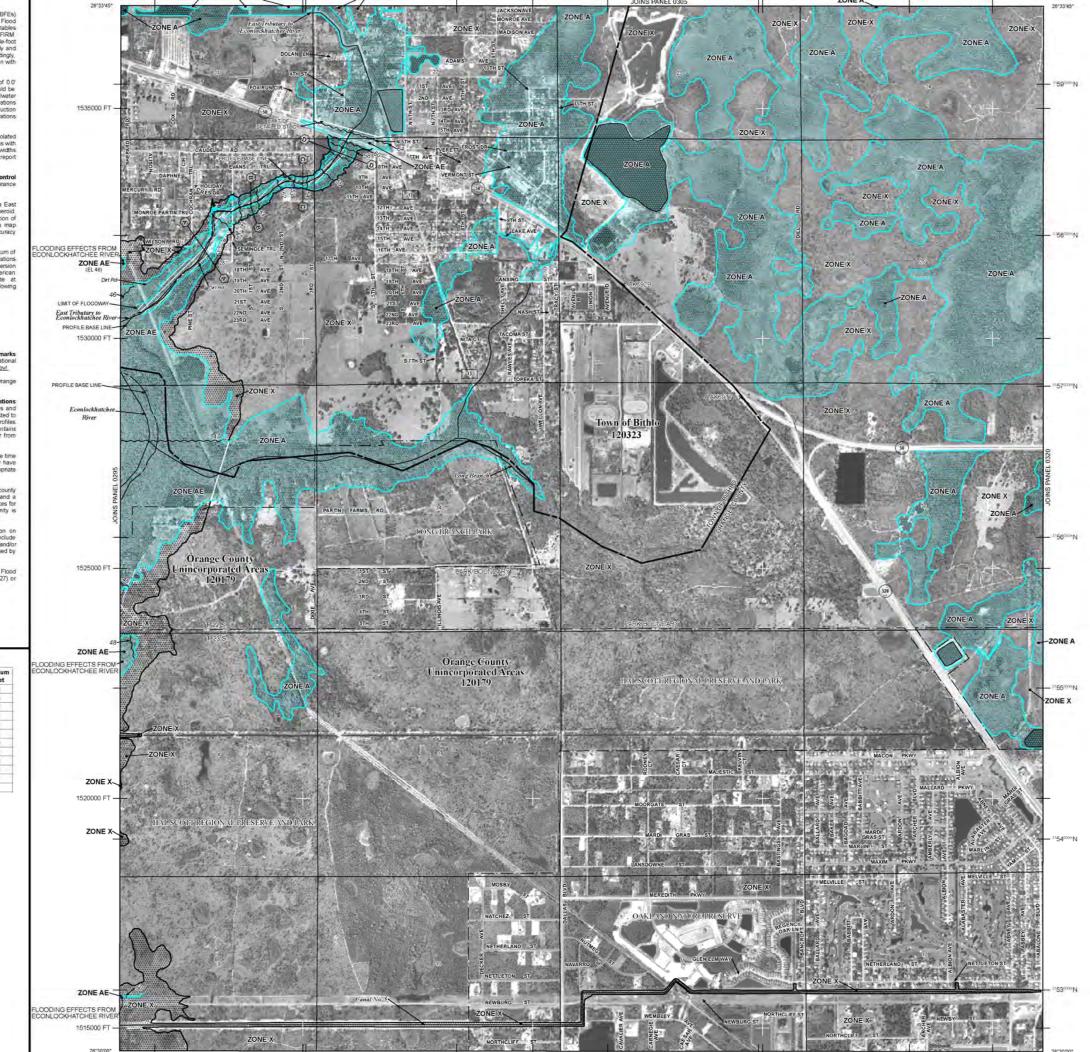
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Reedy Creek	-0.88	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14



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B-4

MAP NUMBER 12095C0315F

Appendix: C

USDA NRCS Soil Report



NRCS

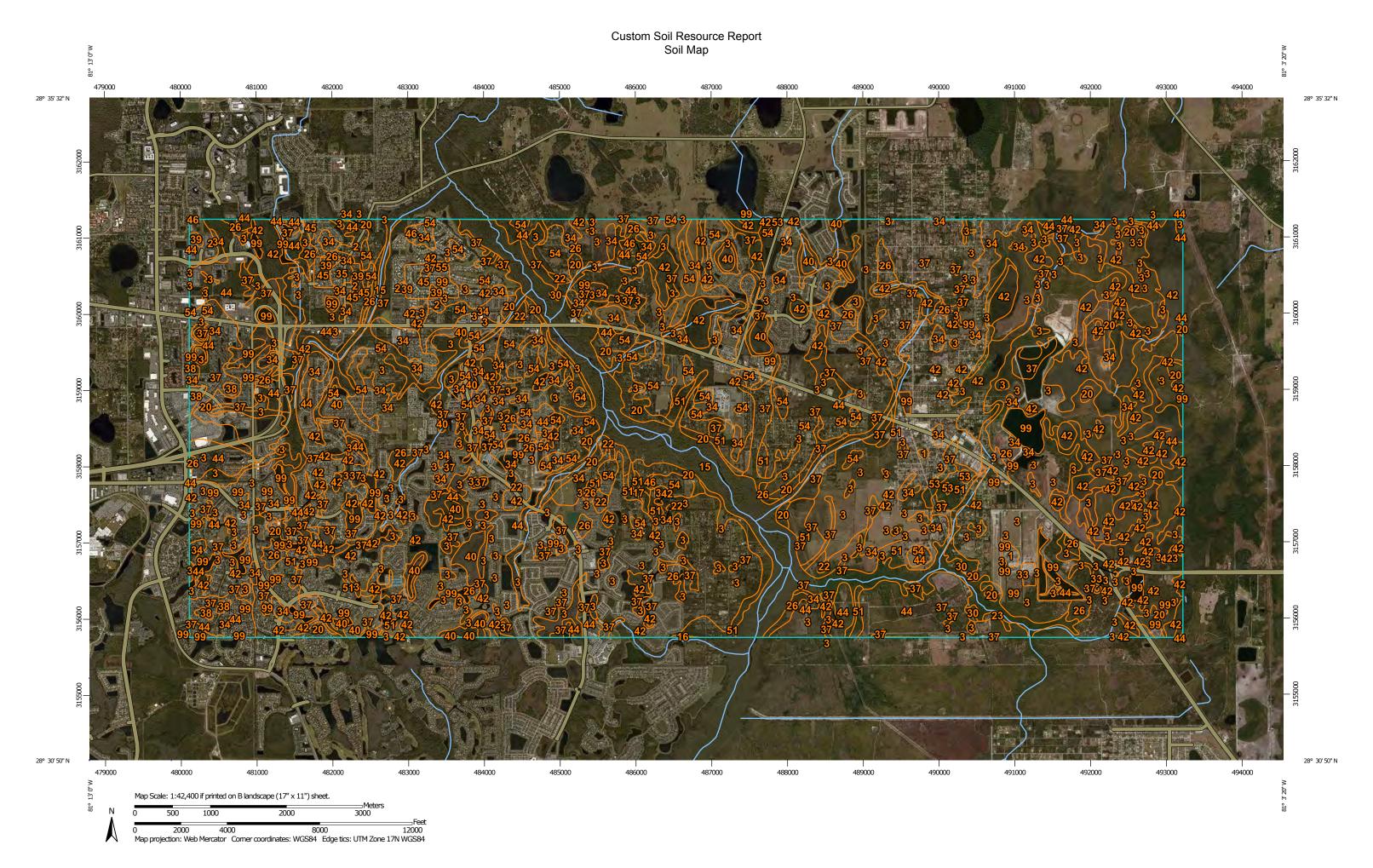
Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Orange County,

SR 408 Soil Data

Florida





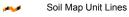
MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons



Soil Map Unit Points

Special Point Features

Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

A Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Perennial Water

→ Saline Spot

** Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

LIND

Spoil Area

Stony Spot

Very Stony Spot

Wet Spot

Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

+++ Rails

Interstate Highways

US Routes

Major Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:20,000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Orange County, Florida Survey Area Data: Version 12, Nov 19, 2015

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 12, 2011—Feb 20, 2015

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Orange County, Florida (FL095)				
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
1	Arents, nearly level	16.4	0.1%	
2	Archbold fine sand, 0 to 5 percent slopes	73.1	0.4%	
3	Basinger fine sand, depressional, 0 to 1 percent slopes	1,106.2	6.2%	
15	Felda fine sand, frequently flooded	1,060.0	5.9%	
16	Floridana fine sand, frequently flooded	1.5	0.0%	
17	Floridana mucky fine sand, depressional	13.6	0.1%	
20	Immokalee fine sand	754.8	4.2%	
22	Lochloosa fine sand	57.6	0.3%	
23	Malabar fine sand	7.3	0.0%	
26	Ona fine sand	193.0	1.1%	
27	Ona-Urban land complex	4.8	0.0%	
30	Pineda fine sand	28.5	0.2%	
33	Pits	13.4	0.1%	
34	Pomello fine sand, 0 to 5 percent slopes	986.4	5.5%	
35	Pomello-Urban land complex, 0 to 5 percent slopes	19.4	0.1%	
37	St. Johns fine sand	920.5	5.2%	
38	St. Lucie fine sand, 0 to 5 percent slopes	34.7	0.2%	
39	St. Lucie-Urban land complex, 0 to 5 percent slopes	29.9	0.2%	
40	Samsula muck	145.3	0.8%	
42	Sanibel muck	1,496.8	8.4%	
44	Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes	9,067.4	50.9%	
45	Smyrna-Urban land complex	80.9	0.5%	
46	Tavares fine sand, 0 to 5 percent slopes	11.6	0.1%	
51	Wabasso fine sand, 0 to 2 percent slopes	669.4	3.8%	
53	Wauberg fine sand	26.8	0.2%	
54	Zolfo fine sand, 0 to 2 percent slopes	717.2	4.0%	
55	Zolfo-Urban land complex	11.2	0.1%	
99	Water	277.9	1.6%	
Totals for Area of Interest		17,825.4	100.0%	

3—Basinger fine sand, depressional, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2v16v

Elevation: 0 to 160 feet

Mean annual precipitation: 38 to 62 inches
Mean annual air temperature: 68 to 77 degrees F

Frost-free period: 300 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Basinger, depressional, and similar soils: 90 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Basinger, Depressional

Setting

Landform: Depressions on marine terraces, drainageways on marine terraces

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 14 inches: fine sand Bh/E - 14 to 36 inches: fine sand Cg - 36 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00

to 20.00 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Calcium carbonate, maximum in profile: 1 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: A/D

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL),

Sandy soils on stream terraces, flood plains, or in depressions

(G155XB145FL)

Hydric soil rating: Yes

Minor Components

Smyrna, hydric

Percent of map unit: 5 percent Landform: — error in exists on —

Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Samsula, muck

Percent of map unit: 3 percent

Landform: Depressions on marine terraces

Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave Across-slope shape: Concave

Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL),

Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Floridana, hydric

Percent of map unit: 2 percent

Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Other vegetative classification: Cypress Woodlands (MCV026CA), Sandy over

loamy soils on stream terraces, flood plains, or in depressions

(G155XB245FL) Hydric soil rating: Yes

20—Immokalee fine sand

Map Unit Setting

National map unit symbol: bv7n

Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Immokalee, non-hydric, and similar soils: 82 percent Immokalee, hydric, and similar soils: 10 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Immokalee, Non-hydric

Setting

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 35 inches: fine sand Bh - 35 to 67 inches: fine sand C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.57 to 1.98 in/hr)

Depth to water table: About 6 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

Description of Immokalee, Hydric

Setting

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 35 inches: fine sand

Bh - 35 to 67 inches: fine sand C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.57 to 1.98 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: Yes

Minor Components

Pineda

Percent of map unit: 4 percent Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic

lowlands (G155XB241FL)

Hydric soil rating: Yes

Wabasso

Percent of map unit: 4 percent

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

34—Pomello fine sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2v16y

Elevation: 0 to 180 feet

Mean annual precipitation: 44 to 52 inches Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 342 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Pomello and similar soils: 95 percent Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pomello

Setting

Landform: Knolls on marine terraces, ridges on marine terraces

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve, riser

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 47 inches: fine sand Bh - 47 to 58 inches: fine sand Bw - 58 to 65 inches: fine sand C - 65 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 5 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Moderately well drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 6.00 in/hr)

Depth to water table: About 24 to 42 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 5.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Other vegetative classification: Sand Pine Scrub (R155XY001FL), Sandy soils on

rises and knolls of mesic uplands (G155XB131FL)

Minor Components

Smyrna

Percent of map unit: 3 percent Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

Tavares

Percent of map unit: 1 percent

Landform: Ridges on marine terraces, flats on marine terraces

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Linear

Ecological site: Longleaf Pine-Turkey Oak Hills (R154XY002FL)

Other vegetative classification: Sandy soils on rises, knolls, and ridges of mesic

uplands (G154XB121FL)

Hydric soil rating: No

Bulow

Percent of map unit: 1 percent

Landform: Ridges on marine terraces

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy over loamy soils on knolls and ridges of

mesic uplands (G155XB211FL)

37—St. Johns fine sand

Map Unit Setting

National map unit symbol: bv87

Elevation: 30 to 150 feet

Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

St. johns, non-hydric, and similar soils: 60 percent St. johns, hydric, and similar soils: 30 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of St. Johns, Non-hydric

Setting

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.20 to 1.98 in/hr)

Depth to water table: About 6 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

Description of St. Johns, Hydric

Setting

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.20 to 1.98 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 5 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

Immokalee, non-hydric

Percent of map unit: 5 percent

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

42—Sanibel muck

Map Unit Setting

National map unit symbol: bv8f

Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Sanibel, undrained, and similar soils: 65 percent Sanibel, drained, and similar soils: 25 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Sanibel, Undrained

Setting

Landform: Marshes on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck
A - 11 to 15 inches: fine sand
C - 15 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95

to 19.98 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7w

Hydrologic Soil Group: A/D

Other vegetative classification: Organic soils in depressions and on flood plains

(G155XB645FL) Hydric soil rating: Yes

Description of Sanibel, Drained

Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck
A - 11 to 15 inches: fine sand
C - 15 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95

to 19.98 in/hr)

Depth to water table: About 0 to 24 inches

Frequency of flooding: None Frequency of ponding: Frequent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: A/D

Other vegetative classification: Organic soils in depressions and on flood plains

(G155XB645FL) Hydric soil rating: Yes

Minor Components

Hontoon, undrained

Percent of map unit: 5 percent

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Other vegetative classification: Organic soils in depressions and on flood plains

(G155XB645FL) Hydric soil rating: Yes

Samsula

Percent of map unit: 5 percent

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Other vegetative classification: Organic soils in depressions and on flood plains

(G155XB645FL) Hydric soil rating: Yes

44—Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2v171

Elevation: 0 to 150 feet

Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F

Frost-free period: 300 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Smyrna, non-hydric, and similar soils: 76 percent Smyrna, hydric, and similar soils: 20 percent

Minor components: 4 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Smyrna, Non-hydric

Setting

Landform: Flatwoods on marine terraces, flats on marine terraces

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 17 inches: fine sand

Bh - 17 to 27 inches: loamy fine sand

C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 6.00 in/hr)

Depth to water table: About 6 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: A/D

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Description of Smyrna, Hydric

Setting

Landform: Flats on marine terraces, flatwoods on marine terraces

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 17 inches: fine sand

Bh - 17 to 27 inches: loamy fine sand

C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.60 to 6.00 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: A/D

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Minor Components

Basinger, depressional

Percent of map unit: 2 percent

Landform: Depressions on marine terraces
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Other vegetative classification: Sandy soils on stream terraces, flood plains, or in

depressions (G155XB145FL)

Hydric soil rating: Yes

Pomona, non-hydric

Percent of map unit: 1 percent

Landform: Flatwoods on marine terraces

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL) Hydric soil rating: No

Eaugallie, hydric

Percent of map unit: 1 percent

Landform: Flatwoods on marine terraces, flats on marine terraces

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Dip

Down-slope shape: Linear Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R154XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G154XB141FL)

Hydric soil rating: Yes

Across-slope shape: Linear

Other vegetative classification: North Florida Flatwoods (R154XY004FL), Sandy

soils on rises and knolls of mesic uplands (G155XB131FL)

51—Wabasso fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2svzg

Elevation: 0 to 130 feet

Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F

Frost-free period: 300 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Wabasso and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wabasso

Setting

Landform: Flatwoods on flats on marine terraces Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits over loamy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 16 inches: fine sand Bh - 16 to 28 inches: fine sand E' - 28 to 32 inches: fine sand

Btg - 32 to 48 inches: fine sandy loam Cg - 48 to 80 inches: loamy fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: 12 to 63 inches to strongly contrasting textural

stratification

Natural drainage class: Poorly drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: About 6 to 18 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: A/D

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Minor Components

Basinger

Percent of map unit: 4 percent

Landform: Drainageways on flatwoods on marine terraces Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Convex, linear, concave Across-slope shape: Linear, convex, concave

Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of

mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Felda

Percent of map unit: 4 percent

Landform: Flatwoods on drainageways on marine terraces Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Linear

Across-slope shape: Concave, linear Ecological site: Slough (R155XY011FL)

Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils

on stream terraces, flood plains, or in depressions (G155XB245FL)

Hydric soil rating: Yes

Riviera

Percent of map unit: 4 percent

Landform: Flatwoods on drainageways on marine terraces Landform position (three-dimensional): Tread, talf, dip

Down-slope shape: Linear, convex Across-slope shape: Concave, linear Ecological site: Slough (R155XY011FL)

Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils

on flats of hydric or mesic lowlands (G156AC241FL)

Hydric soil rating: Yes

Boca

Percent of map unit: 3 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex Across-slope shape: Linear

Ecological site: South Florida Flatwoods (R155XY003FL)

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

53—Wauberg fine sand

Map Unit Setting

National map unit symbol: bv8t

Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F

Frost-free period: 350 to 365 days

Farmland classification: Not prime farmland

Map Unit Composition

Wauberg and similar soils: 94 percent

Minor components: 6 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wauberg

Setting

Landform: Flats on marine terraces

Landform position (three-dimensional): Talf

Down-slope shape: Linear Across-slope shape: Linear

Parent material: Sandy and loamy marine deposits

Typical profile

A - 0 to 8 inches: fine sand E - 8 to 28 inches: fine sand

B - 28 to 60 inches: sandy clay loam C - 60 to 80 inches: sandy clay

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.06 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 5.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic

lowlands (G155XB241FL)

Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 6 percent

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands

(G155XB141FL)

Hydric soil rating: No

54—Zolfo fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2w0q1

Elevation: 30 to 160 feet

Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F

Frost-free period: 324 to 365 days

Farmland classification: Farmland of unique importance

Map Unit Composition

Zolfo and similar soils: 88 percent Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Zolfo

Setting

Landform: Rises on marine terraces, knolls on marine terraces Landform position (two-dimensional): Summit, footslope

Landform position (three-dimensional): Interfluve, side slope, riser

Down-slope shape: Convex Across-slope shape: Linear

Parent material: Sandy marine deposits

Typical profile

A - 0 to 6 inches: fine sand E - 6 to 53 inches: fine sand Bh - 53 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches Natural drainage class: Somewhat poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to

high (0.57 to 1.98 in/hr)

Depth to water table: About 24 to 42 inches

Frequency of flooding: None Frequency of ponding: None

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0

mmhos/cm)

Sodium adsorption ratio, maximum in profile: 4.0 Available water storage in profile: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: A

Other vegetative classification: North Florida Flatwoods (R154XY004FL), South Florida Flatwoods (R154XY003FL), Sandy soils on rises and knolls of mesic

uplands (G154XB131FL)

Minor Components

Myakka

Percent of map unit: 4 percent

Landform: Flatwoods on marine terraces

Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

Tavares

Percent of map unit: 3 percent

Landform: Ridges on marine terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Interfluve, tread, rise

Down-slope shape: Linear, convex

Across-slope shape: Linear

Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)

Hydric soil rating: No

Millhopper

Percent of map unit: 3 percent

Landform: Ridges on marine terraces, knolls on marine terraces, flatwoods on

marine terraces

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Interfluve

Down-slope shape: Convex, concave

Across-slope shape: Linear

Other vegetative classification: Upland Hardwood Hammock (R154XY008FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)

Hydric soil rating: No

Lochloosa

Percent of map unit: 1 percent Landform: Rises on marine terraces

Landform position (three-dimensional): Interfluve, rise

Down-slope shape: Convex

Across-slope shape: Linear

Other vegetative classification: Sandy over loamy soils on rises and knolls of

mesic uplands (G155XB231FL)

Hydric soil rating: No

Malabar

Percent of map unit: 1 percent

Landform: Drainageways on marine terraces Landform position (three-dimensional): Dip

Down-slope shape: Linear, convex Across-slope shape: Concave, linear

Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of

mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

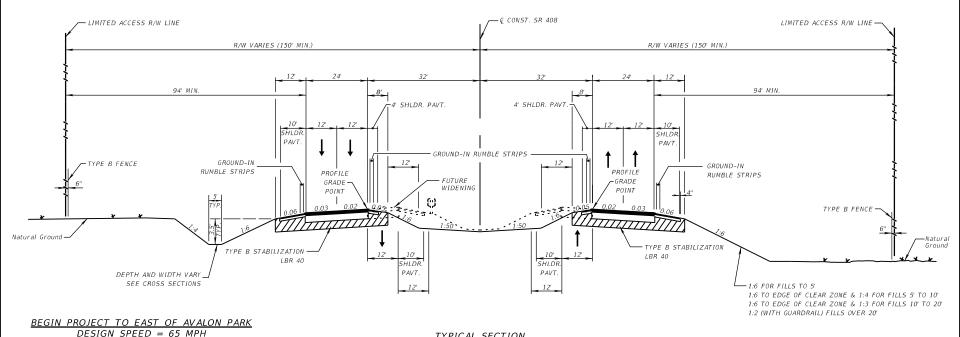
Appendix: D

SR-408 Typical Section

PROJECT IDENTIFICATION

CFX PROJECT NO. 408-254	FEDERAL AID PROJEC	CT NO. N/A	COUNTY NAME ORANGE
SECTION NO75008160	ROAD DESIGNATION _	SR 408	LIMITS/MILEPOST N/A
PROJECT DESCRIPTION SR 408 EASTERN EXTENS	ION PD&E STUDY (FROM	M CURRENT EASTERN TERMINUS NEAF	R WOODBURY ROAD TO SR 50, NEAR SR 520)

PROPOSED ROADWAY TYPICAL SECTION



DESIGN SPEED = 65 MPH

EAST OF AVALON PARK TO END PROJECT DESIGN SPEED = 70 MPH

TYPICAL SECTION SR 408 STA 358+41.08 TO STA 731+27.29

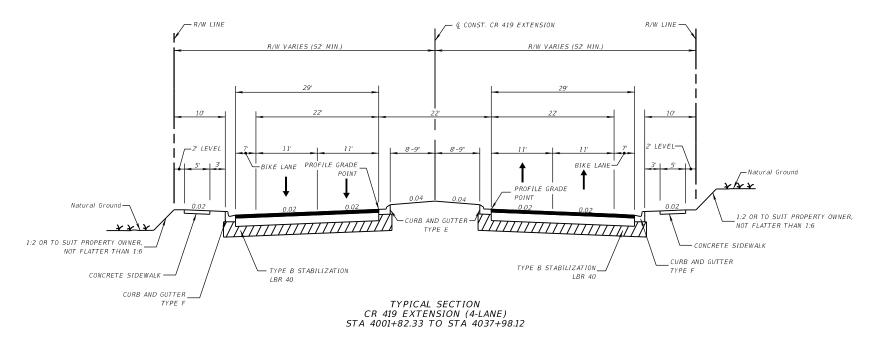
APPROVED BY: C. Brian Fuller, P.E. License No.: 49524	CFX CONCURRENCE	CFX APPROVAL
Engineer Of Record Signature Date		Glenn M. Pressimone, PE Date CFX Director of Engineering

jrice

PROJECT IDENTIFICATION

CFX PROJECT NO. 408-254	FEDERAL AID PROJECT NO. N/A	COUNTY NAMEORANGE
SECTION NO75008160	ROAD DESIGNATION SR 408	LIMITS/MILEPOST N/A
PROJECT DESCRIPTION SR 408 EASTERN EXTENS	ION PD&E STUDY (FROM CURRENT EASTERN TERMINUS NEAF	WOODBURY ROAD TO SR 50, NEAR SR 520)

PROPOSED ROADWAY TYPICAL SECTION



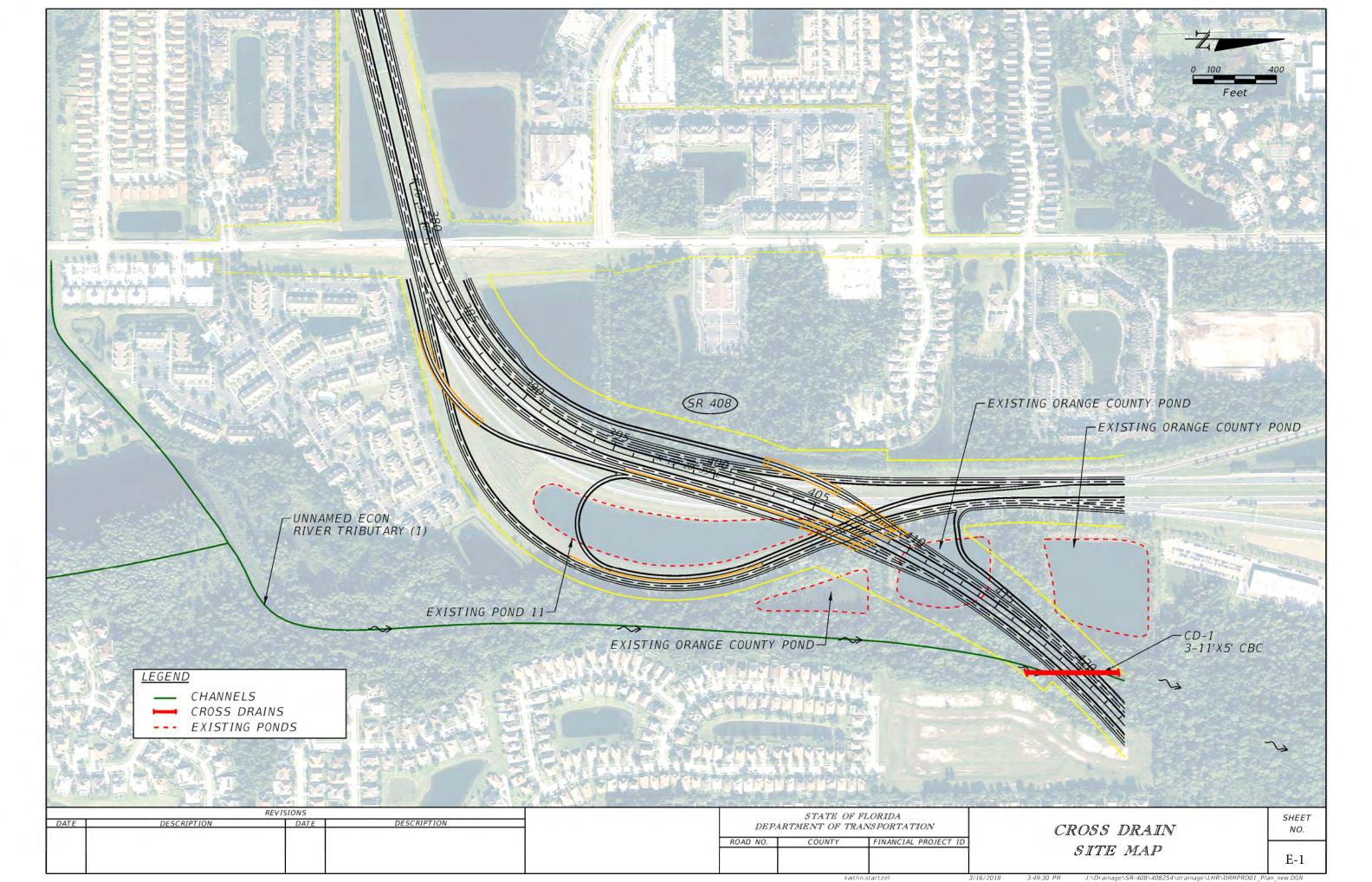
DESIGN SPEED = 40 MPH

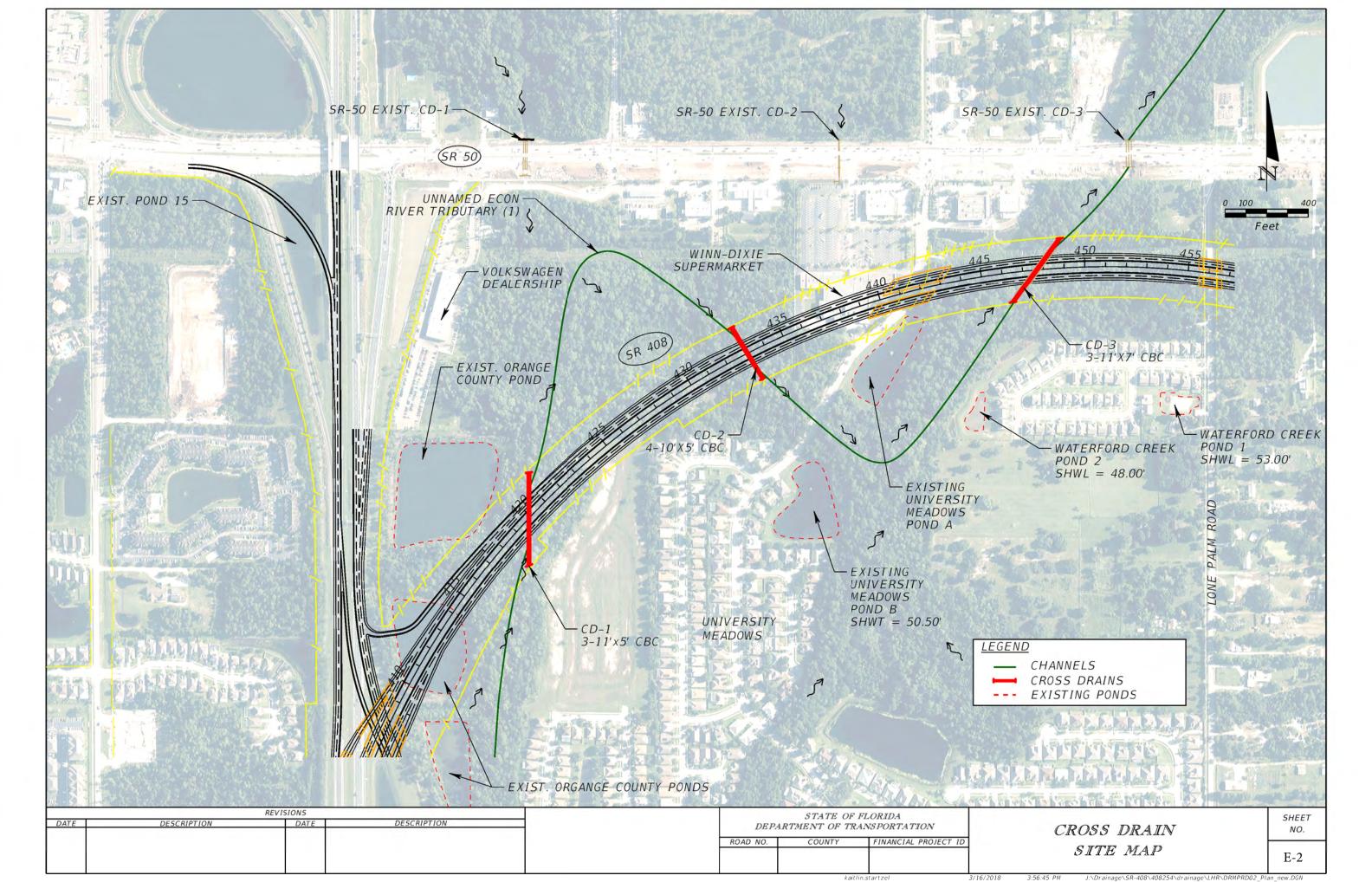
APPROVED BY: C. Brian Fuller, P.E. License No.: 49524	CFX CONCURRENCE	CFX APPROVAL
Engineer Of Record Signature Date	 Jonathan Williamson, AICP Date CFX Project Manager	Glenn M. Pressimone, PE Date CFX Director of Engineering

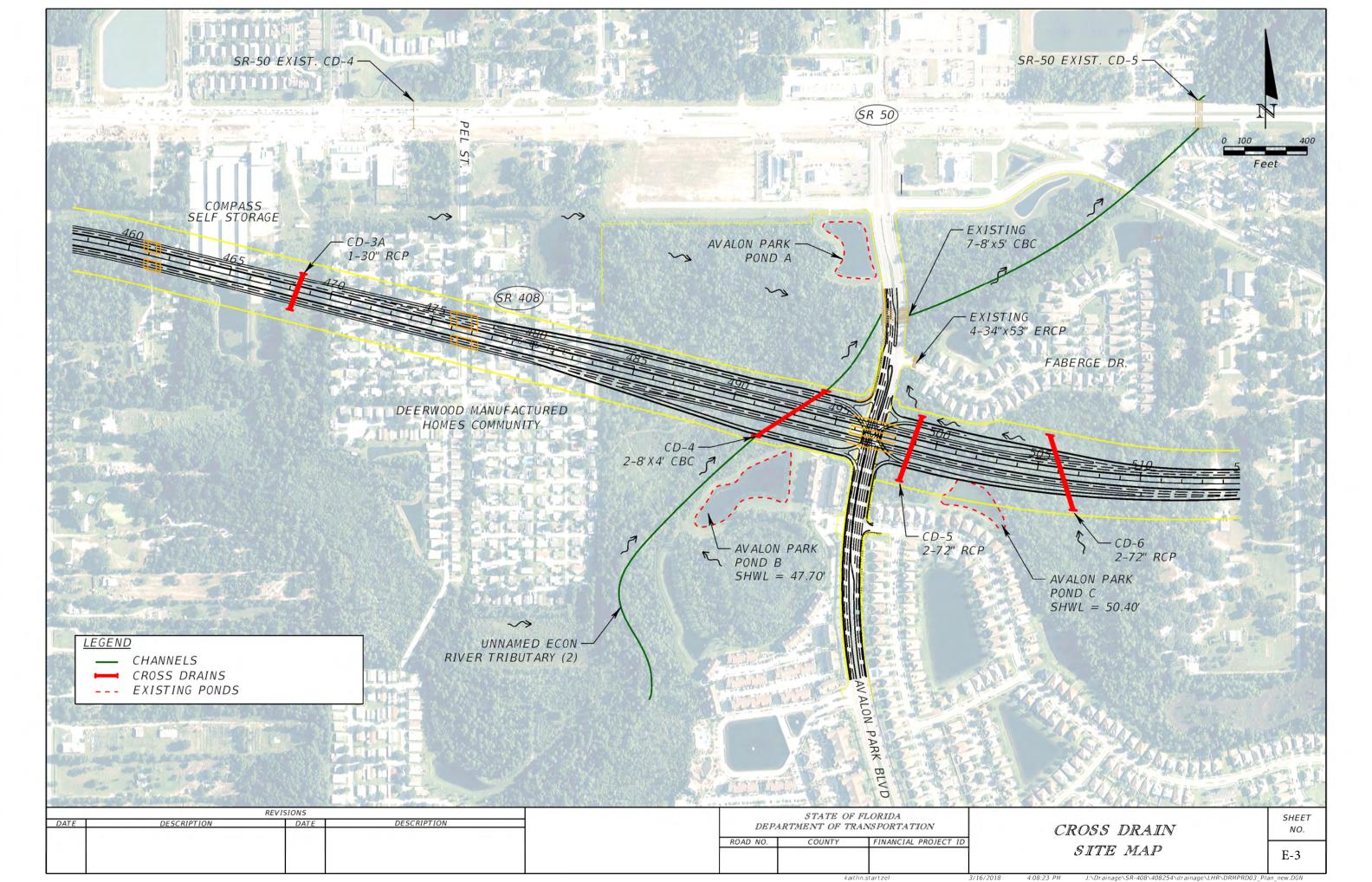
Appendix: E

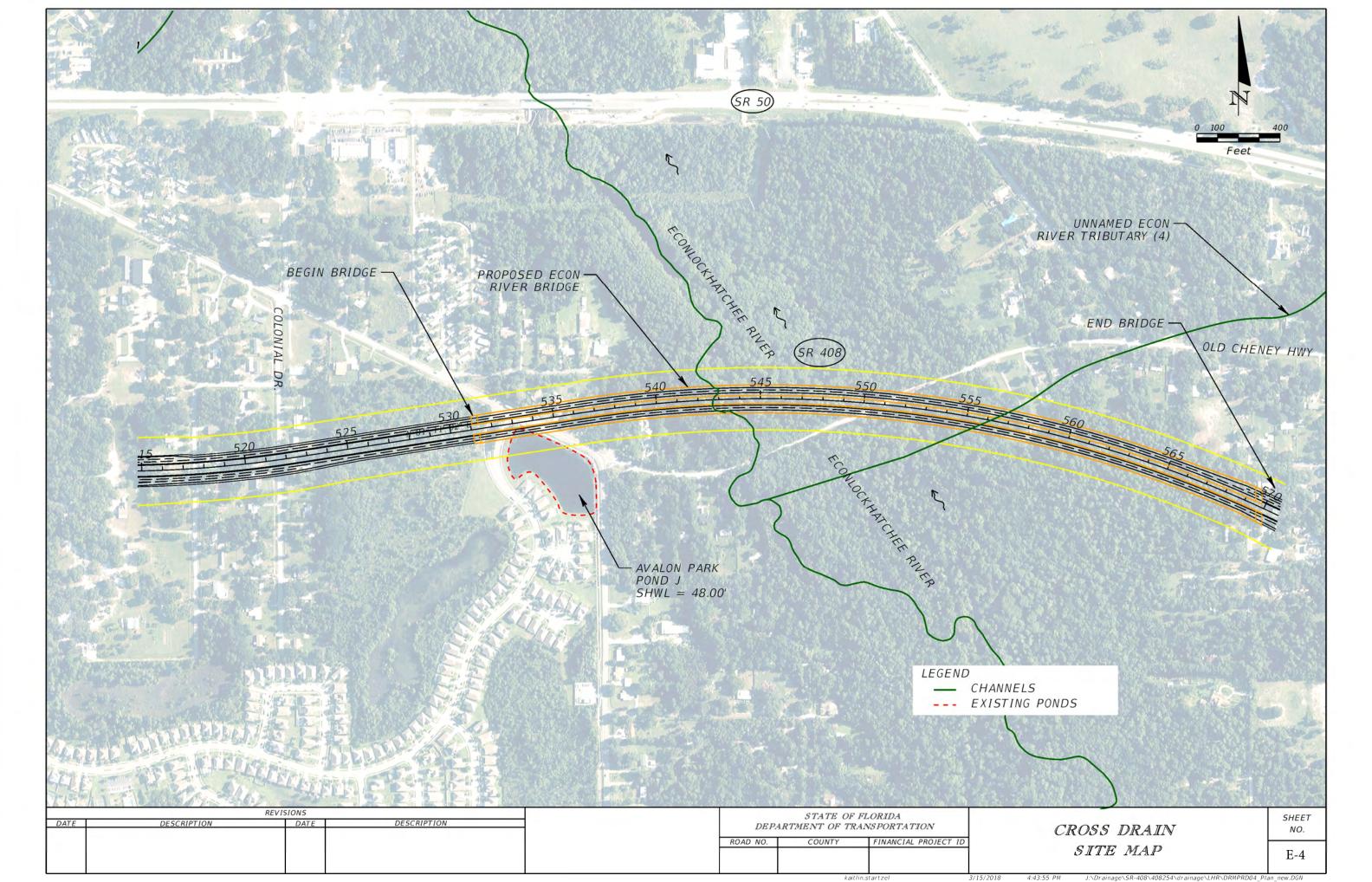
Cross Drain Exhibits

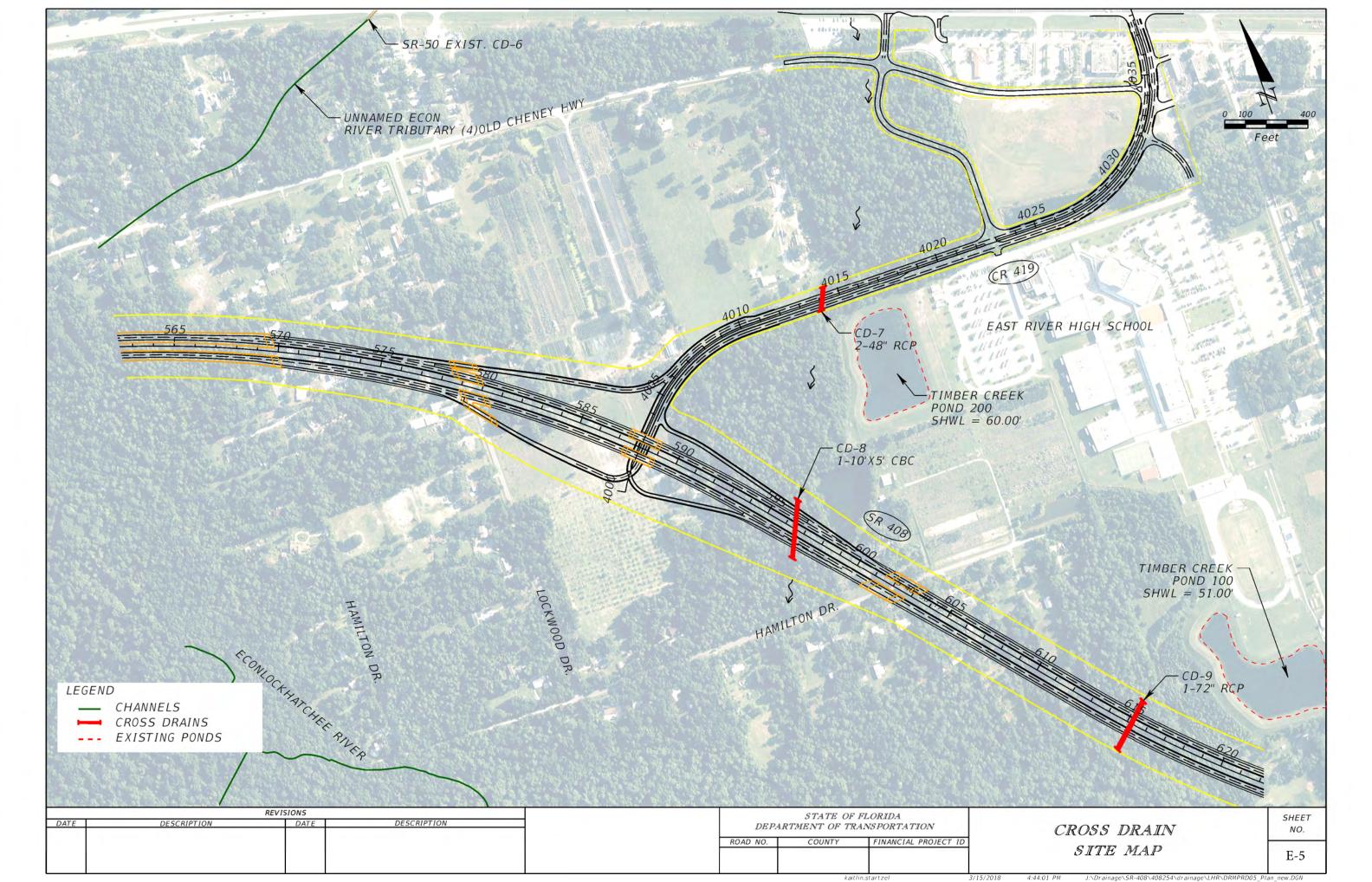
Cross Drains Site Maps



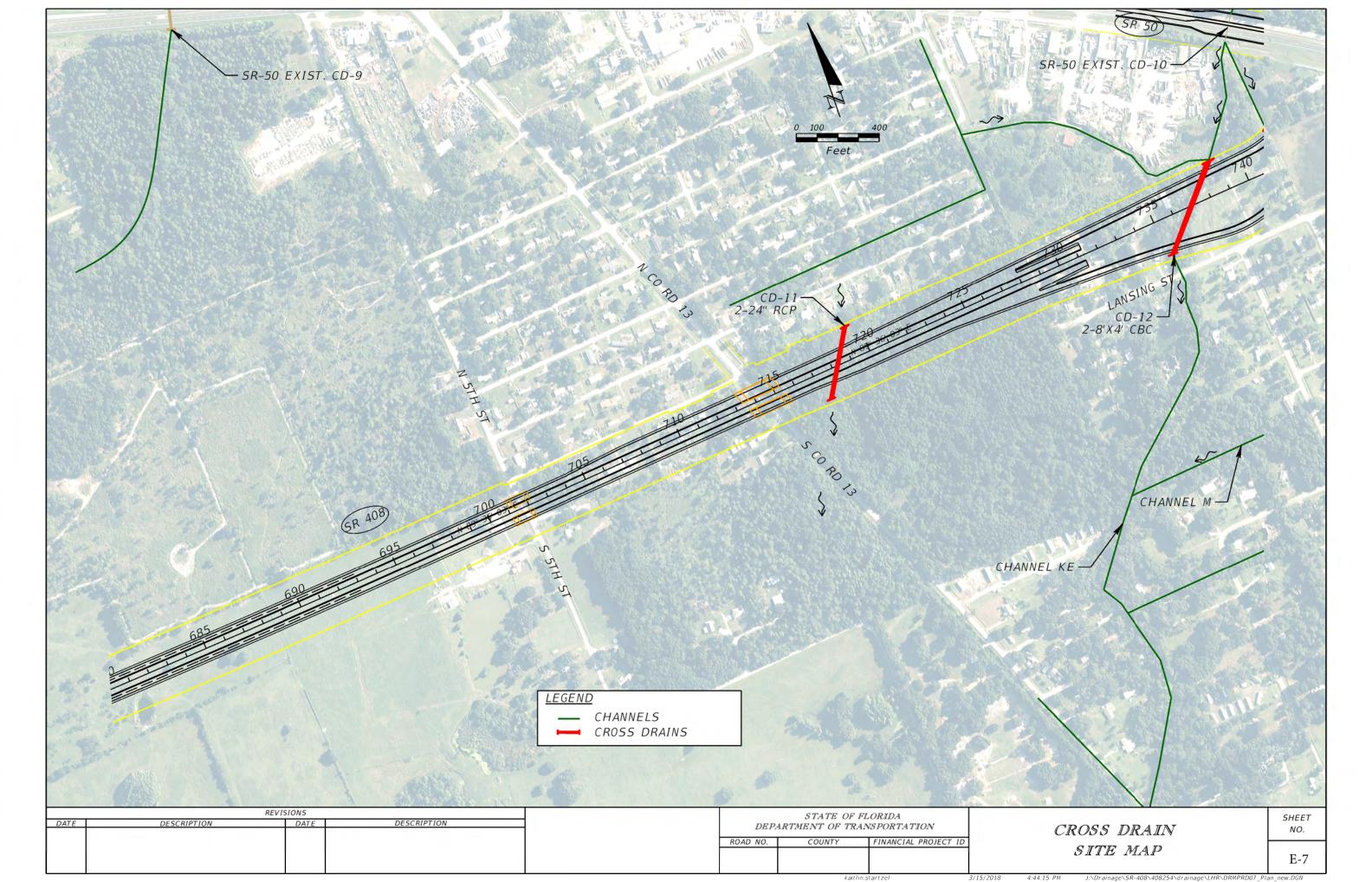


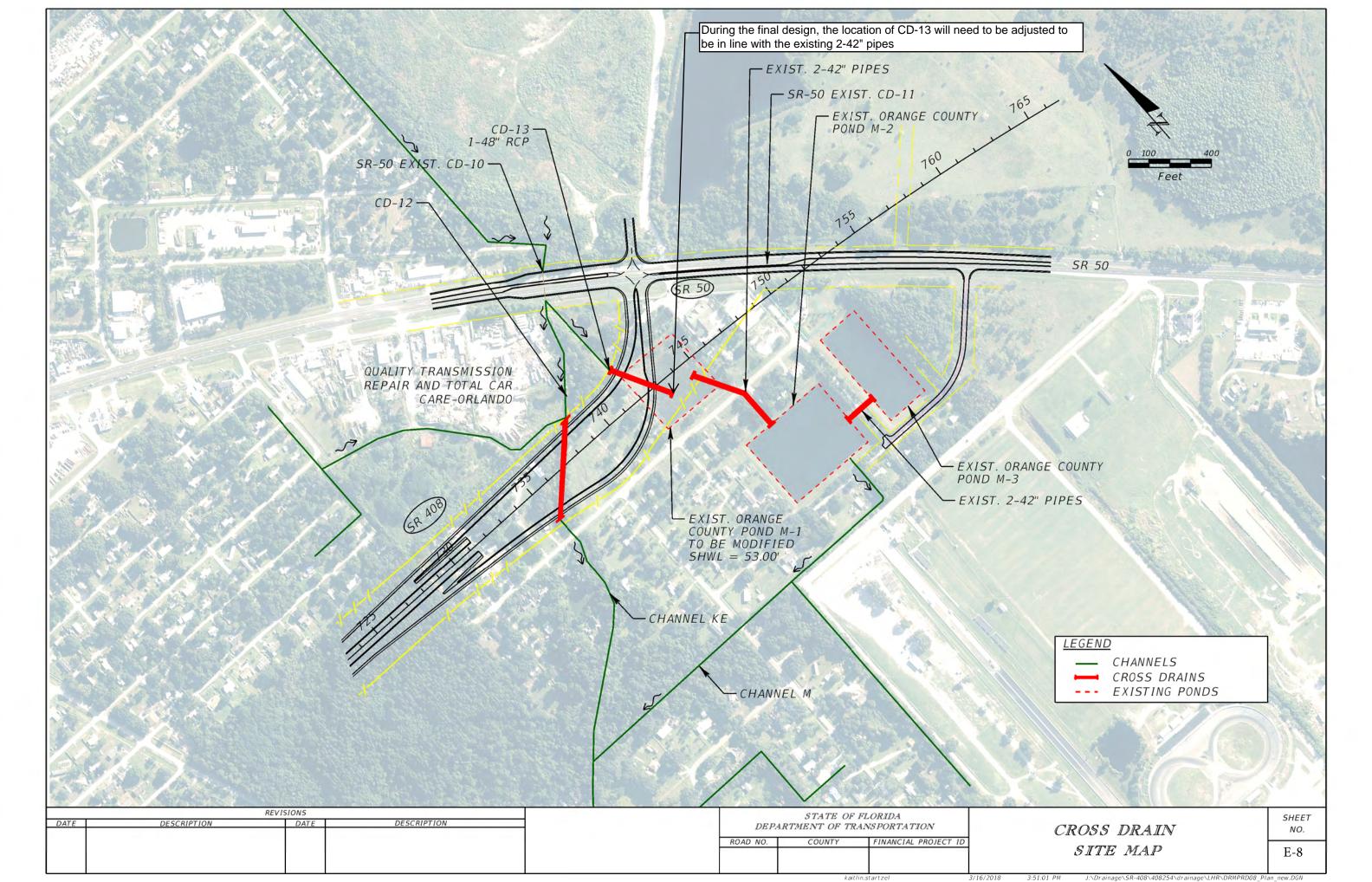




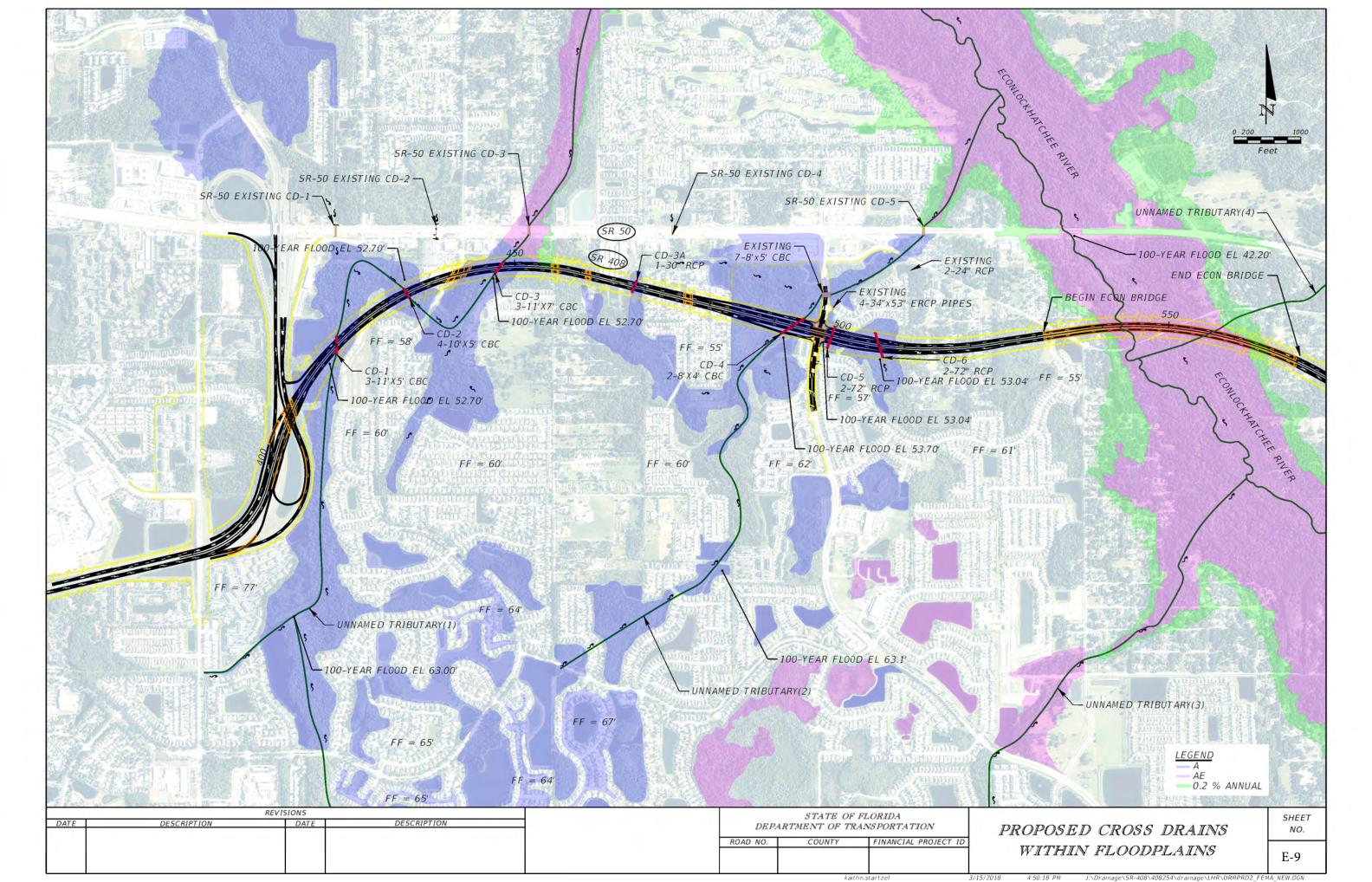


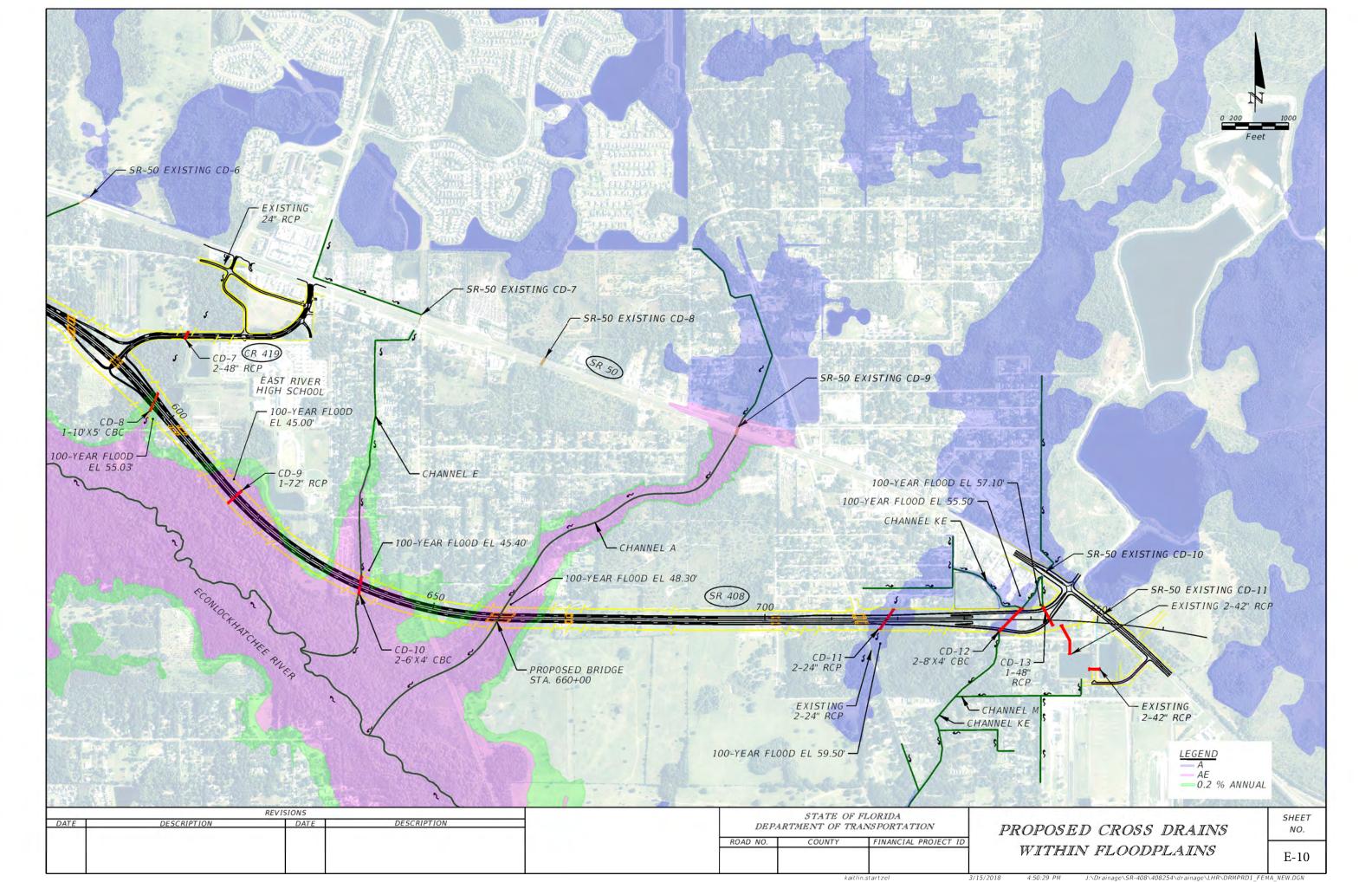




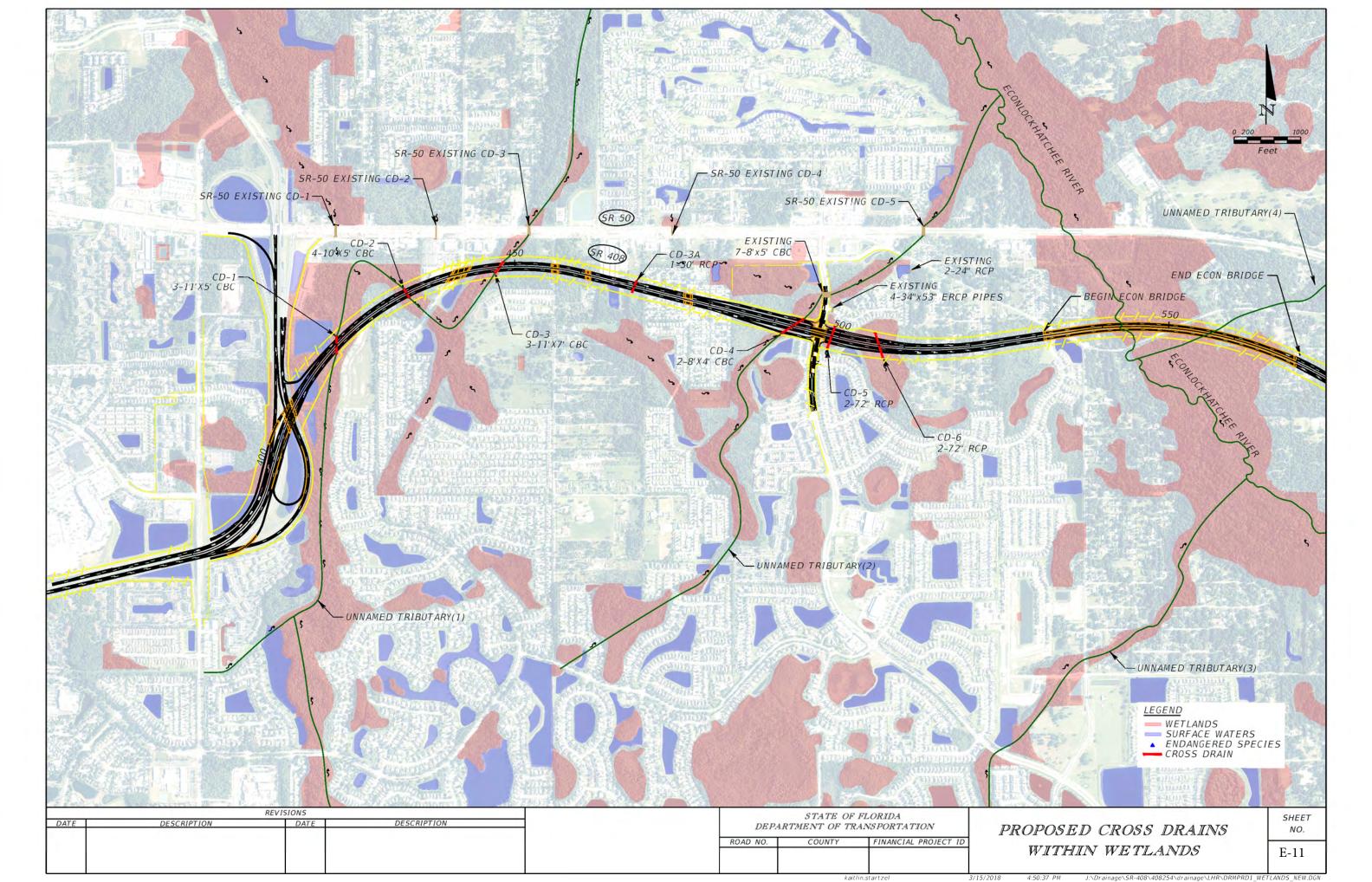


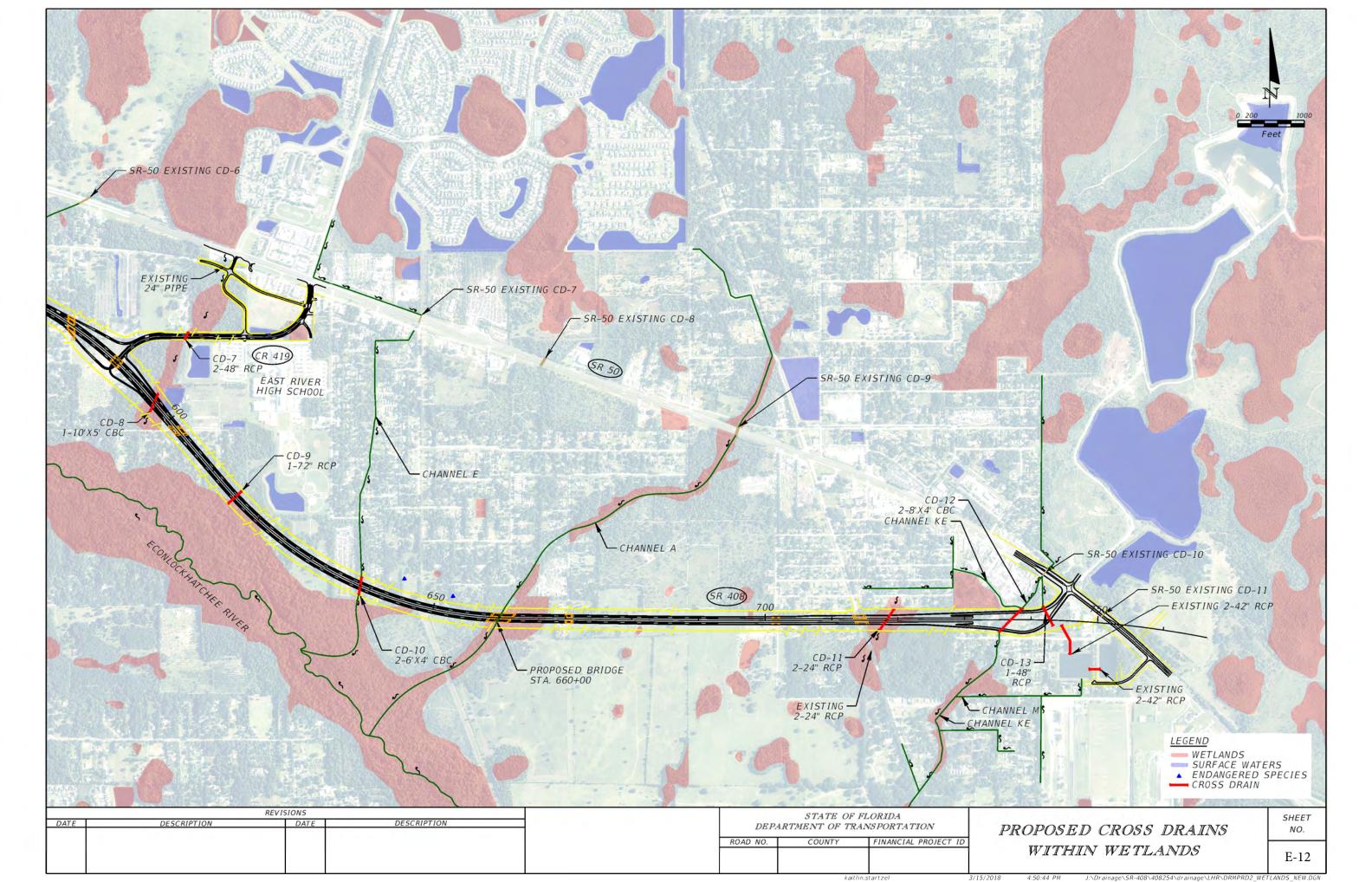
Proposed Cross Drains Within Floodplains





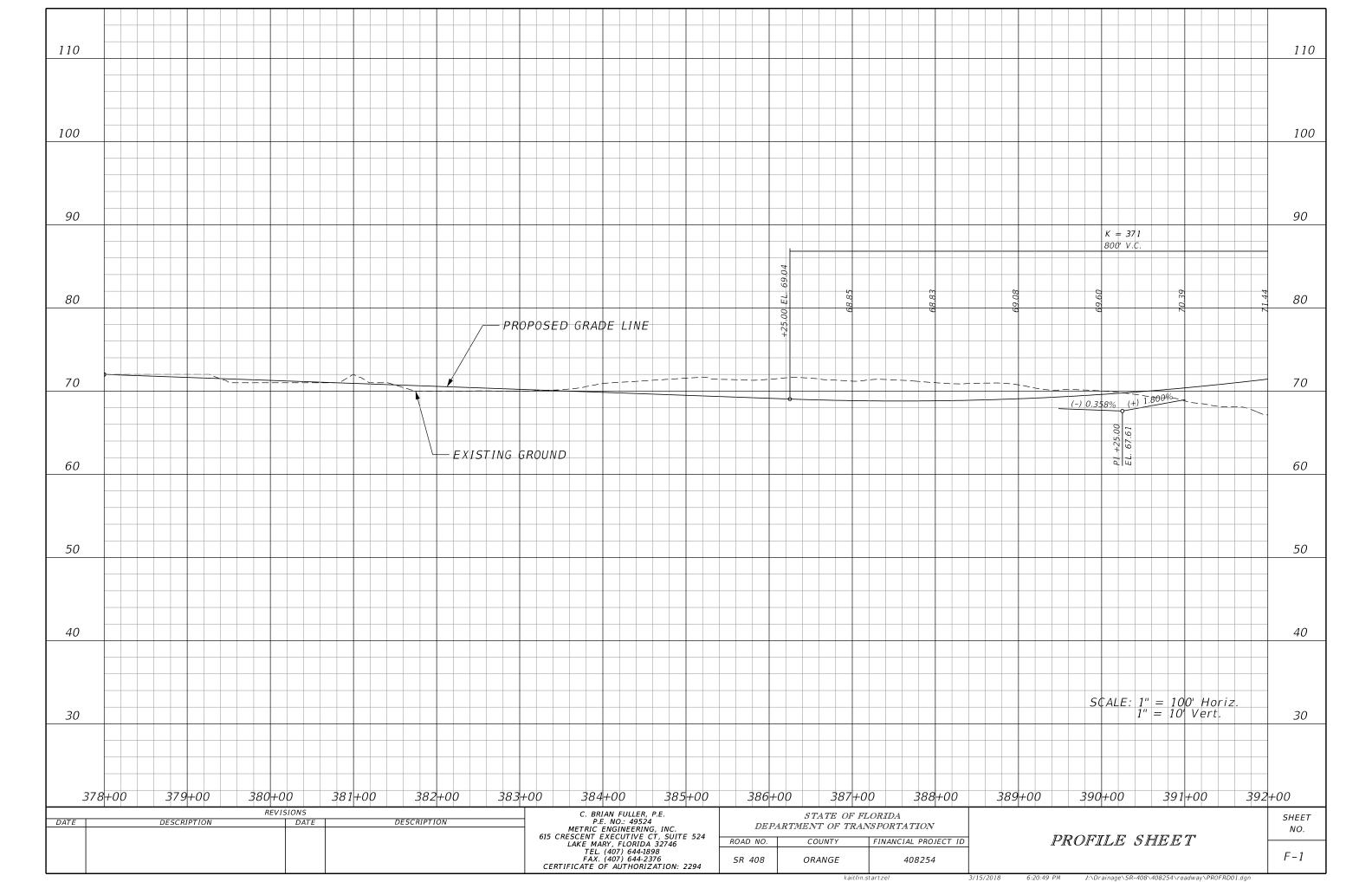
Proposed Cross Drains Within Wetlands

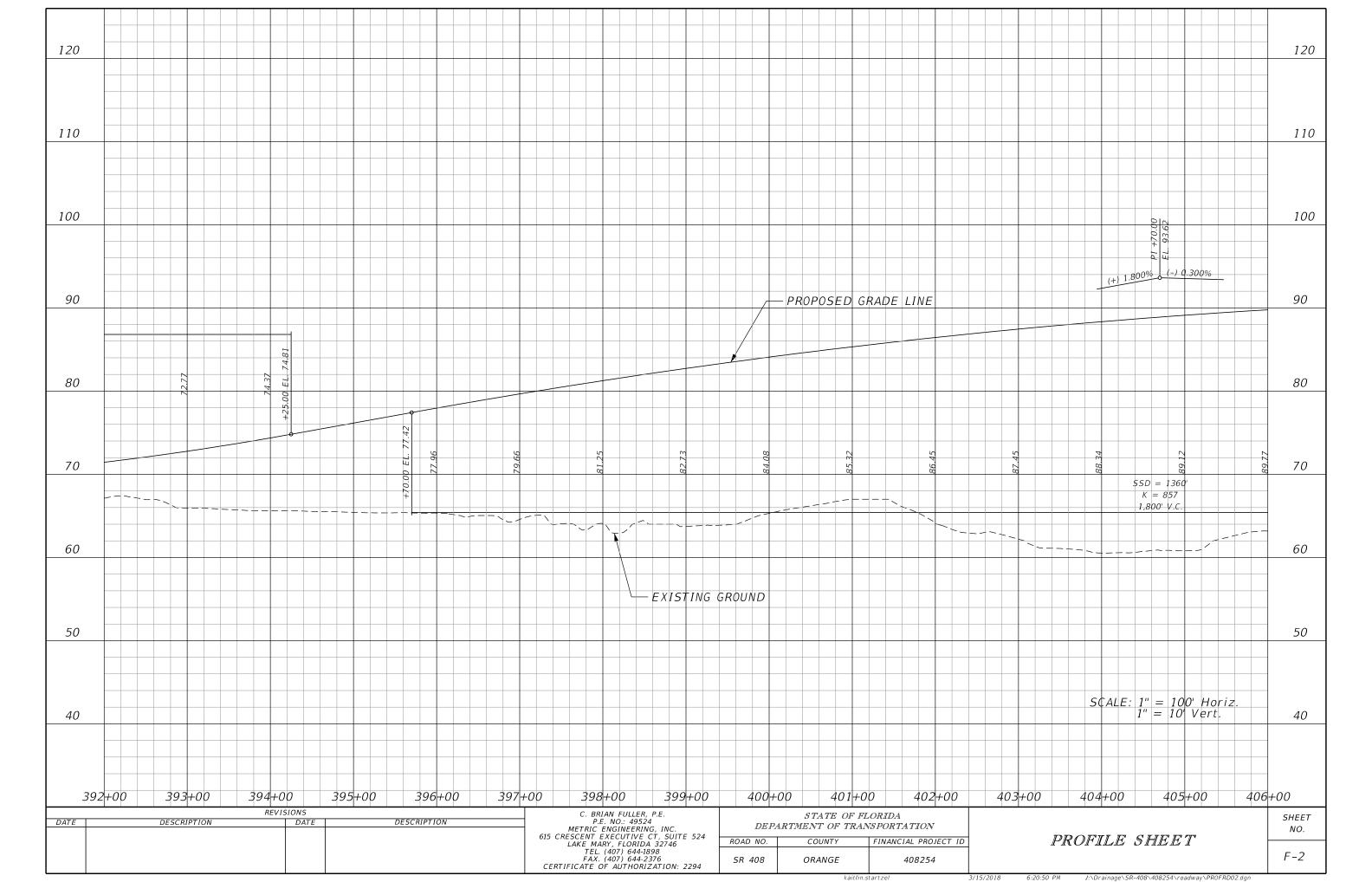


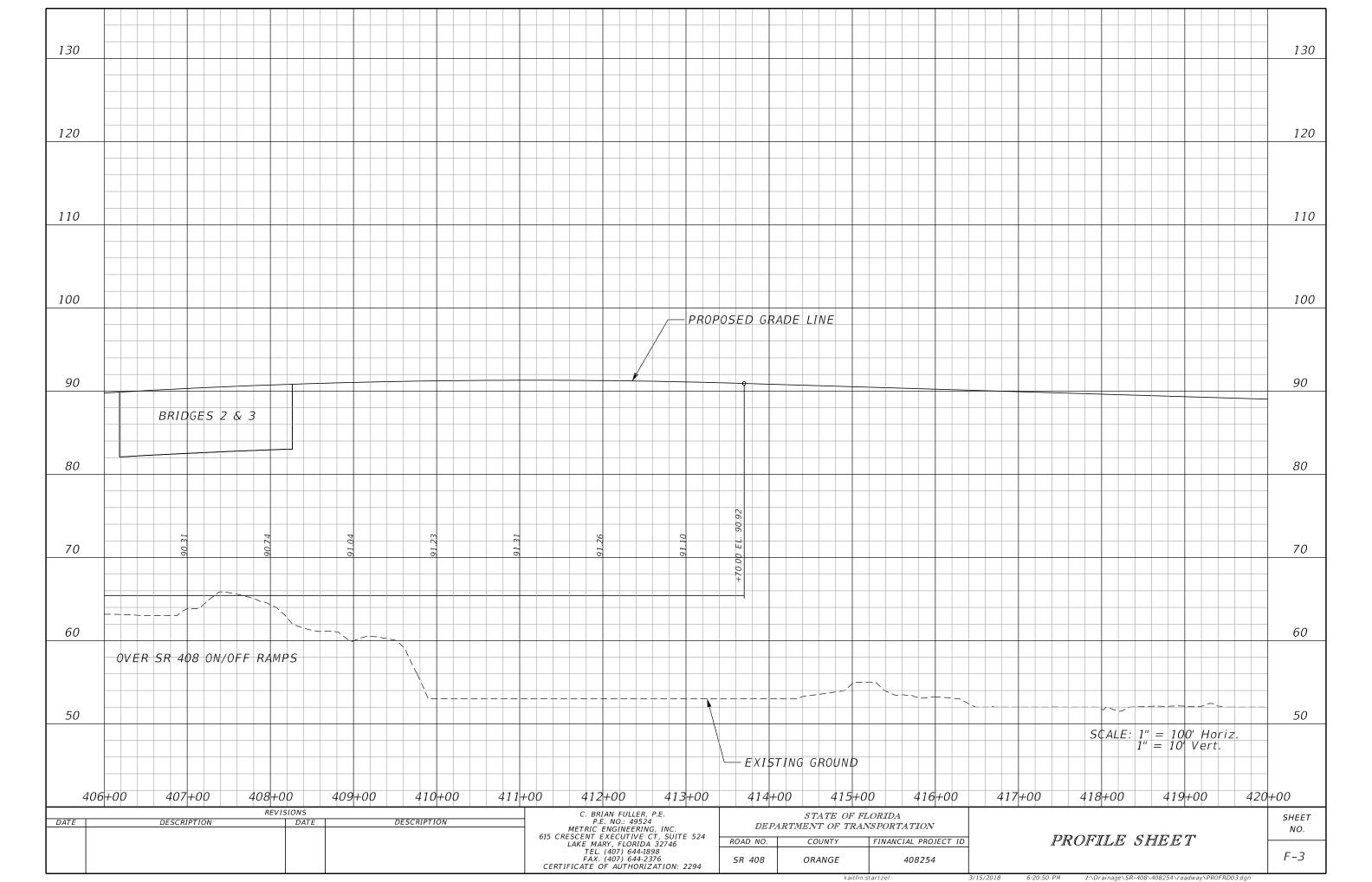


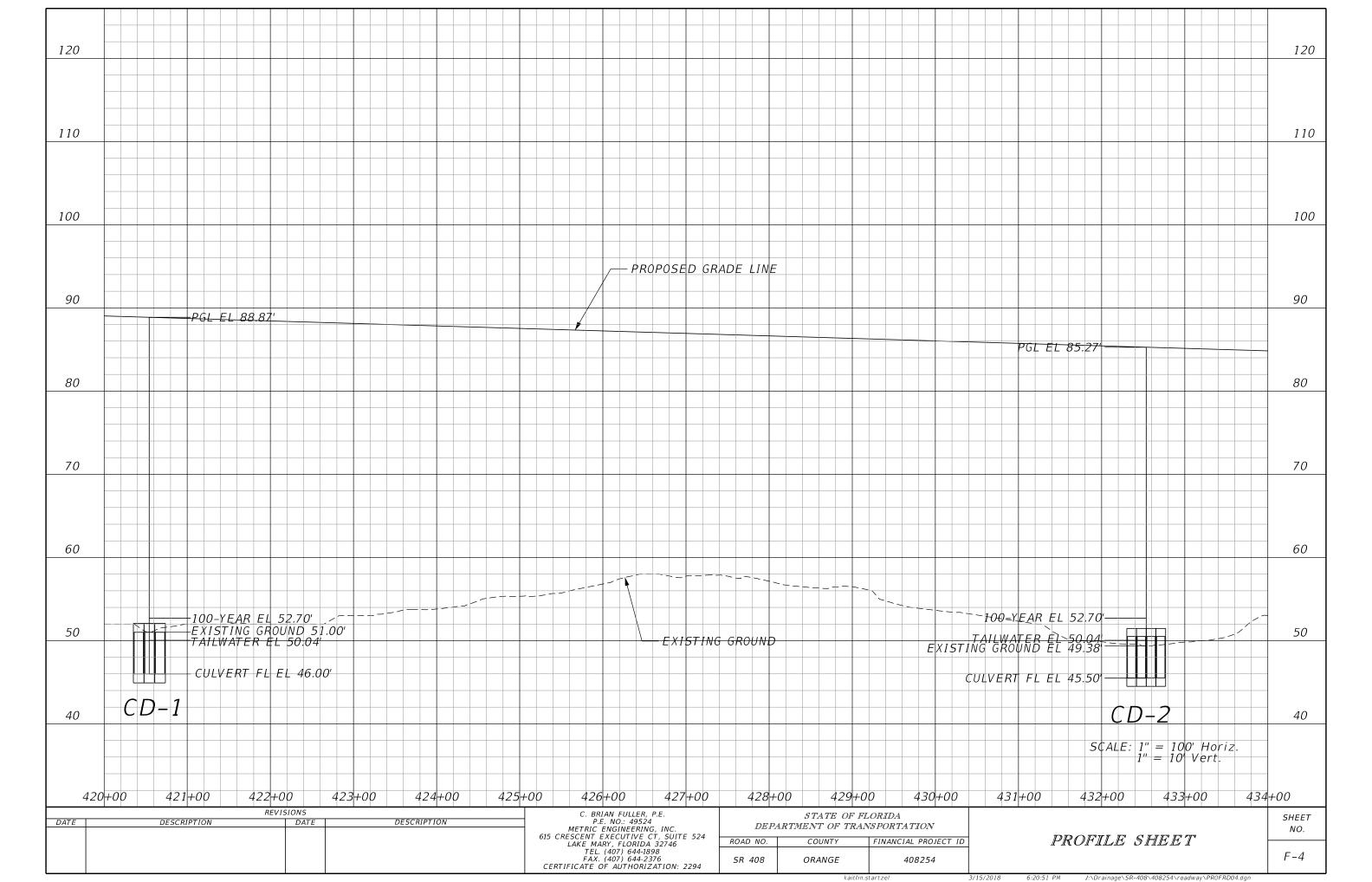
Appendix: F

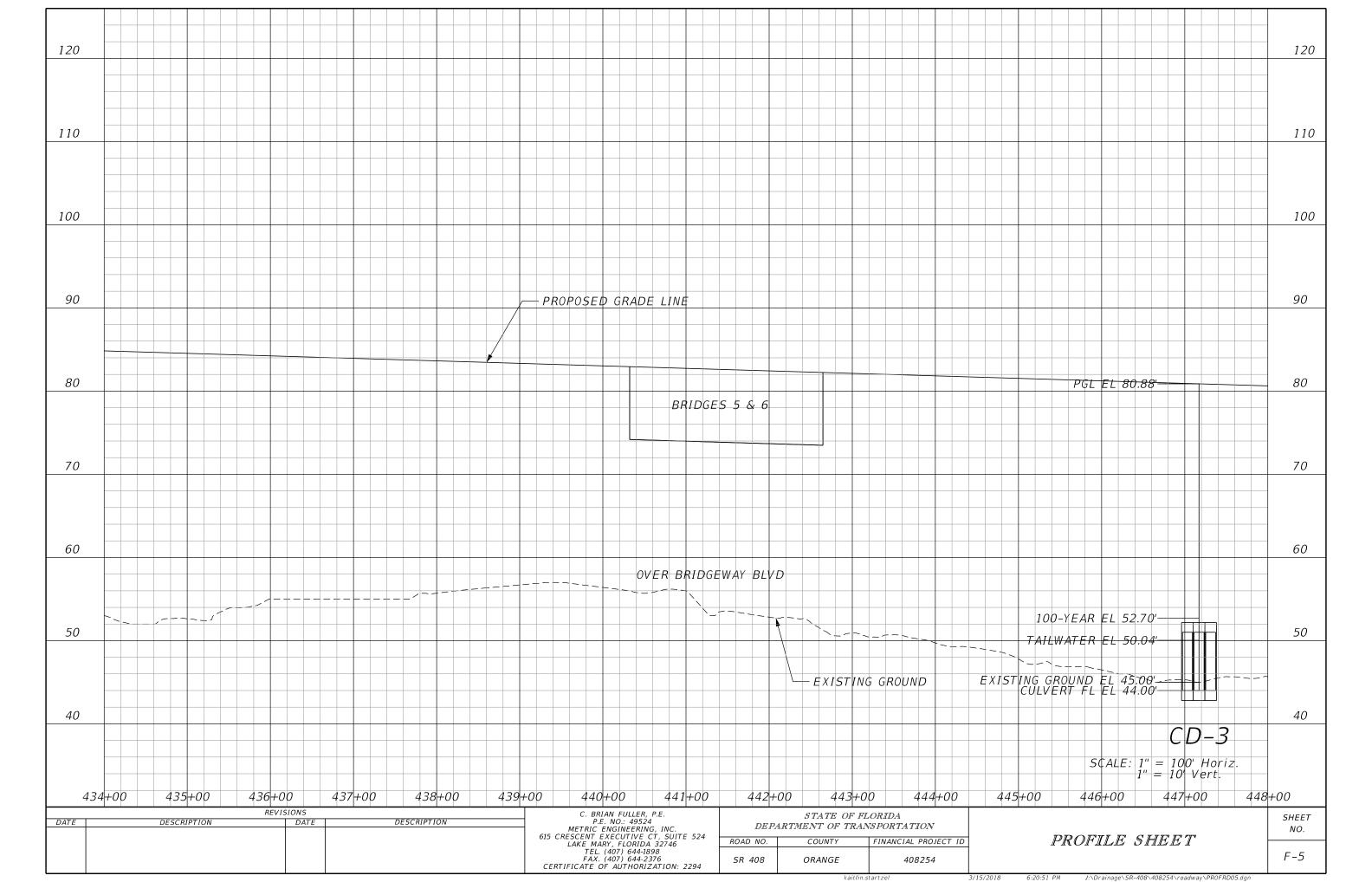
Cross Drain and Bridge Profiles

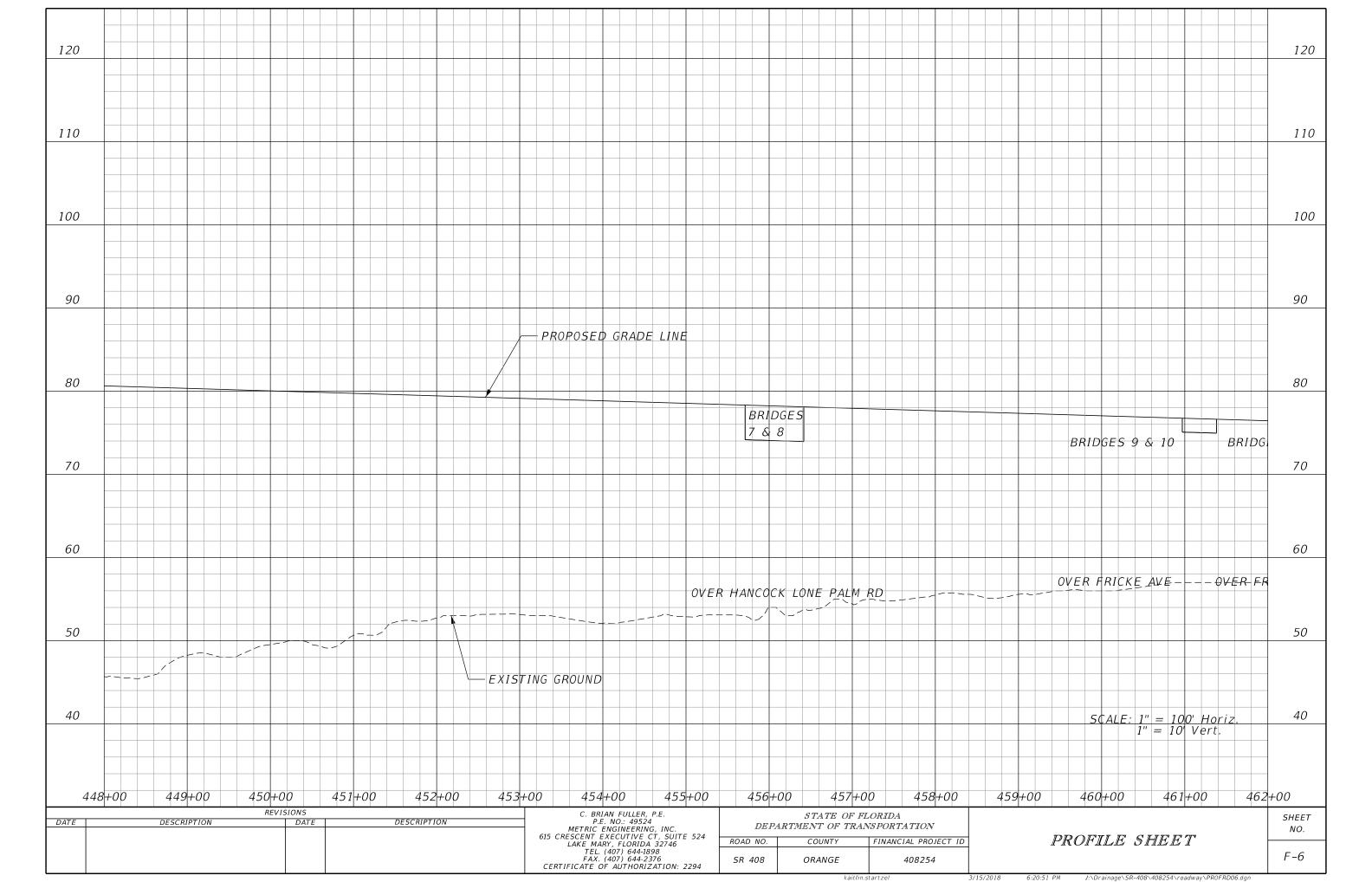


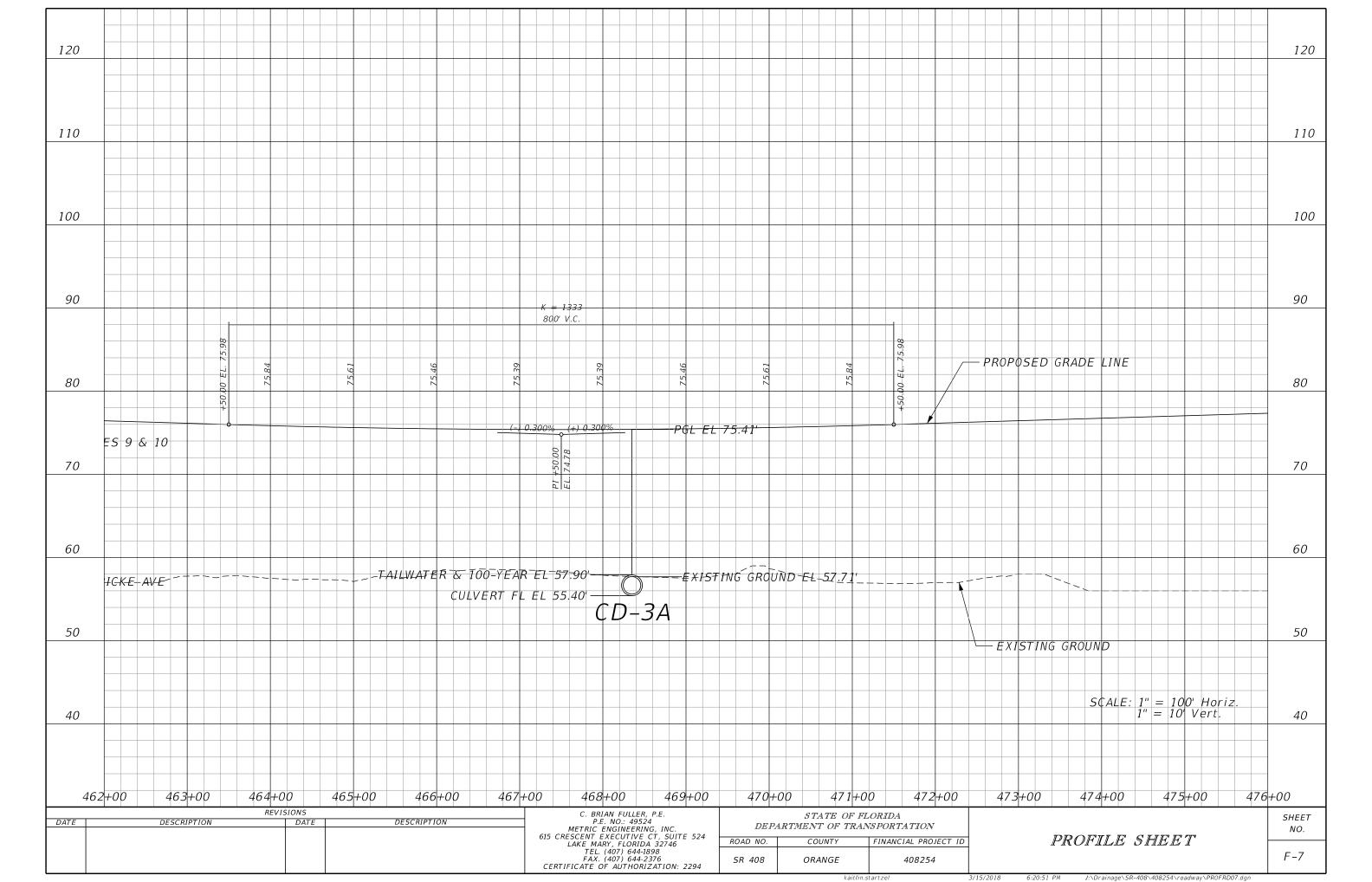


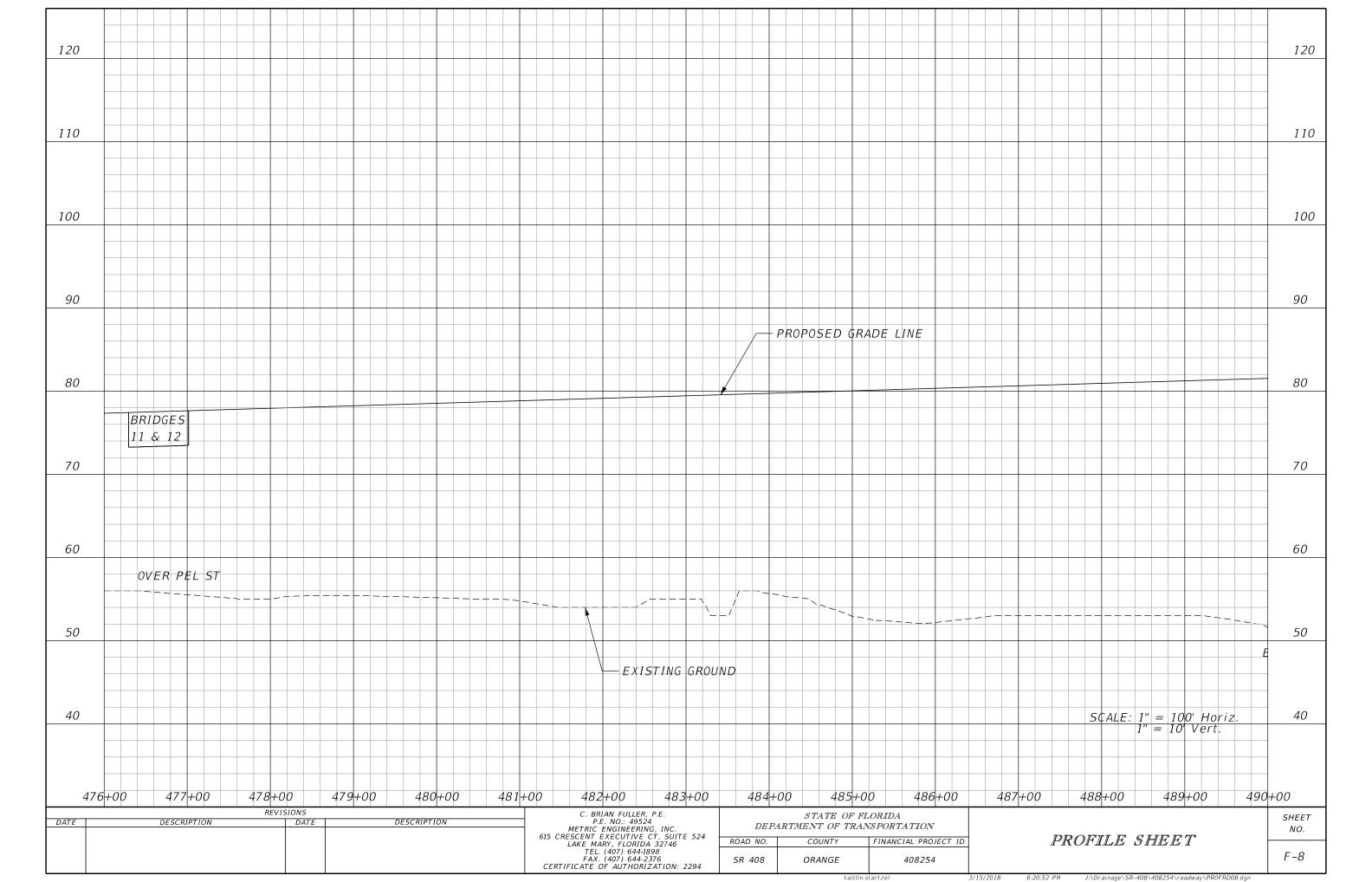


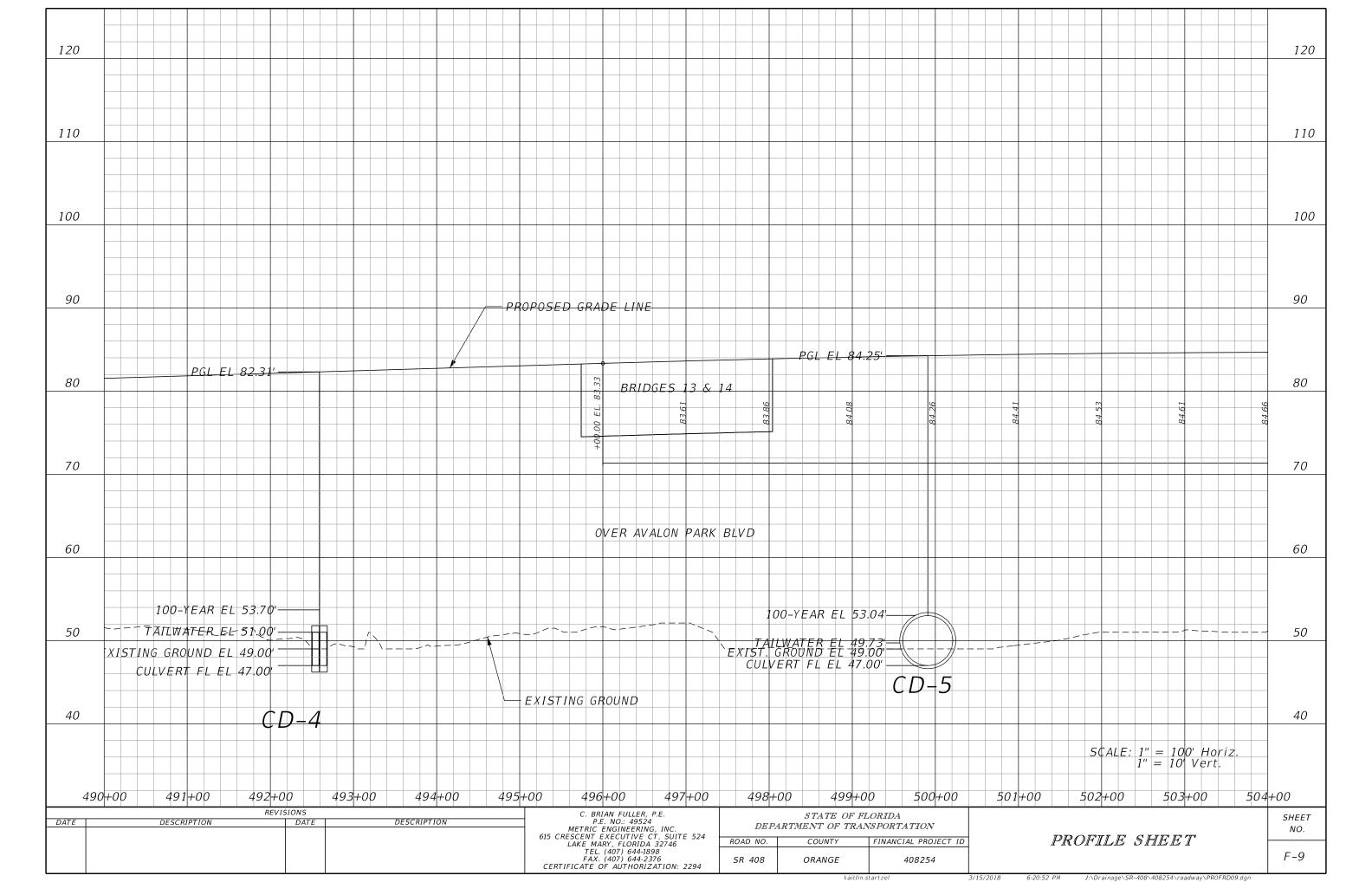


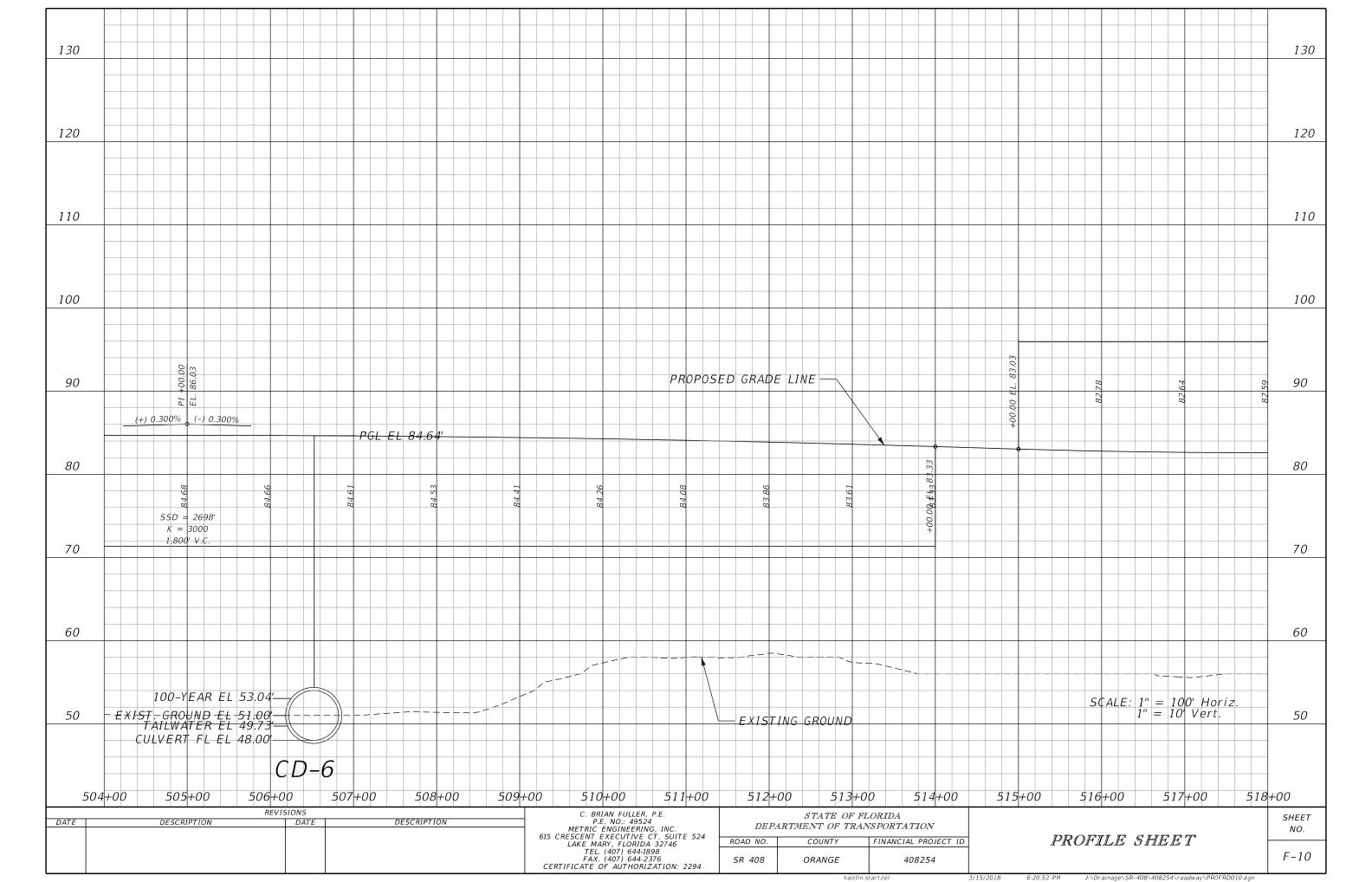


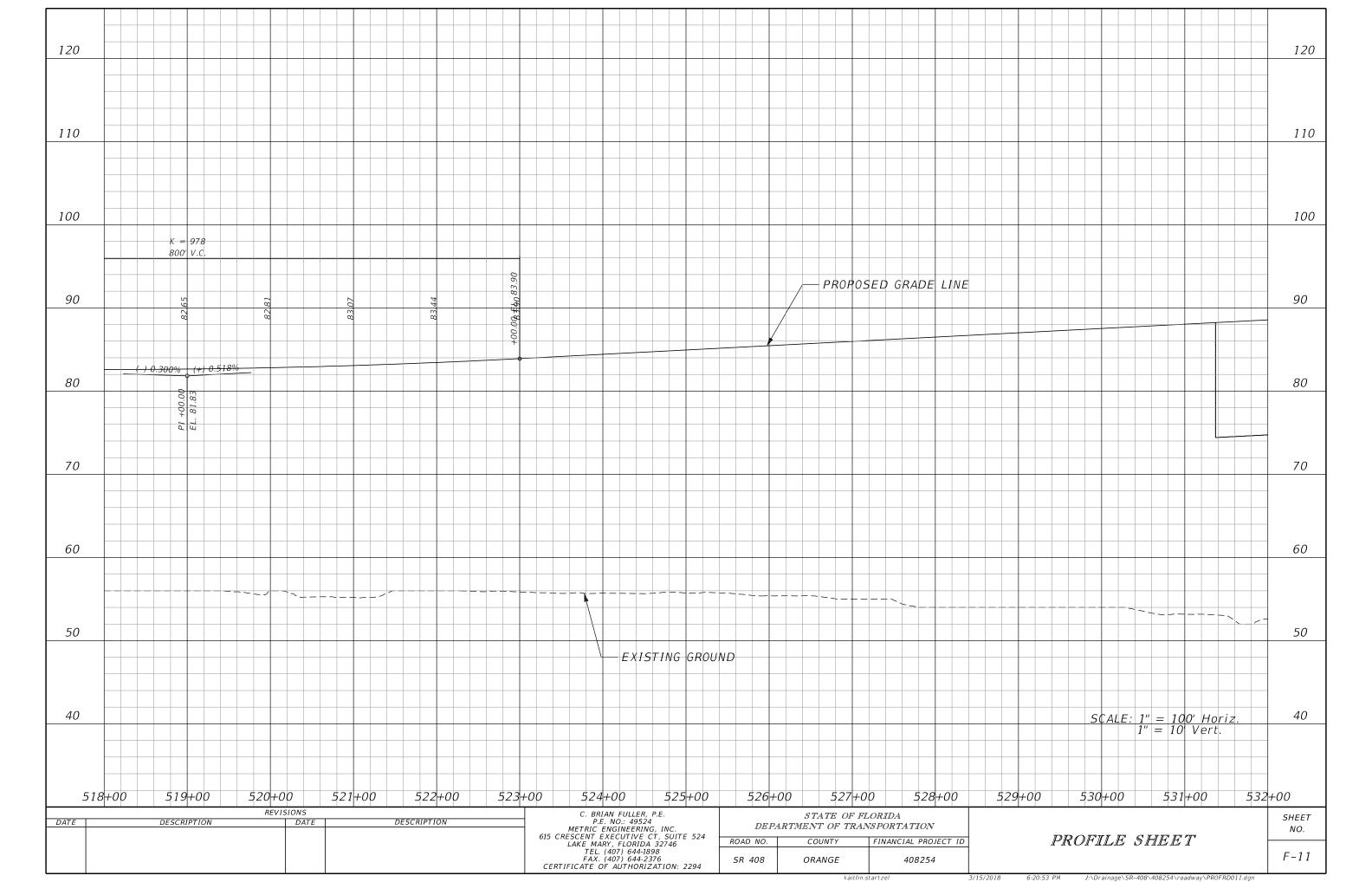


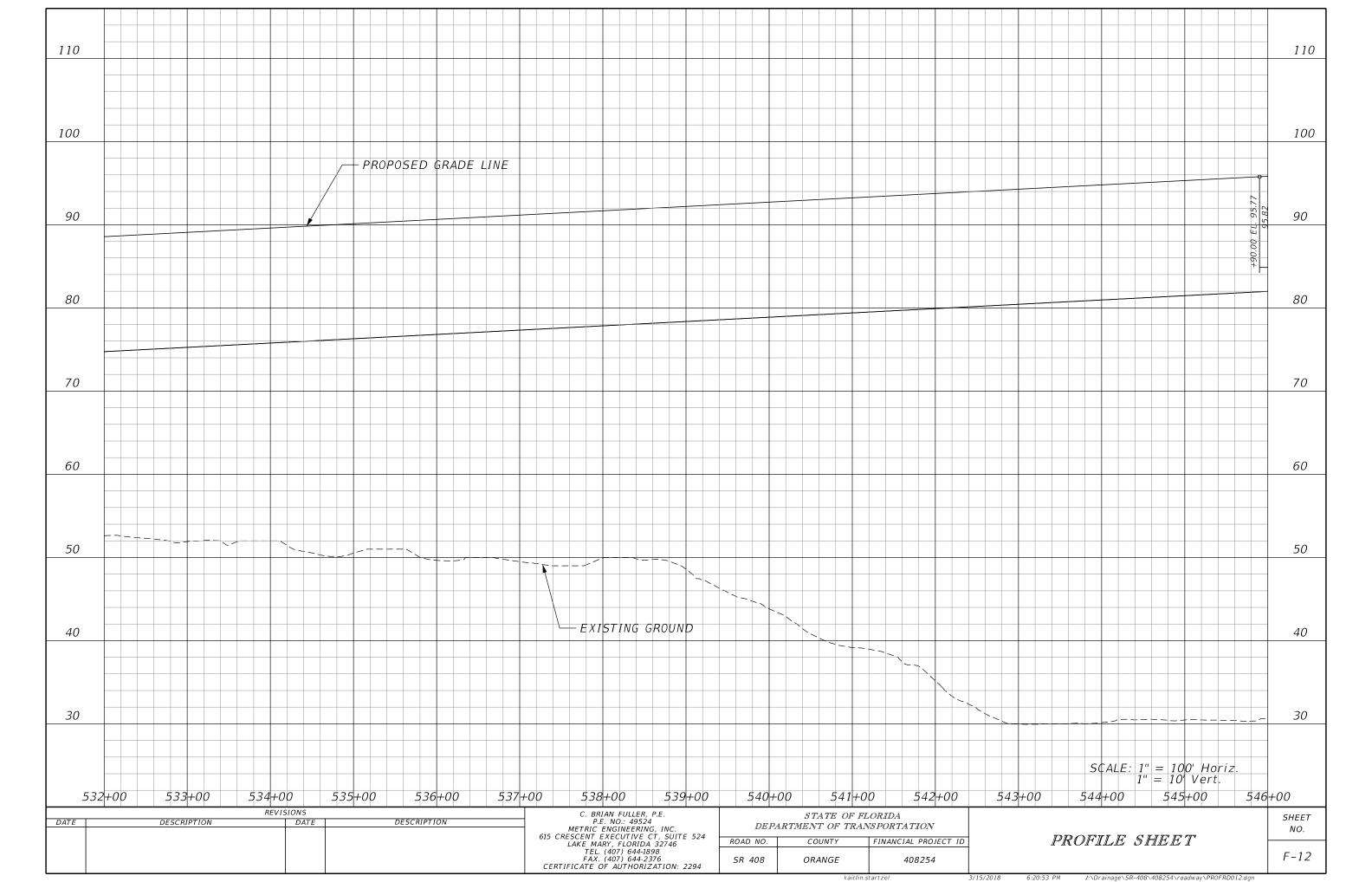


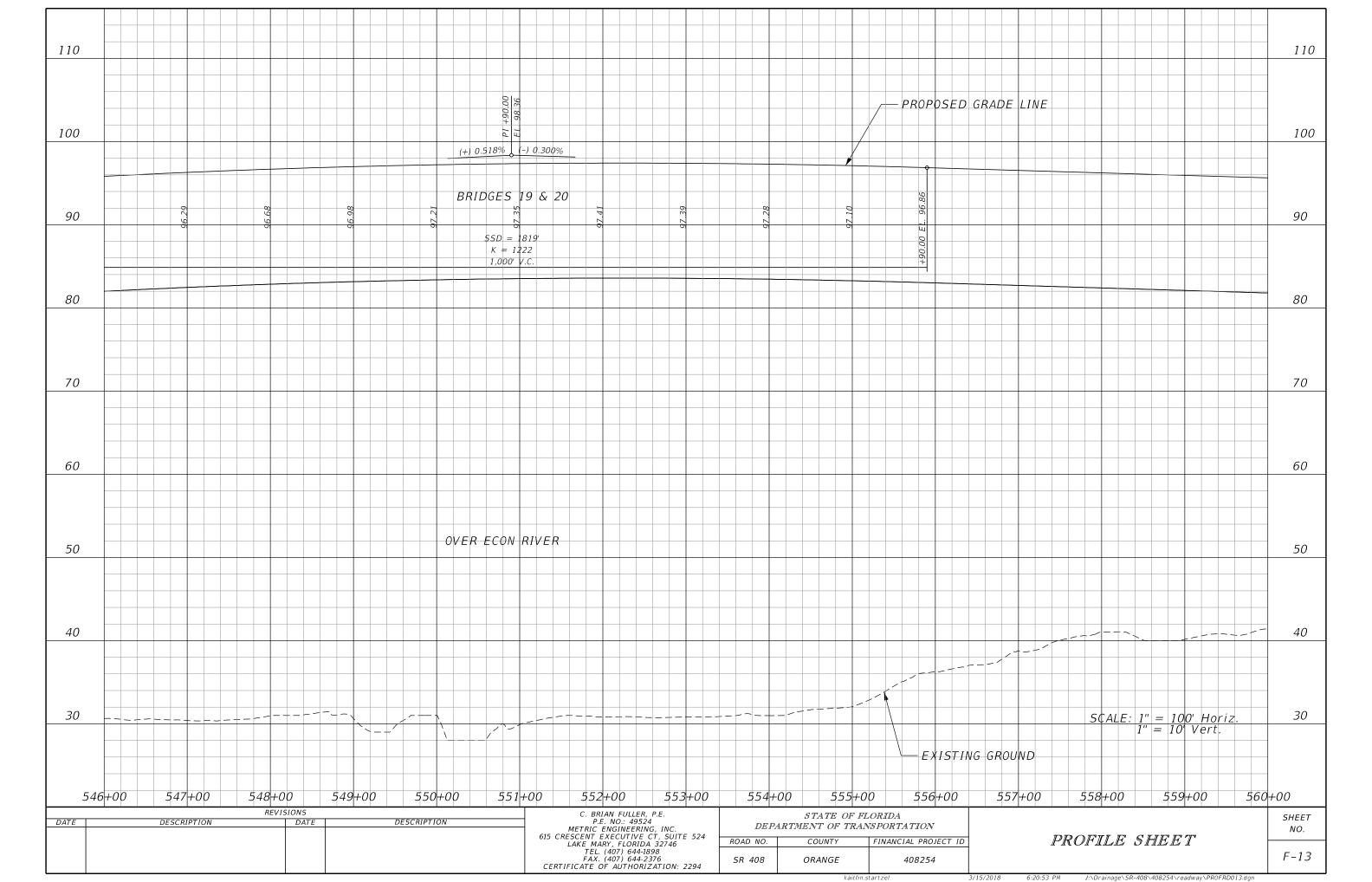


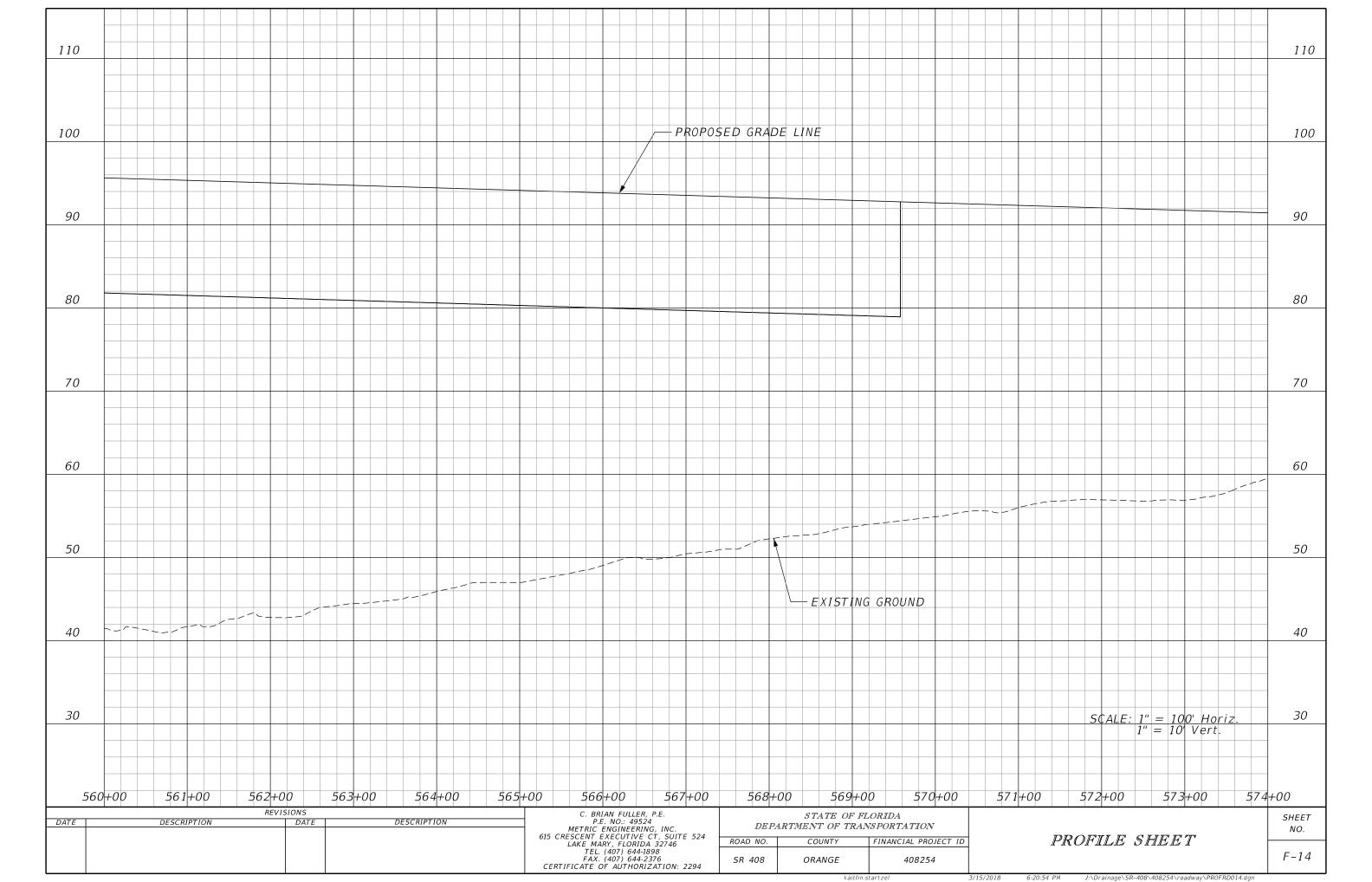


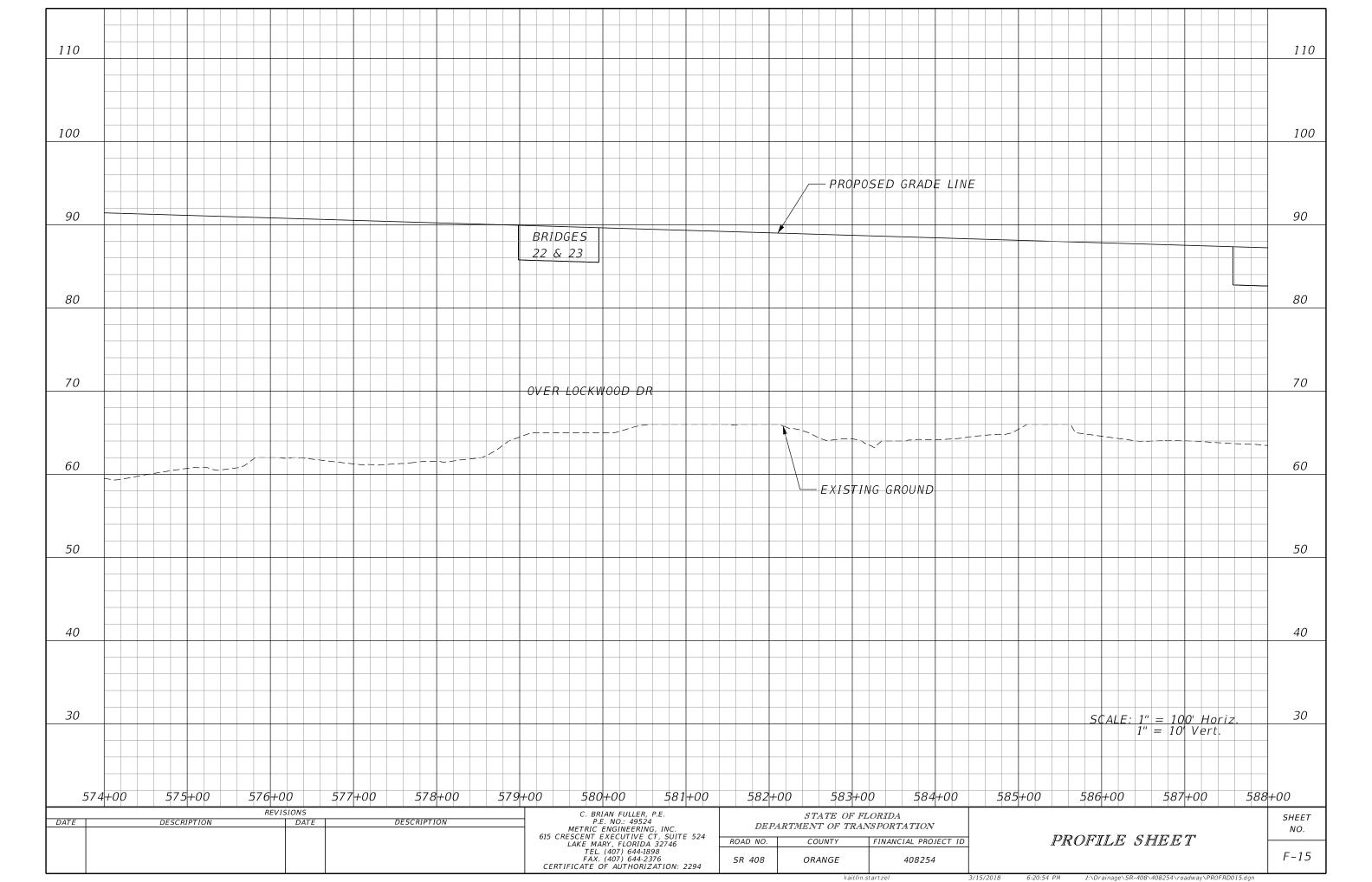


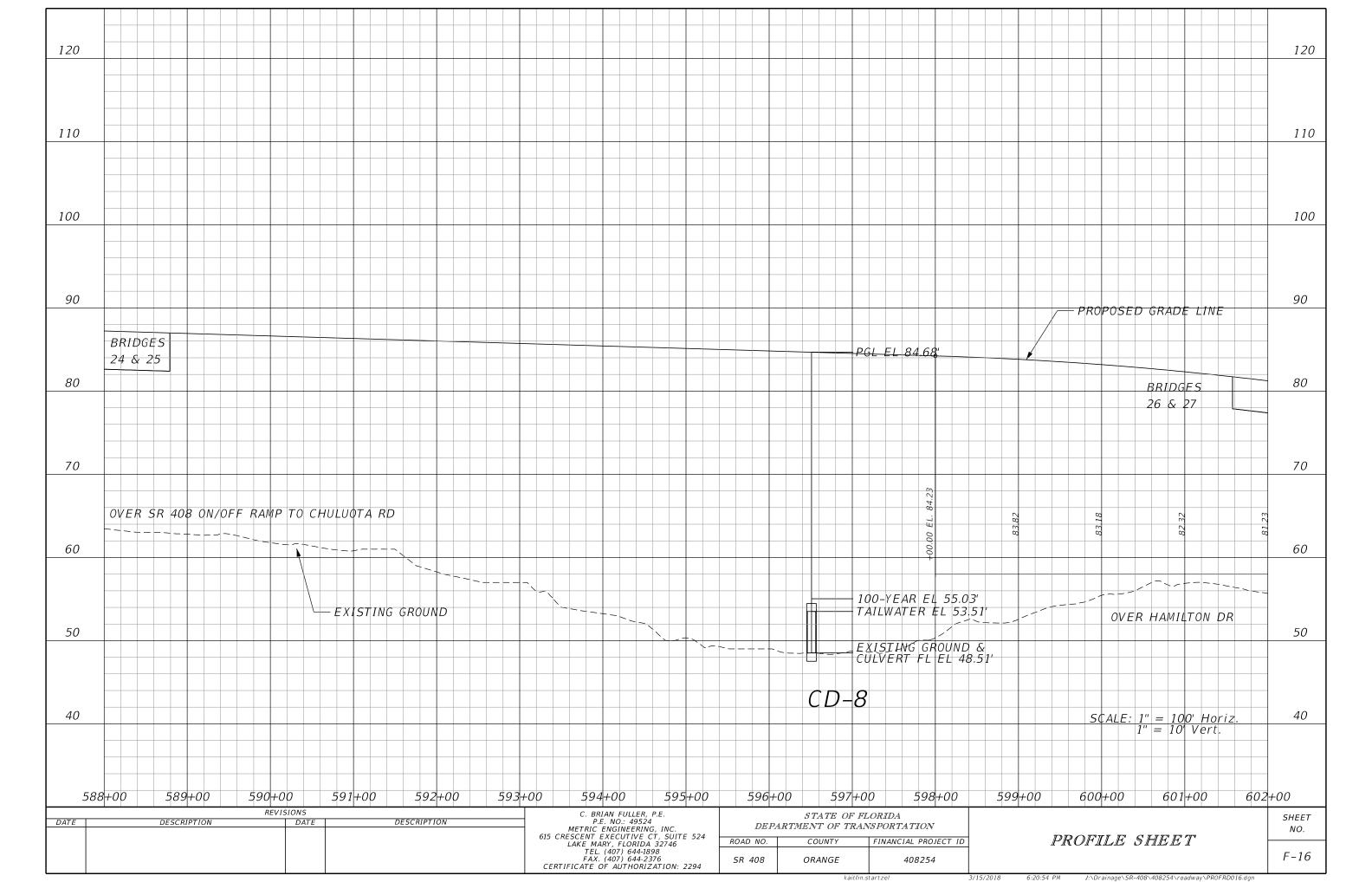


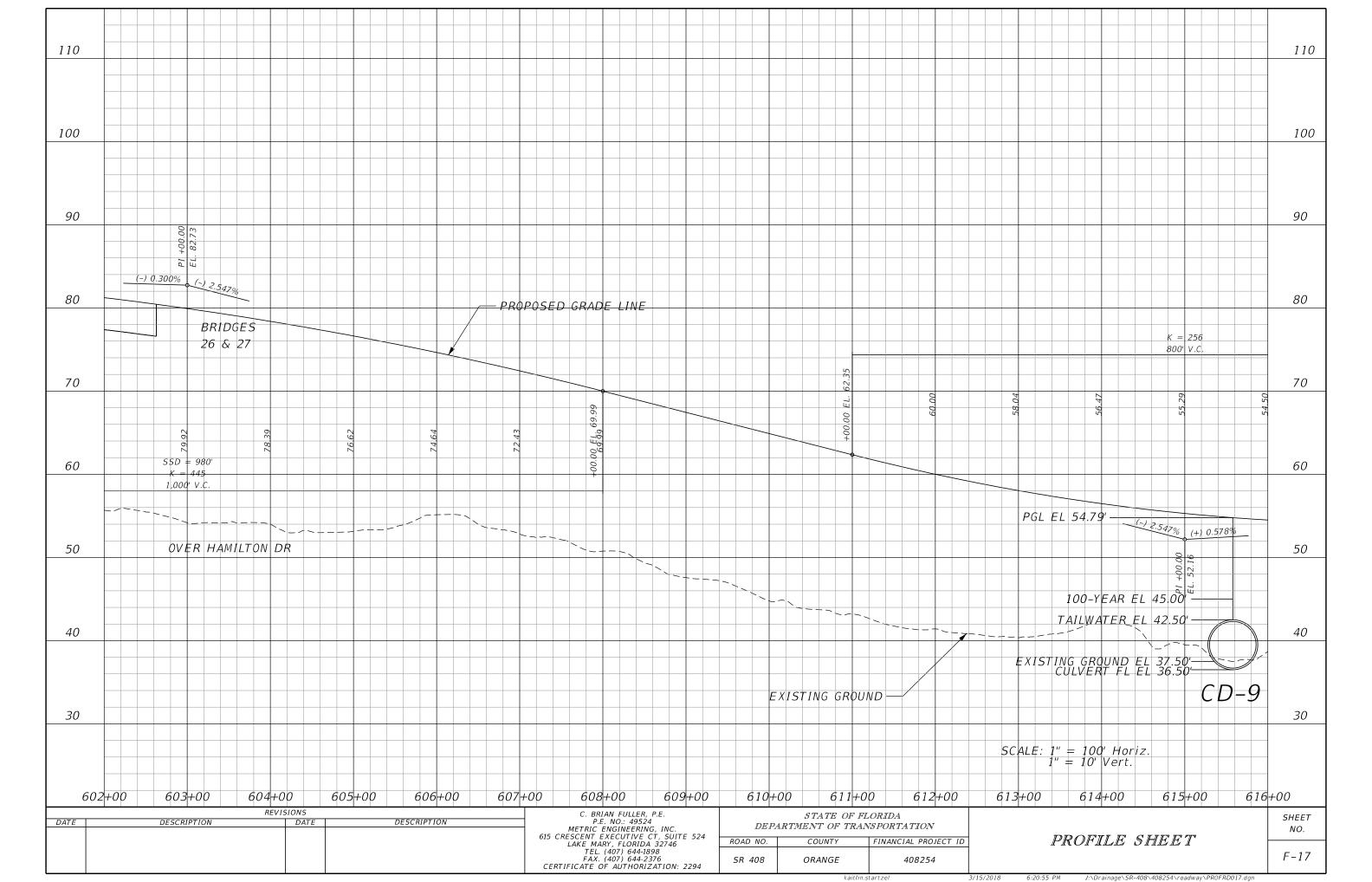


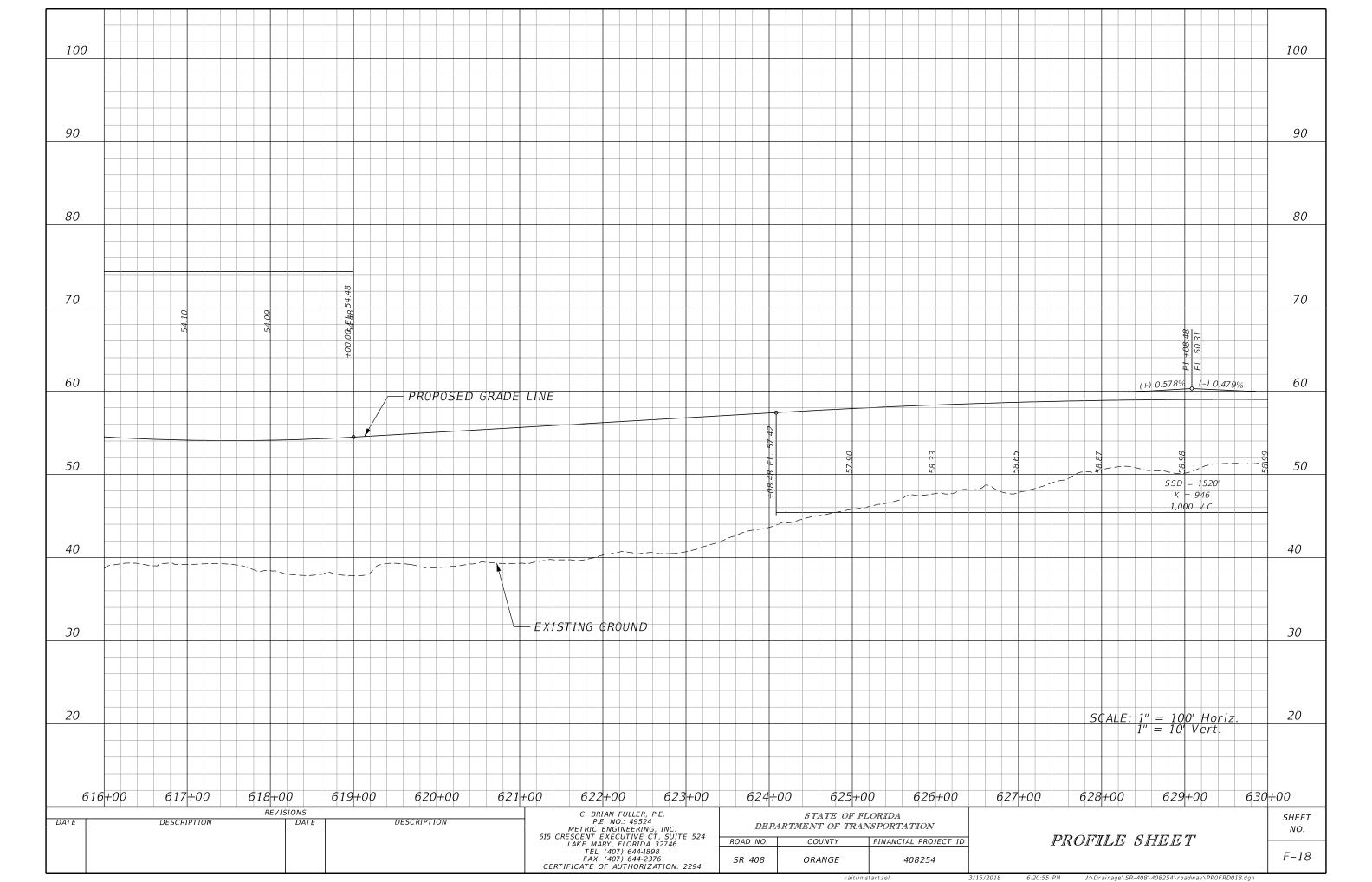


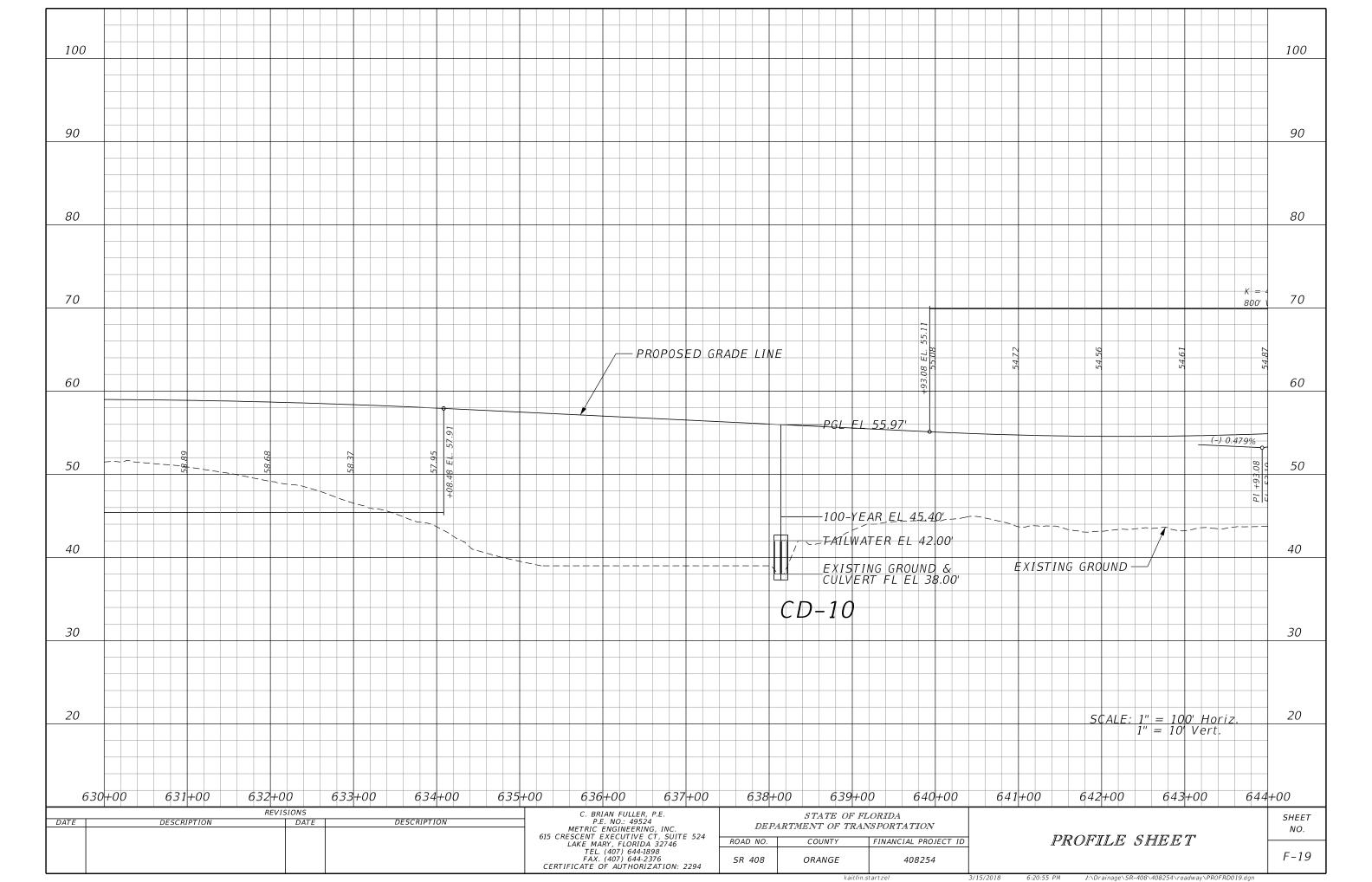


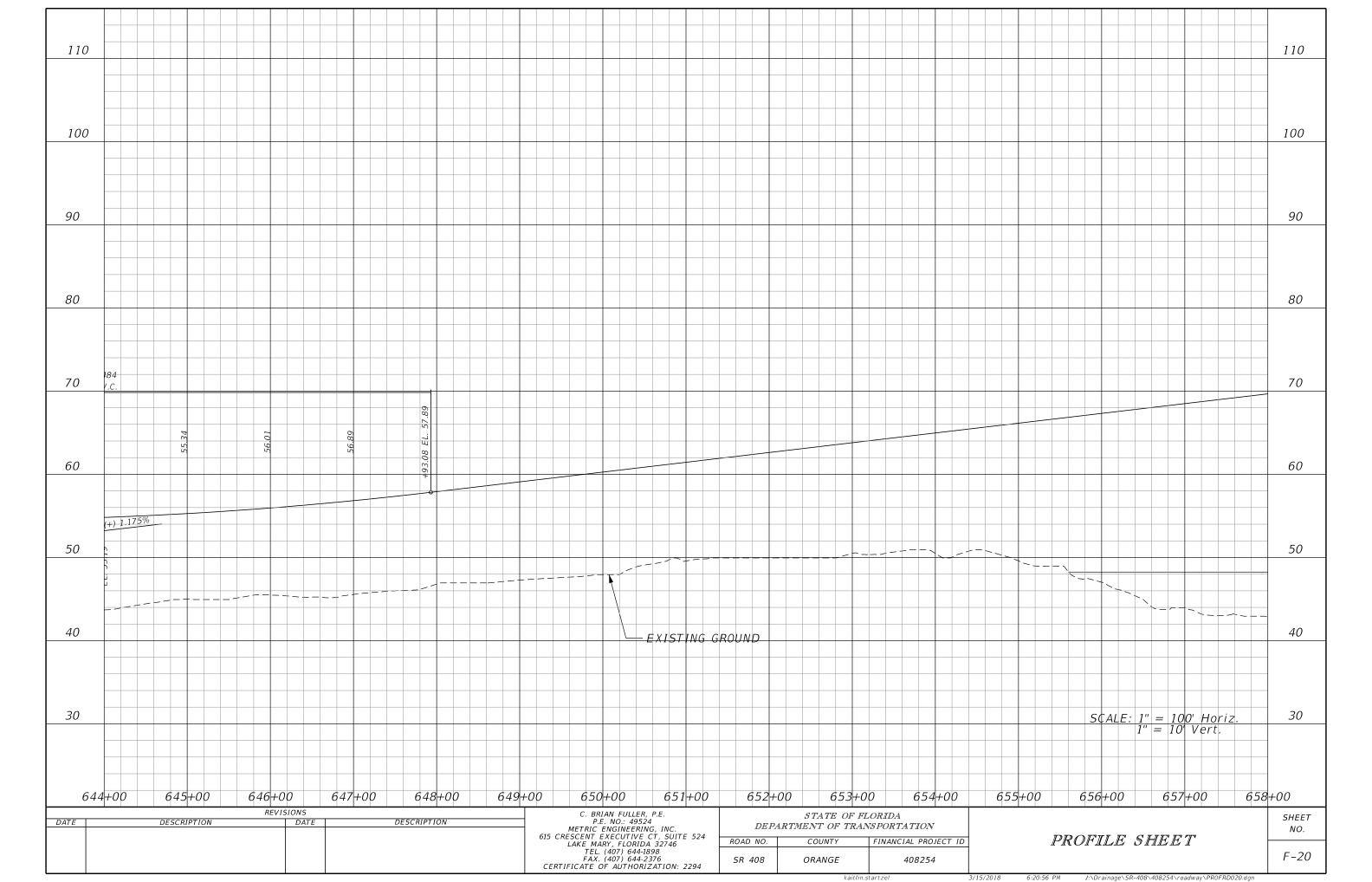


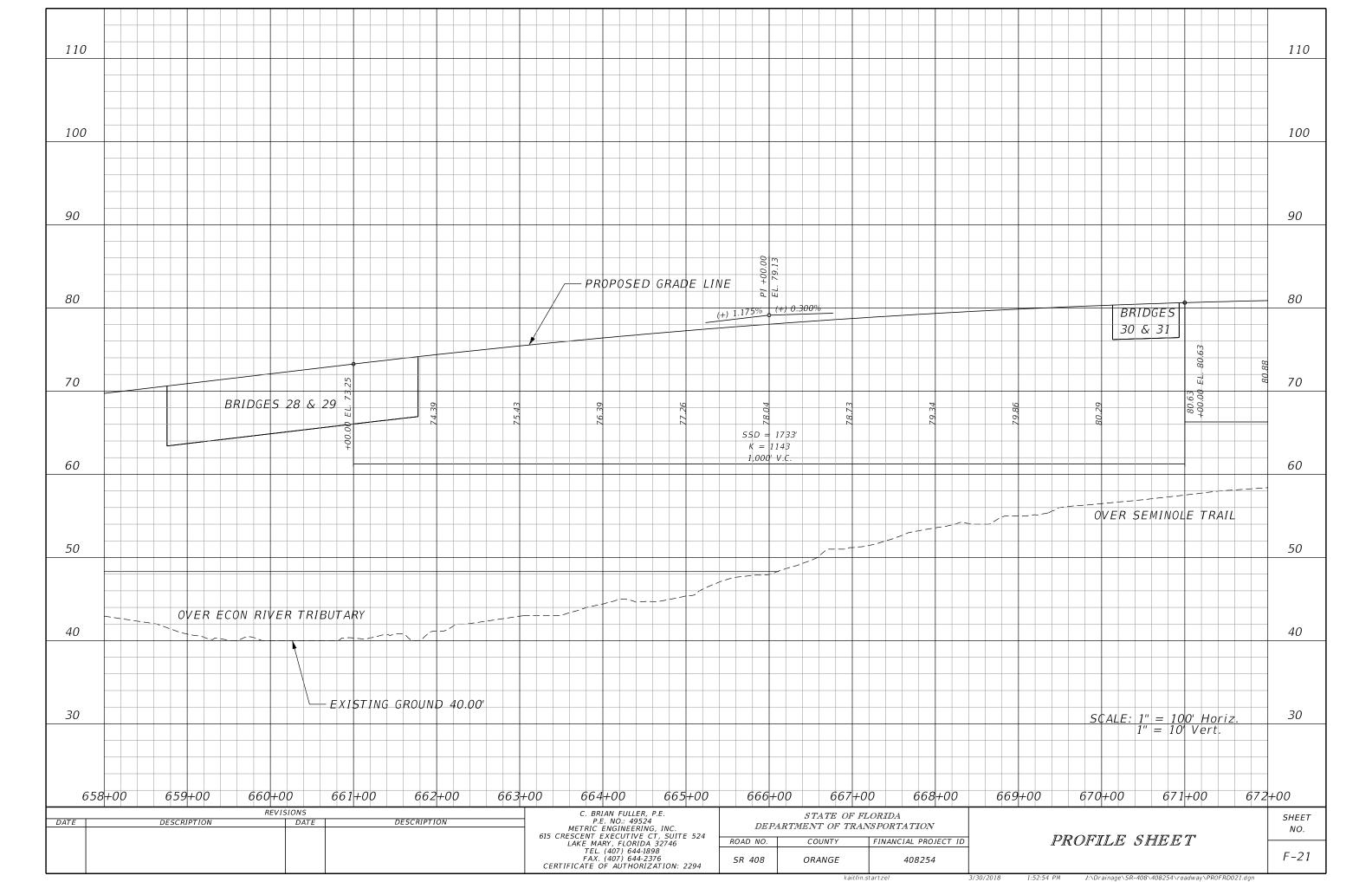


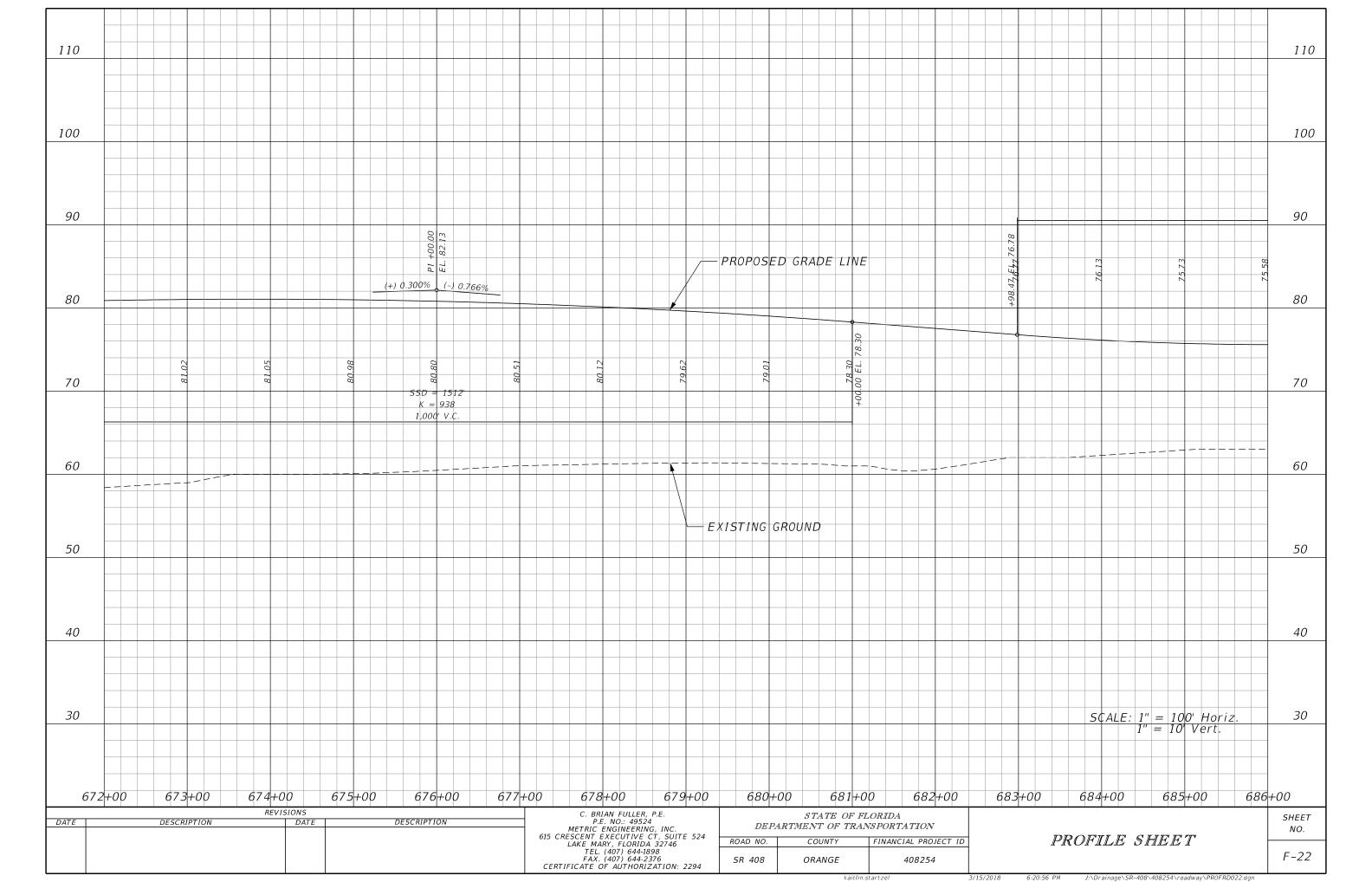


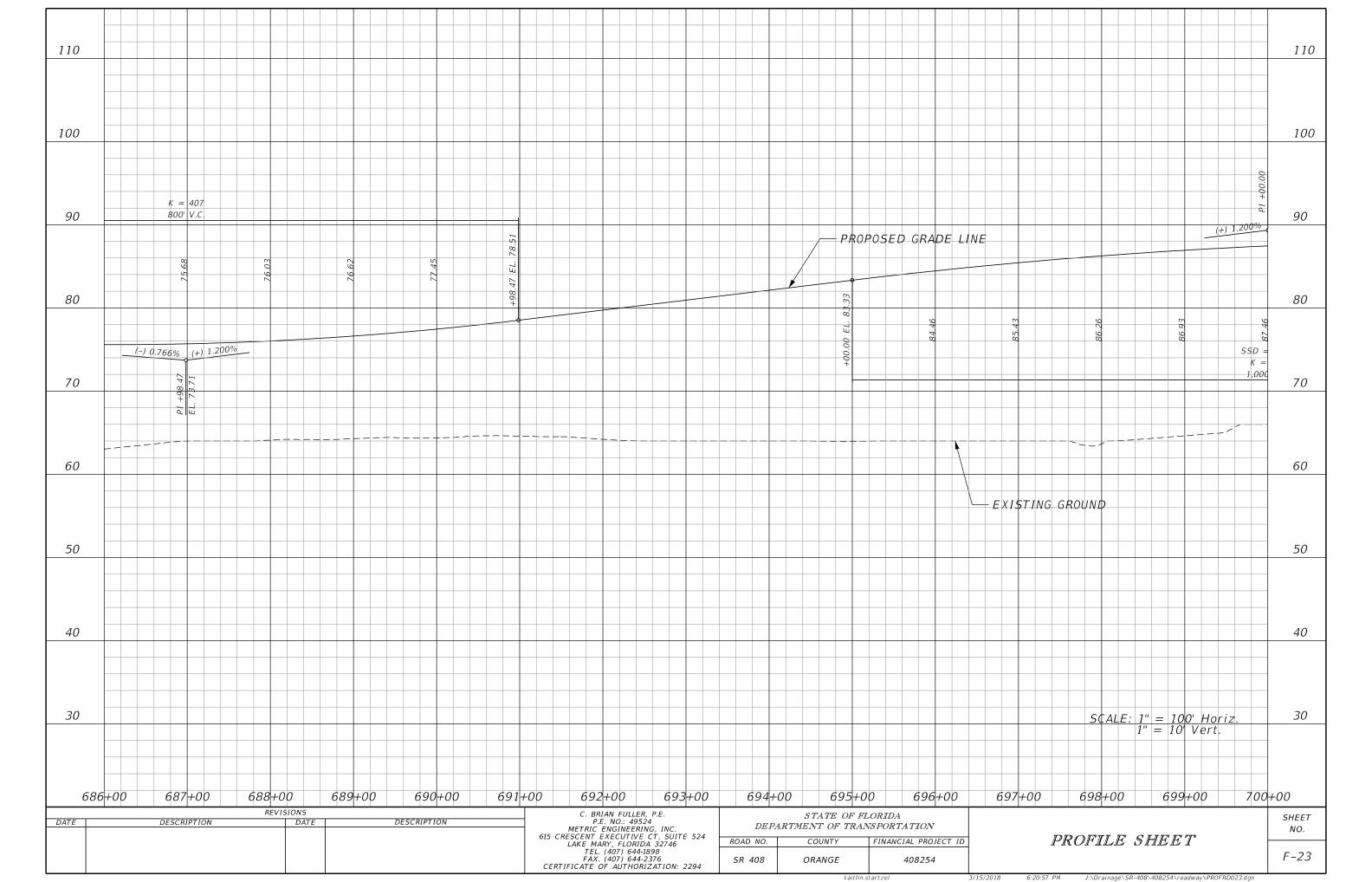


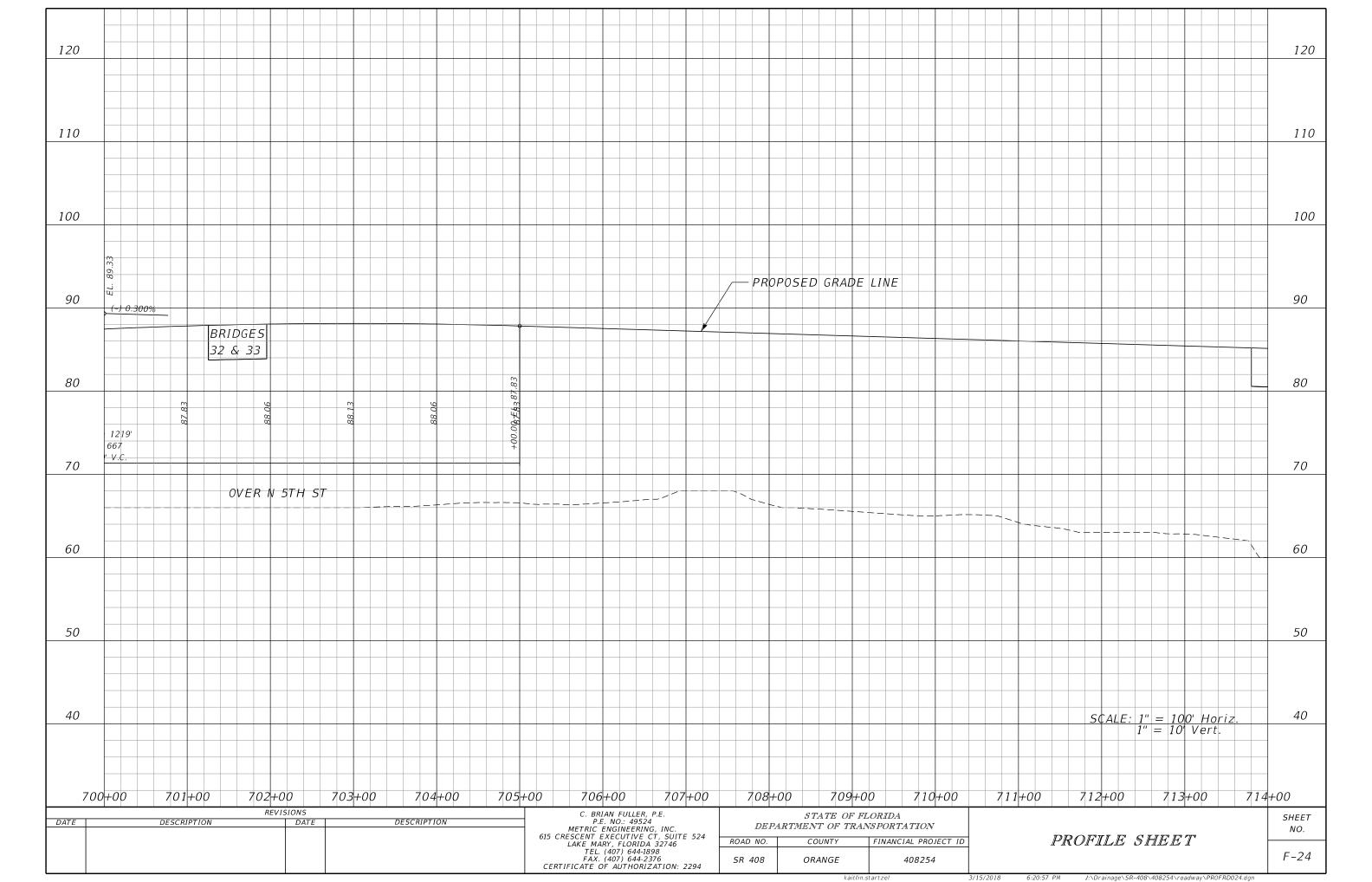


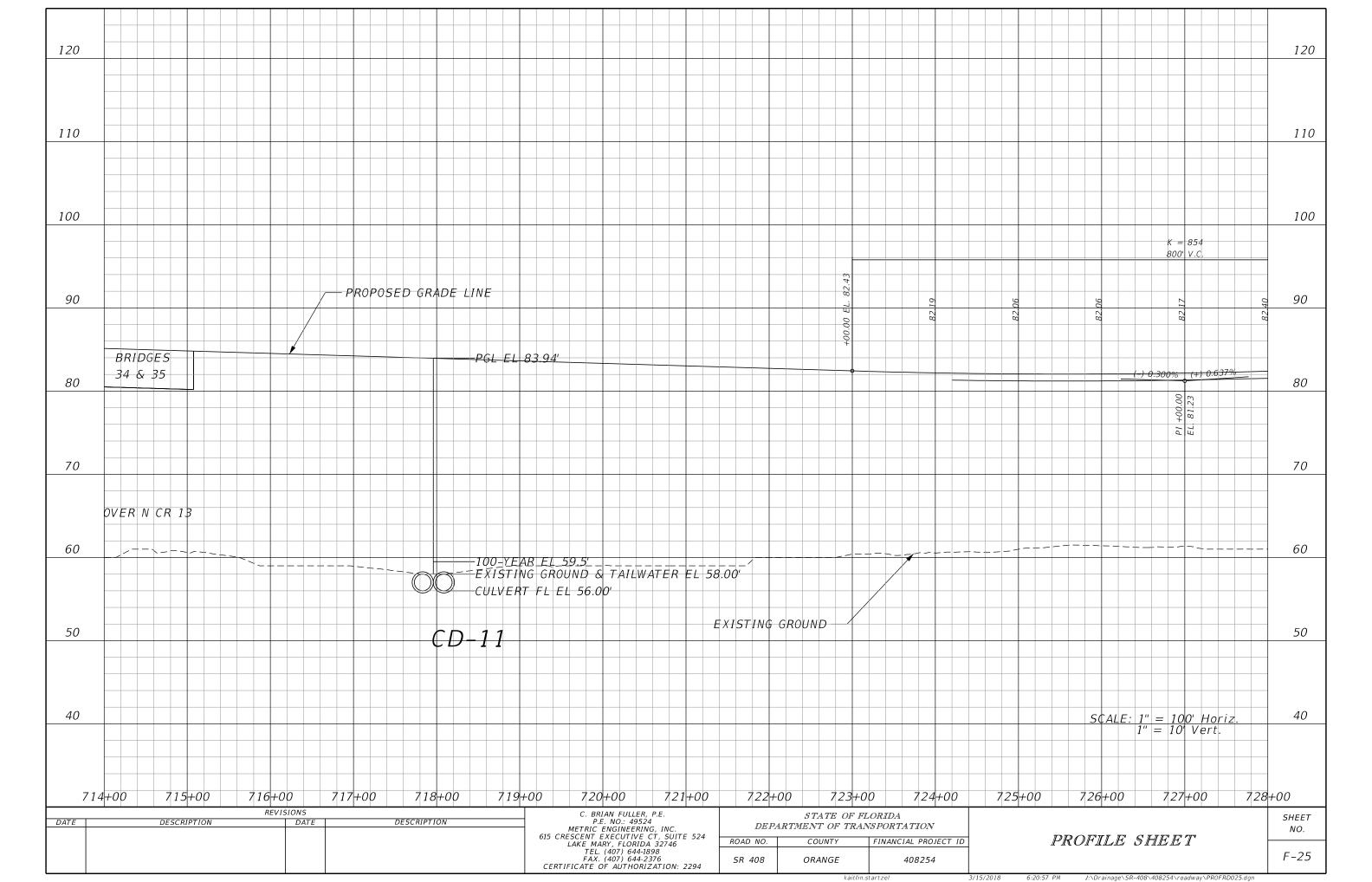


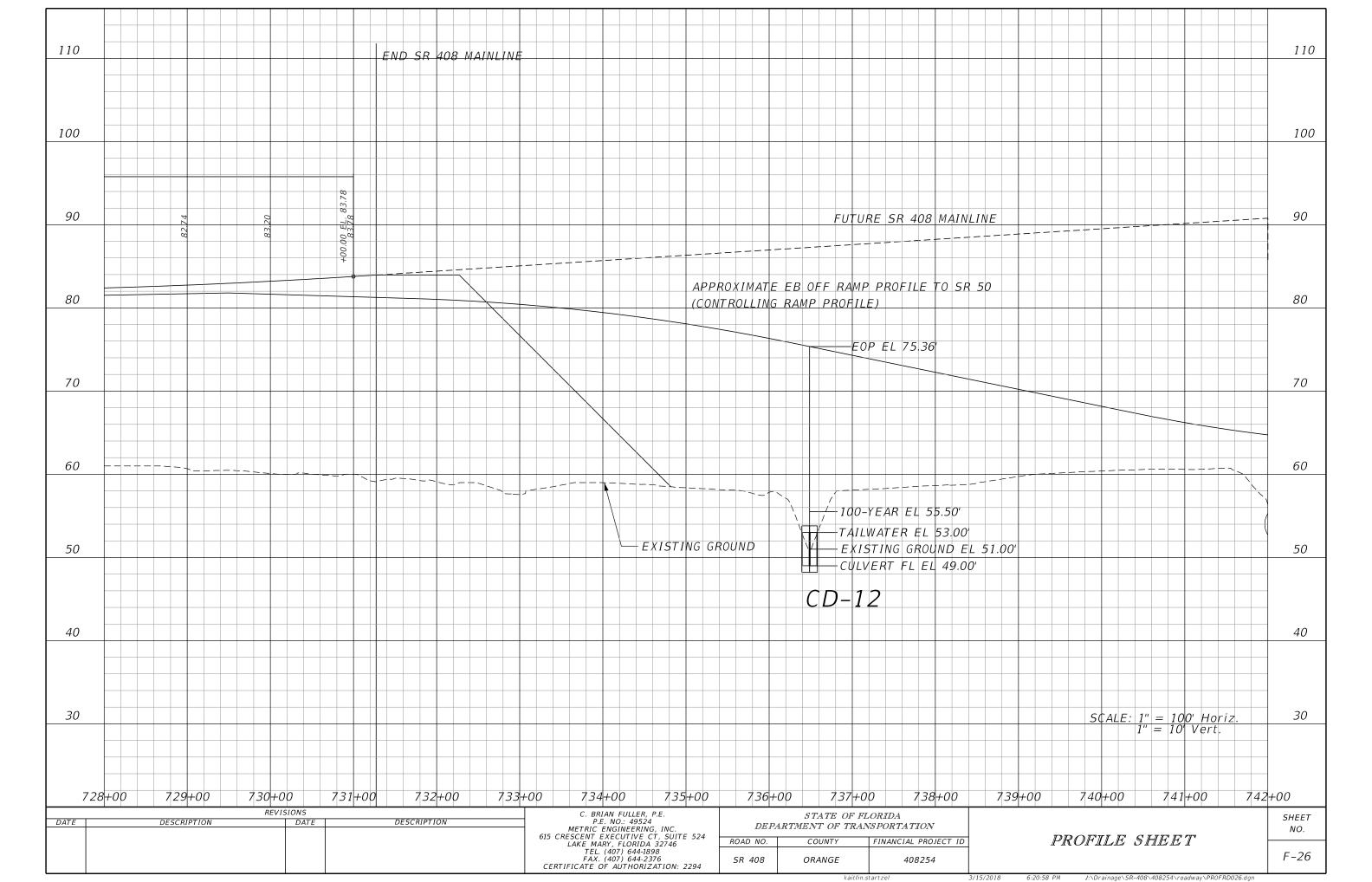


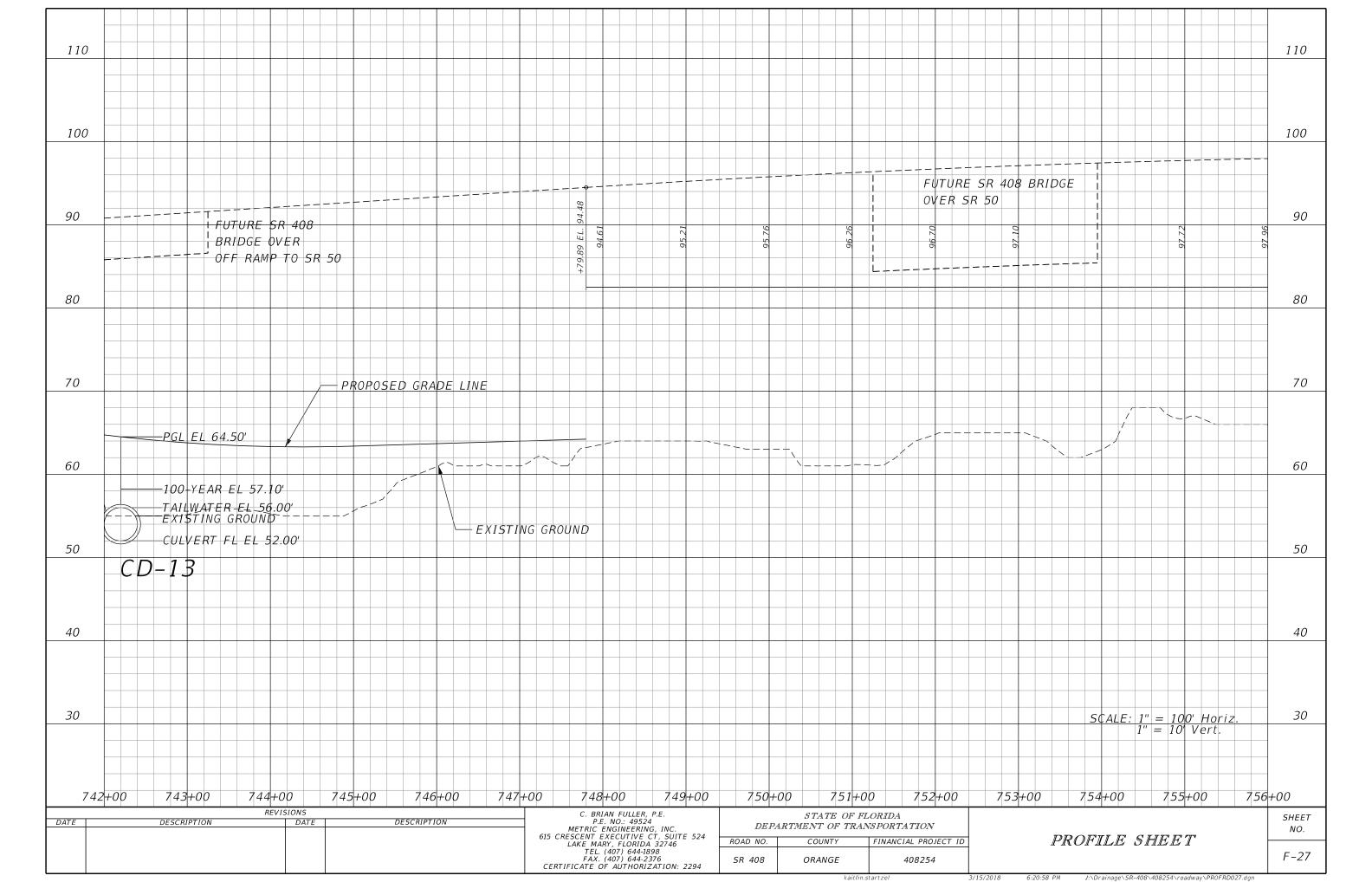


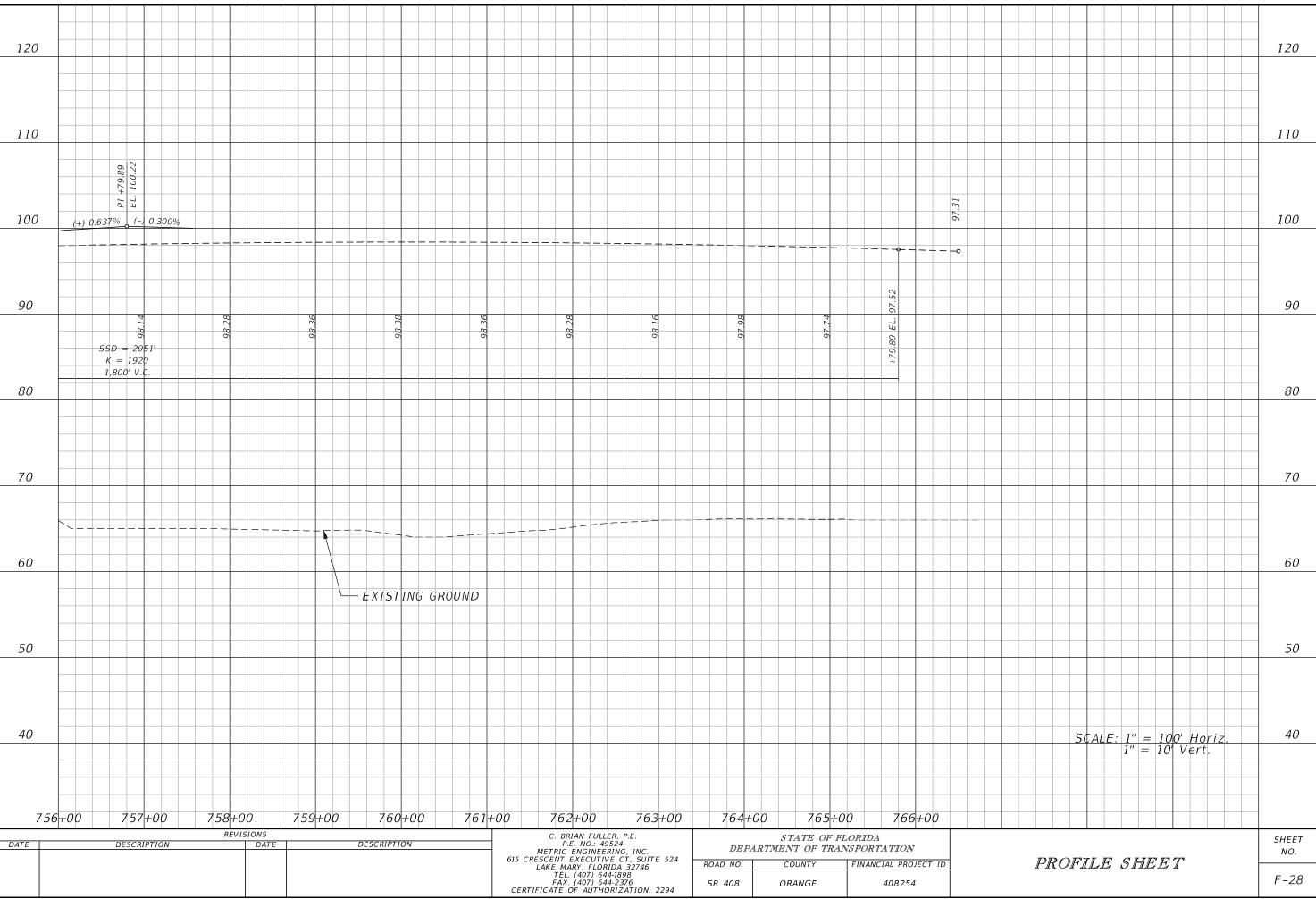


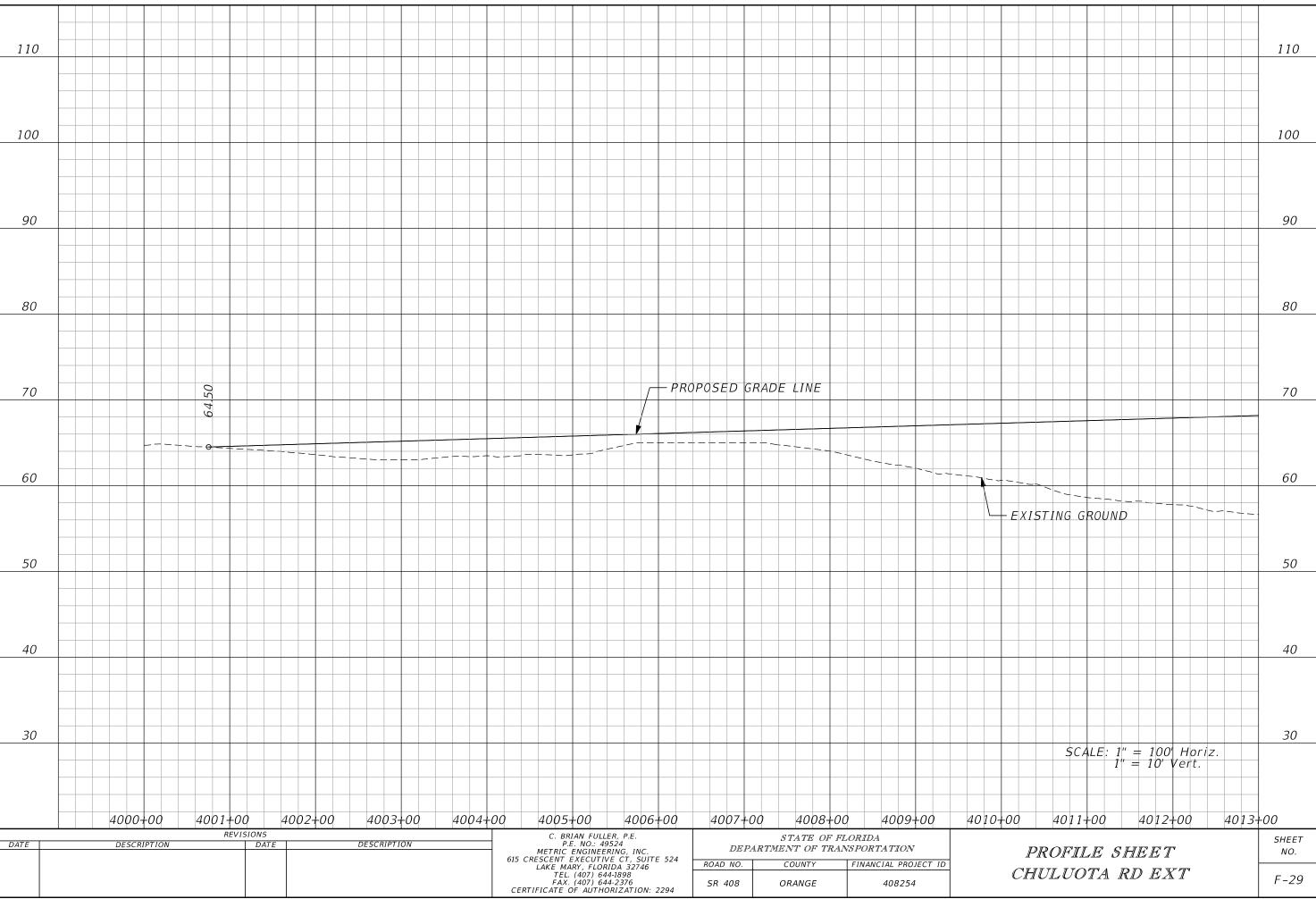


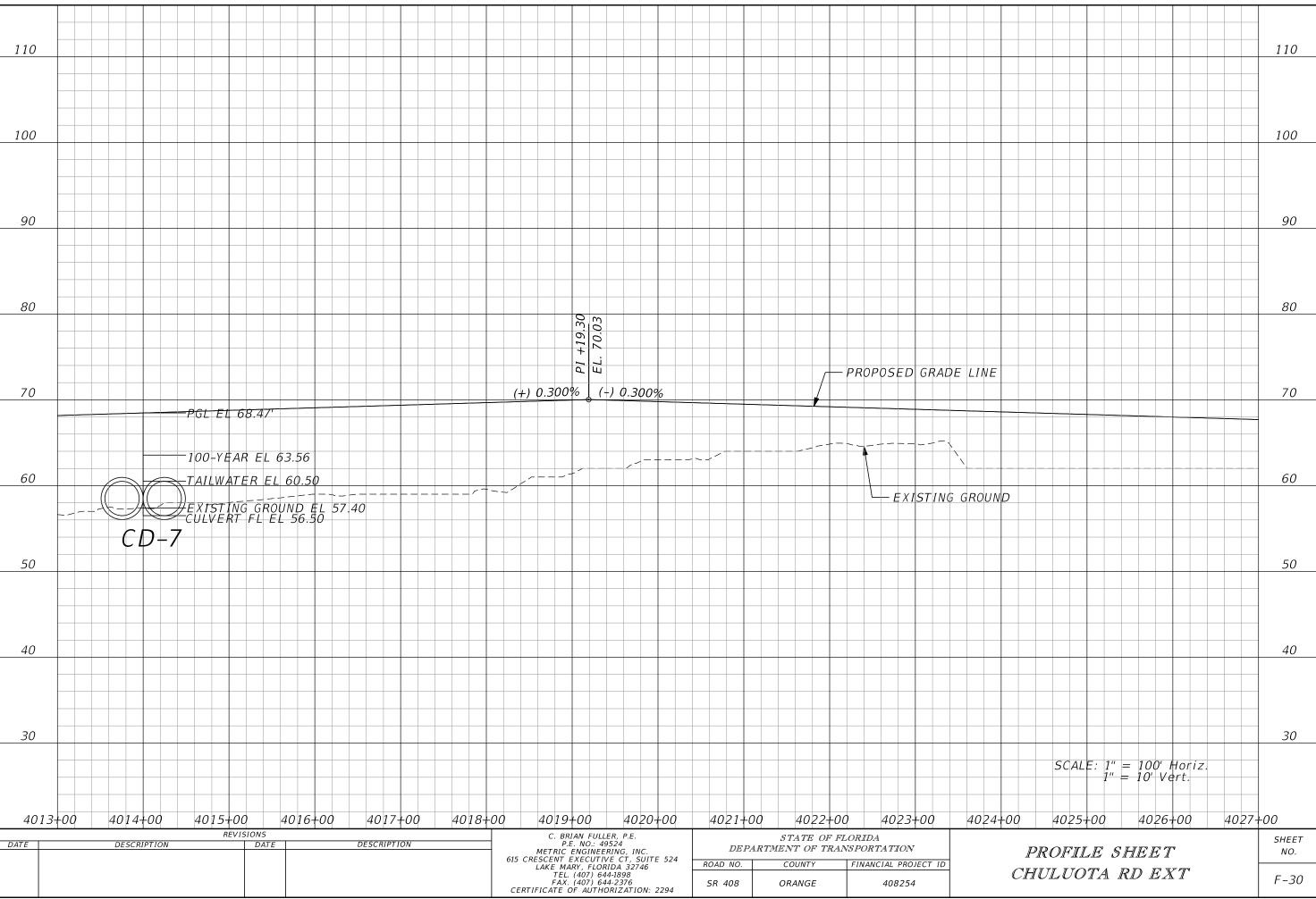


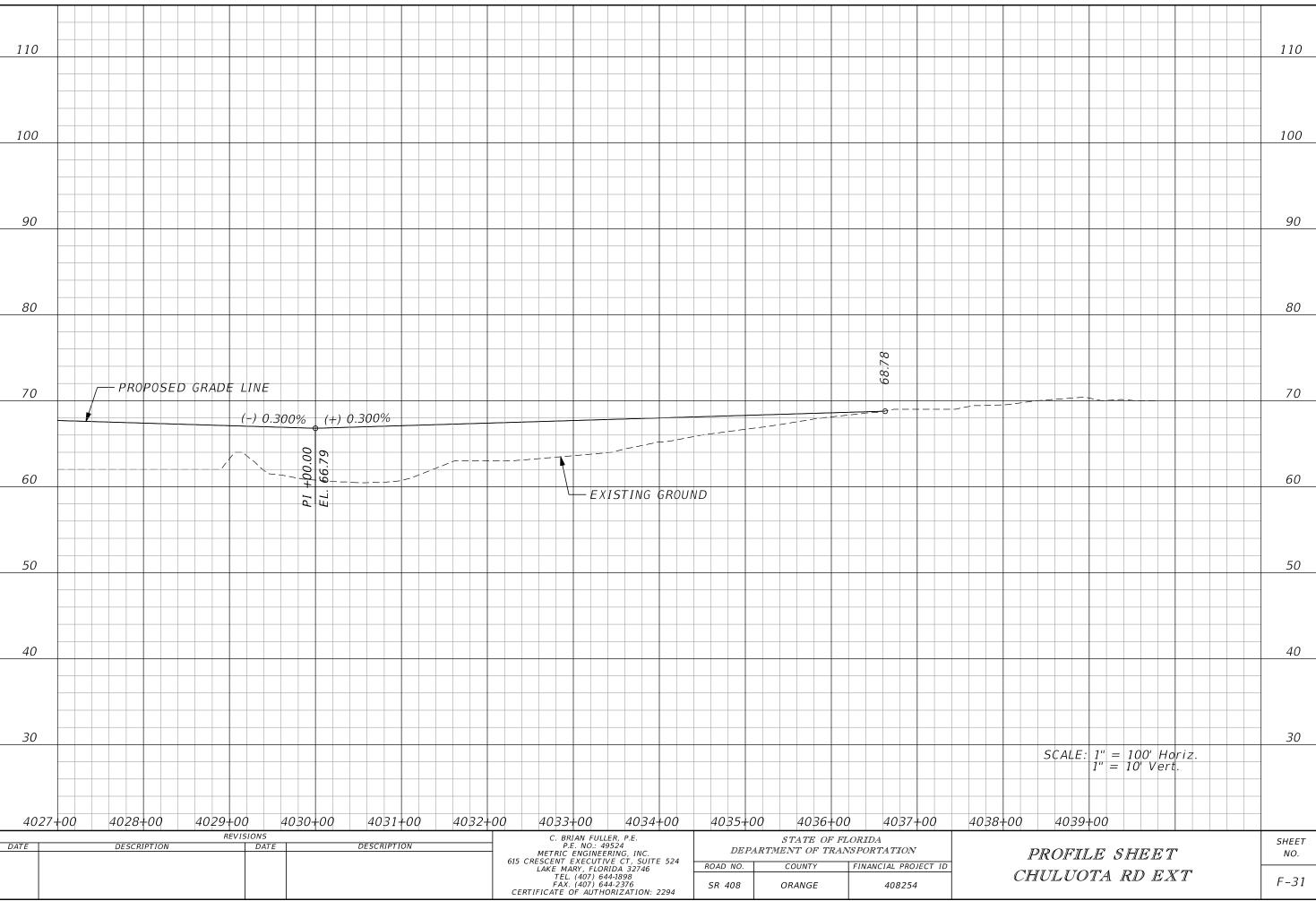


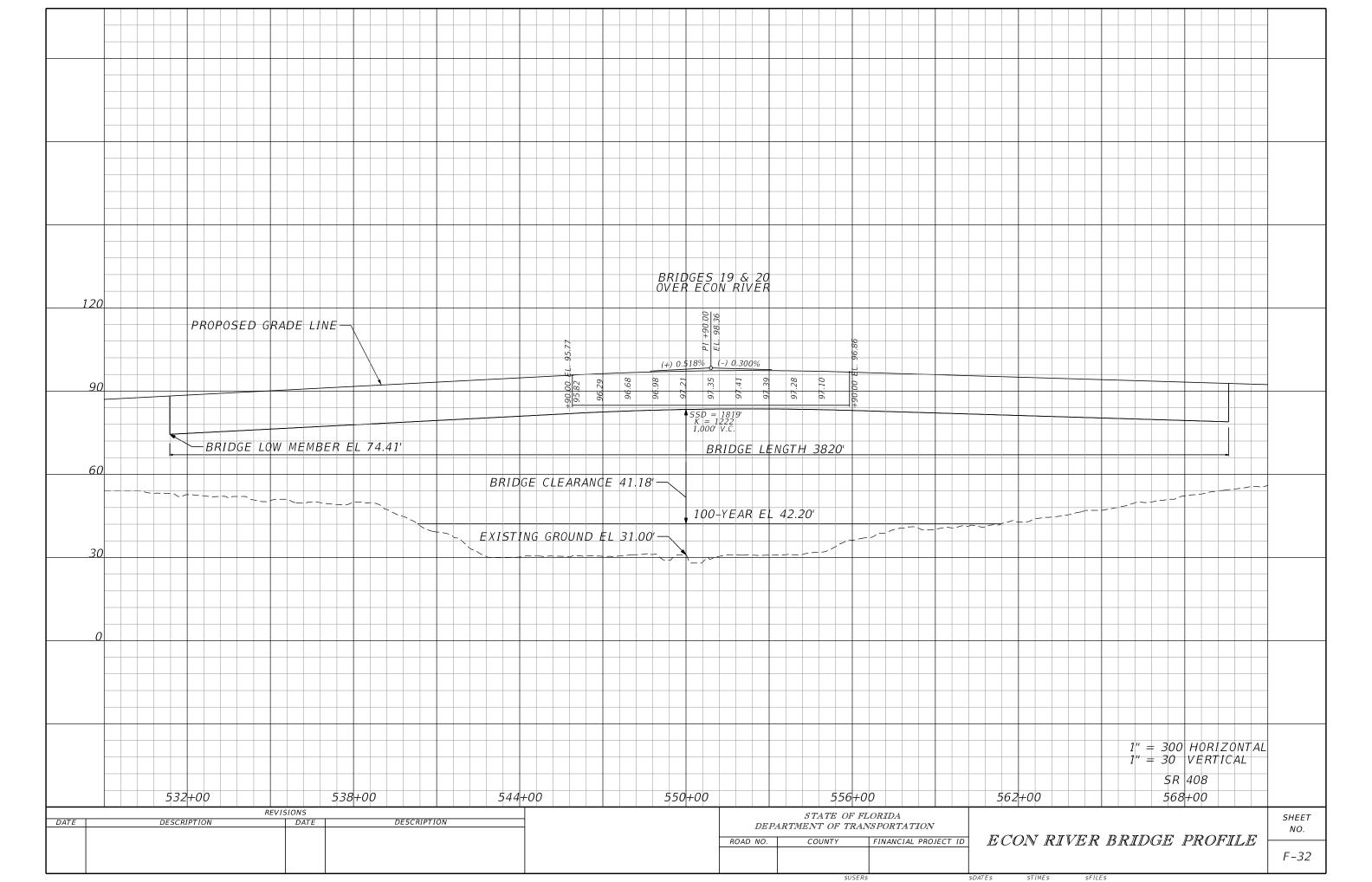


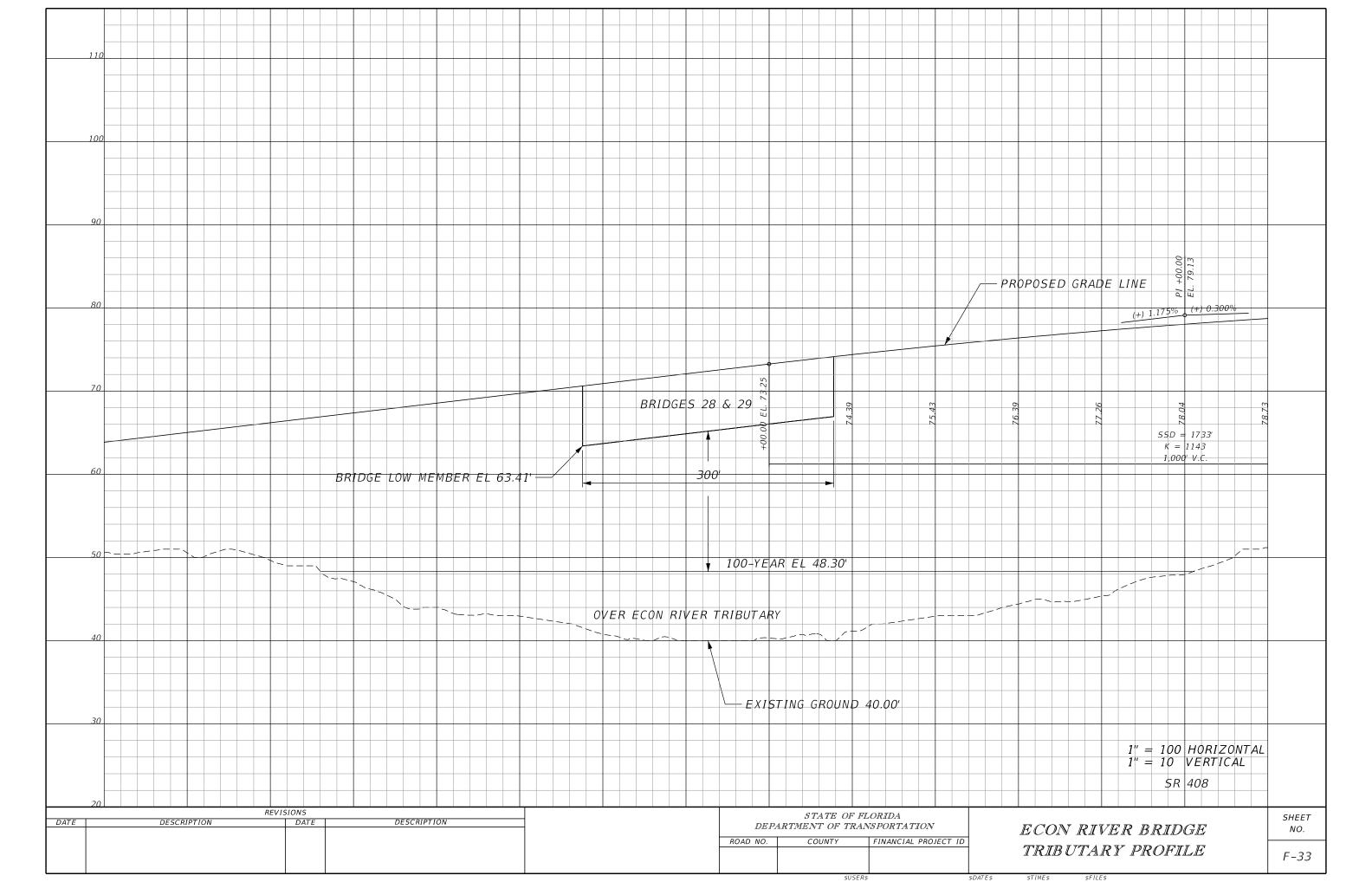












Appendix: G

Cross Drain Hydraulic Analysis

Cross Drain 1

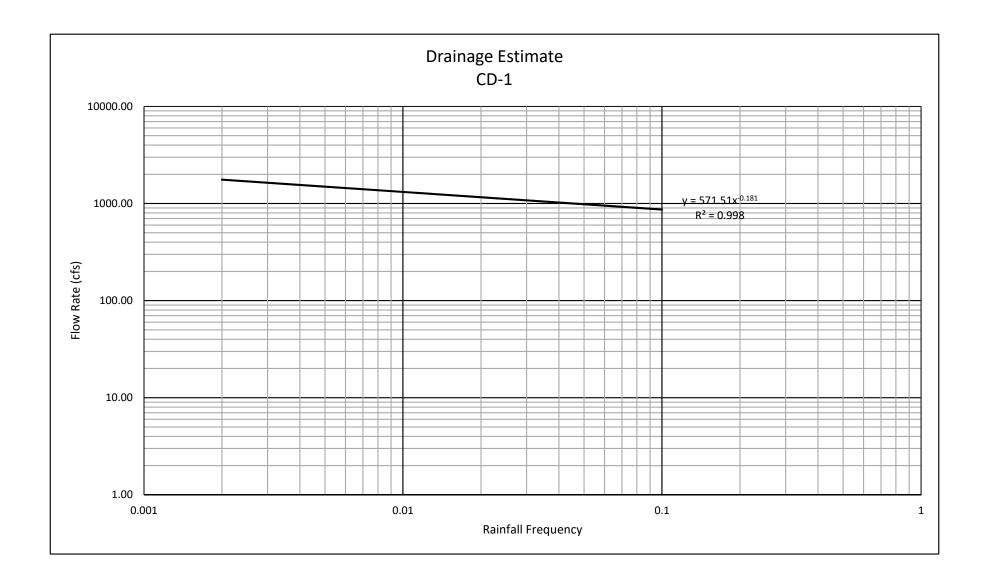
CD-1 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-1.

3-11'x5' CBC

873 ft ³ /s
1013 ft ³ /s
1160 ft ³ /s
1322 ft ³ /s
1760 ft ³ /s
485 ft
0.50 ft
0.012
13.66 ft
163.95 in
146.60 ft ²

Proposed Size =



CD-1 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 873 cfs
Design Flow: 1160 cfs
Maximum Flow: 1322 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-1

Headwater Elevation (ft)	Total Discharge (cfs)	CD-1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.20	873.00	873.00	0.00	1
51.31	917.90	917.90	0.00	1
51.79	962.80	962.80	0.00	1
51.87	1007.70	1007.70	0.00	1
51.72	1052.60	1052.60	0.00	1
51.79	1097.50	1097.50	0.00	1
51.92	1142.40	1142.40	0.00	1
51.97	1160.00	1160.00	0.00	1
52.18	1232.20	1232.20	0.00	1
52.31	1277.10	1277.10	0.00	1
52.45	1322.00	1322.00	0.00	1
88.87	4902.10	4902.10	0.00	Overtopping

Rating Curve Plot for Crossing: CD-1

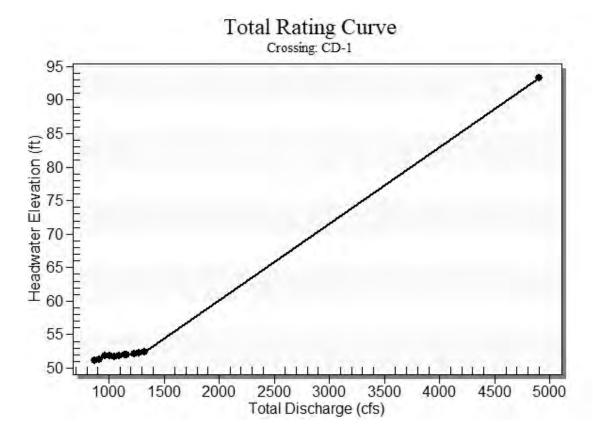


Table 2 - Culvert Summary Table: CD-1

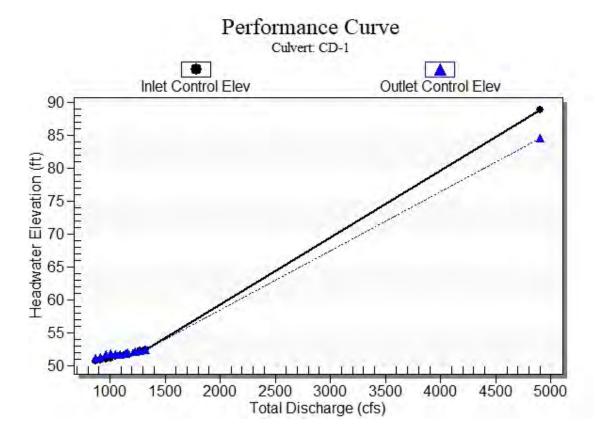
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
873.00	873.00	51.20	4.724	5.199	7-M1t	3.751	2.791	4.540	4.040	5.827	0.000
917.90	917.90	51.31	4.890	5.312	7-M1t	3.889	2.886	4.540	4.040	6.127	0.000
962.80	962.80	51.79	5.057	5.793	7-M2t	5.000	2.979	4.540	4.040	6.426	0.000
1007.70	1007.70	51.87	5.224	5.869	7-M2t	5.000	3.071	4.540	4.040	6.726	0.000
1052.60	1052.60	51.72	5.392	5.722	3-M2t	5.000	3.161	4.540	4.040	7.026	0.000
1097.50	1097.50	51.79	5.562	5.793	3-M2t	5.000	3.251	4.540	4.040	7.325	0.000
1142.40	1142.40	51.92	5.734	5.919	3-M2t	5.000	3.339	4.540	4.040	7.625	0.000
1160.00	1160.00	51.97	5.802	5.970	3-M2t	5.000	3.373	4.540	4.040	7.743	0.000
1232.20	1232.20	52.18	6.085	6.177	3-M2t	5.000	3.512	4.540	4.040	8.225	0.000
1277.10	1277.10	52.31	6.266	6.308	3-M2t	5.000	3.596	4.540	4.040	8.524	0.000
1322.00	1322.00	52.45	6.449	6.440	3-M2t	5.000	3.680	4.540	4.040	8.824	0.000

Straight Culvert

Inlet Elevation (invert): 46.00 ft, Outlet Elevation (invert): 45.50 ft

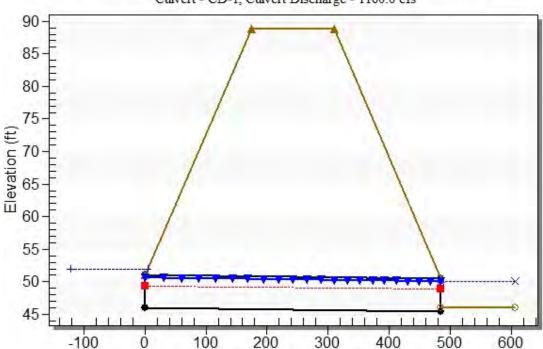
Culvert Length: 485.00 ft, Culvert Slope: 0.0010

Culvert Performance Curve Plot: CD-1



Water Surface Profile Plot for Culvert: CD-1

Crossing - CD-1, Design Discharge - 1160.0 cfs Culvert - CD-1, Culvert Discharge - 1160.0 cfs



Station (ft)

Site Data - CD-1

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 46.00 ft
Outlet Station: 485.00 ft
Outlet Elevation: 45.50 ft
Number of Barrels: 3

Culvert Data Summary - CD-1

Barrel Shape: Concrete Box

Barrel Span: 11.00 ft Barrel Rise: 5.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-1)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
873.00	50.04	4.04
917.90	50.04	4.04
962.80	50.04	4.04
1007.70	50.04	4.04
1052.60	50.04	4.04
1097.50	50.04	4.04
1142.40	50.04	4.04
1160.00	50.04	4.04
1232.20	50.04	4.04
1277.10	50.04	4.04
1322.00	50.04	4.04

Tailwater Channel Data - CD-1

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 50.04 ft

Roadway Data for Crossing: CD-1

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 88.87 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 2

CD-2 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-2.

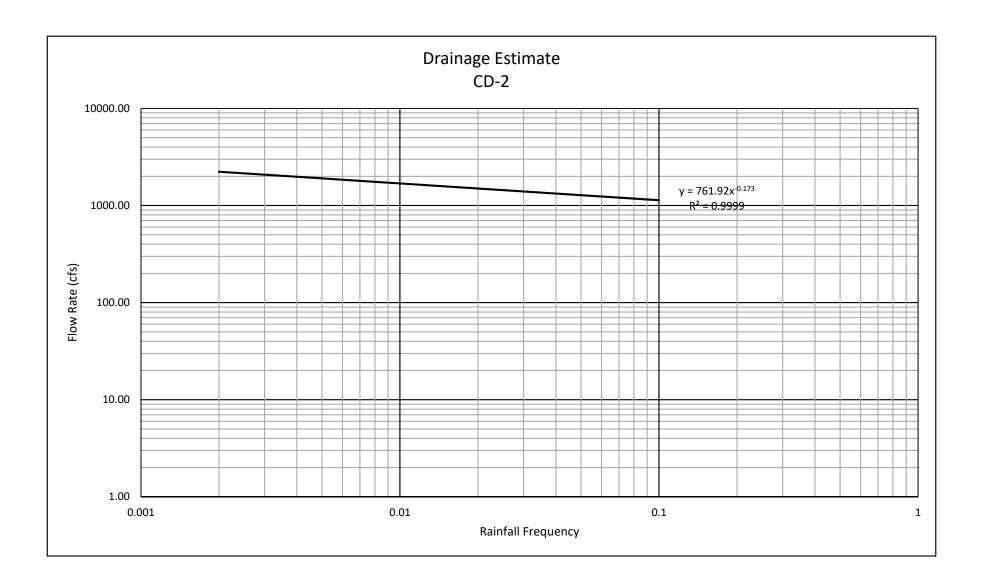
147.56 ft²

4-10'x5' CBC

Flow Rate 10 =	1136 ft ³ /s
Flow Rate 25 =	$1325 \text{ ft}^3/\text{s}$
Flow Rate 50 =	$1499 \text{ ft}^3/\text{s}$
Flow Rate 100 =	$1690 \text{ ft}^3/\text{s}$
Flow Rate 500 =	$2233 \text{ ft}^3/\text{s}$
Pipe Length =	302 ft
Change in FL Elevation from Upstream to Downstream =	0.50 ft
•	0.012
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	13.71 ft
D =	164.48 in

A =

Proposed Size =



CD-2 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 1136 cfs Design Flow: 1499 cfs Maximum Flow: 1690 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-2

Headwater Elevation (ft)	Total Discharge (cfs)	CD-2 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.06	1136.00	1136.00	0.00	1
51.16	1191.40	1191.40	0.00	1
51.27	1246.80	1246.80	0.00	1
51.40	1302.20	1302.20	0.00	1
51.57	1357.60	1357.60	0.00	1
51.70	1413.00	1413.00	0.00	1
51.83	1468.40	1468.40	0.00	1
51.91	1499.00	1499.00	0.00	1
52.11	1579.20	1579.20	0.00	1
52.26	1634.60	1634.60	0.00	1
52.41	1690.00	1690.00	0.00	1
85.27	5709.63	5709.63	0.00	Overtopping

Rating Curve Plot for Crossing: CD-2

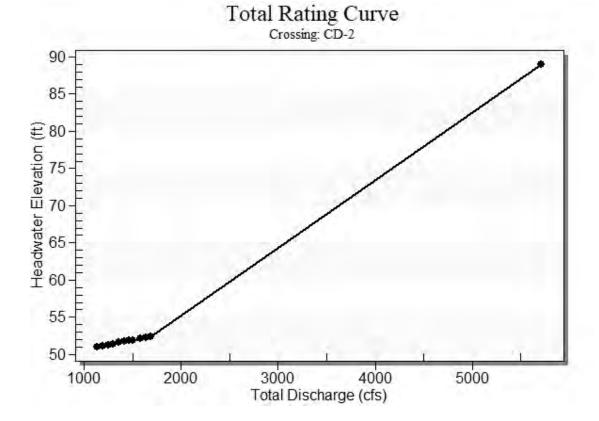


Table 2 - Culvert Summary Table: CD-2

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
1136.00	1136.00	51.06	4.960	5.557	3-M1f	3.393	2.926	5.000	4.540	5.680	0.000
1191.40	1191.40	51.16	5.130	5.659	3-M1f	3.511	3.020	5.000	4.540	5.957	0.000
1246.80	1246.80	51.27	5.301	5.770	3-M1f	3.629	3.113	5.000	4.540	6.234	0.000
1302.20	1302.20	51.40	5.473	5.895	3-M1f	3.745	3.205	5.000	4.540	6.511	0.000
1357.60	1357.60	51.57	5.647	6.071	3-M1f	3.860	3.295	5.000	4.540	6.788	0.000
1413.00	1413.00	51.70	5.823	6.197	4-FFf	3.974	3.384	5.000	4.540	7.065	0.000
1468.40	1468.40	51.83	6.002	6.330	4-FFf	5.000	3.472	5.000	4.540	7.342	0.000
1499.00	1499.00	51.91	6.102	6.405	4-FFf	5.000	3.520	5.000	4.540	7.495	0.000
1579.20	1579.20	52.11	6.369	6.610	4-FFf	5.000	3.644	5.000	4.540	7.896	0.000
1634.60	1634.60	52.26	6.558	6.758	4-FFf	5.000	3.729	5.000	4.540	8.173	0.000
1690.00	1690.00	52.41	6.751	6.911	4-FFf	5.000	3.813	5.000	4.540	8.450	0.000

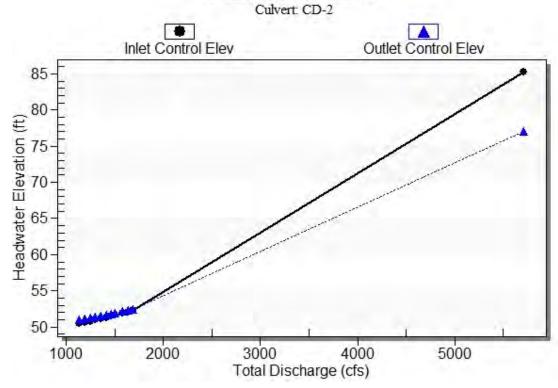
Straight Culvert

Inlet Elevation (invert): 45.50 ft, Outlet Elevation (invert): 45.00 ft

Culvert Length: 302.00 ft, Culvert Slope: 0.0017

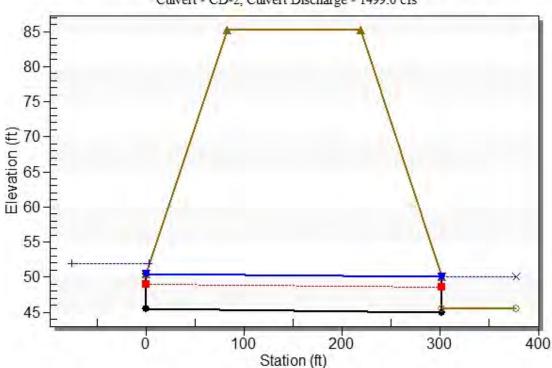
Culvert Performance Curve Plot: CD-2

Performance Curve



Water Surface Profile Plot for Culvert: CD-2

Crossing - CD-2, Design Discharge - 1499.0 cfs Culvert - CD-2, Culvert Discharge - 1499.0 cfs



Site Data - CD-2

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 45.50 ft
Outlet Station: 302.00 ft
Outlet Elevation: 45.00 ft
Number of Barrels: 4

Culvert Data Summary - CD-2

Barrel Shape: Concrete Box

Barrel Span: 10.00 ft Barrel Rise: 5.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-2)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
1136.00	50.04	4.54
1191.40	50.04	4.54
1246.80	50.04	4.54
1302.20	50.04	4.54
1357.60	50.04	4.54
1413.00	50.04	4.54
1468.40	50.04	4.54
1499.00	50.04	4.54
1579.20	50.04	4.54
1634.60	50.04	4.54
1690.00	50.04	4.54

Tailwater Channel Data - CD-2

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 50.04 ft

Roadway Data for Crossing: CD-2

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 85.27 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

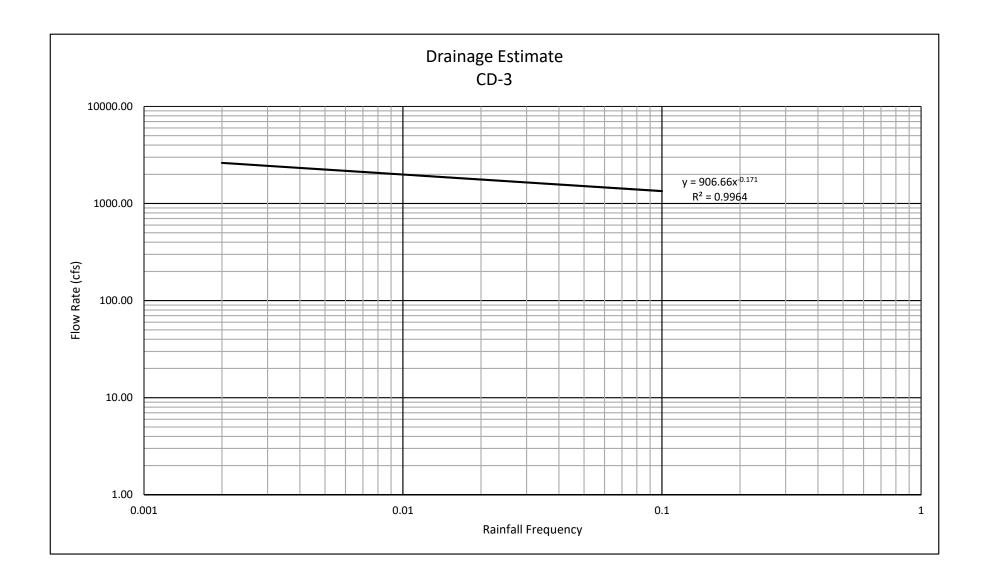
Cross Drain 3

CD-3 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-3.

Flow Rate 10 =	1354 ft ³ /s
Flow Rate 25 =	1549 ft ³ /s
Flow Rate 50 =	1770 ft ³ /s
Flow Rate 100 =	$2000 \text{ ft}^3/\text{s}$
Flow Rate 500 =	2624 ft ³ /s
Pipe Length =	400 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= $(2.159 \text{ Qn/S}^{0.5})^{3/8}$	

D = 15.39 ft D = 184.69 in $A = 186.04 \text{ ft}^2$ Proposed Size = 3-11'x7' CBC



CD-3 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 1354 cfs Design Flow: 1770 cfs Maximum Flow: 2000 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-3

Headwater Elevation (ft)	Total Discharge (cfs)	CD-3 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.24	1354.00	1354.00	0.00	1
51.36	1418.60	1418.60	0.00	1
51.47	1483.20	1483.20	0.00	1
51.60	1547.80	1547.80	0.00	1
51.72	1612.40	1612.40	0.00	1
51.85	1677.00	1677.00	0.00	1
51.99	1741.60	1741.60	0.00	1
52.05	1770.00	1770.00	0.00	1
52.26	1870.80	1870.80	0.00	1
52.41	1935.40	1935.40	0.00	1
52.51	2000.00	2000.00	0.00	1
80.88	6240.70	6240.70	0.00	Overtopping

Rating Curve Plot for Crossing: CD-3

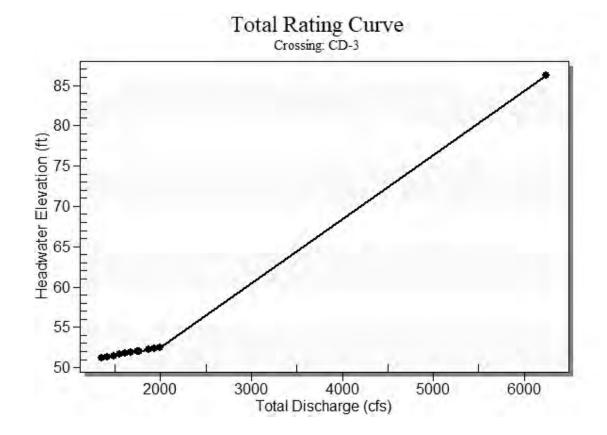


Table 2 - Culvert Summary Table: CD-3

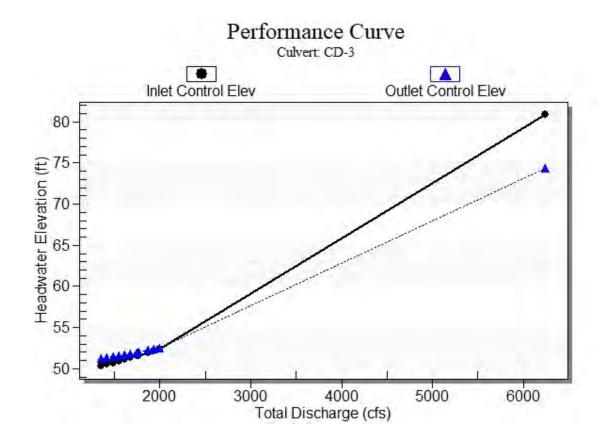
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
1354.00	1354.00	51.24	6.323	7.243	7-M1t	4.816	3.739	6.540	6.040	6.274	0.000
1418.60	1418.60	51.36	6.526	7.356	7-M1t	4.985	3.857	6.540	6.040	6.573	0.000
1483.20	1483.20	51.47	6.729	7.474	7-M1t	5.153	3.973	6.540	6.040	6.872	0.000
1547.80	1547.80	51.60	6.931	7.596	7-M1t	5.320	4.088	6.540	6.040	7.172	0.000
1612.40	1612.40	51.72	7.134	7.723	7-M1t	5.486	4.201	6.540	6.040	7.471	0.000
1677.00	1677.00	51.85	7.337	7.853	7-M1t	5.651	4.312	6.540	6.040	7.770	0.000
1741.60	1741.60	51.99	7.542	7.986	7-M1t	5.815	4.423	6.540	6.040	8.070	0.000
1770.00	1770.00	52.05	7.633	8.046	7-M1t	5.886	4.470	6.540	6.040	8.201	0.000
1870.80	1870.80	52.26	7.957	8.264	7-M1t	6.140	4.639	6.540	6.040	8.668	0.000
1935.40	1935.40	52.41	8.168	8.407	7-M1t	6.301	4.745	6.540	6.040	8.968	0.000
2000.00	2000.00	52.51	8.381	8.512	7-M1t	6.462	4.850	6.540	6.040	9.267	0.000

Straight Culvert

Inlet Elevation (invert): 44.00 ft, Outlet Elevation (invert): 43.50 ft

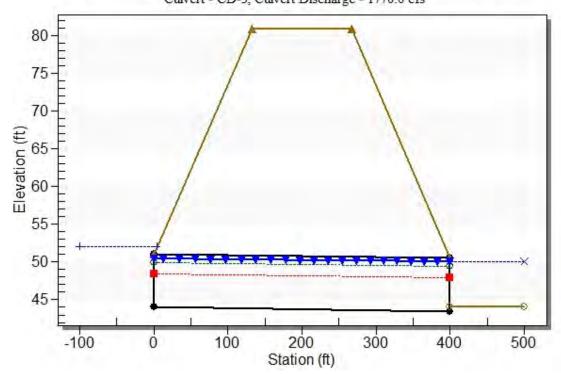
Culvert Length: 400.00 ft, Culvert Slope: 0.0013

Culvert Performance Curve Plot: CD-3



Water Surface Profile Plot for Culvert: CD-3

Crossing - CD-3, Design Discharge - 1770.0 cfs Culvert - CD-3, Culvert Discharge - 1770.0 cfs



Site Data - CD-3

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 44.00 ft
Outlet Station: 400.00 ft
Outlet Elevation: 43.50 ft
Number of Barrels: 3

Culvert Data Summary - CD-3

Barrel Shape: Concrete Box

Barrel Span: 11.00 ft Barrel Rise: 7.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
1354.00	50.04	6.04
1418.60	50.04	6.04
1483.20	50.04	6.04
1547.80	50.04	6.04
1612.40	50.04	6.04
1677.00	50.04	6.04
1741.60	50.04	6.04
1770.00	50.04	6.04
1870.80	50.04	6.04
1935.40	50.04	6.04
2000.00	50.04	6.04

Tailwater Channel Data - CD-3

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 50.04 ft

Roadway Data for Crossing: CD-3

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 80.88 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 3A

CD-3A Preliminary Culvert Sizing

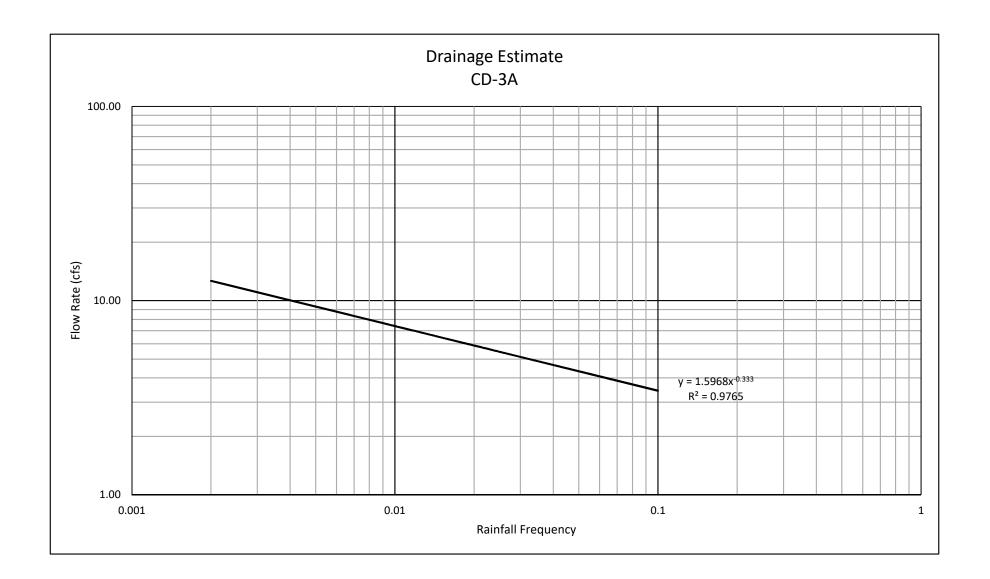
The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-3A.

Flow Rate 10 =	$3.59 \text{ ft}^3/\text{s}$
Flow Rate 25 =	$4.38 \text{ ft}^3/\text{s}$
Flow Rate 50 =	$5.76 \text{ft}^3/\text{s}$
Flow Rate 100 =	$7.69 \text{ ft}^3/\text{s}$
Flow Rate 500 =	$12.65 \text{ ft}^3/\text{s}$
Pipe Length =	303 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	1.82 ft
D =	21.78 in
A =	2.59 ft ²
Proposed Size =	1-30" RCP

CD-3A Rational Method							
Runoff Coefficient Calculations							
Land Use	Slope	Land Cover (%)	Runoff	Area (acre) - A	Product		
			Coefficient				
Residential	0-2%		0.45	0.00	0.00		
Commercial	0-2%	5	0.95	0.13	0.13		
Lawn flat 2%	0-2%	20	0.20	0.47	0.09		
Woods/Wetlands	0-2%	75	0.15	1.76	0.26		
			Total	2.35	0.49		
			Compos	0.21			
	Contributing	g Flow Rate for Va	rious Storm Fr	equency			
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q		
	Factor	tor Frequency		Coefficient - C	(cfs)		
10-Year	1	0.1	7.4	0.21	3.59		
25-Year	1.1	0.04	8.2	0.23	4.38		
50-Year	1.2	0.02	9	0.27	5.76		
100-Year	1.25	0.01	9.6	0.34	7.69		
500-Year	-	0.002			12.65		
Rational Formula							
Q = CIA							

^{**}Time of Concentration was assumed to be 10 minutes for an area this small.

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-3A HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 3.59 cfs Design Flow: 5.76 cfs Maximum Flow: 7.69 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-3A

Headwater Elevation (ft)	Total Discharge (cfs)	CD-3A Discharge (cfs)	Roadway Discharge (cfs)	Iterations
57.83	3.59	3.59	0.00	1
57.84	4.00	4.00	0.00	1
57.85	4.41	4.41	0.00	1
57.86	4.82	4.82	0.00	1
57.87	5.23	5.23	0.00	1
57.88	5.64	5.64	0.00	1
57.88	5.76	5.76	0.00	1
57.90	6.46	6.46	0.00	1
57.92	6.87	6.87	0.00	1
57.93	7.28	7.28	0.00	1
57.95	7.69	7.69	0.00	1
75.41	84.31	84.31	0.00	Overtopping

Rating Curve Plot for Crossing: CD-3A

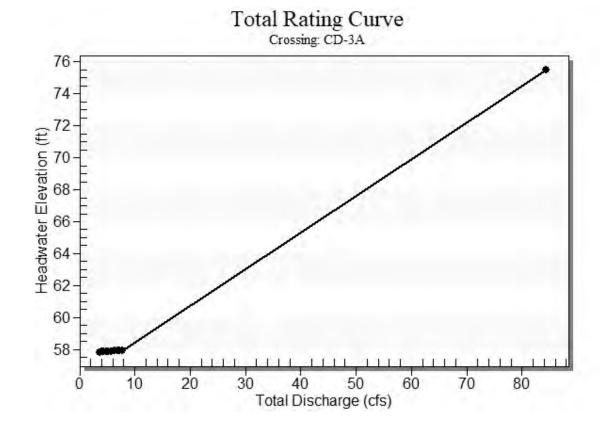


Table 2 - Culvert Summary Table: CD-3A

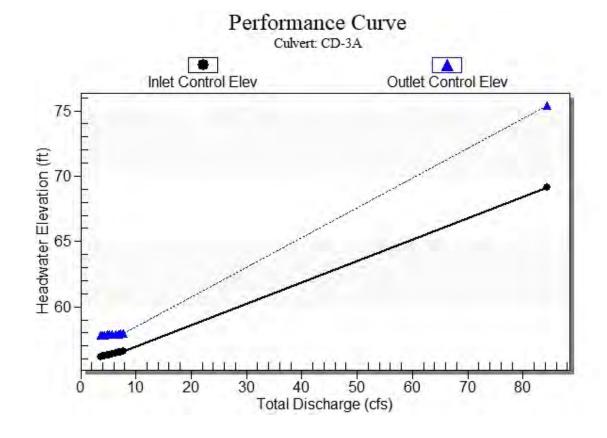
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
3.59	3.59	57.83	0.852	2.532	4-FFf	0.733	0.619	2.500	2.500	0.731	0.000
4.00	4.00	57.84	0.900	2.540	4-FFf	0.776	0.655	2.500	2.500	0.815	0.000
4.41	4.41	57.85	0.949	2.548	4-FFf	0.817	0.686	2.500	2.500	0.898	0.000
4.82	4.82	57.86	0.994	2.558	4-FFf	0.856	0.719	2.500	2.500	0.982	0.000
5.23	5.23	57.87	1.038	2.568	4-FFf	0.894	0.751	2.500	2.500	1.065	0.000
5.64	5.64	57.88	1.080	2.579	4-FFf	0.931	0.782	2.500	2.500	1.149	0.000
5.76	5.76	57.88	1.092	2.582	4-FFf	0.942	0.790	2.500	2.500	1.173	0.000
6.46	6.46	57.90	1.161	2.603	4-FFf	1.003	0.839	2.500	2.500	1.316	0.000
6.87	6.87	57.92	1.201	2.617	4-FFf	1.038	0.864	2.500	2.500	1.400	0.000
7.28	7.28	57.93	1.238	2.631	4-FFf	1.072	0.891	2.500	2.500	1.483	0.000
7.69	7.69	57.95	1.280	2.647	4-FFf	1.106	0.918	2.500	2.500	1.567	0.000

Straight Culvert

Inlet Elevation (invert): 55.30 ft, Outlet Elevation (invert): 54.80 ft

Culvert Length: 300.00 ft, Culvert Slope: 0.0017

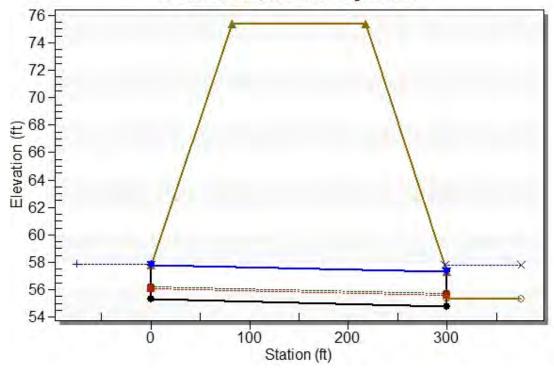
Culvert Performance Curve Plot: CD-3A



Water Surface Profile Plot for Culvert: CD-3A

Crossing - CD-3A, Design Discharge - 5.8 cfs

Culvert - CD-3A, Culvert Discharge - 5.8 cfs



Site Data - CD-3A

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 55.30 ft
Outlet Station: 300.00 ft
Outlet Elevation: 54.80 ft
Number of Barrels: 1

Culvert Data Summary - CD-3A

Barrel Shape: Circular
Barrel Diameter: 2.50 ft
Barrel Material: Concrete
Embedment: 0.00 in

Barrel Manning's n: 0.0120 Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3A)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
3.59	57.80	2.50
4.00	57.80	2.50
4.41	57.80	2.50
4.82	57.80	2.50
5.23	57.80	2.50
5.64	57.80	2.50
5.76	57.80	2.50
6.46	57.80	2.50
6.87	57.80	2.50
7.28	57.80	2.50
7.69	57.80	2.50

Tailwater Channel Data - CD-3A

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 57.80 ft

Roadway Data for Crossing: CD-3A

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 75.41 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 4

CD-4 Preliminary Culvert Sizing

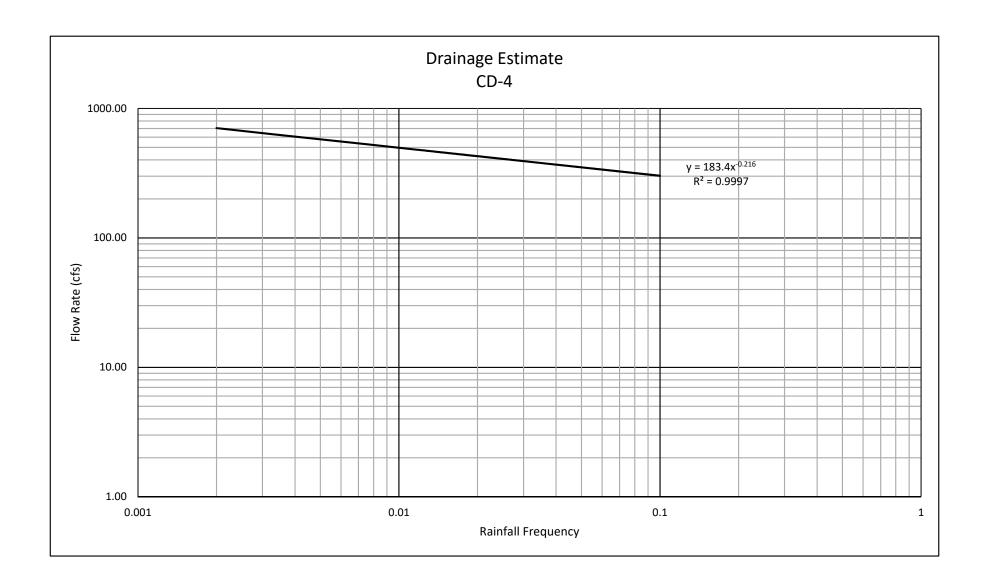
The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-4.

Flow Rate 10 =	301 ft ³ /s
Flow Rate 25 =	370 ft ³ /s
Flow Rate 50 =	427 ft ³ /s
Flow Rate 100 =	496 ft ³ /s
Flow Rate 500 =	$702 \text{ ft}^3/\text{s}$
Pipe Length =	456 ft
Change in FL Elevation from	

Upstream to Downstream = 0.50 ft Manning's "n" value = 0.012

 $D = (2.159 \text{ Qn/S}^{0.5})^{3/8}$

D =	9.35 ft
D =	112.21 in
A =	68.67 ft ²
Proposed Size =	2-8'x4' CBC



CD-4 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 301 cfs Design Flow: 427 cfs Maximum Flow: 496 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-4

Headwater Elevation (ft)	Total Discharge (cfs)	CD-4 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.27	301.00	301.00	0.00	1
51.38	320.50	320.50	0.00	1
51.49	340.00	340.00	0.00	1
51.61	359.50	359.50	0.00	1
51.72	379.00	379.00	0.00	1
51.84	398.50	398.50	0.00	1
51.97	418.00	418.00	0.00	1
52.03	427.00	427.00	0.00	1
52.46	457.00	457.00	0.00	1
52.72	476.50	476.50	0.00	1
52.95	496.00	496.00	0.00	1
82.31	1727.16	1727.16	0.00	Overtopping

Rating Curve Plot for Crossing: CD-4

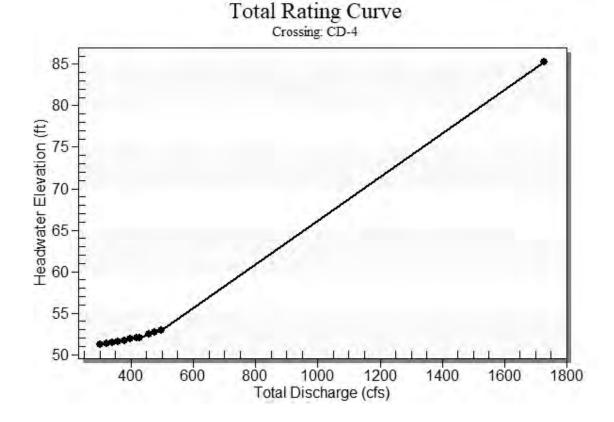


Table 2 - Culvert Summary Table: CD-4

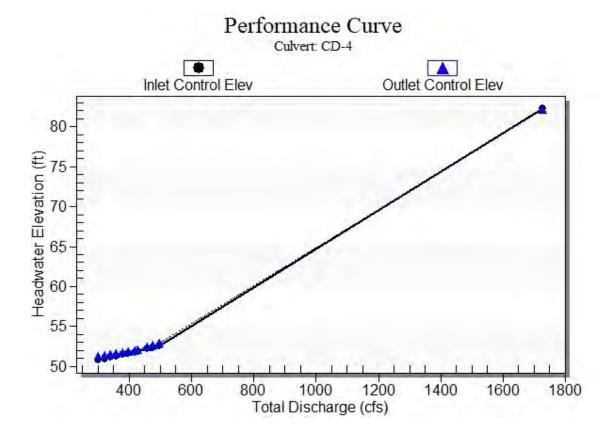
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
301.00	301.00	51.27	3.763	4.273	7-M1t	3.061	2.223	3.900	3.400	4.824	0.000
320.50	320.50	51.38	3.930	4.380	7-M1t	3.204	2.318	3.900	3.400	5.136	0.000
340.00	340.00	51.49	4.096	4.491	7-M1t	3.346	2.412	3.900	3.400	5.449	0.000
359.50	359.50	51.61	4.265	4.606	7-M1t	3.487	2.503	3.900	3.400	5.761	0.000
379.00	379.00	51.72	4.434	4.724	7-M1t	3.626	2.593	3.900	3.400	6.074	0.000
398.50	398.50	51.84	4.606	4.844	7-M1t	3.764	2.681	3.900	3.400	6.386	0.000
418.00	418.00	51.97	4.782	4.968	3-M2t	4.000	2.767	3.900	3.400	6.699	0.000
427.00	427.00	52.03	4.864	5.025	3-M2t	4.000	2.807	3.900	3.400	6.843	0.000
457.00	457.00	52.46	5.144	5.464	7-M2t	4.000	2.937	3.900	3.400	7.324	0.000
476.50	476.50	52.72	5.331	5.717	7-M2t	4.000	3.020	3.900	3.400	7.636	0.000
496.00	496.00	52.95	5.524	5.954	7-M2t	4.000	3.102	3.900	3.400	7.949	0.000

Straight Culvert

Inlet Elevation (invert): 47.00 ft, Outlet Elevation (invert): 46.50 ft

Culvert Length: 456.00 ft, Culvert Slope: 0.0011

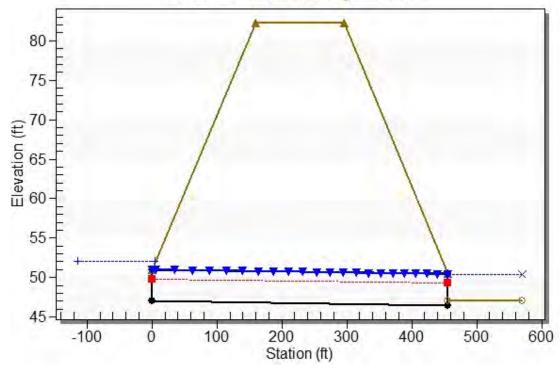
Culvert Performance Curve Plot: CD-4



Water Surface Profile Plot for Culvert: CD-4

Crossing - CD-4, Design Discharge - 427.0 cfs

Culvert - CD-4, Culvert Discharge - 427.0 cfs



Site Data - CD-4

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft Inlet Elevation: 47.00 ft Outlet Station: 456.00 ft Outlet Elevation: 46.50 ft Number of Barrels: 2

Culvert Data Summary - CD-4

Barrel Shape: Concrete Box

Barrel Span: 8.00 ft Barrel Rise: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-4)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
301.00	50.40	3.40
320.50	50.40	3.40
340.00	50.40	3.40
359.50	50.40	3.40
379.00	50.40	3.40
398.50	50.40	3.40
418.00	50.40	3.40
427.00	50.40	3.40
457.00	50.40	3.40
476.50	50.40	3.40
496.00	50.40	3.40

Tailwater Channel Data - CD-4

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 50.40 ft

Roadway Data for Crossing: CD-4

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 82.31 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 5

CD-5 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-5.

Flow Rate 10 =	134 ft ³ /s
Flow Rate 25 =	171 ft ³ /s
Flow Rate 50 =	$226 \text{ ft}^3/\text{s}$
Flow Rate 100 =	312 ft ³ /s
Flow Rate 500 =	541 ft ³ /s
Pipe Length =	374 ft

Change in FL Elevation from

Upstream to Downstream = 0.50 ft

Manning's "n" value = 0.012

D= $(2.159 \text{ Qn/S}^{0.5})^{3/8}$

D =	7.58 ft
D =	90.92 in
A =	45.08 ft ²
Proposed Size =	2-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: STATE ROAD NO. 408 EASTERN EXTENSION

LOCATION: ORANGE COUNTY

BASIN NAME: CD-5

CC	NDITIONS
Pre-Development	Х
Post-Development	
Rainfall Zone:	7

COMPUTE	VARIABLE
T⊡dc	X
Т	⊡dt
Frequency:	

Water Reso	urces Group	Date
Computed By	KS	09/05/17
Checked By	CR	

TOTAL TIME (hr)

TOTAL TIME (min)

1.39

83.2

NUMBER:

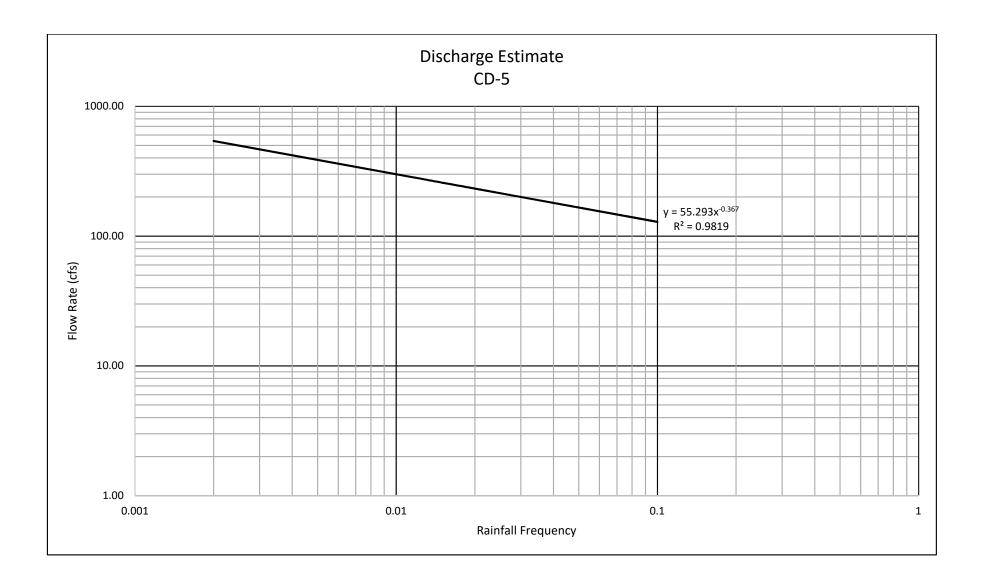
FILE:

SHEET FLOW (Applicable To T⊡dc□Only)				
(Applicable to Facebrilly)	Segment ID			
1) SURFACE DESCRIPTION (table 5-4)	3			
2) MANNNING'S ROUGHNESS COEFF., [n] (table 5-4)		0.08		
3) FLOW LENGTH, [L] (TOTAL L <= 300 ft)	ft	300		
4) HIGH ELEVATION, [A]	ft	70.0		
5) LOW ELEVATION, [B]	ft	68.0		
6) TWO YEAR 24-hr RAINFALL , [P]	in	4.92		
7) LAND SLOPE, [s]	ft/ft	0.007		
8) COMPUTE Tdt: Tdt: (.007*(n*L)^0.8)/(P^0.5 * s^0.4)	hr	0.291 +		0.291
			min	= 17.4
SHALLOW CONCENTRATED FLOW				
	Segment ID			
9) SURFACE DESCRIPTION Enter 1 (Paved) or 2 (Unpaved)		1		
10) FLOW LENGTH, [L]	ft	4687		
11) HIGH ELEVATION, [C]		68.0		
12) LOW ELEVATION, [D]		52.0		
13) WATERCOURSE SLOPE, [s]	ft/ft	0.0034		
14) AVERAGE VELOCITY, [V] **	ft/sec	1.19		
15) COMPUTE Tdt Tdt = L/3600*V	hr	1.10 +		= 1.10
			min	= 65.8
CHANNEL FLOW				
	Segment ID			
16) CROSS SECTIONAL FLOW AREA, [a]	ft^2			
17) WETTED PERIMETER, [Pīdwi]	ft			
18) HYDRAULIC RADIUS, [r] = a / P dw □	ft			
19) FLOW LENGTH, [L]	ft			
20) HIGH ELEVATION, [D]	ft			
21) LOW ELEVATION, [E]	ft			
22) CHANNEL SLOPE, [s]	ft/ft			
23) MANNNING'S ROUGHNESS COEFF., [n]				
24) COMPUTE V: $V = (1.49*r^2/3 * s^1/2) / n$	ft/sec			
25) COMPUTE Tdt: Tdt: = L/3600*V	hr			=
			min	= 0.0

^{**} Reference: FDOT Drainage Manual Chapter 5.5, TR-55 Chapter 3 & APP-F.

CD-5 Rational Method								
Runoff Coefficient Calculations								
Land Use	Slope	Land Cover (%)	Runoff Area (acre) - A Prod					
			Coefficient					
Residential	0-2%	40	0.45	43.61	19.63			
Commercial	0-2%	25	0.95	27.26	25.89			
Lawn flat 2%	0-2%	25	0.20	27.26	5.45			
Woods/Wetlands	0-2%	10	0.15	10.90	1.64			
			Total	109.03	52.61			
			Compos	ite Coefficient	0.48			
	Contributing	g Flow Rate for Va	rious Storm Fr	equency				
Storm Frequency	Storm Frequency	Rainfall	Intensity - I Adjusted Runoff		Runoff Rate - Q			
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)			
10-Year	1	0.1	2.55	0.48	134.15			
25-Year	1.1	0.04	2.95	0.53	170.71			
50-Year	1.2	0.02	3.25	0.64	225.68			
100-Year	1.25	0.01	3.60	0.80	312.49			
500-Year	-	0.002	-	-	540.99			
	Rational Formula							
		Q = CIA						

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-5 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 134 cfs Design Flow: 226 cfs Maximum Flow: 312 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-5

Headwater Elevation (ft)	Total Discharge (cfs)	CD-5 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
50.50	134.00	134.00	0.00	1
50.68	151.80	151.80	0.00	1
50.88	169.60	169.60	0.00	1
51.08	187.40	187.40	0.00	1
51.27	205.20	205.20	0.00	1
51.48	223.00	223.00	0.00	1
51.51	226.00	226.00	0.00	1
51.87	258.60	258.60	0.00	1
52.07	276.40	276.40	0.00	1
52.26	294.20	294.20	0.00	1
52.46	312.00	312.00	0.00	1
84.25	1603.28	1603.28	0.00	Overtopping

Rating Curve Plot for Crossing: CD-5

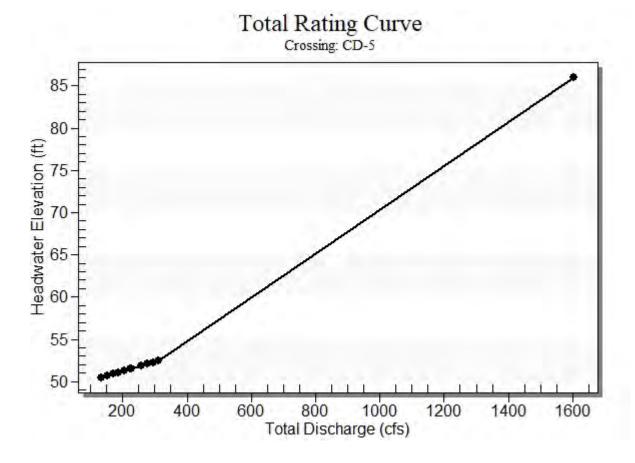


Table 2 - Culvert Summary Table: CD-5

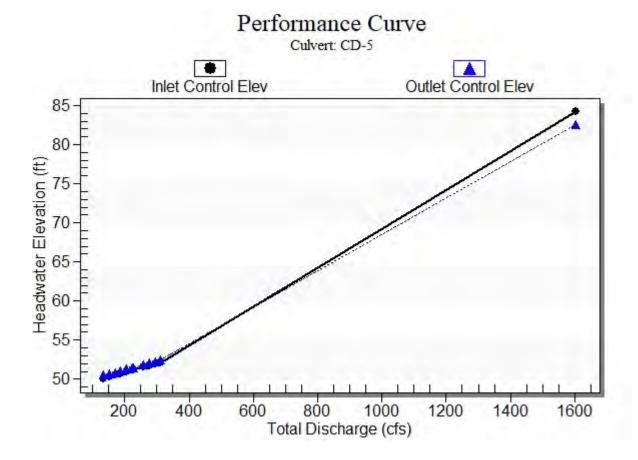
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
134.00	134.00	50.50	3.027	3.495	3-M1t	2.566	2.181	3.230	2.730	4.318	0.000
151.80	151.80	50.68	3.278	3.682	3-M1t	2.755	2.325	3.230	2.730	4.892	0.000
169.60	169.60	50.88	3.516	3.876	3-M1t	2.938	2.466	3.230	2.730	5.465	0.000
187.40	187.40	51.08	3.741	4.075	3-M1t	3.119	2.598	3.230	2.730	6.039	0.000
205.20	205.20	51.27	3.957	4.266	3-M2t	3.299	2.727	3.230	2.730	6.613	0.000
223.00	223.00	51.48	4.164	4.475	3-M2t	3.479	2.849	3.230	2.730	7.186	0.000
226.00	226.00	51.51	4.198	4.509	3-M2t	3.509	2.869	3.230	2.730	7.283	0.000
258.60	258.60	51.87	4.558	4.871	3-M2t	3.845	3.076	3.230	2.730	8.333	0.000
276.40	276.40	52.07	4.747	5.067	3-M2t	4.037	3.182	3.230	2.730	8.907	0.000
294.20	294.20	52.26	4.934	5.262	2-M2c	4.238	3.289	3.289	2.730	9.269	0.000
312.00	312.00	52.46	5.117	5.455	2-M2c	4.453	3.390	3.390	2.730	9.472	0.000

Straight Culvert

Inlet Elevation (invert): 47.00 ft, Outlet Elevation (invert): 46.50 ft

Culvert Length: 374.00 ft, Culvert Slope: 0.0013

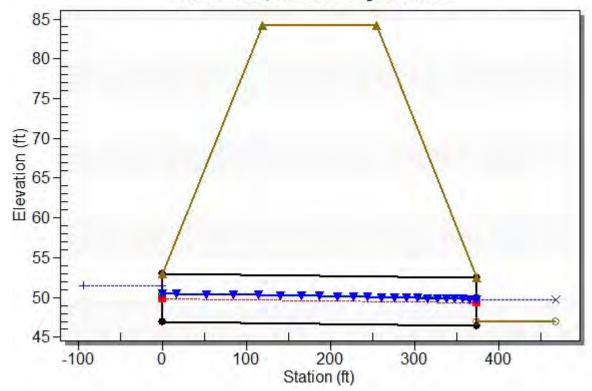
Culvert Performance Curve Plot: CD-5



Water Surface Profile Plot for Culvert: CD-5

Crossing - CD-5, Design Discharge - 226.0 cfs

Culvert - CD-5, Culvert Discharge - 226.0 cfs



Site Data - CD-5

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft Inlet Elevation: 47.00 ft Outlet Station: 374.00 ft Outlet Elevation: 46.50 ft Number of Barrels: 2

Culvert Data Summary - CD-5

Barrel Shape: Circular Barrel Diameter: 6.00 ft Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-5)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
134.00	49.73	2.73
151.80	49.73	2.73
169.60	49.73	2.73
187.40	49.73	2.73
205.20	49.73	2.73
223.00	49.73	2.73
226.00	49.73	2.73
258.60	49.73	2.73
276.40	49.73	2.73
294.20	49.73	2.73
312.00	49.73	2.73

Tailwater Channel Data - CD-5

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 49.73 ft

Roadway Data for Crossing: CD-5

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft
Crest Elevation: 84.25 ft
Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 6

CD-6 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-6.

112 ft ³ /s
141 ft ³ /s
190 ft ³ /s
259 ft ³ /s
449 ft ³ /s
427 ft

Change in FL Elevation from

Upstream to Downstream = 0.50 ft

Manning's "n" value = 0.012

 $D = (2.159 \text{ Qn/S}^{0.5})^{3/8}$

D =	7.24 ft
D =	86.92 in
A =	41.21 ft ²
Proposed Size =	2-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: STATE ROAD NO. 408 EASTERN EXTENSION

** Reference: FDOT Drainage Manual Chapter 5.5, TR-55 Chapter 3 & APP-F.

LOCATION: ORANGE COUNTY

BASIN NAME: CD-6

ONDITIONS
X
7

COMPUTE	D VARIABLE
T⊡dc	X
Т	`⊡dt
Frequency:	

Water Reso	urces Group	Date
Computed By	KS	09/05/17
Checked By	CR	

NUMBER:

FILE:

SHEET FLOW (Applicable To Tcdc:Only)				
(TP,)	Segment ID			
1) SURFACE DESCRIPTION (table 5-4)	oogmont ib			
2) MANNNING'S ROUGHNESS COEFF., [n] (table 5-4)		0.14		
3) FLOW LENGTH, [L] (TOTAL L <= 300 ft)	ft	300		
4) HIGH ELEVATION, [A]	ft	66.0		
5) LOW ELEVATION, [B]	ft	65.0		
6) TWO YEAR 24-hr RAINFALL, [P]	in	4.92		
7) LAND SLOPE, [s]	ft/ft	0.003		
		0.626 +		0.000
8) COMPUTE Tata $Tata = (.007*(n*L)^0.8)/(P^0.5*s^0.4)$	hr	0.020 +		= 37.6
OUVIL ON CONCENTRATED FLOW			min	= 37.6
SHALLOW CONCENTRATED FLOW				
	Segment ID			
9) SURFACE DESCRIPTION Enter 1 (Paved) or 2 (Unpaved)		1		
10) FLOW LENGTH, [L]	ft	3667		
11) HIGH ELEVATION, [C]		65.0		
12) LOW ELEVATION, [D]		51.0		
13) WATERCOURSE SLOPE, [s]	ft/ft	0.0038		
14) AVERAGE VELOCITY, [V] **	ft/sec	1.26		
15) COMPUTE Todt □ Todt □ = L / 3600*V	hr	0.81 +		= 0.81
			min	= 48.7
CHANNEL FLOW				
	Segment ID			
16) CROSS SECTIONAL FLOW AREA, [a]	ft^2			
17) WETTED PERIMETER, [P@w1]	ft			
18) HYDRAULIC RADIUS, [r] = a / P.dw□	ft			
19) FLOW LENGTH, [L]	ft			
20) HIGH ELEVATION, [D]	ft			
21) LOW ELEVATION, [E]	ft			
22) CHANNEL SLOPE, [s]	ft/ft			
23) MANNNING'S ROUGHNESS COEFF., [n]	1010			
24) COMPUTE V: V = (1.49*r^2/3 * s^1/2) / n	ft/sec			
25) COMPUTE Tidt = L / 3600*V	hr			=
20) CON OTE THE THE THE P. 1 3000 V	111		min	
			111111	- 0.0
		ΤΟ.	TAL TIME (hr	1.44
		10	IVE LIME (III	1.44

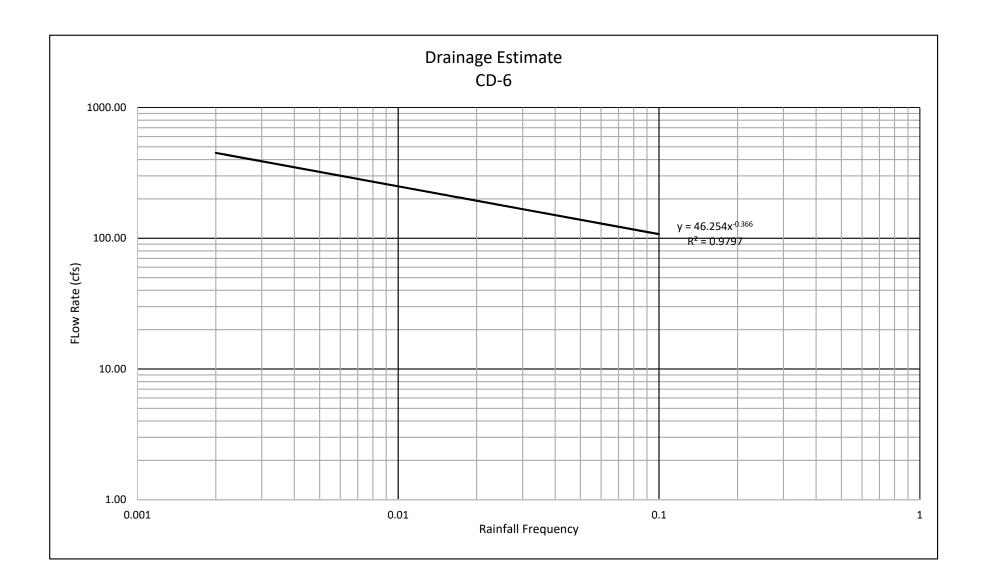
86.2

TOTAL TIME (min)

G-41

CD-6 Rational Method							
Runoff Coefficient Calculations							
Land Use	Slope	Land Cover (%)	Runoff Area (acre) - A Product				
			Coefficient				
Residential	0-2%	75	0.45	89.26	40.17		
Commercial	0-2%	0	0.95	0.00	0.00		
Lawn flat 2%	0-2%	5	0.20	5.95	1.19		
Woods/Wetlands	0-2%	20	0.15	23.80	3.57		
			Total	119.01	44.93		
			Compos	ite Coefficient	0.38		
	Contributin	g Flow Rate for Va	arious Storm F	requency			
Storm Frequency	Storm Frequency	Rainfall	Intensity - I Adjusted Runoff		Runoff Rate - Q		
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)		
10-Year	1	0.1	2.5	0.38	112.32		
25-Year	1.1	0.04	2.85	0.42	140.84		
50-Year	1.2	0.02	3.2	0.50	189.77		
100-Year	1.25	0.01	3.5	0.62	259.45		
500-Year	-	0.002	-	-	448.87		
Rational Formula							
	Q = CIA						

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-6 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 112 cfs Design Flow: 190 cfs Maximum Flow: 259 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-6

Headwater Elevation (ft)	Total Discharge (cfs)	CD-6 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.06	112.00	112.00	0.00	1
51.27	126.70	126.70	0.00	1
51.48	141.40	141.40	0.00	1
51.67	156.10	156.10	0.00	1
51.86	170.80	170.80	0.00	1
52.04	185.50	185.50	0.00	1
52.10	190.00	190.00	0.00	1
52.40	214.90	214.90	0.00	1
52.57	229.60	229.60	0.00	1
52.74	244.30	244.30	0.00	1
52.91	259.00	259.00	0.00	1
84.64	1588.91	1588.91	0.00	Overtopping

Rating Curve Plot for Crossing: CD-6

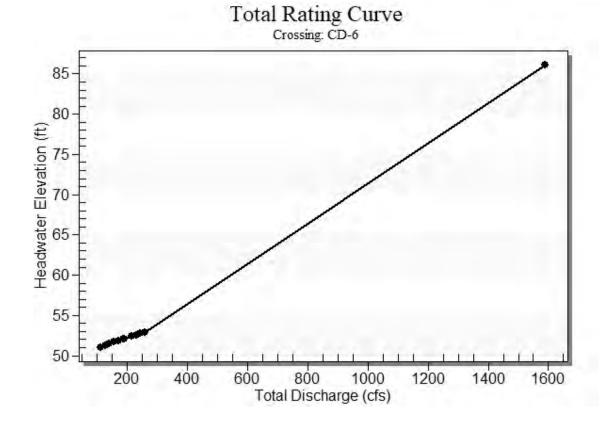


Table 2 - Culvert Summary Table: CD-6

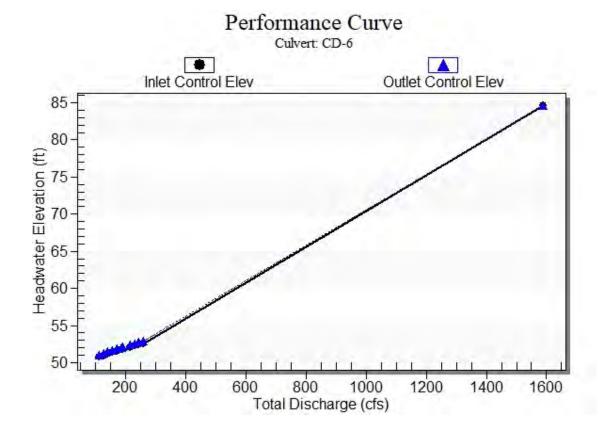
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
112.00	112.00	51.06	2.745	3.058	3-M2t	2.409	1.988	2.230	1.730	5.853	0.000
126.70	126.70	51.27	2.933	3.274	3-M2t	2.581	2.117	2.230	1.730	6.621	0.000
141.40	141.40	51.48	3.134	3.477	2-M2c	2.747	2.243	2.243	1.730	7.331	0.000
156.10	156.10	51.67	3.337	3.671	2-M2c	2.910	2.359	2.359	1.730	7.561	0.000
170.80	170.80	51.86	3.532	3.860	2-M2c	3.070	2.475	2.475	1.730	7.761	0.000
185.50	185.50	52.04	3.718	4.043	2-M2c	3.228	2.584	2.584	1.730	7.964	0.000
190.00	190.00	52.10	3.774	4.099	2-M2c	3.277	2.617	2.617	1.730	8.020	0.000
214.90	214.90	52.40	4.071	4.398	2-M2c	3.546	2.794	2.794	1.730	8.327	0.000
229.60	229.60	52.57	4.239	4.569	2-M2c	3.707	2.893	2.893	1.730	8.507	0.000
244.30	244.30	52.74	4.403	4.739	2-M2c	3.871	2.988	2.988	1.730	8.686	0.000
259.00	259.00	52.91	4.563	4.906	2-M2c	4.041	3.078	3.078	1.730	8.865	0.000

Straight Culvert

Inlet Elevation (invert): 48.00 ft, Outlet Elevation (invert): 47.50 ft

Culvert Length: 427.00 ft, Culvert Slope: 0.0012

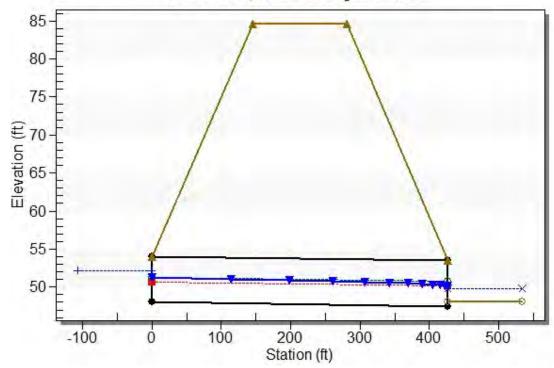
Culvert Performance Curve Plot: CD-6



Water Surface Profile Plot for Culvert: CD-6

Crossing - CD-6, Design Discharge - 190.0 cfs

Culvert - CD-6, Culvert Discharge - 190.0 cfs



Site Data - CD-6

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 48.00 ft
Outlet Station: 427.00 ft
Outlet Elevation: 47.50 ft
Number of Barrels: 2

Culvert Data Summary - CD-6

Barrel Shape: Circular
Barrel Diameter: 6.00 ft
Barrel Material: Concrete
Embedment: 0.00 in

Barrel Manning's n: 0.0120 Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-6)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
112.00	49.73	1.73
126.70	49.73	1.73
141.40	49.73	1.73
156.10	49.73	1.73
170.80	49.73	1.73
185.50	49.73	1.73
190.00	49.73	1.73
214.90	49.73	1.73
229.60	49.73	1.73
244.30	49.73	1.73
259.00	49.73	1.73

Tailwater Channel Data - CD-6

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 49.73 ft

Roadway Data for Crossing: CD-6

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 84.64 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 7

CD-7 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-7.

Flow Rate 10 = 98 ft 3 /s Flow Rate 25 = 125 ft 3 /s Flow Rate 50 = 165 ft 3 /s Flow Rate 100 = 231 ft 3 /s Flow Rate 500 = 401 ft 3 /s Pipe Length = 129 ft

Change in FL Elevation from

Upstream to Downstream = 0.50 ft

Manning's "n" value = 0.012

 $D = (2.159 \text{ Qn/S}^{0.5})^{3/8}$

D = 5.54 ft D = 66.437 in $A = 24.074 \text{ ft}^2$ Proposed Size = 2-48" RCP

TIME OF CONCENTRATION

PROJECT TITLE: STATE ROAD NO. 408 EASTERN EXTENSION

LOCATION: ORANGE COUNTY

BASIN NAME: CD-7

CC	NDITIONS
Pre-Development	Х
Post-Development	
Rainfall Zone:	7

COMPUTE	VARIABLE
T⊡dc	Х
Т	⊡dt
Frequency:	

Water Reso	urces Group	Date
Computed By	KS	09/05/17
Checked By	CR	

NUMBER:

FILE:

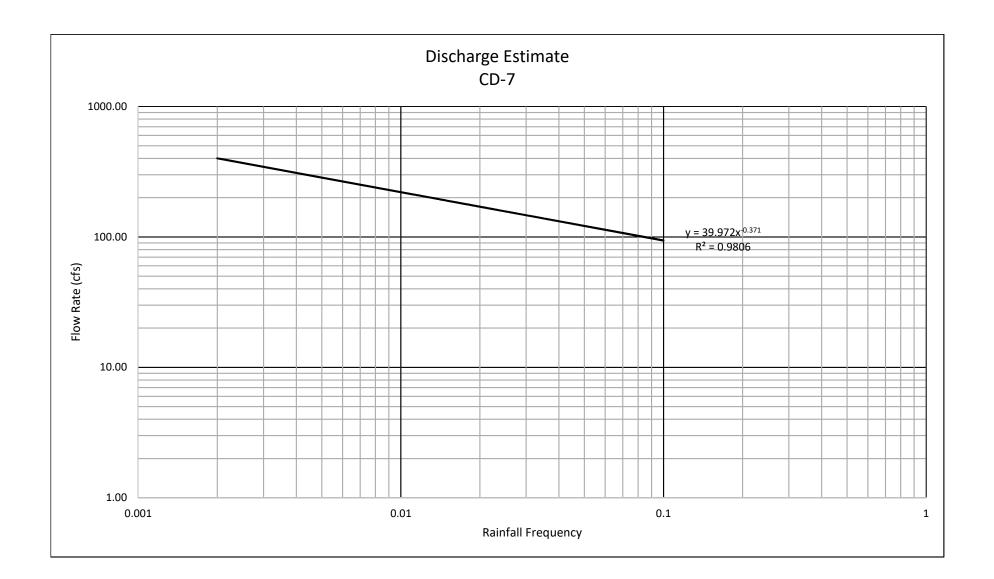
Rainfall Zone:	7 Fre	equency:			
SHEET FLOW	(Applicable To T⊡dc⊡Only)				
		Segment ID			
1) SURFACE DESCR	IPTION (table 5-4)				
2) MANNNING'S RO	JGHNESS COEFF., [n] (table 5-	4)	0.36		
3) FLOW LENGTH, [I	_] (TOTAL L <= 300 ft)	ft	300		
4) HIGH ELEVATION	[A]	ft	68.0		
5) LOW ELEVATION,	[B]	ft	67.0		
6) TWO YEAR 24-hr F	RAINFALL, [P]	in	4.92		
7) LAND SLOPE, [s]		ft/ft	0.003		
8) COMPUTE Tdt	$T = (.007*(n*L)^0.8)/(P^0.5*s)$	s^0.4) hr	1.315 +		1.315
				min =	78.9
SHALLOW CC	NCENTRATED FLOW				
		Segment ID			
9) SURFACE DESCR	IPTION Enter 1 (Paved) or 2 (Un	· ·	1		
10) FLOW LENGTH,	, , ,	ft	1400		
11) HIGH ELEVATION			67.0		
12) LOW ELEVATION	7 6 3		57.0		
13) WATERCOURSE		ft/ft	0.0071		
14) AVERAGE VELO	CITY. IVI **	ft/sec	1.72		
15) COMPUTE Total	7 L 3	hr	0.23 +	=	0.23
-,				min =	
CHANNEL FLOW					
		Segment ID			
16) CROSS SECTION	NAL FLOW AREA, [a]	ft^2			
17) WETTED PERIME		ft			
18) HYDRAULIC RAD		ft			
19) FLOW LENGTH,	,	ft			
20) HIGH ELEVATION		ft			
21) LOW ELEVATION	7 6 3	ft			
22) CHANNEL SLOPE		ft/ft			
,	OUGHNESS COEFF., [n]	.010			
,	V = (1.49*r^2/3 * s^1/2) / n	ft/sec			
25) COMPUTE Todt		hr			
20, COM OTE TEME	1 3 E / 0000 V	111			0.0

TOTAL TIME	(hr)	1.54
** Reference: FDOT Drainage Manual Chapter 5.5, TR-55 Chapter 3 & APP-F. TOTAL TIME	(min)	92.5

0.0

CD-7 Rational Method								
Runoff Coefficient Calculations								
			Runoff					
Land Use	Slope	Land Cover (%)	Coefficient	Area (acre) - A	Product			
Residential	0-2%	5	0.45	3.8975	1.75			
Commercial	0-2%	45	0.95	35.0775	33.32			
Lawn flat 2%	0-2%	20	0.20	15.59	3.12			
Woods/Wetlands	0-2%	30	0.15	23.385	3.51			
			Total	77.95	41.70			
			Composi	te Coefficient	0.54			
	Contributing	g Flow Rate for Va	rious Storm Fr	equency				
Storm Frequency	Storm Frequency	Rainfall	Intensity Adjusted Runoff Run		Runoff Rate - Q			
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)			
10-Year	1	0.1	2.35	0.54	98.00			
25-Year	1.1	0.04	2.72	0.59	124.78			
50-Year	1.2	0.02	3	0.71	165.14			
100-Year	1.25	0.01	3.35	0.88	230.51			
500-Year	-	0.002	-	-	400.93			
		Rational For	rmula					
Q = CIA								

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-7 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 98 cfs Design Flow: 165 cfs Maximum Flow: 231 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-7

Headwater Elevation (ft)	Total Discharge (cfs)	CD-7 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
60.98	98.00	98.00	0.00	1
61.12	111.30	111.30	0.00	1
61.28	124.60	124.60	0.00	1
61.45	137.90	137.90	0.00	1
61.65	151.20	151.20	0.00	1
61.86	164.50	164.50	0.00	1
61.86	165.00	165.00	0.00	1
62.33	191.10	191.10	0.00	1
62.59	204.40	204.40	0.00	1
62.88	217.70	217.70	0.00	1
63.17	231.00	231.00	0.00	1
68.47	384.40	384.40	0.00	Overtopping

Rating Curve Plot for Crossing: CD-7

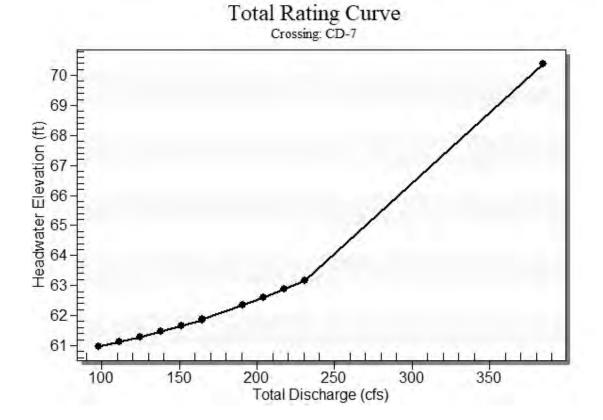


Table 2 - Culvert Summary Table: CD-7

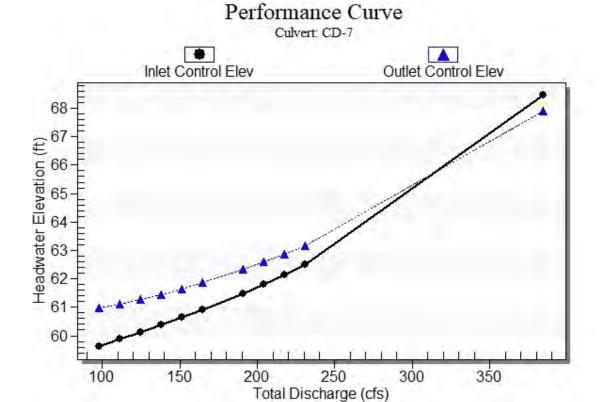
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
98.00	98.00	60.98	3.115	4.481	4-FFf	1.960	2.096	4.000	4.000	3.899	0.000
111.30	111.30	61.12	3.370	4.621	4-FFf	2.115	2.240	4.000	4.000	4.428	0.000
124.60	124.60	61.28	3.621	4.778	4-FFf	2.270	2.377	4.000	4.000	4.958	0.000
137.90	137.90	61.45	3.873	4.953	4-FFf	2.426	2.505	4.000	4.000	5.487	0.000
151.20	151.20	61.65	4.132	5.146	4-FFf	2.586	2.629	4.000	4.000	6.016	0.000
164.50	164.50	61.86	4.401	5.356	4-FFf	2.754	2.745	4.000	4.000	6.545	0.000
165.00	165.00	61.86	4.411	5.364	4-FFf	2.760	2.749	4.000	4.000	6.565	0.000
191.10	191.10	62.33	4.985	5.830	4-FFf	3.142	2.959	4.000	4.000	7.604	0.000
204.40	204.40	62.59	5.305	6.094	4-FFf	4.000	3.058	4.000	4.000	8.133	0.000
217.70	217.70	62.88	5.647	6.375	4-FFf	4.000	3.151	4.000	4.000	8.662	0.000
231.00	231.00	63.17	6.012	6.674	4-FFf	4.000	3.239	4.000	4.000	9.191	0.000

Straight Culvert

Inlet Elevation (invert): 56.50 ft, Outlet Elevation (invert): 56.00 ft

Culvert Length: 129.00 ft, Culvert Slope: 0.0039

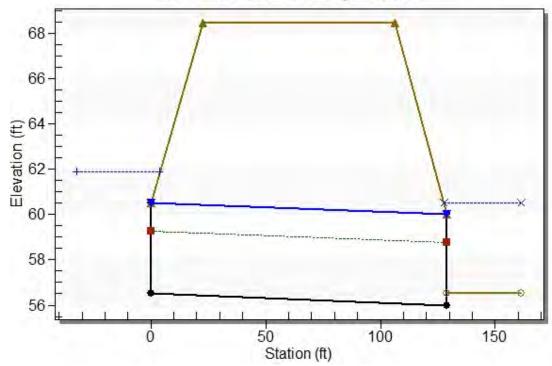
Culvert Performance Curve Plot: CD-7



Water Surface Profile Plot for Culvert: CD-7

Crossing - CD-7, Design Discharge - 165.0 cfs

Culvert - CD-7, Culvert Discharge - 165.0 cfs



Site Data - CD-7

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft Inlet Elevation: 56.50 ft Outlet Station: 129.00 ft Outlet Elevation: 56.00 ft Number of Barrels: 2

Culvert Data Summary - CD-7

Barrel Shape: Circular Barrel Diameter: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-7)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
98.00	60.50	4.00
111.30	60.50	4.00
124.60	60.50	4.00
137.90	60.50	4.00
151.20	60.50	4.00
164.50	60.50	4.00
165.00	60.50	4.00
191.10	60.50	4.00
204.40	60.50	4.00
217.70	60.50	4.00
231.00	60.50	4.00

Tailwater Channel Data - CD-7

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 60.50 ft

Roadway Data for Crossing: CD-7

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft
Crest Elevation: 68.47 ft
Roadway Surface: Paved
Roadway Top Width: 84.00 ft

Cross Drain 8

CD-8 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-8.

Flow Rate 10 =	133 ft ³ /s
Flow Rate 25 =	169 ft ³ /s
Flow Rate 50 =	223 ft ³ /s
Flow Rate 100 =	309 ft ³ /s
Flow Rate 500 =	535 ft ³ /s
Pipe Length =	447 ft

Change in FL Elevation from

Upstream to Downstream = 0.50 ft

Manning's "n" value = 0.012

 $D = (2.159 \text{ Qn/S}^{0.5})^{3/8}$

D = 7.80 ft D = 93.615 in $A = 47.80 \text{ ft}^2$ Proposed Size = 1-10'x5' CBC

TIME OF CONCENTRATION

PROJECT TITLE: STATE ROAD NO. 408 EASTERN EXTENSION

LOCATION: **ORANGE COUNTY**

BASIN NAME: CD-8

CC	NDITIONS
Pre-Development	Х
Post-Development	
Rainfall Zone:	7

25) COMPUTE Tdt Tdt = L/3600*V

COMPUTE	VARIABLE
T⊡dc	Х
Т	⊡dt
Frequency:	

Water Reso	urces Group	Date
Computed By	KS	09/05/17
Checked By	CR	

NUMBER:

FILE:

Rainfall Zone: 7 Frequency:				·
SHEET FLOW (Applicable To T⊡dc⊡Only)				
	Segment ID			
1) SURFACE DESCRIPTION (table 5-4)	· ·			
2) MANNNING'S ROUGHNESS COEFF., [n] (table 5-4)		0.36		
3) FLOW LENGTH, [L] (TOTAL L <= 300 ft)	ft	300		
4) HIGH ELEVATION, [A]	ft	68.0		
5) LOW ELEVATION, [B]	ft	67.0		
6) TWO YEAR 24-hr RAINFALL, [P]	in	4.92		
7) LAND SLOPE, [s]	ft/ft	0.003		
8) COMPUTE Tdt \Box Tdt \Box = (.007*(n*L)^0.8)/(P^0.5 * s^0.4)	hr	1.315 +		1.315
			min	= 78.9
SHALLOW CONCENTRATED FLOW				
	Segment ID			
9) SURFACE DESCRIPTION Enter 1 (Paved) or 2 (Unpaved)	· ·	1		
10) FLOW LENGTH, [L]	ft	2300		
11) HIGH ELEVATION, [C]		67.0		
12) LOW ELEVATION, [D]		50.0		
13) WATERCOURSE SLOPE, [s]	ft/ft	0.0074		
14) AVERAGE VELOCITY, [V] **	ft/sec	1.75		
15) COMPUTE Tott Tott = L / 3600*V	hr	0.37 +		= 0.37
			min	= 21.9
CHANNEL FLOW				
	Segment ID			
16) CROSS SECTIONAL FLOW AREA, [a]	ft^2			
17) WETTED PERIMETER, [Pldw]	ft			
18) HYDRAULIC RADIUS, [r] = a / P dw □	ft			
19) FLOW LENGTH, [L]	ft			
20) HIGH ELEVATION, [D]	ft			
21) LOW ELEVATION, [E]	ft			
22) CHANNEL SLOPE, [s]	ft/ft			
23) MANNNING'S ROUGHNESS COEFF., [n]				
24) COMPUTE V: $V = (1.49*r^2/3 * s^1/2) / n$	ft/sec			
25) COMPLITE TEHE TEHE - 1 / 2600*\/	hr			_

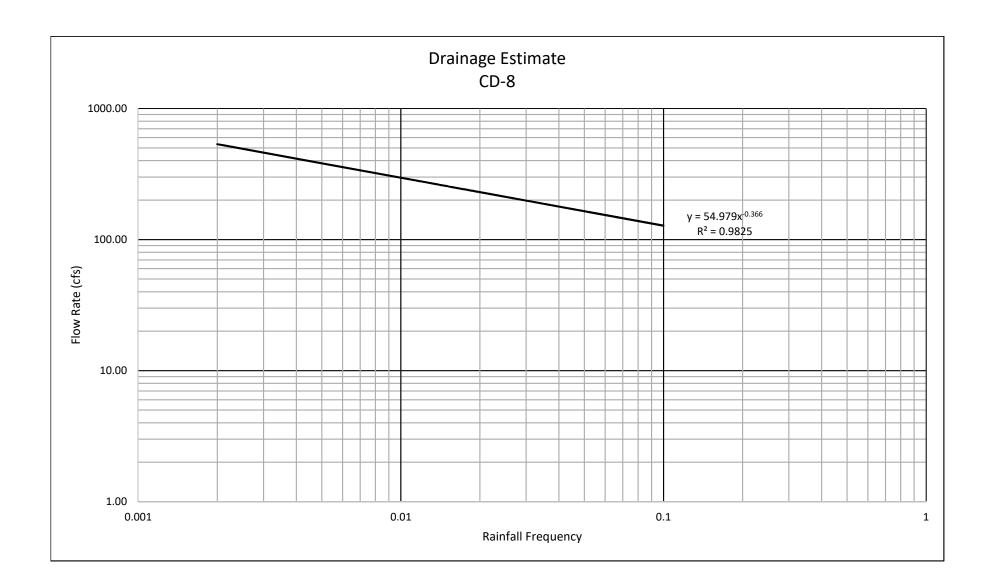
TOTAL TIME (hr) 1.68 ** Reference: FDOT Drainage Manual Chapter 5.5, TR-55 Chapter 3 & APP-F. TOTAL TIME (min) 100.8

hr

0.0

		CD-8 Rational	Method		
	R	unoff Coefficient	Calculations		
Land Use	Slope	Land Cover (%)	Runoff	Area (acre) - A	Product
			Coefficient		
Residential	0-2%	5	0.45	6.072	2.73
Commercial	0-2%	40	0.95	48.576	46.15
Lawn flat 2%	0-2%	25	0.20	30.36	6.07
Woods/Wetlands	0-2%	30	0.15	36.432	5.46
			Total	121.44	60.42
			Compos	ite Coefficient	0.50
	Contributin	g Flow Rate for Va	arious Storm F	requency	
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)
10-Year	1	0.1	2.2	0.50	132.92
25-Year	1.1	0.04	2.55	0.55	169.47
50-Year	1.2	0.02	2.8	0.66	223.30
100-Year	1.25	0.01	3.1	0.82	309.03
500-Year	-	0.002	-	-	534.59
		Rational Fo	rmula		
		Q = CIA			

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-8 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 133 cfs Design Flow: 223 cfs Maximum Flow: 309 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-8

Headwater Elevation (ft)	Total Discharge (cfs)	CD-8 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
53.78	133.00	133.00	0.00	1
53.85	150.60	150.60	0.00	1
53.94	168.20	168.20	0.00	1
54.03	185.80	185.80	0.00	1
54.14	203.40	203.40	0.00	1
54.25	221.00	221.00	0.00	1
54.27	223.00	223.00	0.00	1
54.51	256.20	256.20	0.00	1
54.65	273.80	273.80	0.00	1
54.80	291.40	291.40	0.00	1
54.96	309.00	309.00	0.00	1
84.68	1356.63	1356.63	0.00	Overtopping

Rating Curve Plot for Crossing: CD-8

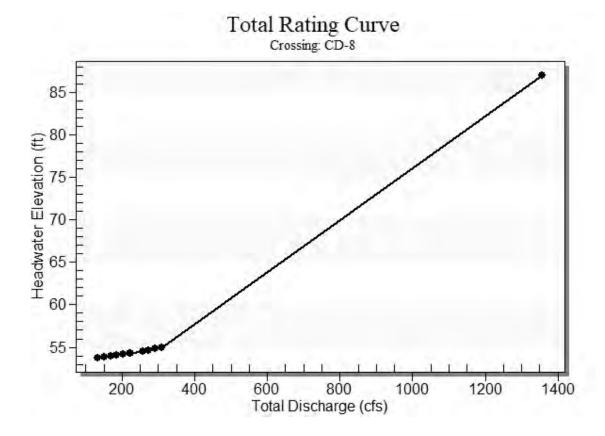


Table 2 - Culvert Summary Table: CD-8

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
133.00	133.00	53.78	3.008	5.269	4-FFf	2.270	1.764	5.000	5.000	2.660	0.000
150.60	150.60	53.85	3.259	5.344	4-FFf	2.473	1.917	5.000	5.000	3.012	0.000
168.20	168.20	53.94	3.501	5.430	4-FFf	2.671	2.063	5.000	5.000	3.364	0.000
185.80	185.80	54.03	3.735	5.524	4-FFf	2.865	2.205	5.000	5.000	3.716	0.000
203.40	203.40	54.14	3.963	5.628	4-FFf	3.054	2.342	5.000	5.000	4.068	0.000
221.00	221.00	54.25	4.186	5.742	4-FFf	3.240	2.475	5.000	5.000	4.420	0.000
223.00	223.00	54.27	4.211	5.755	4-FFf	3.261	2.490	5.000	5.000	4.460	0.000
256.20	256.20	54.51	4.621	5.997	4-FFf	3.603	2.732	5.000	5.000	5.124	0.000
273.80	273.80	54.65	4.837	6.138	4-FFf	3.780	2.855	5.000	5.000	5.476	0.000
291.40	291.40	54.80	5.052	6.289	4-FFf	3.956	2.977	5.000	5.000	5.828	0.000
309.00	309.00	54.96	5.269	6.450	4-FFf	5.000	3.095	5.000	5.000	6.180	0.000

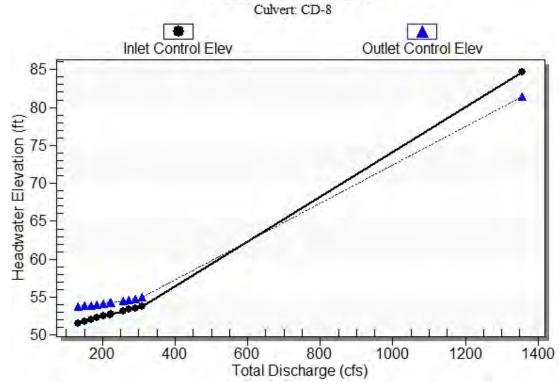
Straight Culvert

Inlet Elevation (invert): 48.51 ft, Outlet Elevation (invert): 48.00 ft

Culvert Length: 447.00 ft, Culvert Slope: 0.0011

Culvert Performance Curve Plot: CD-8

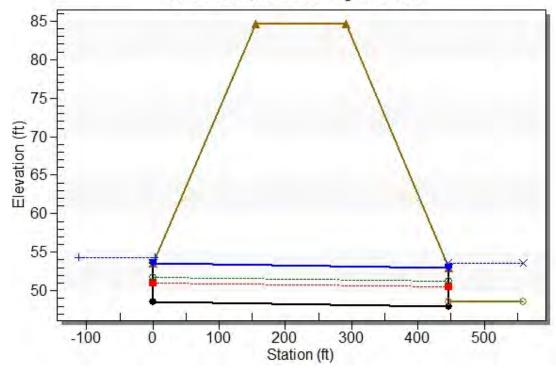
Performance Curve



Water Surface Profile Plot for Culvert: CD-8

Crossing - CD-8, Design Discharge - 223.0 cfs

Culvert - CD-8, Culvert Discharge - 223.0 cfs



Site Data - CD-8

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 48.51 ft
Outlet Station: 447.00 ft
Outlet Elevation: 48.00 ft
Number of Barrels: 1

Culvert Data Summary - CD-8

Barrel Shape: Concrete Box

Barrel Span: 10.00 ft Barrel Rise: 5.00 ft

Barrel Material: Concrete Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-8)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
133.00	53.51	5.00
150.60	53.51	5.00
168.20	53.51	5.00
185.80	53.51	5.00
203.40	53.51	5.00
221.00	53.51	5.00
223.00	53.51	5.00
256.20	53.51	5.00
273.80	53.51	5.00
291.40	53.51	5.00
309.00	53.51	5.00

Tailwater Channel Data - CD-8

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 53.51 ft

Roadway Data for Crossing: CD-8

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 84.68 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Cross Drain 9

CD-9 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-9.

Flow Rate 10 =	92 ft ³ /s
Flow Rate 25 =	117 ft ³ /s
Flow Rate 50 =	153 ft ³ /s
Flow Rate 100 =	212 ft ³ /s
Flow Rate 500 =	364 ft ³ /s
Pipe Length =	300 ft

Change in FL Elevation from

Upstream to Downstream = 0.50 ft

Manning's "n" value = 0.012

 $D = (2.159 \text{ Qn/S}^{0.5})^{3/8}$

D = 6.28 ft D = 75.397 in $A = 31.006 \text{ ft}^2$ Proposed Size = 1-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: STATE ROAD NO. 408 EASTERN EXTENSION

LOCATION: ORANGE COUNTY

BASIN NAME: CD-9

CC	NDITIONS
Pre-Development	X
Post-Development	
Rainfall Zone:	7

COMPUTE	D VARIABLE
T⊡dc	X
Т	`⊡dt
Frequency:	

Water Reso	urces Group	Date
Computed By	KS	09/05/17
Checked By	CR	

TOTAL TIME (hr)

TOTAL TIME (min)

1.66

99.7

NUMBER:

FILE:

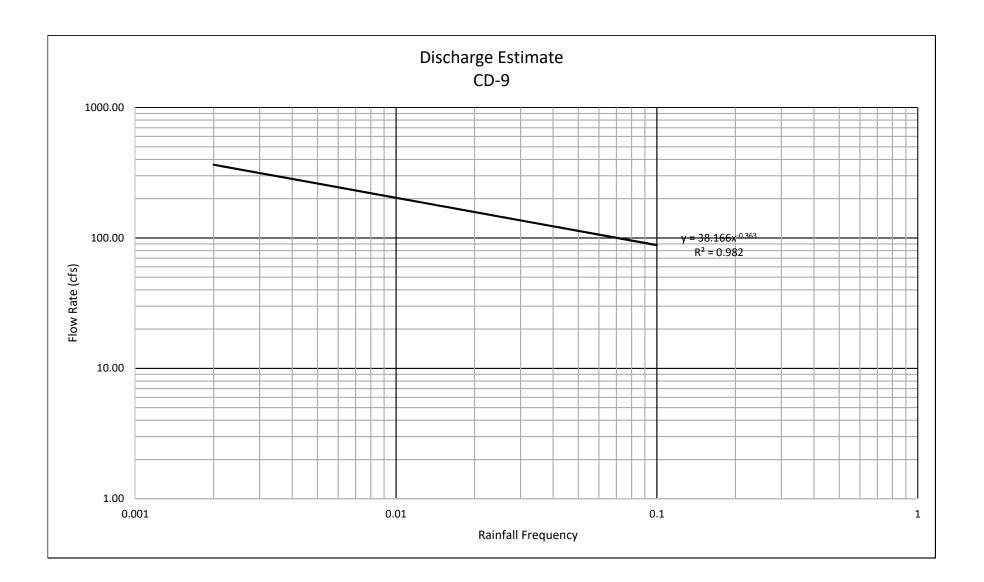
railliali Zolle.				
SHEET FLOW (Applicable To T⊡c⊏Only)				
	Segment ID			
1) SURFACE DESCRIPTION (table 5-4)	•	·		
2) MANNNING'S ROUGHNESS COEFF., [n] (table 5-4)		0.41		
3) FLOW LENGTH, [L] (TOTAL L <= 300 ft)	ft	300		
4) HIGH ELEVATION, [A]	ft	67.0		
5) LOW ELEVATION, [B]	ft	66.0		
6) TWO YEAR 24-hr RAINFALL, [P]	in	4.92		
7) LAND SLOPE, [s]	ft/ft	0.003		
8) COMPUTE Tata Tata = (.007*(n*L)^0.8)/(P^0.5 * s^0.4)	hr	1.441 +		1.441
(.66. (2) 6.6) (6.6. 6.6.)	•••		min	
SHALLOW CONCENTRATED FLOW				33.3
	Segment ID			
9) SURFACE DESCRIPTION Enter 1 (Paved) or 2 (Unpaved)	•	2		
10) FLOW LENGTH, [L]	ft	1665		
11) HIGH ELEVATION, [C]		66.0		
12) LOW ELEVATION, [D]		38.0		
13) WATERCOURSE SLOPE, [s]	ft/ft	0.0168		
14) AVERAGE VELOCITY, [V] **	ft/sec	2.09		
15) COMPUTE Tidt: Tidt: = L / 3600*V	hr	0.22 +		= 0.22
.,			min	
CHANNEL FLOW				
	Segment ID			
16) CROSS SECTIONAL FLOW AREA, [a]	ft^2			
17) WETTED PERIMETER, [Pīdwi]	ft			
18) HYDRAULIC RADIUS, [r] = a / P dw□	ft			
19) FLOW LENGTH, [L]	ft			
20) HIGH ELEVATION. [D]	ft			
21) LOW ELEVATION, [E]	ft			
22) CHANNEL SLOPE, [s]	ft/ft			
	IVIL			
23) MANNNING'S ROUGHNESS COEFF., [n]	ft/sec			
24) COMPUTE V: $V = (1.49 \cdot r^2 / 3 \cdot s^4 / 2) / n$				
25) COMPUTE Tdt: Tdt = L/3600*V	hr			=
			min	= 0.0

^{**} Reference: FDOT Drainage Manual Chapter 5.5, TR-55 Chapter 3 & APP-F.

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CD-9 Rational Method								
Runoff Coefficient Calculations								
Land Use	Slope	Land Cover (%)	Runoff Area (acre) - A		Product			
			Coefficient					
Residential	0-2%	5	0.45	3.79	1.71			
Commercial	0-2%	45	0.95	34.12	32.41			
Lawn flat 2%	0-2%	25	0.20	18.96	3.79			
Woods/Wetlands	0-2%	25	0.15	18.96	2.84			
			Total	75.82	40.75			
			Compos	site Coefficient	0.54			
	Contributing	g Flow Rate for Va	arious Storm F	requency				
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q			
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)			
10-Year	1	0.1	2.25	0.54	91.69			
25-Year	1.1	0.04	2.6	0.59	116.55			
50-Year	1.2	0.02	2.85	0.71	153.31			
100-Year	1.25	0.01	3.15	0.89	211.82			
500-Year	•	0.002	-	-	364.25			
		Rational Fo	rmula					
		Q = CIA						

^{**} The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-9 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 92 cfs Design Flow: 153 cfs Maximum Flow: 212 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-9

Headwater Elevation (ft)	Total Discharge (cfs)	CD-9 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
42.87	92.00	92.00	0.00	1
42.97	104.00	104.00	0.00	1
43.08	116.00	116.00	0.00	1
43.21	128.00	128.00	0.00	1
43.35	140.00	140.00	0.00	1
43.50	152.00	152.00	0.00	1
43.51	153.00	153.00	0.00	1
43.84	176.00	176.00	0.00	1
44.03	188.00	188.00	0.00	1
44.23	200.00	200.00	0.00	1
44.45	212.00	212.00	0.00	1
54.79	532.70	532.70	0.00	Overtopping

Rating Curve Plot for Crossing: CD-9

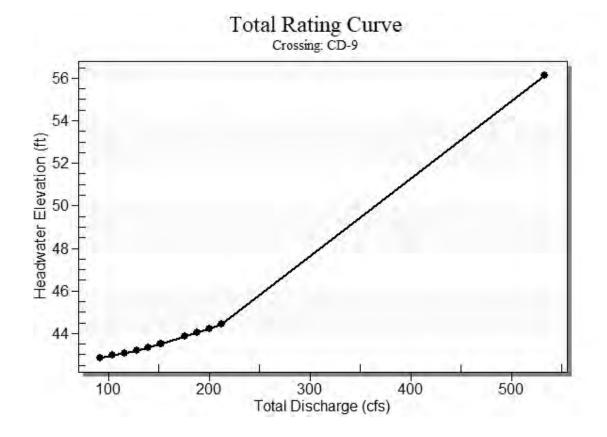


Table 2 - Culvert Summary Table: CD-9

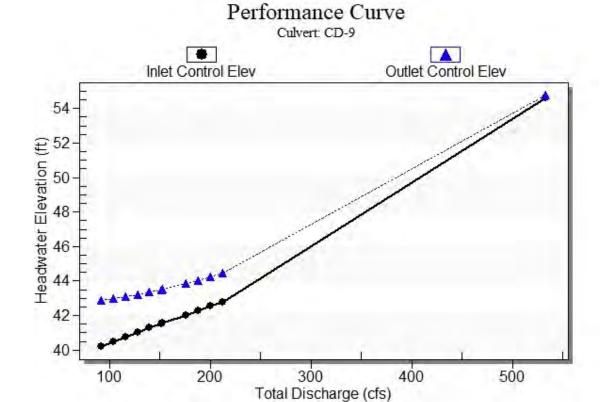
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
92.00	92.00	42.87	3.698	6.367	4-FFf	2.889	2.572	6.000	6.000	3.254	0.000
104.00	104.00	42.97	3.989	6.468	4-FFf	3.108	2.747	6.000	6.000	3.678	0.000
116.00	116.00	43.08	4.265	6.583	4-FFf	3.325	2.909	6.000	6.000	4.103	0.000
128.00	128.00	43.21	4.529	6.710	4-FFf	3.542	3.060	6.000	6.000	4.527	0.000
140.00	140.00	43.35	4.784	6.849	4-FFf	3.764	3.206	6.000	6.000	4.951	0.000
152.00	152.00	43.50	5.034	7.001	4-FFf	3.991	3.345	6.000	6.000	5.376	0.000
153.00	153.00	43.51	5.055	7.014	4-FFf	4.011	3.356	6.000	6.000	5.411	0.000
176.00	176.00	43.84	5.527	7.341	4-FFf	4.496	3.612	6.000	6.000	6.225	0.000
188.00	188.00	44.03	5.775	7.531	4-FFf	6.000	3.741	6.000	6.000	6.649	0.000
200.00	200.00	44.23	6.026	7.732	4-FFf	6.000	3.862	6.000	6.000	7.074	0.000
212.00	212.00	44.45	6.284	7.946	4-FFf	6.000	3.980	6.000	6.000	7.498	0.000

Straight Culvert

Inlet Elevation (invert): 36.50 ft, Outlet Elevation (invert): 36.00 ft

Culvert Length: 300.00 ft, Culvert Slope: 0.0017

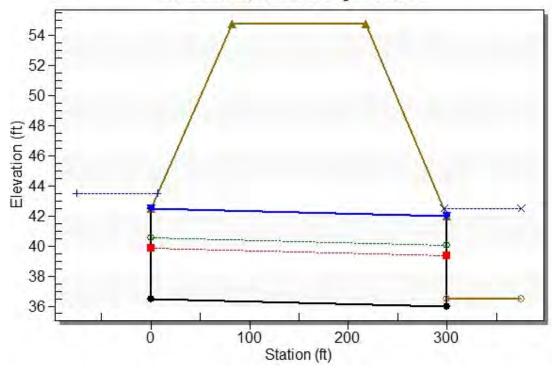
Culvert Performance Curve Plot: CD-9



Water Surface Profile Plot for Culvert: CD-9

Crossing - CD-9, Design Discharge - 153.0 cfs

Culvert - CD-9, Culvert Discharge - 153.0 cfs



Site Data - CD-9

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 36.50 ft
Outlet Station: 300.00 ft
Outlet Elevation: 36.00 ft
Number of Barrels: 1

Culvert Data Summary - CD-9

Barrel Shape: Circular
Barrel Diameter: 6.00 ft
Barrel Material: Concrete
Embedment: 0.00 in

Barrel Manning's n: 0.0120 Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-9)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
92.00	42.50	6.00
104.00	42.50	6.00
116.00	42.50	6.00
128.00	42.50	6.00
140.00	42.50	6.00
152.00	42.50	6.00
153.00	42.50	6.00
176.00	42.50	6.00
188.00	42.50	6.00
200.00	42.50	6.00
212.00	42.50	6.00

Tailwater Channel Data - CD-9

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 42.50 ft

Roadway Data for Crossing: CD-9

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 54.79 ft Roadway Surface: Paved

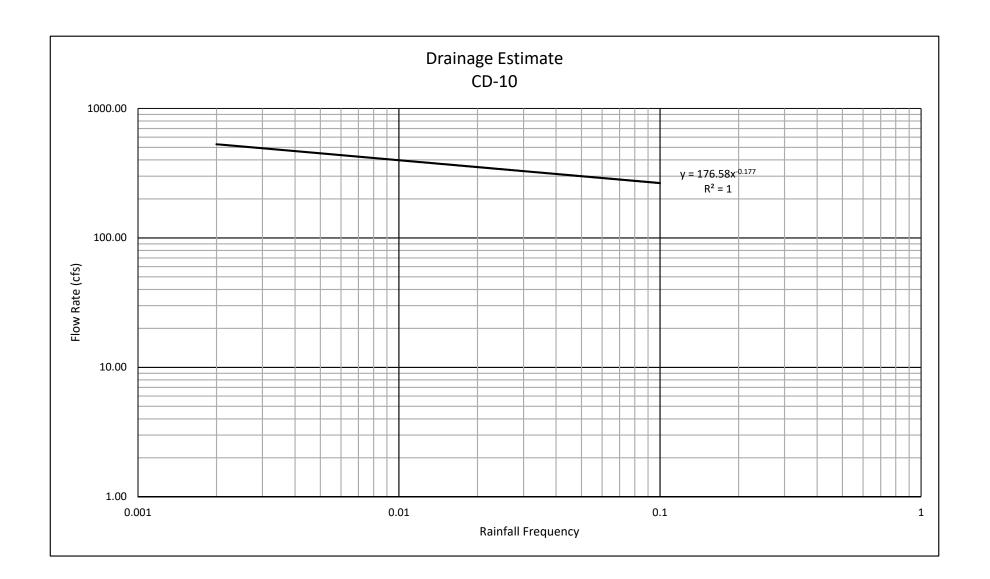
Roadway Top Width: 136.00 ft

Cross Drain 10

CD-10 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-10.

Flow Rate 10 =	265 ft ³ /s
Flow Rate 25 =	312 ft ³ /s
Flow Rate 50 =	353 ft ³ /s
Flow Rate 100 =	398 ft ³ /s
Flow Rate 500 =	530 ft ³ /s
Pipe Length =	310 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	8.01 ft
D =	96.11 in
A =	50.38 ft ²
Proposed Size =	2-6'x4' CBC



CD-10 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 265 cfs Design Flow: 353 cfs Maximum Flow: 398 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-10

Headwater Elevation (ft)	Total Discharge (cfs)	CD-10 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
43.19	265.00	265.00	0.00	1
43.31	278.30	278.30	0.00	1
43.44	291.60	291.60	0.00	1
43.58	304.90	304.90	0.00	1
43.72	318.20	318.20	0.00	1
43.86	331.50	331.50	0.00	1
44.02	344.80	344.80	0.00	1
44.11	353.00	353.00	0.00	1
44.34	371.40	371.40	0.00	1
44.51	384.70	384.70	0.00	1
44.69	398.00	398.00	0.00	1
55.97	896.98	896.98	0.00	Overtopping

Rating Curve Plot for Crossing: CD-10

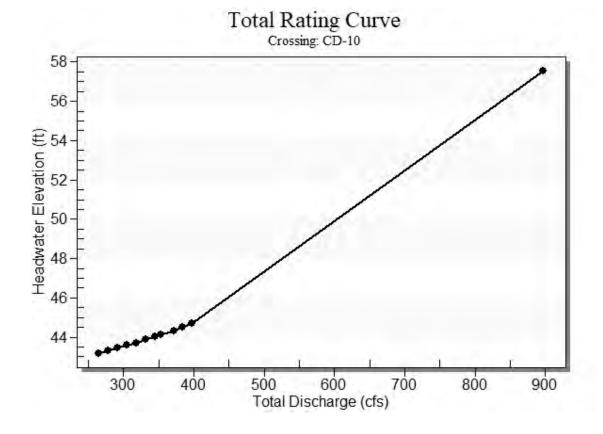


Table 2 - Culvert Summary Table: CD-10

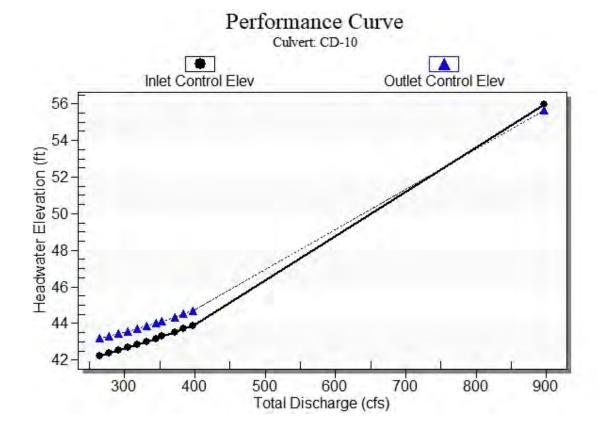
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
265.00	265.00	43.19	4.210	5.190	4-FFf	3.199	2.474	4.000	4.000	5.521	0.000
278.30	278.30	43.31	4.364	5.313	4-FFf	3.321	2.556	4.000	4.000	5.798	0.000
291.60	291.60	43.44	4.519	5.441	4-FFf	3.441	2.637	4.000	4.000	6.075	0.000
304.90	304.90	43.58	4.677	5.576	4-FFf	3.561	2.717	4.000	4.000	6.352	0.000
318.20	318.20	43.72	4.838	5.716	4-FFf	3.680	2.795	4.000	4.000	6.629	0.000
331.50	331.50	43.86	5.001	5.863	4-FFf	3.799	2.872	4.000	4.000	6.906	0.000
344.80	344.80	44.02	5.169	6.015	4-FFf	4.000	2.949	4.000	4.000	7.183	0.000
353.00	353.00	44.11	5.274	6.112	4-FFf	4.000	2.995	4.000	4.000	7.354	0.000
371.40	371.40	44.34	5.515	6.338	4-FFf	4.000	3.099	4.000	4.000	7.737	0.000
384.70	384.70	44.51	5.695	6.509	4-FFf	4.000	3.172	4.000	4.000	8.015	0.000
398.00	398.00	44.69	5.880	6.685	4-FFf	4.000	3.245	4.000	4.000	8.292	0.000

Straight Culvert

Inlet Elevation (invert): 38.00 ft, Outlet Elevation (invert): 37.50 ft

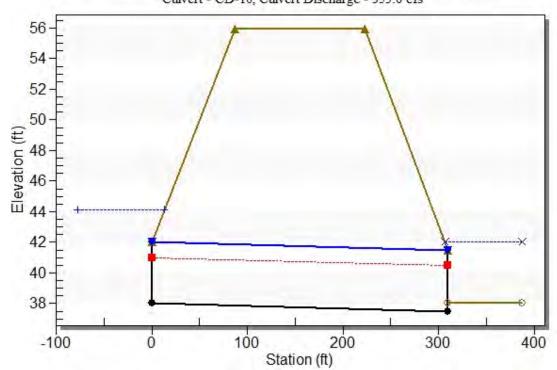
Culvert Length: 310.00 ft, Culvert Slope: 0.0016

Culvert Performance Curve Plot: CD-10



Water Surface Profile Plot for Culvert: CD-10

Crossing - CD-10, Design Discharge - 353.0 cfs Culvert - CD-10, Culvert Discharge - 353.0 cfs



Site Data - CD-10

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 38.00 ft
Outlet Station: 310.00 ft
Outlet Elevation: 37.50 ft
Number of Barrels: 2

Culvert Data Summary - CD-10

Barrel Shape: Concrete Box

Barrel Span: 6.00 ft Barrel Rise: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-10)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
265.00	42.00	4.00
278.30	42.00	4.00
291.60	42.00	4.00
304.90	42.00	4.00
318.20	42.00	4.00
331.50	42.00	4.00
344.80	42.00	4.00
353.00	42.00	4.00
371.40	42.00	4.00
384.70	42.00	4.00
398.00	42.00	4.00

Tailwater Channel Data - CD-10

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 42.00 ft

Roadway Data for Crossing: CD-10

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 55.97 ft Roadway Surface: Paved

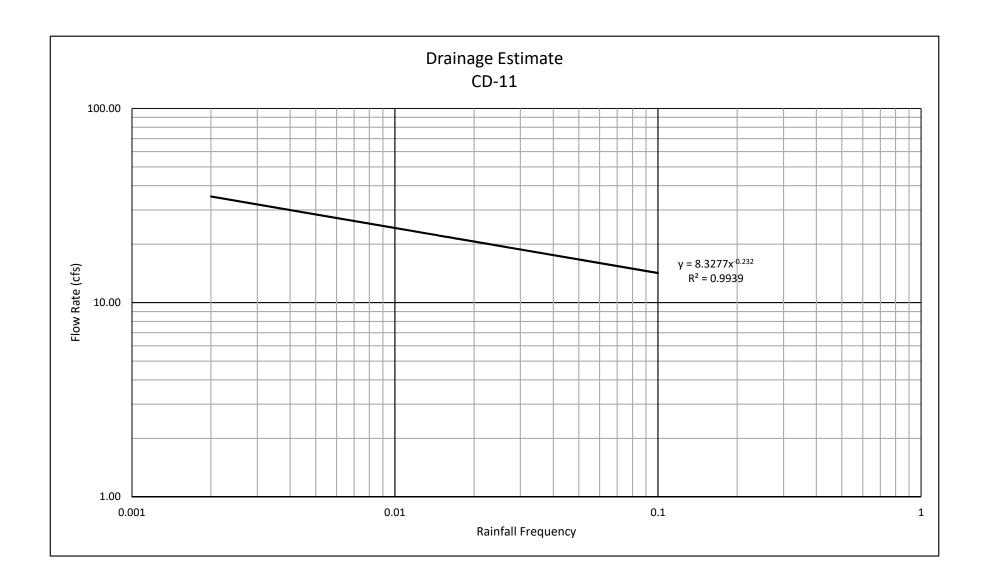
Roadway Top Width: 136.00 ft

Cross Drain 11

CD-11 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-11.

Flow Rate 10 =	14 ft ³ /s
Flow Rate 25 =	18 ft ³ /s
Flow Rate 50 =	21 ft ³ /s
Flow Rate 100 =	$24 \text{ ft}^3/\text{s}$
Flow Rate 500 =	35 ft ³ /s
Pipe Length =	395 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= $(2.159 \text{ Qn/S}^{0.5})^{3/8}$	
D =	2.92 ft
D =	35.08 in
A =	6.71 ft ²
Proposed Size =	2-24" RCP



CD-11 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 14 cfs Design Flow: 21 cfs Maximum Flow: 24 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-11

Headwater Elevation (ft)	Total Discharge (cfs)	CD-11 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
58.44	14.00	14.00	0.00	1
58.50	15.00	15.00	0.00	1
58.57	16.00	16.00	0.00	1
58.64	17.00	17.00	0.00	1
58.72	18.00	18.00	0.00	1
58.80	19.00	19.00	0.00	1
58.89	20.00	20.00	0.00	1
58.98	21.00	21.00	0.00	1
59.08	22.00	22.00	0.00	1
59.18	23.00	23.00	0.00	1
59.28	24.00	24.00	0.00	1
83.94	107.98	107.98	0.00	Overtopping

Rating Curve Plot for Crossing: CD-11

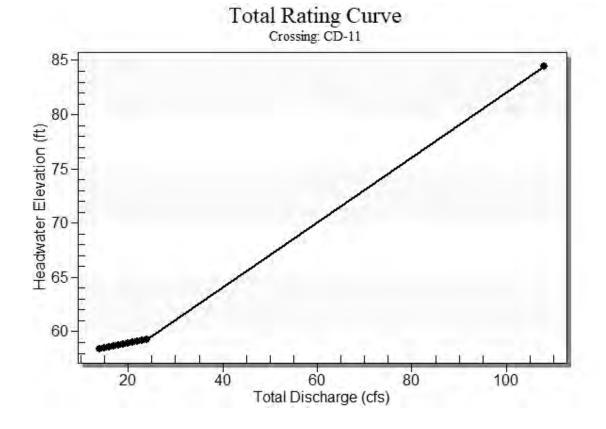


Table 2 - Culvert Summary Table: CD-11

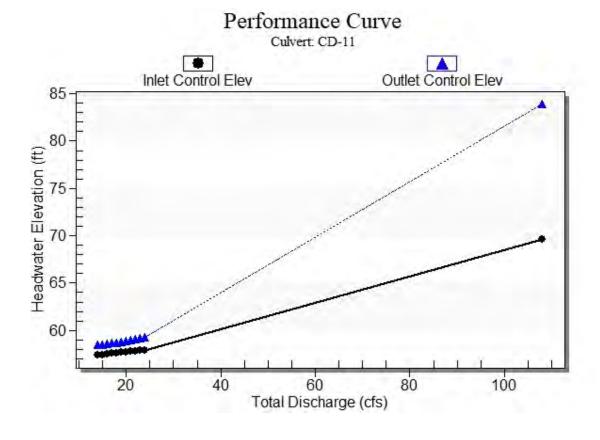
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
14.00	14.00	58.44	1.370	2.436	4-FFf	1.320	0.939	2.000	2.000	2.228	0.000
15.00	15.00	58.50	1.429	2.501	4-FFf	1.391	0.974	2.000	2.000	2.387	0.000
16.00	16.00	58.57	1.486	2.570	4-FFf	1.467	1.006	2.000	2.000	2.546	0.000
17.00	17.00	58.64	1.542	2.643	4-FFf	1.552	1.038	2.000	2.000	2.706	0.000
18.00	18.00	58.72	1.597	2.721	4-FFf	2.000	1.069	2.000	2.000	2.865	0.000
19.00	19.00	58.80	1.651	2.803	4-FFf	2.000	1.098	2.000	2.000	3.024	0.000
20.00	20.00	58.89	1.705	2.890	4-FFf	2.000	1.126	2.000	2.000	3.183	0.000
21.00	21.00	58.98	1.758	2.981	4-FFf	2.000	1.158	2.000	2.000	3.342	0.000
22.00	22.00	59.08	1.812	3.077	4-FFf	2.000	1.186	2.000	2.000	3.501	0.000
23.00	23.00	59.18	1.865	3.177	4-FFf	2.000	1.213	2.000	2.000	3.661	0.000
24.00	24.00	59.28	1.919	3.282	4-FFf	2.000	1.239	2.000	2.000	3.820	0.000

Straight Culvert

Inlet Elevation (invert): 56.00 ft, Outlet Elevation (invert): 55.50 ft

Culvert Length: 395.00 ft, Culvert Slope: 0.0013

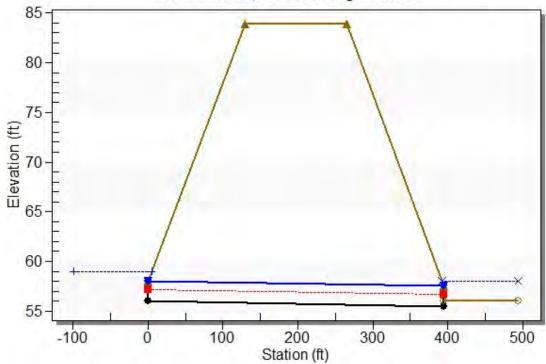
Culvert Performance Curve Plot: CD-11



Water Surface Profile Plot for Culvert: CD-11

Crossing - CD-11, Design Discharge - 21.0 cfs

Culvert - CD-11, Culvert Discharge - 21.0 cfs



Site Data - CD-11

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 56.00 ft
Outlet Station: 395.00 ft
Outlet Elevation: 55.50 ft
Number of Barrels: 2

Culvert Data Summary - CD-11

Barrel Shape: Circular
Barrel Diameter: 2.00 ft
Barrel Material: Concrete
Embedment: 0.00 in

Barrel Manning's n: 0.0120 Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-11)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
14.00	58.00	2.00
15.00	58.00	2.00
16.00	58.00	2.00
17.00	58.00	2.00
18.00	58.00	2.00
19.00	58.00	2.00
20.00	58.00	2.00
21.00	58.00	2.00
22.00	58.00	2.00
23.00	58.00	2.00
24.00	58.00	2.00

Tailwater Channel Data - CD-11

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 58.00 ft

Roadway Data for Crossing: CD-11

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 83.94 ft Roadway Surface: Paved

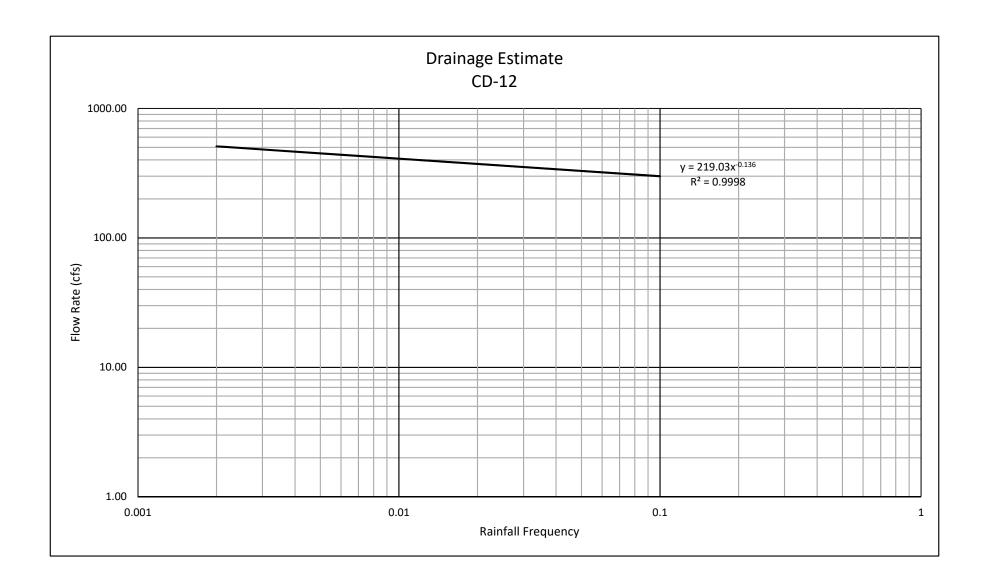
Roadway Top Width: 136.00 ft

Cross Drain 12

CD-12 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-12.

Flow Rate 10 =	299 ft ³ /s
Flow Rate 25 =	340 ft ³ /s
Flow Rate 50 =	373 ft ³ /s
Flow Rate 100 =	409 ft ³ /s
Flow Rate 500 =	510 ft ³ /s
Pipe Length =	522 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	8.92 ft
D =	107.059 in
A =	62.51 ft ²
Proposed Size =	2-8'x4' CBC



CD-12 HY-8 Culvert Analysis Report

Crossing Discharge Data

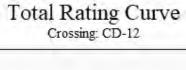
Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 299 cfs Design Flow: 373 cfs Maximum Flow: 409 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-12

Headwater Elevation (ft)	Total Discharge (cfs)	CD-12 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
54.01	299.00	299.00	0.00	1
54.09	310.00	310.00	0.00	1
54.17	321.00	321.00	0.00	1
54.25	332.00	332.00	0.00	1
54.33	343.00	343.00	0.00	1
54.42	354.00	354.00	0.00	1
54.51	365.00	365.00	0.00	1
54.57	373.00	373.00	0.00	1
54.70	387.00	387.00	0.00	1
54.79	398.00	398.00	0.00	1
54.89	409.00	409.00	0.00	1
75.36	1405.58	1405.58	0.00	Overtopping

Rating Curve Plot for Crossing: CD-12



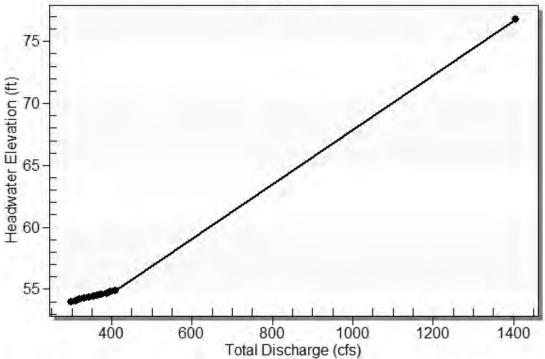


Table 2 - Culvert Summary Table: CD-12

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
299.00	299.00	54.01	3.746	5.012	4-FFf	3.200	2.214	4.000	4.000	4.672	0.000
310.00	310.00	54.09	3.840	5.088	4-FFf	3.286	2.267	4.000	4.000	4.844	0.000
321.00	321.00	54.17	3.934	5.166	4-FFf	3.371	2.321	4.000	4.000	5.016	0.000
332.00	332.00	54.25	4.028	5.247	4-FFf	3.456	2.374	4.000	4.000	5.188	0.000
343.00	343.00	54.33	4.123	5.332	4-FFf	3.541	2.426	4.000	4.000	5.359	0.000
354.00	354.00	54.42	4.217	5.418	4-FFf	3.624	2.477	4.000	4.000	5.531	0.000
365.00	365.00	54.51	4.312	5.508	4-FFf	3.708	2.528	4.000	4.000	5.703	0.000
373.00	373.00	54.57	4.382	5.575	4-FFf	3.768	2.565	4.000	4.000	5.828	0.000
387.00	387.00	54.70	4.505	5.695	4-FFf	3.874	2.629	4.000	4.000	6.047	0.000
398.00	398.00	54.79	4.602	5.793	4-FFf	4.000	2.678	4.000	4.000	6.219	0.000
409.00	409.00	54.89	4.701	5.893	4-FFf	4.000	2.728	4.000	4.000	6.391	0.000

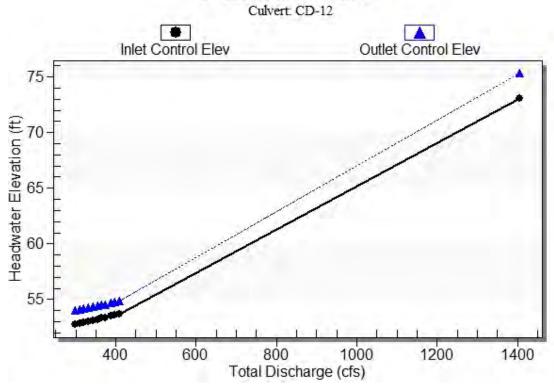
Straight Culvert

Inlet Elevation (invert): 49.00 ft, Outlet Elevation (invert): 48.50 ft

Culvert Length: 522.00 ft, Culvert Slope: 0.0010

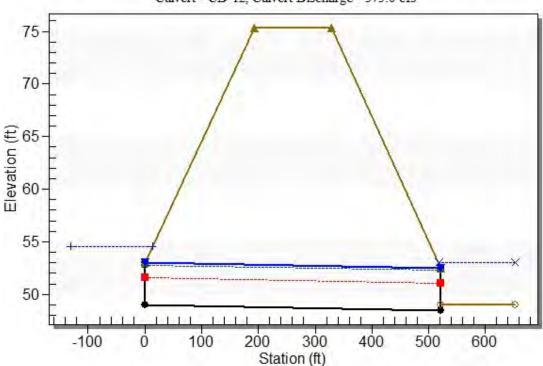
Culvert Performance Curve Plot: CD-12

Performance Curve



Water Surface Profile Plot for Culvert: CD-12

Crossing - CD-12, Design Discharge - 373.0 cfs Culvert - CD-12, Culvert Discharge - 373.0 cfs



Site Data - CD-12

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 49.00 ft
Outlet Station: 522.00 ft
Outlet Elevation: 48.50 ft
Number of Barrels: 2

Culvert Data Summary - CD-12

Barrel Shape: Concrete Box

Barrel Span: 8.00 ft Barrel Rise: 4.00 ft

Barrel Material: Concrete

Embedment: 0.00 in

Barrel Manning's n: 0.0120

Culvert Type: Straight

Inlet Configuration: Square Edge (90°) Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-12)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
299.00	53.00	4.00
310.00	53.00	4.00
321.00	53.00	4.00
332.00	53.00	4.00
343.00	53.00	4.00
354.00	53.00	4.00
365.00	53.00	4.00
373.00	53.00	4.00
387.00	53.00	4.00
398.00	53.00	4.00
409.00	53.00	4.00

Tailwater Channel Data - CD-12

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 53.00 ft

Roadway Data for Crossing: CD-12

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 75.36 ft Roadway Surface: Paved

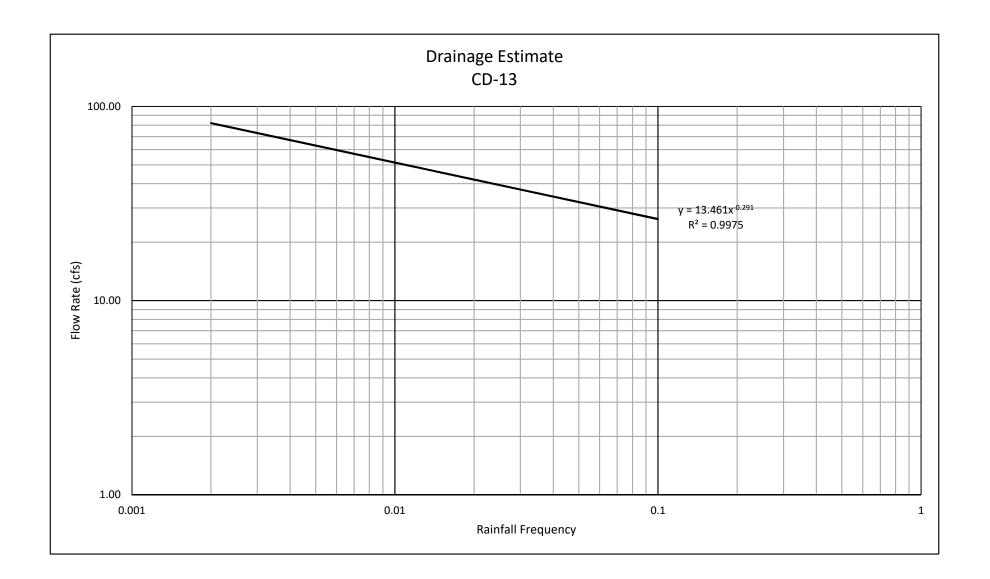
Roadway Top Width: 136.00 ft

Cross Drain 13

CD-13 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-13.

Flow Rate 10 =	26 ft ³ /s
Flow Rate 25 =	35 ft ³ /s
Flow Rate 50 =	$42 \text{ ft}^3/\text{s}$
Flow Rate 100 =	51 ft ³ /s
Flow Rate 500 =	82 ft ³ /s
Pipe Length =	325 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= $(2.159 \text{ Qn/S}^{0.5})^{3/8}$	
D =	3.74 ft
D =	44.872 in
A =	10.98 ft ²
Proposed Size =	1-48" RCP



CD-13 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 26 cfs Design Flow: 42 cfs Maximum Flow: 51 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-13

Headwater Elevation (ft)	Total Discharge (cfs)	CD-13 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
56.19	26.00	26.00	0.00	1
56.23	28.50	28.50	0.00	1
56.27	31.00	31.00	0.00	1
56.32	33.50	33.50	0.00	1
56.36	36.00	36.00	0.00	1
56.42	38.50	38.50	0.00	1
56.47	41.00	41.00	0.00	1
56.50	42.00	42.00	0.00	1
56.59	46.00	46.00	0.00	1
56.66	48.50	48.50	0.00	1
56.73	51.00	51.00	0.00	1
64.50	173.94	173.94	0.00	Overtopping

Rating Curve Plot for Crossing: CD-13



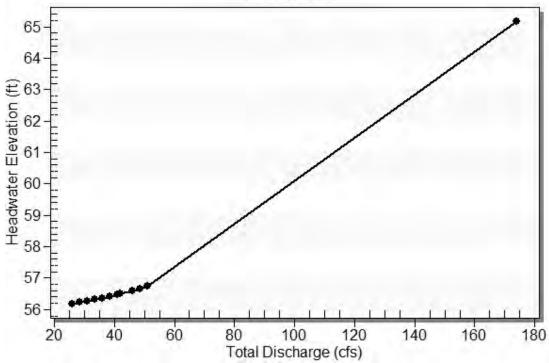


Table 2 - Culvert Summary Table: CD-13

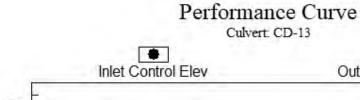
Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
26.00	26.00	56.19	2.106	4.190	4-FFf	1.774	1.503	4.000	4.000	2.069	0.000
28.50	28.50	56.23	2.233	4.228	4-FFf	1.870	1.578	4.000	4.000	2.268	0.000
31.00	31.00	56.27	2.354	4.270	4-FFf	1.964	1.647	4.000	4.000	2.467	0.000
33.50	33.50	56.32	2.471	4.315	4-FFf	2.058	1.718	4.000	4.000	2.666	0.000
36.00	36.00	56.36	2.583	4.364	4-FFf	2.150	1.786	4.000	4.000	2.865	0.000
38.50	38.50	56.42	2.692	4.416	4-FFf	2.243	1.850	4.000	4.000	3.064	0.000
41.00	41.00	56.47	2.798	4.472	4-FFf	2.335	1.913	4.000	4.000	3.263	0.000
42.00	42.00	56.50	2.840	4.496	4-FFf	2.372	1.937	4.000	4.000	3.342	0.000
46.00	46.00	56.59	3.002	4.594	4-FFf	2.524	2.030	4.000	4.000	3.661	0.000
48.50	48.50	56.66	3.100	4.661	4-FFf	2.621	2.086	4.000	4.000	3.860	0.000
51.00	51.00	56.73	3.197	4.731	4-FFf	2.720	2.139	4.000	4.000	4.058	0.000

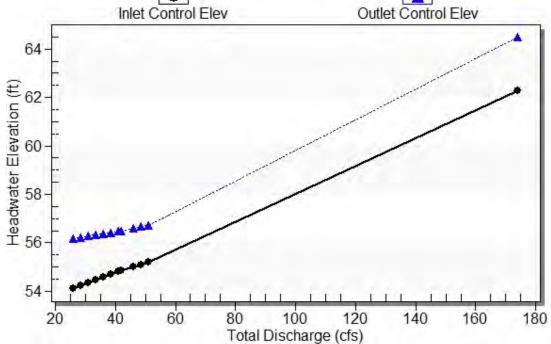
Straight Culvert

Inlet Elevation (invert): 52.00 ft, Outlet Elevation (invert): 51.50 ft

Culvert Length: 325.00 ft, Culvert Slope: 0.0015

Culvert Performance Curve Plot: CD-13

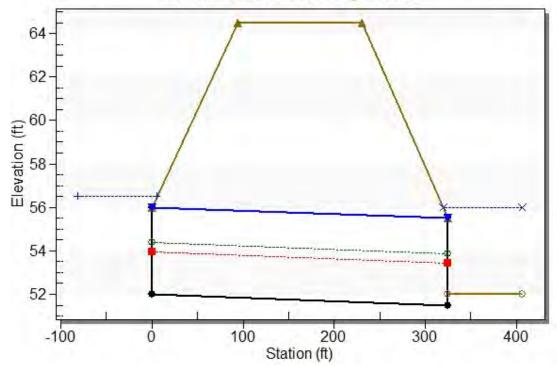




Water Surface Profile Plot for Culvert: CD-13

Crossing - CD-13, Design Discharge - 42.0 cfs

Culvert - CD-13, Culvert Discharge - 42.0 cfs



Site Data - CD-13

Site Data Option: Culvert Invert Data

Inlet Station: 0.00 ft
Inlet Elevation: 52.00 ft
Outlet Station: 325.00 ft
Outlet Elevation: 51.50 ft
Number of Barrels: 1

Culvert Data Summary - CD-13

Barrel Shape: Circular
Barrel Diameter: 4.00 ft
Barrel Material: Concrete
Embedment: 0.00 in

Barrel Manning's n: 0.0120 Culvert Type: Straight

Inlet Configuration: Square Edge with Headwall

Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-13)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
26.00	56.00	4.00
28.50	56.00	4.00
31.00	56.00	4.00
33.50	56.00	4.00
36.00	56.00	4.00
38.50	56.00	4.00
41.00	56.00	4.00
42.00	56.00	4.00
46.00	56.00	4.00
48.50	56.00	4.00
51.00	56.00	4.00

Tailwater Channel Data - CD-13

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 56.00 ft

Roadway Data for Crossing: CD-13

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft Crest Elevation: 64.50 ft Roadway Surface: Paved

Roadway Top Width: 136.00 ft

Appendix: H

Design Aids

FDOT Drainage Manual

4.3 DESIGN FREQUENCY

4.3.1 Permanent Facilities

Standard design frequencies for permanent culverts, bridge-culverts, and bridges are as follows:

Effective: January 2018

Table 4.1: Design Storm Frequencies of Permanent Facilities

FACILITY	FREQUENCY
Mainline Interstate	50 years
High Use or Essential: Projected 20-year AADT* > 1,500	50 years
Other: Projected 20-year AADT* < 1,500	25 years
Roadside ditch culvertsPedestrian and trail bridges	10 years

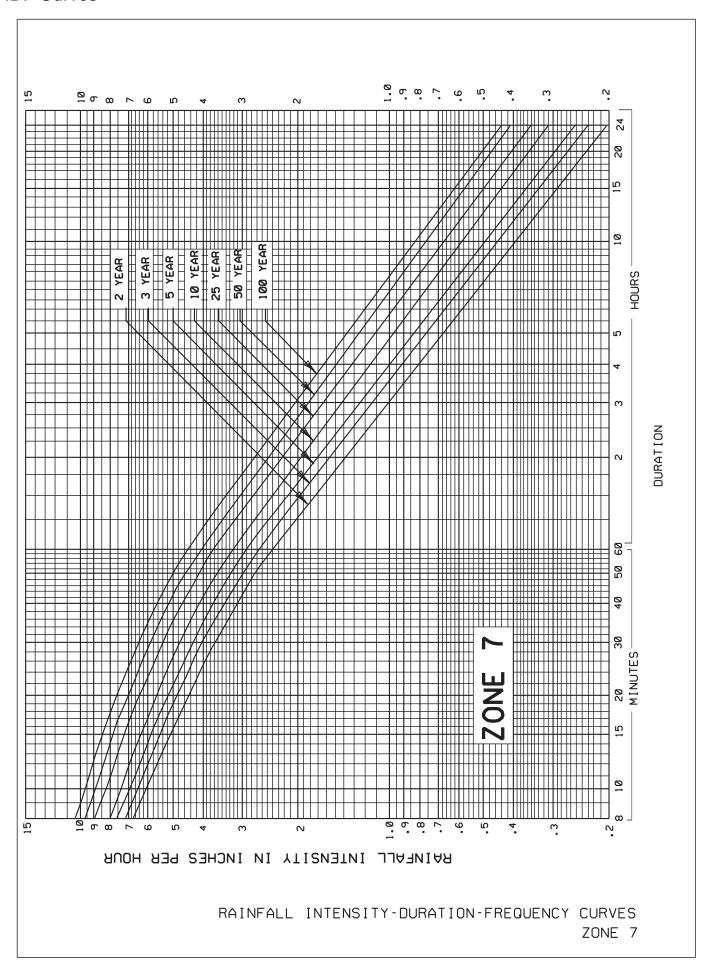
^{*} AADT preferred but if not available ADT may be used.

Note: The flood frequencies used for scour analysis differ. See **Section 4.9.2**.

4.3.2 Temporary Facilities

Design temporary traversing works accounting for the permitted duration of the work. Temporary traversing work will cause no more than a one-foot increase in the Design Storm Frequency (DSF) flood elevation immediately upstream and no more than one tenth of a foot increase in the DSF flood elevation 500 feet upstream.

Minimum standard design frequencies for temporary culverts, bridge-culverts, and bridges are as follows:



FDOT Drainage Design Guide

4.7.2 Small Cross Drains

This information applies to cross drains having an area of opening up through a 48-inchdiameter round culvert or the equivalent.

Conduct hydrologic analysis

Estimate discharges for design year frequency, base flood, and greatest flood. Use one of the following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Rational Equation (up to 600 acres)
- Regional or Local Regression Equation
- Select trial culvert size based on the following:

$$A = Q/V$$

Where:

A = Culvert area (square feet)

Q = Design discharge (e.g., 50 year)

V = Average velocity (feet per second); use an average velocity of four feet per second

- **Estimate tailwater.** If the outlet is in a free-flowing condition, the crown of the pipe at the outlet may be assumed.
- Conduct hydraulic analysis using techniques provided in FHWA HDS 5. Compute headwater conditions for the selected size for the design flood, base flood, and greatest flood or overtopping flood as appropriate.
- Check hydraulic results against design standards for backwater, minimum size, and scour. If these standards are satisfied, the trial culvert size is acceptable.
- **Determine the most economical culvert size** that satisfies all standards. If the trial selected size does not satisfy all design standards, obtain a variance.
- Document as required in the Drainage Manual.

Example 4.7-3 illustrates this procedure.

Example 4.7-3—Design of Small Cross Drain

Referring back to Example 4.7-2, you determined that the two-foot x two-foot concrete box culvert should be replaced. A design frequency of 50 years was determined as the minimum for this roadway. The existing length of the two-foot x two-foot concrete box culvert was 50 feet. However, since the structure will have to be extended four feet on each side, the design length of the proposed structure will be 58 feet.

Proposed Elevations are as follows: Allowable headwater (edge of travel lane) = 104.6 ft Flow line (upstream) = 100.1 ft Flow line (downstream) = 99.7 ft

Conduct hydrologic analysis

Estimate discharges for design-year frequency, base flood, and greatest flood. Use one of following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Rational Equation (up to 600 acres)
- Regional or Local Regression Equation

Use the same discharges from Example 4.7-2:

$$Q(50) = 35 \text{ ft}^3/\text{sec}$$

 $Q(100) = 52 \text{ ft}^3/\text{sec}$
 $Q(500) = 88 \text{ ft}^3/\text{sec}$

Select trial culvert size

$$A = \frac{Q}{V} = \frac{35 \ ft^3/s}{4 \ ft/s} = 8.8 \ ft^2$$

D = 3.3 ft., so try D = 36-inch pipe and 42-inch pipe

• Conduct hydraulic analysis using FHWA HDS 5 procedures.

The hydraulic analysis would be similar to what was done in Example 4.7-1 and Example 4.7-2. A worksheet of the calculations for the 50-year frequency is shown in Figure 4.7-3. The other frequencies also would need to be analyzed for an actual project. The analysis shown in Figure 4.7-3 is for the proposed conditions.

Check hydraulic results against design standards.

Review of the worksheet in Figure 4.7-3 indicates that the roadway will not overtop for the 50-year frequency for either culvert size. There is very little difference between the 36-inch and 42 inch pipe as far as controlling headwater. Therefore, either pipe size would be adequate. However, it is recommended that the 36-inch pipe be installed since it would be slightly less in cost than the 42-inch pipe. In addition, it would be recommended that a rubble ditch lining design be installed at the outlet end due to velocities exceeding six feet per second.

• If design does not meet standards or if you can use more economical culvert size that satisfies the standards, then perform new computations for that design.

Document as required in the *Drainage Manual*.

4.7.3 Large Cross Drains

This information applies to cross drains having an area of opening greater than a 48-inch diameter pipe and less than a 20-foot bridge. The procedure for large cross drains is similar to that for small cross drains except that a greater level of effort and detail is expected in developing the hydrologic estimates and the determination of tailwater conditions.

Conduct hydrologic analysis

Estimate discharges for design-year frequency, base flood, and greatest flood. Use one of following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Frequency analysis of observed conditions
- Regional or Local Regression Equation
- Rational Equation (up to 600 acres)

The remaining steps are the same as those identified in Section 4.7.2 for small cross drains.

Table B-1: Overland Flow Manning's n Values

	<u>Value</u>	Recommended Range of Values
Concrete	0.011	0.010 - 0.013
Asphalt	0.012	0.010 - 0.015
Bare sand ^a	0.010	0.010 - 0.016
Graveled surface ^a	0.012	0.012 - 0.030
Bare clay-loam (eroded) ^a	0.012	0.012 - 0.033
Fallow (no residue) b	0.05	0.006 - 0.16
Chisel plow (<1/4 tons/acre residue)	0.07	0.006 - 0.17
Chisel plow (1/4 - 1 tons/acre residue)	0.18	0.070 - 0.34
Chisel plow (1 - 3 tons/acre residue)	0.30	0.190 - 0.47
Chisel plow (>3 tons/acre residue)	0.40	0.340 - 0.46
Disk/Harrow (<1/4 tons/acre residue)	0.08	0.008 - 0.41
Disk/Harrow (1/4 - 1 tons/acre residue)	0.16	0.100 - 0.25
Disk/Harrow (1 - 3 tons/acre residue)	0.25	0.140 - 0.53
Disk/Harrow (>3 tons/acre residue)	0.30	
No till (4 tons/acre residue)</td <td>0.04</td> <td>0.030 - 0.07</td>	0.04	0.030 - 0.07
No till (1/4 - 1 tons/acre residue)	0.07	0.010 - 0.13
No till (1 - 3 tons/acre residue)	0.30	0.160 - 0.47
Plow (Fall)	0.06	0.020 - 0.10
Coulter	0.10	0.050 - 0.13
Range (natural)	0.13	0.010 - 0.32
Range (clipped)	0.08	0.020 - 0.24
Grass (bluegrass sod)	0.45	0.390 - 0.63
Short grass prairie ^a	0.15	0.100 - 0.20
Dense grass ^c	0.24	0.170 - 0.30
Bermuda grass ^c	0.41	0.300 - 0.48
Woods	0.45	

All values are from Engman (1983), unless noted otherwise.

Note: These values were determined specifically for overland flow conditions and are not appropriate for conventional open channel flow calculations. See Chapter 3, for open channel flow procedures.

^aWoolhiser (1975).

^bFallow has been idle for one year and is fairly smooth.

^CPalmer (1946). Weeping love grass, bluegrass, buffalo grass, blue gamma grass, native grass mix (OK), alfalfa, lespedeza.

Table B-5: Design Storm Frequency Factors for Pervious Area Runoff Coefficients*

Return Period (years)	Design Storm $\underline{Frequency Factor, X_T}$
2 to 10	1.0
25	1.1
50	1.2
100	1.25

Reference: Wright-McLaughlin Engineers (1969).

^{*} DUE TO THE INCREASE IN THE DURATION TIME THAT THE PEAK OR NEAR PEAK DISCHARGE RATE IS RELEASED FROM STORMWATER MANAGEMENT SYSTEMS, THE USE OF THESE SHORT DURATION PEAK RATE DISCHARGE ADJUSTMENT FACTORS IS NOT APPROPRIATE FOR FLOOD ROUTING COMPUTATIONS.

Appendix: I

Big Econ River Basin Stormwater Management Master Plan

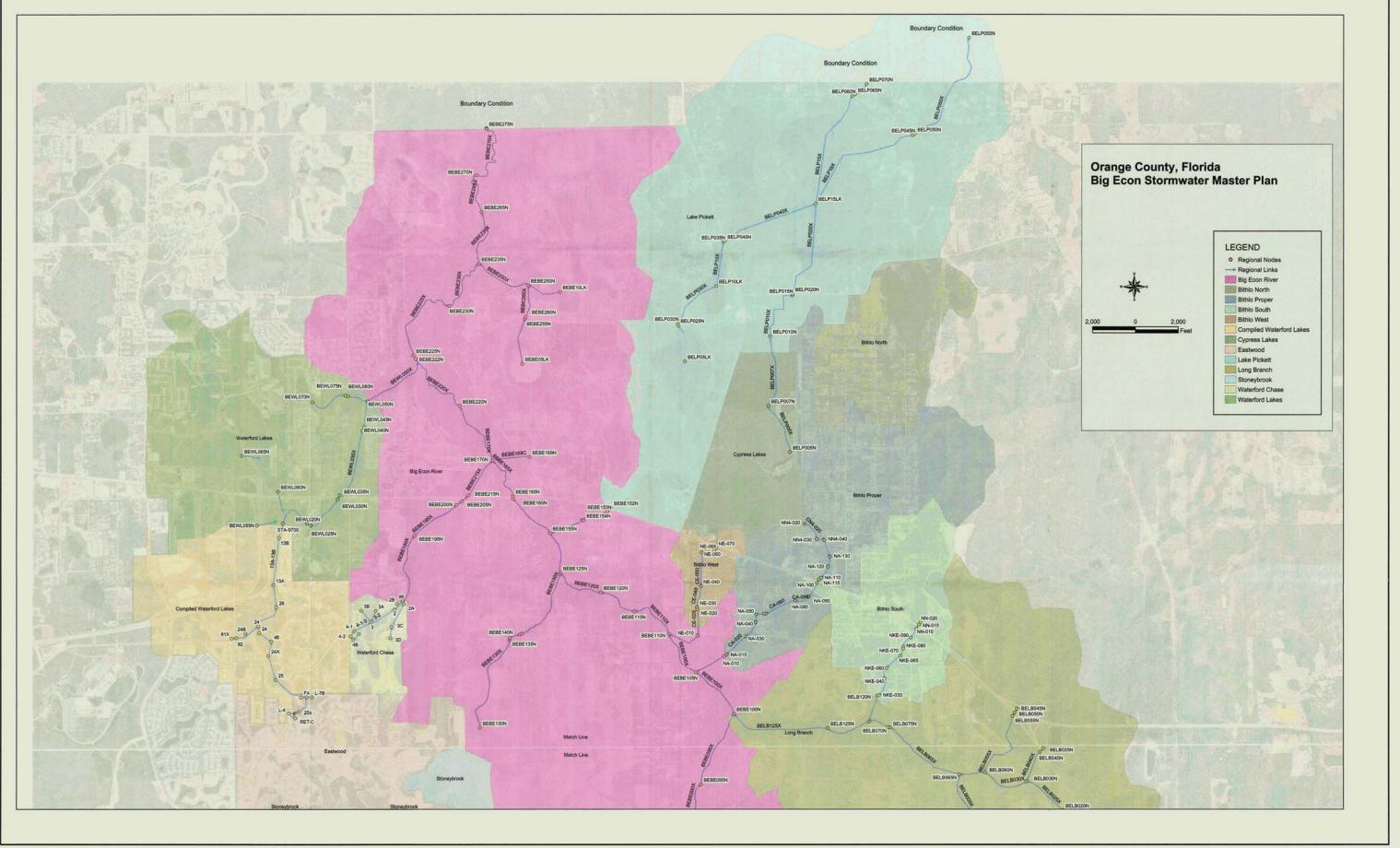


Table 5-1
Big Econ Stormwater Management Master Plan
Orange County, Florida
Existing Conditions Results

Model ID BEBE010C		D/S Node	Critical Elevation			Mean Ann	ual	10 Year - 24 Hour				1.00	25 Year - 24	Hour	ALC: Y	100 Year - 2					
	U/S Node			Location	U/S Stage ³	D/S Stage	Flooding	Flow ²	U/S Stage	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow	Comments
	BEBE010N		65.8	Wewahootee Road	62.4	61.8		89	63.9	62.3		170	64.5	62.4		197	65.2	62.5	-	224	
EBE011C	BEBE010N	BEBE015N	65.8	Wewahootee Road	62.4	61.8	1000	172	63.9	62.3	-	347	64.5	62.4		416	65.2	62.5	1	498	
EBE010W	BEBE010N	BEBE015N	65.8	Wewahoolee Road - Overflow	62.4	61.8		0	63.9	62.3	1.00	0	64.5	62.4		0	65.2	62.5		0	
EBE015X	BEBE015N	BEBE020N	57.6	TO SHALL HAVE COME TO SHALL SH	61.8	55.2		393	62.3	56.8	12.00	732	62,4	57.3	1 2	863	62.5	58.1	0.5	1011	
EBE020X	BEBE020N	BEBE025N	62.1	Beeline Bridge Equivalent	55.2	55.2	1	998	56.8	56.8		1967	57.3	57.3		2338	58.1	58.1	-	3067	
EBE020W	BEBE020N	BEBE025N	62,15	Beeline - Overflow	55.2	55.2		0	56.8	56.8	4	0	57.3	57.3		0	58.1	58.1		0	
	BEBE025N	BEBE030N	56.6	Dealine - Overnow	55.2	53.8		992	56.8	55.8		1931	57.3	56.4	-	2291	58.1	57,2	0.5	3023	
BEBE025X BEBE030X	BEBE030N	BEBE035N	57.4		53.8	53.6		971	55.8	55.7		1861	56.4	56.3		2186	57.2	57.0	0.0	2961	
			50.2		53.6	52.5	2.3	2300	55.7	54.8	4.6	4418	56.3	55.4	5.2	5169	57.0	56.1	5.9	6007	Hal Scott - flooding not a problem
SEBE035X	BEBE035N				52.5	52.1	2.3	2371	54.8	54.2	4.4	4758	55.4	54.8	5.0	5638	56.1	55.5	5.7	6735	
BEBE040X	BEBE040N	BEBE045N	49.8		52.1	45.5	2.0	2519	54.2	48.1		5187	54.8	48.8	0.5		55.5	49.8			Hal Scott - flooding not a problem
BEBE045X	BEBE045N	BEBE050N	48.3													6181			1.5	7516	Hal Scott - flooding not a problem
BEBE050X	BEBE050N	BEBE055N	47		45.5	44.7	4.5	2529	48.1	47.4	0.4	5310	48.8	48.1	1.1	6360	49.8	49.2	2.2	7843	Hal Scott - flooding not a problem
BEBE055X	BEBE055N	BEBE060N	43.1		44.7	44.6	1.5	2813	47.4	47.2	4.1	5700	48.1	47.9	4.8	6883	49.2	49.0	5.9	8642	Hal Scott - flooding not a problem
BEBE05X	BEBEO5LK	BEBE255N	49.2		47.6	46.3		18	48.4	47.5		48	48.7	47.8	10.5	60	49.2	48.5		83	Hal Scott - flooding not a problem
BEBE060X	BEBE060N		37.4		44.6	44.6	7.2	2967	47.2	47.2	9.8	6150	47.9	47.9	10.5	7360	49.0	49.0	11.6	9211	Hal Scott - flooding not a problem
EBE065C	BEBE065N	BEBE070N	44.7	Powerline Bridge Equivalent	44.6	44.5	×	178	47.2	47.2	2.5	186	47.9	47.9	3.2	188	49.0	49.0	4.3	159	Hal Scott - flooding not a problem
EBE065W	BEBE065N	BEBE070N	44.7	Powerline Overflow	44.6	44.5		0	47.2	47.2	2.5	419	47.9	47.9	3.2	492	49.0	49.0	4.3	542	Hal Scott - flooding not a problem
EBE065X	BEBE065N	BEBE070N	44.7		44.6	44.5		2779	47.2	47.2	2.5	5606	47.9	47,9	3.2	6766	49.0	49.0	4.3	8661	Hal Scott - flooding not a problem
EBE070X	BEBE070N	BEBE075N	44.8		44.5	44.4	-	2900	47.2	47.0	2.2	6086	47.9	47.8	3.0	7302	49.0	48.8	4.0	9145	Hal Scott - flooding not a problem
EBE075X	BEBE075N	BEBE080N	43.4		44.4	44.1	0.7	3025	47.0	46.6	3.2	6435	47.8	47.3	3.9	7783	48.8	48.4	5.0	9697	Floodplain of Big Econ
EBE080X	BEBE080N	BEBE085N	42.9		44.1	43.9	1.0	2957	46.6	46.4	3.5	6390	47.3	47.1	4.2	7736	48.4	48.2	5.3	9579	Floodplain of Big Econ
BEBE085X	BEBE085N	BEBE090N	42.8		43.9	43.6	0.8	2904	46.4	46.1	3.3	6358	47.1	46.8	4.0	7719	48.2	47.9	5.1	9566	Floodplain of Big Econ
BEBE090X	BEBE090N	BEBE095N	40.6		43.6	43.3	2.7	2862	46.1	45.6	5.0	6437	46.8	46.3	5.7	7852	47.9	47.4	6.8	9855	Floodplain of Blg Econ
BEBE095X	BEBE095N	BEBE100N	40.7		43.3	41.1	0.4	2824	45.6	43.7	3.0	6355	46.3	44.6	3.9	7724	47.4	46.1	5.3	9761	Floodplain of Big Econ
SEBE100X	BEBE100N	BEBE105N	38.4		41.1	40.5	2.1	2852	43.7	43.1	4.7	6497	44.6	43.9	5.5	7943	46.1	45.5	7.1	10316	Floodplain of Big Econ
BEBE105X	BEBE 105N	BEBE110N	39.3		40.5	39.6	0.3	2879	43.1	42.2	2.9	6567	43.9	43.2	3.9	8029	45.5	44.9	5.6	10462	Floodplain of Big Econ
BEBE10X	BEBE10LK	BEBE250N	41.7		45.3	39.7		35	46.3	40.5		93	46.6	40.8		118	47.1	41.6	1 2	173	
BEBE110X	BEBE110N	BEBE115N	37.8		39.6	39.1	1.3	2866	42.2	41.7	3.9	6510	43.2	42.8	5.0	7969	44.9	44.6	6.8	10388	Floodplain of Big Econ
SEBE115X	BEBE115N	BEBE120N	38		39.1	37.9		2855	41.7	41.1	3.1	6453	42.8	42.2	4.2	7909	44.6	44.2	6.2	10322	Floodplain of Big Econ
	BEBE120N	BEBE125N	37.9		37.9	37.7		2832	41.1	40.9	3.0	6379	42.2	42.0	4.1	7840	44.2	44.0	6.1	10295	Floodplain of Big Econ
SEBE120X			35.1		37.7	36.6	1.5	2812	40.9	40.3	5.2	6312	42.0	41.5	6.4	7792	44.0	43.6	8.5	10364	Floodplain of Big Econ
BEBE125X	BEBE125N				72.4	51.9	1.5	117	72.7	53.8	3,2	233	72.8	54.2	0.4	277	72.9	55.2	0,5	360	Produpiain of Big Econ
SEBE130X		BEBE135N	61.8	Scotlanda Trail Establica	51.9	51.5	-	109	53.8	53.0	0.4	207	54.2	53.8	0.8	209	55.2	55.2	1.8	208	Dealles Assaula Confirm 7 II
BEBE135C	BEBE135N		53.4	Sunflower Trail Extension		51.5	-							53.8				55.2			Problem Area 12 - Sunflower Trail
BEBE135W	BEBE135N		53.4	Sunflower Trail - Overflow	51.9			0	53.8	53.0	0.4	59	54.2		0.8	154	55.2		1.8	301	Problem Area 12 - Sunflower Trail
BEBE145C	BEBE145N	BEBE150N	55.8	Sunflower Trail	51.5	50.5	-	140	53.0	51.2	-	284	53.8	51,3		343	55.2	51.5		420	
BEBE145W	BEBE145N		55.8	Sunflower Trail - Overflow	51.5	50.5		0	53.0	51.2	-	0	53.8	51.3		0	55.2	51.5		0	
BEBE150X	BEBE150N		37.9		50.5	37.7	-	139	51.2	40.9	3.0	283	51.3	42.0	4.1	342	51.5	44.0	6.1	420	Floodplain of Big Econ
BEBE152C	BEBE152N		62	State Road 50	59.6	57.4		84	60.6	58.3		200	61.1	58.4		200	61.9	58.6		201	
BEBE152W	BEBE152N	BEBE153N	62	State Road 50 - Overflow	59.6	57.4		0	60.6	58.3		0	61.1	58.4	100	0	61.9	58.6	1	0	
BEBE153X	BEBE153N	BEBE154N	52		57.4	50.8		128	58.3	53.6	1.6	171	58.4	53.7	1.7	180	58.6	53.7	1.7	200	Floodplain of Big Econ Tributary
BEBE154C	BEBE154N	BEBE155N	54	Old Cheney Highway	50.8	36.6	1	84	53.6	40.3		152	53.7	41.5	1	153	53.7	43.6		154	
BEBE154W	BEBE154N	BEBE155N	54	Old Cheney - Overflow	50.8	36.6		0	53.6	40.3		19	53.7	41.5		27	53.7	43.6		45	
BEBE155X	BEBE155N	BEBE160N	32.7		36.6	36.5	3.8	2780	40.3	40.1	7.4	6250	41.5	41.3	8.6	7742	43.6	43.3	10.6	10366	Floodplain of Big Econ
BEBE160X	BEBE160N	BEBE165N	44.7	SR 50 Bridge Equivalent	36.5	36,4		2763	40.1	40.1		6220	41.3	41.3		7716	43.3	43.3	1	10360	
BEBE160W	BEBE160N	BEBE165N	44.6	SR 50 Bridge - Overflow	36.5	36.4		0	40.1	40.1	-	0	41.3	41.3		0	43.3	43.3	- 4	0	
BEBE165X	BEBE165N	BEBE170N	36.5		36.4	35.7		2752	40.1	39.6	3.1	6194	41.3	40.8	4.3	7693	43.3	42.9	6.4	10356	Floodplain of Big Econ
BEBE169C	BEBE169N	BEBE170N	41.3	South Tanner Road	35.7	35.7	1	167	40.3	39.6		291	41.6	40.8	0.3	266	42.9	42.9	1.6	171	Overtopping due largely to tailwater in
BEBE169W	BEBE169N	BEBE170N	41.3	South Tanner - Overflow	35.7	35.7		0	40.3	39.6	700	0	41.6	40.8	0.3	49	42.9	42.9	1.6	299	Overtopping due largely to tailwater in
BEBE170X	BEBE170N	BEBE220N	31.7		35.7	35.4	3.7	2711	39.6	39.3	7.6	6121	40.8	40.5	8.8	7620	42.9	42.7	11.0	10338	Floodplain of Big Econ
4A-4B	4A	4B	65.4	Waterford Chase Parkway - d/s of pond 4A	64.9	64.9	1	4	65.5	65.3	0.1	9	65.7	65.4	0.3	12	66.1	65.5	0.7	17	Problem Area 10 - Maple Creek Driv
4B-4-2	4B	4-2	66.5	Control structure out of pond 4-B	64.9	63.6	100	0	65.3	64.3		11	65.4	64.7		16	65.5	65.4		24	The state of the s
4-1-4-2	4-1	4-2	66.5	Waterford Chase Parkway - d/s wetland 4-2	63.6	63.6		0	64.3	64.3		0	64.6	64.7		0	65.2	65.4		0	
4-1-3	4-1	3	66	Drop structure - Maple Creek Drive	63.6	63.6		2	64.3	64.1	-	8	64.6	64.3	-	10	65.2	64.6		12	
3-2	3	2	66.5	Oak Chase Drive	63.6	63.6		20	64.1	64.0	-	42	64.3	64.2		61	64.6	64.4		96	
	2	BEBE190N		Waterford Chase outfall	63.6	59.4		10	64.0	59.9	-	16	64.2	60.1	-	17	64.4	60.4	-	19	
2-99		BEBE190N	66	Waterford Chase outfall Waterford Chase outfall	63.6	59.4	· ·	2	64.0	59.9	- : ·	27	64.2	60.1	-	38	64.4	60.4	-	48	
2-99A	2			Waterford Chase outfall	63.6	59.4	-	0	64.0	59.9	-	0	64.2	60.1		7	64.4	60.4	-	30	
2-99B	2	BEBE190N		wateriord Chase outrail																	FIGURE TO F
BEBE190X	BEBE190N				59.4	54.6	2.1	108	59.9	54.7	2.2	252	60.1	54.8	2.3	311	60.4	54.8	2.3	419	Floodplain of Big Econ Tributary
	BEBE195N		47,8		54.6	46.5		169	54.7	47.8	0.0	301	54.8	48.3	0.5	370	54.8	49.3	1.5	496	Floodplain of Big Econ Tributary
	BEBE200N		49.5	Old Cheney Highway Bridge Equivalent	46.5	44.7		258	47.8	45.2	1 1000	513	48.3	45.7		621	49.3	47.5		817	
BEBE200W		BEBE205N		Old Cheney - Overflow	46.5	44.7		0	47.8	45.2		0	48.3	45.7		0	49.3	47.5		0	
		BEBE215N		SR 50	44.7	44.6		353	45.2	45.0	91	512	45.7	45.4		621	47.5	47.1		807	
BEBE210W	BEBE205N	BEBE215N		SR 50 - Overflow	44.7	44.6		0	45.2	45.0		0	45.7	45.4		0	47.5	47.1		0	
BEBE215X	BEBE215N	BEBE170N	36.5		44.6	35.7		403	45.0	39.6	3.1	512	45.4	40.8	4.3	621	47.1	42.9	6.4	805	Floodplain of Big Econ Tributary
BEBE220X	BEBE220N	BEBE222N	34.6		35,4	34.8	0.2	2676	39.3	38.9	4.3	6051	40.5	40.1	5.5	7568	42.7	42.3	7.7	10318	Floodplain of Big Econ
BEBE222X		BEBE225N		Lake Pickett Bridge Equivalent	34.8	34.8		2724	38.9	38.9	J. E. W. St.	6137	40.1	40.1		7792	42.3	42.3	-	10408	
		BEBE225N		Lake Pickett - Overflow	34.8	34.8		0	38.9	38.9	A	0	40.1	40.1		0	42.3	42.3	0.9	194	Floodplain of Big Econ
BEBE225X		BEBE230N			34,8	32.5		2723	38.9	35.9		6135	40.1	37.6		7700	42.3	40.5	2.2	10601	Floodplain of Big Econ
		BEBE235N			32,5	32.2	1 2 2	2719	35.9	35.6		6129		37.3		7696	40.5	40.3	-	10600	i waspinit of big boot
UEDEZJUA	DEDESOUN	I DEDESON	1 417		02,0	JEIL		47.10	00.0	00.0		0120	41.0	27,0		1.000	1010	10.0		1 .0000	

Notes:

1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels.

2) Flow taken from Link Maximum Conditions Report (cfs)

3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Table 5-1
Big Econ Stormwater Management Master Plan
Orange County, Florida
Existing Conditions Results

Model ID BEBE010C			D/S Node	Critical Elevation ¹			Mean Ann	nual		10 7 6 3	10 Year - 24	Hour	20		25 Year - 24	Hour		15.77	100 Year - 2	4 Hour	7, 27	
	U/S No	lode			Location	U/S Stage ³	D/S Stage	Flooding	Flow ²	U/S Stage	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow	Comments
	BEBEC	_	BEBE015N	65.8	Wewahootee Road	62.4	61.8		89	63.9	62.3	- X	170	64.5	62.4		197	65.2	62.5		224	
BEBE011C	BEBEC		BEBE015N	65.8	Wewahootee Road	62.4	61.8	100	172	63.9	62.3	-	347	64.5	62.4		416	65.2	62.5		498	
EBE010W	BEBEC	010N	BEBE015N	65.8	Wewahootee Road - Overflow	62.4	61.8		0	63.9	62.3	1 191 1	0	64.5	62.4		0	65.2	62.5		0	
SEBE015X	BEBEC	015N I	BEBE020N	57.6		61.8	55.2		393	62.3	56.8	9-5	732	62,4	57.3	- 2-	863	62.5	58,1	0.5	1011	
BEBE020X	BEBEC	020N	BEBE025N	62.1	Beeline Bridge Equivalent	55,2	55.2		998	56.8	56.8		1967	57.3	57.3		2338	58.1	58.1		3067	
EBE020W	BEBEC	020N	BEBE025N	62,15	Beeline - Overflow	55.2	55.2		0	56.8	56.8		0	57.3	57.3		0	58.1	58.1	100	0	
EBE025X	BEBEC	025N	BEBE030N	56.6		55.2	53.8	-	992	56.8	55.8	6	1931	57.3	56.4		2291	58.1	57.2	0.5	3023	
BEBE030X	BEBE		BEBE035N	57.4		53.8	53.6	1 A7 41	971	55.8	55.7	the Table Print	1861	56.4	56.3		2186	57.2	57.0	- A-	2961	
BEBE035X	BEBE	035N	BEBE040N	50.2		53.6	52.5	2.3	2300	55.7	54.8	4.6	4418	56.3	55.4	5.2	5169	57.0	56.1	5.9	6007	Hal Scott - flooding not a problem
BEBE040X	BEBE	_	BEBE045N	49.8		52.5	52.1	2.3	2371	54.8	54.2	4.4	4758	55.4	54.8	5.0	5638	56.1	55.5	5.7	6735	Hal Scott - flooding not a problem
BEBE045X	BEBE		BEBE050N	48.3		52.1	45.5		2519	54.2	48.1		5187	54.8	48.8	0.5	6181	55.5	49.8	1.5	7516	Hal Scott - flooding not a problem
BEBE050X	BEBE		BEBE055N	47		45.5	44.7	100	2529	48.1	47.4	0.4	5310	48.8	48.1	1.1	6360	49.8	49.2	2.2	7843	Hal Scott - flooding not a problem
BEBE055X	BEBE		BEBE060N	43.1		44.7	44.6	1.5	2813	47.4	47.2	4.1	5700	48.1	47.9	4.8	6883	49.2	49.0	5.9	8642	Hal Scott - flooding not a problem
BEBE05X	BEBE		BEBE255N	49.2		47.6	46.3		18	48.4	47.5	1	48	48.7	47.8		60	49.2	48.5	1	83	Hal Scott - flooding not a problem
BEBE060X	BEBE		BEBE065N	37.4		44.6	44.6	7.2	2967	47.2	47.2	9.8	6150	47.9	47.9	10.5	7360	49.0	49.0	11.6	9211	Hal Scott - flooding not a problem
BEBE065C	BEBE		BEBE070N	44.7	Powerline Bridge Equivalent	44.6	44.5	- × -	178	47.2	47.2	2.5	186	47.9	47.9	3.2	188	49.0	49.0	4.3	159	Hal Scott - flooding not a problem
EBE065W	BEBE		BEBE070N	44.7	Powerline Overflow	44.6	44.5		0	47.2	47.2	2.5	419	47.9	47.9	3.2	492	49.0	49.0	4.3	542	Hal Scott - flooding not a problem
BEBE065X	BEBE		BEBE070N	44.7		44.6	44.5		2779	47.2	47.2	2.5	5606	47.9	47.9	3.2	6766	49.0	49.0	4.3	8661	Hal Scott - flooding not a problem
BEBE070X	BEBE		BEBE075N	44.8		44.5	44.4		2900	47.2	47.0	2.2	6086	47.9	47.8	3.0	7302	49.0	48.8	4.0	9145	Hal Scott - flooding not a problem
BEBE075X	BEBE		BEBE080N	43.4		44.4	44.1	0.7	3025	47.0	46.6	3.2	6435	47.8	47.3	3.9	7783	48.8	48.4	5.0	9697	Floodplain of Big Econ
SEBE080X	BEBE		BEBE085N	42.9		44.1	43.9	1.0	2957	46.6	46.4	3.5	6390	47.3	47.1	4.2	7736	48.4	48.2	5.3	9579	Floodplain of Big Econ
BEBE085X	BEBE		BEBE090N	42.8		43.9	43.6	0.8	2904	46.4	46.1	3.3	6358	47.1	46.8	4.0	7719	48.2	47.9	5.1	9566	Floodplain of Big Econ
BEBE090X	BEBE		BEBE095N	40.6	·	43.6	43.3	2.7	2862	46.1	45.6	5.0	6437	46.8	46.3	5.7	7852	47.9	47.4	6.8	9855	Floodplain of Big Econ
BEBE095X	BEBE		BEBE100N	40.7		43.3	41.1	0.4	2824	45.6	43.7	3.0	6355	46.3	44.6	3.9	7724	47.4	46.1	5.3	9761	Floodplain of Big Econ
BEBE100X	BEBE		BEBE105N	38.4	-	41.1	40.5	2.1	2852	43.7	43.1	4.7	6497	44.6	43.9	5.5	7943	46.1	45.5	7.1	10316	
BEBE105X	BEBE		BEBE110N	39.3		40.5	39.6	0.3	2879	43.1	42.2	2.9	6567	43.9	43.2	3.9	8029	45.5	44.9	5.6	10462	
	BEBE		BEBE250N	41.7		45.3	39.7		35	46.3	40.5		93	46.6	40.8	- 0.0	118	47.1	41.6	5.0	173	1 loddplair of big Econ
BEBE10X			BEBE115N			39.6	39.1	1.3	2866	42.2	41.7	3.9	6510	43.2	42.8	5.0	7969	44.9	44.6	6.8	10388	Floodplain of Big Econ
BEBE110X	BEBE	_	BEBE110N	38		39.1	37.9	1.5	2855	41.7	41.1	3.1	6453	42.8	42.2	4.2	7909	44.6	44.2	6.2	10322	Floodplain of Big Econ
BEBE115X	-			37.9		37.9	37.7	-	2832	41,1	40.9	3.0	6379	42.2	42.0	4.1	7840	44.2	44.0	6.1	10295	
BEBE120X	BEBE	_	BEBE125N			37.7	36.6	1.5	2812	40.9	40.3	5.2	6312	42.0	41.5	6.4	7792	44.0	43.6	8.5	10364	Floodplain of Big Econ
BEBE125X	BEBE		BEBE155N			72.4	51.9	1.5	117	72.7	53.8	3.2	233	72.8	54.2	0.4	277	72.9	55.2	0.5	360	Floodplain of Big Econ
BEBE130X	BEBE		BEBE135N		Cualitatives Trail Education	51.9	51.5	-	109	53.8	53.0	-	207	54.2	53.8	0.8	209	55.2	55.2	1.8	208	Dealles Assaula Confessor T. II
BEBE135C	BEBE		BEBE145N		Sunflower Trail Extension	51.9	51.5			53.8		0.4						55.2			_	Problem Area 12 - Sunflower Trail
BEBE135W	BEBE		BEBE145N		Sunflower Trail - Overflow				0		53.0		59	54.2	53.8	0.8	154		55.2	1.8	301	Problem Area 12 - Sunflower Trail
BEBE145C	BEBE		BEBE150N		Sunflower Trail	51.5	50.5		140	53.0	51.2	-	284	53.8	51,3		343	55.2	51.5		420	
BEBE145W	BEBE	_	BEBE150N		Sunflower Trail - Overflow	51.5	50.5	-	0	53.0	51.2	-	0	53.8	51.3		0	55.2	51.5	-	0	
BEBE150X	BEBE	-	BEBE125N		200 5 350	50.5	37.7		139	51.2	40.9	3.0	283	51,3	42.0	4.1	342	51.5	44.0	6.1	420	Floodplain of Big Econ
BEBE152C	BEBE		BEBE153N	62	State Road 50	59.6	57.4		84	60.6	58.3	-	200	61.1	58.4	•	200	61.9	58.6		201	
BEBE152W			BEBE153N		State Fload 50 - Overflow	59.6	57.4		0	60.6	58.3		0	61.1	58.4	1	0	61.9	58.6		0	
BEBE153X	BEBE		BEBE154N			57.4	50.8		128	58.3	53.6	1.6	171	58.4	53.7	1.7	180	58.6	53.7	1.7	200	Floodplain of Big Econ Tributary
BEBE154C	BEBE	_	BEBE155N		Old Cheney Highway	50.8	36.6		84	53.6	40.3	*	152	53.7	41.5		153	53.7	43.6	-	154	
BEBE154W	BEBE		BEBE155N	54	Old Cheney - Overflow	50.8	36.6		0	53.6	40.3		19	53.7	41.5		27	53.7	43,6	1	45	
BEBE155X	BEBE	_	BEBE 160N			36.6	36.5	3.8	2780	40.3	40.1	7.4	6250	41.5	41.3	8.6	7742	43.6	43.3	10.6	10366	Floodplain of Big Econ
BEBE160X	BEBE		BEBE165N	44.7	SR 50 Bridge Equivalent	36.5	36,4		2763	40.1	40.1		6220	41.3	41.3		7716	43.3	43.3		10360	
BEBE160W	BEBE	160N	BEBE165N	44.6	SR 50 Bridge - Overflow	36,5	36.4		0	40.1	40.1		0	41.3	41,3		0	43.3	43.3	* -	0	
BEBE165X	BEBE		BEBE170N	36.5		36.4	35.7		2752	40.1	39.6	3.1	6194	41.3	40.8	4.3	7693	43.3	42.9	6.4	10356	Floodplain of Big Econ
BEBE169C	BEBE	169N	BEBE170N		South Tanner Road	35.7	35.7		167	40.3	39.6		291	41.6	40.8	0.3	266	42.9	42.9	1.6	171	Overtopping due largely to tailwater in E
BEBE169W	BEBE		BEBE170N		South Tanner - Overflow	35.7	35.7		0	40.3	39.6	300	0	41.6	40.8	0.3	49	42.9	42.9	1.6	299	Overtopping due largely to tailwater in B
BEBE170X	BEBE	170N	BEBE220N			35.7	35.4	3.7	2711	39.6	39.3	7.6	6121	40.8	40.5	8.8	7620	42.9	42.7	11.0	10338	Floodplain of Big Econ
4A-4B	4.	A	4B	65.4	Waterford Chase Parkway - d/s of pond 4A	64.9	64.9		4	65.5	65.3	0.1	9	65.7	65.4	0.3	12	66.1	65.5	0.7	17	Problem Area 10 - Maple Creek Drive
4B-4-2	4	В	4-2	66.5	Control structure out of pond 4-B	64.9	63.6		0	65.3	64.3		_ 11	65.4	64.7		16	65.5	65.4		24	
4-1-4-2	4-	-1	4-2	66.5	Waterford Chase Parkway - d/s wetland 4-2	63.6	63.6		0	64.3	64.3		0	64.6	64.7	,	0	65.2	65.4		0	
4-1-3	4-	-1	3	66	Drop structure - Maple Creek Drive	63.6	63.6	1	2	64.3	64.1		8	64.6	64.3	-	10	65.2	64.6	-	12	
3-2	1 3	3	2	66.5	Oak Chase Drive	63.6	63.6		20	64.1	64.0		42	64.3	64.2	-	61	64.6	64.4		96	
2-99	1 2	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4		10	64.0	59.9		16	64.2	60.1		17	64.4	60.4	E 1700 P	19	
2-99A			BEBE190N		Waterford Chase outfall	63.6	59.4		2	64.0	59.9		27	64.2	60.1		38	64.4	60.4		48	
2-99B			BEBE190N		Waterford Chase outfall	63.6	59.4		0	64.0	59.9	1.0	0	64.2	60.1	-	7	64.4	60.4		30	
			BEBE195N			59.4	54.6	2.1	108	59.9	54.7	2.2	252	60.1	54.8	2.3	311	60.4	54.8	2.3	419	Floodplain of Big Econ Tributary
			BEBE200N			54.6	46.5		169	54.7	47.8	0.0	301	54.8	48.3	0.5	370	54.8	49.3	1.5	496	Floodplain of Big Econ Tributary
			BEBE205N		Old Cheney Highway Bridge Equivalent	46.5	44.7		258		45.2		513		45.7		621	49.3	47.5		817	
			BEBE205N		Old Cheney - Overflow	46.5	44.7		0	47.8	45.2		0	48.3	45.7		0	49.3	47.5		0	
			BEBE215N		SR 50	44.7	44.6		353	45.2	45.0	•	512	45.7	45.4		621	47.5	47.1		807	
			BEBE215N		SR 50 - Overflow	44.7	44.6		0	45.2	45.0	-	0	45.7	45.4		0	47.5	47.1		0	
BEDESTEY	PEDE	E215N	BEBE170N	36.5	Sil 55 Stallon	44.6	35.7		403	45.0	39.6	3.1	512	45.4	40.8	4.3	621	47.1	42.9	6.4	805	Floodplain of Big Econ Tributary
BEBE220X			BEBE222N			35,4	34.8	0.2	2676	39.3	38.9	4.3	6051	40.5	40.1	5.5	7568	42.7	42.3	7.7	10318	Floodplain of Big Econ
	_		BEBE225N		Lake Pickett Bridge Equivalent	34.8	34.8	- 0.2	2724	38.9	38.9	4.5	6137	40.1	40.1	- 0.0	7792	42.3	42.3	7.7	10408	r souplain or olg Econ
BEBE222X					Lake Pickett - Overflow	34.8	34.8	1	0	38.9	38.9	-	0	40.1	40.1	-	0	42.3	42.3	0.9	194	Floodalate of Div Face
BEBE222W			BEBE225N		Lake Pickett - Overnow							N					_				_	Floodplain of Big Econ
BEBE225X			BEBE230N			34,8	32.5		2723		35.9		6135	40.1	37.6	-	7700	42.3	40.5	2.2	10601	Floodplain of Big Econ
BEBE230X	BEBE	E230N	BEBE235N	41.7		32,5	32.2		2719	35.9	35.6		6129	37.6	37.3		7696	40.5	40.3		10600	

Notes:

1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels.

2) Flow taken from Link Maximum Conditions Report (cfs)

3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Table 5-1 Big Econ Stormwater Management Master Plan Orange County, Florida Existing Conditions Results

	365	10000	THE PARTY OF THE	Location	Mean Annual			10 Year - 24 Hour				25 Year - 24 Hour					100 Year - 24	4 Hour			
Model ID	U/S Node	D/S Node	Critical Elevation		U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage	D/S Stage ³	Flooding	Flow ²	Comments
CH-4B	CH-4A	CH-4B	51		47.7	47.0	P1 R7	816	49.0	48.2	127.600	1769	49.9	49.3	III. TATAL	2117	50.0	49.1		2778	From Avalon Park FEMA floodplain study
CH-4C	CH-4B	CH-5	49		47.0	46.0	\$1-20°	815	48.2	47.1		1768	49.3	48.8		2116	49.1	48.8		2779	From Avalon Park FEMA floodplain study
CH-5	CH-5	CH-6	50		46.0	44.4	-	820	47.1	47.0	7 - 4 -	1775	48.8	47.8		2114	48.8	48.8		2791	From Avalon Park FEMA floodplain study
CH-6	CH-6	CH-7	50		44.4	44.4		816	47.0	47.0		1736	47.8	47.8	6 1	2047	48.8	48.8		2671	From Avalon Park FEMA floodplain study
CH-7	CH-7	BEBE075N	44.8	W. F. W. T.	44.4	44.4	-	784	47.0	47.0	2.2	1617	47.8	47.8	3.0	1886	48.8	48.8	4.0	2429	From Avalon Park FEMA floodplain study
CONS5-W	BESB050N	C1	78	Weir flow to Alafaya Trail Culverts	76.2 55.6	74.7 53.9		82 498	76.4 56.2	75.4	0.5	196	76.5	75.7		243	76.6	76.1	1.7	326	m 141 4= 15 =
BETC005X	BETCO05N	BETC020N BETC015N	55.4 62.6		73.0	64.8	2.2	1828	73.6	55.9 65.6	3.0	989 2762	56.7 73.8	56.5 65.9	3.3	1161 3132	74.1	57.1 66.4	1,7	1866	Floodplain of Turkey Creek
BETC010X BETC015X	BETC010N BETC015N	BETC020N	48.8		64.8	53.9	5.1	802	65.6	55.9	7.1	1546	65.9	56.5	7.7	1816	66.4	57.1	8.3	3864 2339	Floodplain of Turkey Creek Floodplain of Turkey Creek
BETC020X	BETC020N	BEBE035N	57.4		53.9	53.6		1047	55.9	55.7		2018	56.5	56.3	- 10	2335	57.1	57.0	4,5	2505	Ploodplain of Turkey Greek
BEWF005X	BEWF005N		65.1		65.5	65.4	0.3	448	66.7	66.6	1.5	771	67.0	66.8	1.7	912	67.4	67.2	2.1	1160	Floodplain of Wedgefield Canal
BEWF010P	BEWF010N	BEWF015N	65.3	Culvert Riser in Wedgefield Canal	65.4	61.0	0.1	408	66.6	63.5	1.3	431	66.8	63.7	1.5	433	67.2	64.1	1.9	435	Floodplain of Wedgefield Canal
BEWF010W	BEWF010N	BEWF015N	65.3		65.4	61.0	0.1	13	66.6	63.5	1,3	461	66.8	63.7	1.5	603	67.2	64.1	1.9	851	Floodplain of Wedgefield Canal
BEWF015X	BEWF015N	BEWF020N	61,1		61.0	61.0		667	63.5	63,5	2.4	771	63.7	63.7	2.6	912	64.1	64.1	3.0	1160	Floodplain of Wedgefield Canal
BEWF020P	BEWF020N	BEWF025N	62.3	Culvert Riser in Wedgefield Canal	61.0	57.4	5	401	63.5	59.0	1.2	482	63.7	59.2	1.4	488	64.1	59.6	1.8	494	Floodplain of Wedgefield Canal
BEWF020W	BEWF020N	BEWF025N	62.3	TOTAL STATE OF THE	61.0	57.4	5 M. Co.	0	63.5	59.0	1.2	397	63.7	59.2	1.4	539	64.1	59.6	1,8	784	Floodplain of Wedgefield Canal
BEWF025X	BEWF025N		57.8		57.4	57.4		379	59.0	59.0	1.2	764	59.2	59.2	1.4	909	59.6	59.6	1.8	1155	Floodplain of Wedgefield Canal
BEWF030P	BEWF030N	BEWF035N	57.5	Culvert Riser in Wedgefield Canal	57.4	54.6	-	348	59.0	57.9	1.5	413	59.2	58.1	1.7	421	59.6	58.6	2.1	430	Floodplain of Wedgefield Canal
BEWF030W	BEWF030N	BEWF035N	57.5 54.8		57.4 54.6	54.6 54.6		348	59.0 57.9	57.9 57.9	3.1	571 761	59.2 58.1	58.1 58.1	3.3	720 906	59.6 58.6	58.6	2.1	974	Floodplain of Wedgefield Canal
BEWF035X BEWF040P	BEWF035N BEWF040N	BEWF040N BEWF045N	56.8	Culvert Riser in Wedgefield Canal	54.6	52.1	-	330	57.9	54.2	1.1	465	58.1	54.8	1.3	482	58.6	58.6 55.5	1.8	1153	Floodplain of Wedgefield Canal
BEWF040W	BEWF040N	BEWF045N	56.8	Surent 1000 in 11 bugunda Sundi	54.6	52.1		0	57.9	54.2	1,1	324	58.1	54.8	1.3	477	58.6	55.5	1.8	747	Floodplain of Wedgefield Canal Floodplain of Wedgefield Canal
BEWF045X	BEWF045N		54.6		52.1	52.1	1-1-	322	54.2	54.2		717	54.8	54.8	0.2	858	55.5	55.5	0.9	1098	Floodplain of Wedgefield Canal
BEWF050X	BEWF050N		55		65.3	51.9		414	66.7	52.7		809	67.1	52.8	-	1010	67.5	52.7		1501	Troughlin Troughlind Danai
BEWF055X	BEWF055N		48.3		51.9	45.5	I	668	52.7	48.1	1-6-1	1387	52.8	48.8	0.5	1624	52.7	49.8	1.5	2022	Floodplain of Wedgefield Canal
BEWF060X	BEWF060N	BEWF065N	63.7		60.9	60.3		379	63.4	63.1	6	510	64.2	64.0	0.3	546	65.5	65.3	1.6	651	Floodplain of Wedgefield Canal
BEWF065P	BEWF065N	BEWF070N	64.9	Culvert Riser in Wedgefield Canal	60.3	58.0		379	63.1	59.7	U (4.7	505	64.0	60.3	A- 30 -1	536	65.3	61.1	0.4	569	Floodplain of Wedgefield Canal
BEWF065W	BEWF065N		64.9		60.3	58.0	- 9	0	63.1	59.7		0	64.0	60.3		0	65.3	61.1	0.4	78	Floodplain of Wedgefield Canal
BEWF070X	BEWF070N	BEWF075N	60.3		58.0	58.0	P. C.	727	59.7	59.7		711	60.3	60.3	1-14-1-1	729	61.1	61.1	8.0	713	Floodplain of Wedgefield Canal
BEWF075P	BEWF075N		60.7	Culvert Riser in Wedgefield Canal	58.0	56.2		378	59.7	56.5		502	60.3	56.6	1-10-6	533	61.1	56.9	0.4	570	Floodplain of Wedgefield Canal
BEWF075W	BEWF075N		60.7		58.0	56.2	0.1	0	59.7	56.5	0.4	0	60.3	56.6	0.5	0	61.1	56.9	0.4	74	Floodplain of Wedgefield Canal
BEWF080X	BEWF080N	BEWF085N	56 55.4	Culvert Riser in Wedgefield Canal	56.2 56.1	56.1 49.2	0.1	378 210	56.5 56.4	56,4 50.7	1,0	502 215	56.6 56.5	56,5 51,8	0.5	532 216	56.9 56.7	56.7 53.5	0.7	643	Floodplain of Wedgefield Canal
BEWF085P BEWF085W	BEWF085N	BEWF090N	55.4	Culvert Hiser in Wedgenerd Cartai	56.1	49.2	0.7	168	56.4	50.7	1.0	286	56.5	51.8	1.1	332	56.7	53.5	1.3	216 480	Floodplain of Wedgefield Canal
BEWF090X	BEWF090N	BEWF095N	52.6		49.2	48.6	5	378	50.7	50.3	1.0	500	51.8	51.5		530	53.5	53.4	0.8	643	Floodplain of Wedgefield Canal Floodplain of Wedgefield Canal
BEWF095P	BEWF095N	BEWF100N		Culvert Riser in Wedgefield Canal	48.6	44.6		378	50.3	47.2		497	51.5	47.9		528	53.4	49.0	0.4	591	Floodplain of Wedgefield Canal
BEWF095W	BEWF095N				48.6	44.6		0	50.3	47.2		0	51.5	47.9	i	0	53.4	49.0	0.4	60	Floodplain of Wedgefield Canal
BEWF100X	BEWF100N	BEBEO60N	43.1		44.6	44.6	1.5	378	47.2	47.2	4.1	497	47.9	47.9	4.8	528	49.0	49.0	5.9	642	Floodplain of Wedgefield Canal
BEWF105X	BEWF105N	BEWF110N			63,3	61.7		53	64.1	62.2	- 3.	155	64.4	62,3	1	167	65.0	62.4	- +	194	
BEWF110P	BEWF110N	BEWF115N	64.6	Culvert Riser in Wedgefield Canal	61.7	58.4	-	53	62.2	59.1	Y	155	62.3	59.2	11 27 11	167	62.4	59.3	A4"	194	
BEWF110W	BEWF110N		64.6		61.7	58.4		0	62.2	59.1		0	62.3	59.2	4	0	62.4	59.3		0	
BEWF115X	BEWF115N			0.1-1.00-1-11-0-11-0-11	58.4	58.4		53	59.1	58.9		155	59.2	58.9	- A- 1	167	59.3	59.0	9.00	194	
BEWF120P	BEWF120N			Culvert Riser in Wedgefield Canal	58.4 58.4	53.8 53.8		53	58.9 58.9	54.4 54.4		155	58.9 58.9	54.4 54.4	•	167	59.0	54.6		194	
BEWF120W	BEWF120N		60.5		53.8	53.8		221	54.4	54.4		246	54.4	54.4	1 1	249	59.0 54.6	54.6 54.5	70.0	0	
BEWF125X BEWF130P	BEWF125N BEWF130N		54.9	Culvert Riser in Wedgefield Canal	53.8	50.0		53	54.3	50.6	-	155	54.4	50.7		167	54.5	52,4	-	250 194	
BEWF130W	BEWF130N		54.9	Surran these of trougenous warran	53.8	50.0		0	54.3	50.6	10.00	0	54.4	50.7	. In Taking	0	54.5	52.4	¥	0	
BEWF135X	BEWF135N		57		50.0	50.0	-	53	50.6	50.6		405	50.7	50.7		426	52.4	52.4	-	421	
BEWF140P		N BEWF145N		Culvert Riser in Wedgefield Canal	50.0	46.5	1 4 7	52	50.6	48.3	11-21-1	155	50.7	48.8		166	52.4	50.2	4.5	194	
BEWF140W	BEWF140	N BEWF145N	53.7		50.0	46.5		-0	50.6	48.3		0	50.7	48.8		0	52.4	50.2	- 3	0	
BEWF145X	BEWF145N	N BEWF150N	53.3		46,5	46.4	ALTEROPE III.	52	48.3	48.3		808	48.8	48.8		808	50.2	50.2		799	
BEWF150P	BEWF150	N BEWF155N	50.2	Culvert Riser in Wedgefield Canal	46.4	43.8		52	48.3	46.9		153	48.8	47.1		165	50.2	48.0		191	
BEWF150W	BEWF150	N BEWF155N	50.2		46.4	43.8		0	48.3	46.9		0	48.8	47.1	7 TO 1	0	50.2	48.0	-10-	0	
BEWF155X	BEWF155	N BEWF160N	49	Dukest District Western St. Co.	43.8	43.8		52	46.9	46.9	- 00	153	47.1	47.1		164	48.0	47.9		191	
		N BEWF165N		Culvert Riser in Wedgefield Canal	43.8	43,6		52	46.9	46.1	0.3	149	47.1	46.8	0.5	149	47.9	47.9	1.3	129	Floodplain of Wedgefield Canal
BEWF160W					43.8 43.6	43.6 43.6		52	46.9 46.1	46.1 46.1	0.3	37	47.1	46.8 46.8	0.5	92	47.9	47.9	1.3	172	Floodplain of Wedgefield Canal
BEWF165X	81X	N BEBE090N 82	74	Woodbury Road	69.9	69.3	-	170	71.2	69.9	- :	153 350	46.8 71.6	70.1		164 416	47.9 72.6	47.9 70.6		190	Floodplain of Wedgefield Canal
CULV-2 CHANL-5	81X 82	24	65	Troododly Hoad	69.3	62.8		171	69.9	63.6	- 1	352	70.1	63.8	- 1	416	70.6	63.9		526 526	
CHANL-5	24	26	65		62.8	59.7	- V	200	63.6	61.2		414	63.8	61.6		467	63.9	62.3	-	545	
CULV-10	26	13A	60		59.7	55.4		268	61.2	55.7	1.2	560	61.6	55.9	1.6	656	62.3	56.2	2.3	795	Floodplain of Big Econ Tributary
13A-13B	13A	13B	55		55.4	53.7	0.4	63	55.7	55.0	0.7	72	55.9	55.3	0.9	74	56.2	55.8	1.2	76	Floodplain of Big Econ Tributary
B13A-13B		13B	55		55.4	53.7	0.5	240	55.7	55.0	0.5	570	55.9	55.3	0.5	675	56.2	55.8	0.5	834	Floodplain of Big Econ Tributary
CHN-12-0	13B	STA-9700	57		53.7	52.0		342	55.0	53.2		873		53.3	100	1007		53.7	-	1312	The state of the s
		BEWL020N			52.0	50.1	1.1	339	53.2	50.4	1.4	873		51.1	2.1	1013		52.1	3.1	1322	Floodolain of Big Econ Tributary
		N BEWL025		Bridgeway Blvd - Bridge Equivalent	50.1	50.1		531	50.4	50.3		1136		51.0		1325		52.0		1690	
BEWL020W	BEWL020	N BEWL025N	57.8	Bridgeway Blvd Overflow	50.1	50.1	LLY	0		50.3	N - 0411	0		51.0	g may may	0	52.1		1-0-7	0	
BEWL025X		N BEWL030N			50.1	46.4		531	50.3	49.5	1.7	1136		50.2	2.4	1324	52.0	51.3	3.5	1695	Floodplain of Big Econ Tributary
		N BEWL035	54.4	SR 50	46.4	44.4	-	612	49.5	45.0	10	1354	50.2	45.1		1549	51.3	45.4	- (*)	2000	

Notes:
1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels.
2) Flow taken from Link Maximum Conditions Report (cfs)
3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Appendix: J

Bithlo Area Stormwater Management Master Plan

Stormwater Management Master Plan Update



Final Report

Prepared for



Board of County Commissioners Orange County, Florida

Prepared by



Singhofen & Associates, Inc.
Stormwater Management and Civil Engineering

September 2002



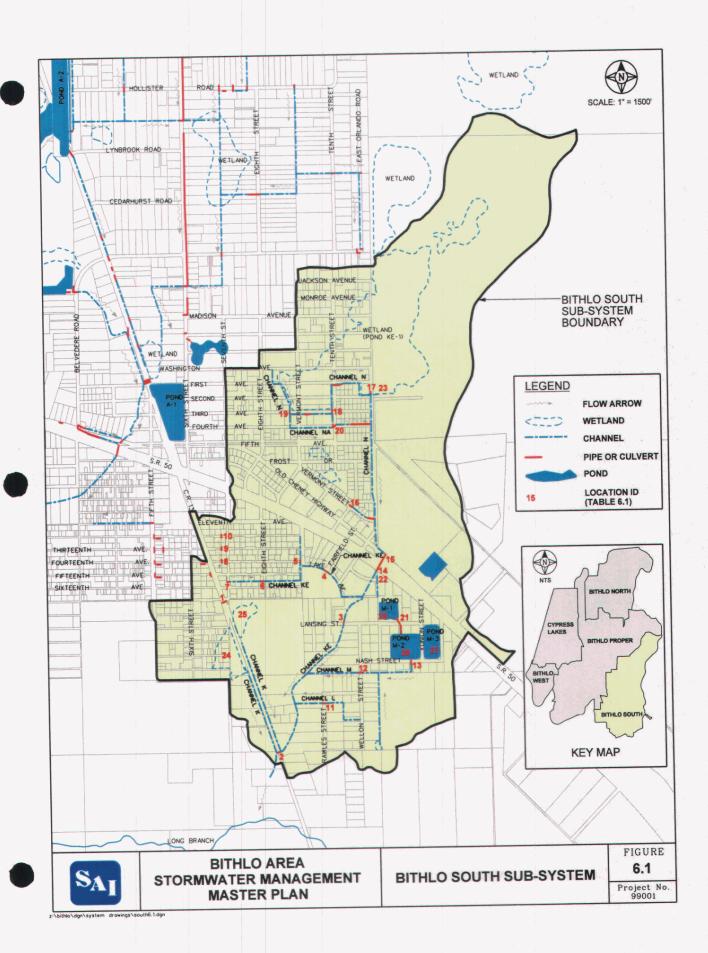


Table 6.1 Identification and Location Information for Structures at Major Crossings and/or Outfalls Bithlo South Sub-System

		Upstream			Calvert	
Location	Link	Node	SEC-TWN-RHG	Span	Rise	Location Description
ID.	Name	Name		(in)	(in)	
Culvert						
1	PK-120	NK-120	27-22\$-32E	24	24	C.R. 13 south of Seventeenth Avenue
2	PKE-030	NKE-030	34-22S-32E	96	84	C.R. 13, Roberts Branch
3	PKE-080A	NKE-080	27-22S-32E	72_	72	Lansing St.
4	PKE-120	NKE-120	27-22S-32E	36	36	Fairfield St.
5	PKE-143	NKE-143	27-22S-32E	30	30	9th St. and 14th Ave.
6	PKE-165	NKE-165	27-22S-32E	24	24	8th St. between 15th and 16th Ave.
7	PKE-225	NKE-225	27-225-32E	18	12	7th St. culvert
8	PKE-245	NKE-245	27-22S-32E	24	24	14th Ave
9	PKE-255	NKE-255	27-22S-32E	24	24	13th Ave
10	PKE-265	NKE-265	27-22S-32E	24	24	12th Ave.
11	PL-020	NL-020	27-22S-32E	30	30	Rawles St.
12	PM-030	NM-030	27-22S-32E	48	48	Wellon St.
13	PM-050	NM-050	26-22S-32E	42	42	South discharge from pond
14	PN-015	NN-015	27-22S-32E	120	48	S.R. 50
15	PN-020	NN-020	26-22S-32E	120	108	Old Cheney Hwy.
16	PN-033	NN-033	27-22S-32E	24	24	Vermont St. and Exeter St.
17	PN-060	NN-060	22-22S-32E	36	36	Containment berm
18	PN-115	NN-110	22-22S-32E	15	15	3rd Ave.
19	PN-150	NN-150	22-22S-32E	24	24	3rd Ave.
20	PNA-030	NNA-030	22-225-32E	45	29	10th St.
		· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·
Drop St	tructures					
21	DM-070	NM-070	26-22S-32E	42	42	Control structure from North pond to South pond (new)
			·			<u> </u>
Weirs						
22	WM-080	NN-010	26-22S-32E	-	-	Overflow spillway from Channel N to M
23	WN-060B	NN-060	22-22S-32E			High stage discharge from Wetland (Pond KE-1)
		<u> </u>				<u> </u>
Other						
24		NK-110	27-22S-32E		-	Wetland west of C.R. 13
25		NK-130	27-22S-32E	-	-	Wetland eastof C.R.13
26	_	NM-050	26-22S-32E		-	Pond M-2
27		NM-060	26-22S-32E		-	Pond M-3
28	-	NM-070	26-22S-32E	-	-	Pond M-1

Notes:

The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 6.1)
 Detailed structure information for culverls, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.

Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).

		Location			Annual Event				ear Event		10-Year Storm Event						Year Event		100-Year Storm Event			
			Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Project		Cur	rent	Pro	ject
LOC	Node ID		Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
Channel	K					J.																
2	NKE-020	C.R. 13, S.	46.4	277	46.4	283	46.8	431	46.8	431	47.0	536	47.0	533	47.1	621	47.1	621	47.34	784	47.35	787
24	NK-110	Wetland, W. of CR13	59.5	28	59.5	32	59.6	46	59.6	54	59.7	59	59.7	71	59.7	71	59.7	84	59.8	97	59.8	110
25	NK-130	Wetland, E. of CR13	60.3	5	60.3	5	60.4	10	60.4	10	60.5	14	60.5	14	60.5	18	60.5	18	60.6	43	60.6	24
Channel	KE		10																			
2	NKE-020	C.R. 13, S.	46.4	277	46.4	283	46.8	431	46.8	431	47.0	536	47.0	533	47.1	621	47.1	621	47.34	784	47.35	787
2	NKE-030	C.R. 13, N.	47.9	244	47.9	247	48.8	375	48.8	366	49.4	465	49.3	449	49.8	537	49.7	523	50.6	668	50.5	659
	NKE-040	Confluence w/ Chan. L	51.1	236	51.2	239	51.8	361	51.7	353	52.2	447	52.1	432	52.5	516	52.5	502	52.8	642	52.8	633
	NKE-060	Confluence w/ Chan. M	52.4	213	52.4	215	53.1	327	53.0	317	53.5	404	53.4	386	53.8	467	53.8	449	54.2	575	54.1	565
3	NKE-080	Lansing St., N.	54.4	169	54.4	173	55.3	256	55.2	250	55.8	311	55.7	299	56.1	353	56,0	340	56.6	410	56.6	409
mah k	NKE-090	Confluence w/ Chan. N	55.10	165	55.15	169	56.0	250	56.0	243	56.5	304	56.4	291	56.9	346	56.8	330	57.3	399	57.3	397
4	NKE-120	Fairfield St., W.	57.6	33	56.7	34	58.7	48	57.3	55	59.5	55	57.7	67	60.4	59	58.2	116	60.7	58	58.8	144
5	NKE-143	14th Ave., N.	58.7	10	58.7	10	59.2	16	59.1	16	59.8	20	59.4	20	60.9	21	59.6	24	61.5	24	60.0	31
6	NKE-165	8th St., W.	59.2	9	58.0	10	59.7	13	58.3	16	60.2	16	58.5	20	60.5	19	58.8	24	60.9	22	59.5	30
7	NKE-220	7th St., E.	61.8	8	60.6	8	61.9	12	60.9	13	62.0	15	61.0	17	62.1	17	61,2	20	62.2	20	61.4	25
7	NKE-225	7th St., W.	63.7	8	1.00	5/81	63.8	11	4 5 4	I e l	63.8	14	15	10-1	63.8	15			63.9	18		
7	NKE-225Z	7th St., W.	E. 6.1		61.5	8	mayb.		61.9	12	The co		62.1	16	3-7-0	-	62.3	19		-	62.6	24
	NKE-235	Between 14th & 15th	65.2	7	62.8	8	65.2	10	63.1	17	65.2	12	63.3	18	65.3	14	63.5	19	65.3	16	63.8	24
8	NKE-245	Between 13th & 14th	65.3	6	63.5	7	65.5	9	63.8	11	65.6	11	64.0	14	65.7	12	64.1	16	65.9	14	64.4	21
9	NKE-255	Between 12th & 13th	65.4	5	64.2	6	65.6	7	64.5	9	65.8	9	64.7	12	66.0	10	64.9	14	66.3	12	65.2	17
10	NKE-265	Between 11th & 12th	65.4	4	64.6	4	65.7	7	64.9	7	66.0	8	65.1	g	66.2	9	65.3	10	66.6	11	65.5	17
Channe	L —							1														
11	NL-020	Rawles St., E.	52.3	13	52.3	13	52.9	21	52.9	21	53.2	30	53.1	29	53.3	33	53.3	33	54.0	42	54.1	42
-	NL-030	Wellon St., W.	55.5	11	55.5	11	55.7	20	55.7	20	55.8	24	55.8	23	55.9	27	55.9	27	56.0	37	56.0	38

Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).

\- \		Location	Mean Annual Storm Event					5-Year Storm Event				10-Year Storm Event					Year Event		100-Year Storm Event			
700			Cur	rent	Pro	ject	Cur	Tent	Pro	ject	Cun	rent	Pro	ject	Current		Project		Cur	rent	Pro	ject
LOC	Node ID		Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	
Channel	M												, All I		i		14.7					
12	NM-030	Wellon St., E.	53.9	26	53.8	23	54.3	43	54.2	38	54.7	58	54.7	59	55.0	71	55.1	76	55.5	95	55.7	107
26	NM-050	Pond M-2	53.9	8	53.6	5	54.4	14	54.3	12	54.8	19	54.8	24	55.0	23	55.2	35	55.5	30	55.9	53
27	NM-060	Pond M-3	53.9	3	53.6	2	54.4	5	54.3	5	54.8	6	54.8	8	55.0	7	55.2	9	55.5	10	55.9	11
28	NM-070	Pond M-1	57.7	10	57.4	0	57.8	15	57.8	13	57.8	19	57.9	26	57.9	22	58.0	35	57.9	28	58.2	51
22	NM-080	Overflow spillway, S.	57.7	0	57.4	0	57.8	0	57.8	6	57.8	0	57.9	15	57.9	0	58.0	24	57.9	0	58.2	36
Channel	N							0										()	1		Y-1	
14	NN-010	S.R. 50, S.	57.3	126	57,4	131	57.9	192	57.8	186	58.2	232	58.1	217	58.4	266	58.2	243	58.7	319	58.5	284
15	NN-015	S.R. 50, N.	61.1	117	61.1	117	61.8	178	61.8	178	62.3	214	62.3	214	62.6	246	62.6	246	63.1	294	63.1	294
15	NN-020	Old Cheney Hwy., N.	61.1	93	61.1	93	61.9	143	61.9	143	62.3	171	62.3	171	62.6	195	62.6	195	63.2	236	63.2	236
17	NN-050	Struct from wetland, N.	61.5	20	61.5	20	62.3	38	62.3	38	62.7	52	62.7	52	63.1	63	63.1	63	63.6	84	63.6	84
18	NN-110	Third Ave., N.	62.0	1	62.0	1	62.9	1	62.9	1	63.4	1	63.4	1	63.9	1	63.9	1	64.5	1	64.5	1
19	NN-150	Third Ave., N.	62.0	10	62.0	10	63.3	15	63.3	15	64.0	21	64.0	21	64.4	25	64.4	25	65.0	33	65.0	33
Channel	NA				J. 1				1 44										TIET!			1 -
20	NNA-030	Intersect 4th & 10th, W.	61.9	19	61.9	19	63.2	24	63.2	24	63.8	34	63.8	34	64,1	38	64.1	38	64.5	49	64.5	49
	NNA-070	4th St., N.	61.6	21	61.6	21	62.5	25	62.5	25	63.0	27	63.0	27	63.3	27	63.3	27	63.8	28	63.8	28

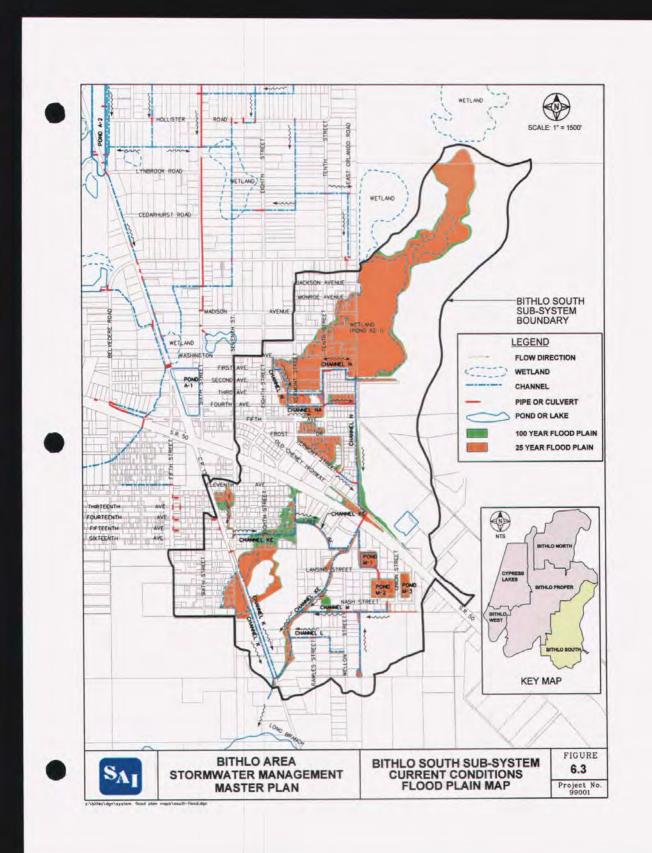
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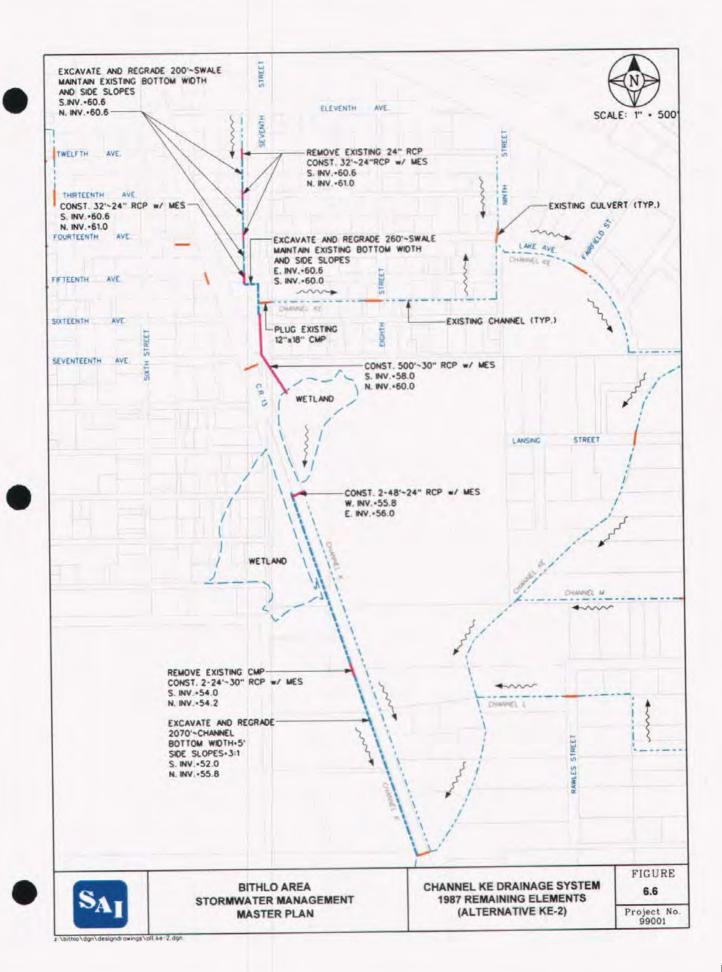
Flow represents the peak outflow at the referenced node.

^{2.} Results are from the Bithlo Current Conditions model <EXIST> and the Bithlo Project Conditions model <B-PROJ1>.

^{3.} The simulated storms are all 24-hr duration storms.

^{4.} The LOC ID numbers associated with each location are included for the purpose of cross referencing to the system map (refer to Figure 6.1)





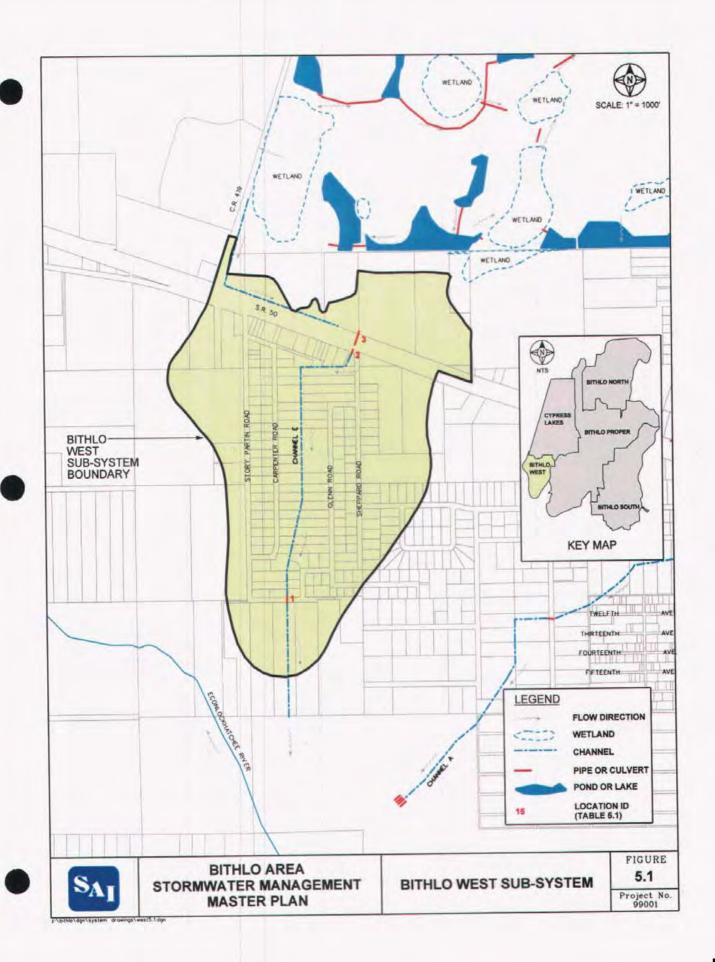


Table 5.1 Identification and Location Information for Structures at Major Crossings and/or Outfalls Bithlo West Sub-System

Upstream Culvert Culvert Location Link Node SEC-TWN-RNG Span Rise	Location Description
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Culverts

1 17 10	PE-030A	NE-030	28-22S-32E	72	72	Story Partin Road
2	PE-070A	NE-070	21-22S-32E	48	48	Old Cheney Hwy, S. of S.R. 50
3	PE-080	NE-080	21-22S-32E	48	51	S.R. 50 (western most crossing)

- Notes:

 1. The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 5.1)

 2. Detailed structure information for culverts, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.

Singholen & Associates, Inc.

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Bithio Stormwater Management Master Plan Update

Table 5.2 Maximum Stages and Flows at Selected Locations in the Bithlo West Sub-System (Current and Project Conditions).

			Mean Annual Storm Event					ear Event		Year Event			Year Event		100-Year Storm Event							
			Cur	rent	Pro	ject	Cur	Current		Project		Current		Project		rent	Project		Current		Pro	ject
LOC	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage		-	
Channel	Ε							!				<u></u>		1	1	13.57	1,	10.07	1,	(010)	1	1019)
3	NE-080	S.R. 50, N.	62.1	35	62.1	35	62.8	52	62.8	52	63.3	65	63.3	65	63.8	78	63.8	78	65.0	106	65.0	106
2	NE-070	Old Cheney Hwy., N.	59.9	38	59.9	38	60.2	57	60.2	57	60.4	72	60.4	72	60.6	86	60.6	86	61.4	132	61.4	131
-	NE-050	Southern turn in chan.	52.9	68	52.9	68	53.3	104	53.3	104	53.6	155	53.6	156	53.8	165	53.8	165	54.2	295	54.2	295
1	NE-030	Story Partin Rd., N.	44.7	121	44.7	121	45.5	189	45.5	189	46.0	242	46.0	242	46.5	291	46.5	291	47.4	364	47.4	364
1	NE-020	Story Partin Rd., S.	44.6	134	44,6	134	45.3	208	45.3	208	45.7	265	45.7	265	46.0	312	46.0	312	46.5	398	46.5	398

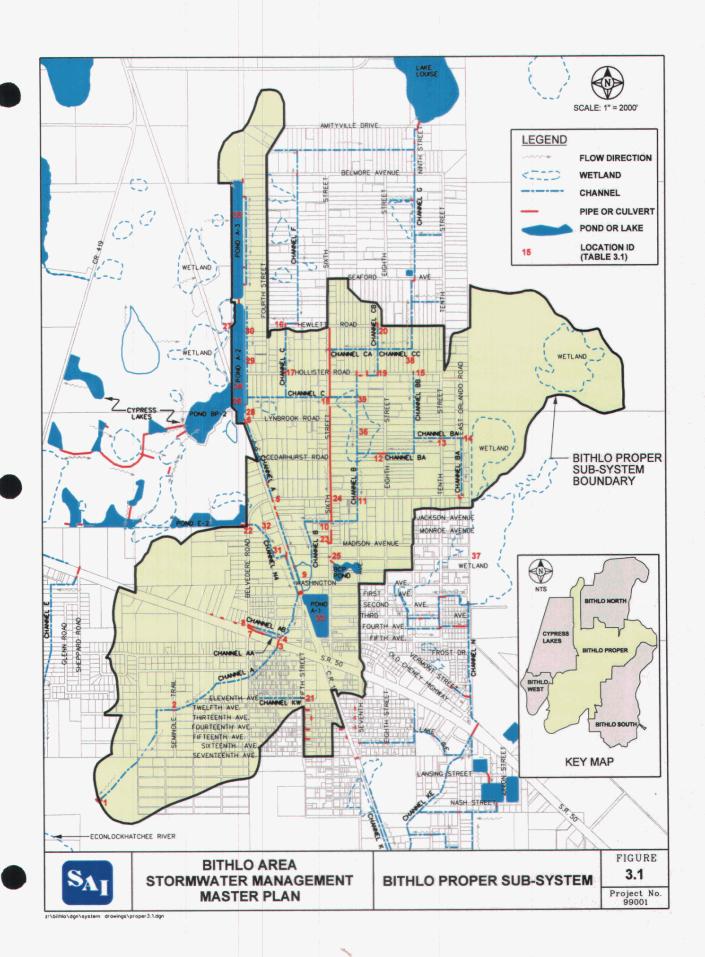


Table 3.1 Identification and Location Information for Structures at Major Crossings and/or Outfalls **Bithlo Proper Sub-System**

	ikkonosasan sanah	Upstream		Culvert	Culvert	
Location	Link	Node	SEC-TWN-RNG		Rise	Location Description
10	Name	Name		(in)	(10)	
	***************************************			A STATE OF THE PERSON NAMED IN		
Culvert	S					
1	PA-015A	NA-015	28-22S-32E	48	48	Utility (power) Easement at south end of Channel A u/s of the Econ River
2	PA-070	NA-070	28-22S-32E	72	72	Seminole Trail
3	PA-110	NA-110	27-22S-32E	96	84	S.R. 50
4	PA-115	NA-115	22-22\$-32E	192	72	Old Cheney Highway
5	PA-220	NA-220	22-22S-32E	36	36	Belvedere Rd. at C.R. 13
6	PA-240	NA-240	21-22S-32E	60	38	Access road to Pond A-2
7	PAA-020	NAA-020	22-22S-32E	18	18	North side of S.R. 50 near Belvedere Rd.
8	PAB-030B	NAB-030	22-22S-32E	23	14	Belvedere Rd. at Old Cheney Hwy.
9	PB-010A	NB-010	22-22S-32E	54	54	C.R. 13
10	PB-040	NB-040	22-22S-32E	36	36	Channel B crossing 6th St.
11	PB-070	NB-070	22-22S-32E	30	30	Channel B crossing at Belvedere Rd.
12	PBA-020	NBA-020	22-22S-32E	36	36	8th St.
13	PBA-050	NBA-040	22-22S-32E	24	24	10th St.
14	PBA-060	NBA-060	22-22S-32E	38	24	East Orlando Rd.
15	PBB-030	NBB-030	15-22S-32E	23	14	Hollister Rd.
16	PF-130	NF-130	15-22S-32E	45	29	Hewlett Rd.
17	PC-025	NC-025	15-22\$-32€	30	19	Hollister Rd.
18	PC-040	NC-030	15-22S-32E	30	19	6th St.
19	PC-080	NC-080	15-22S-32E	30	19	Hollister Rd.
20	PCB-020	NCB-020	15-22S-32E	24	24	Hewlett Rd.
21	PKW-110	NKW-110	27-22S-32E	30	30	5th St.
22	PN4-010	NN4-010	21-22\$-32E	60	38	Under Belvedere Rd. (N-4 channel system)
23	P6-020	N6-020	22-22S-32E	30	19	6th St.
24	P6-050	N6-050	22-22S-32E	30	19	Belvedere Rd.
25	P6A-010	N6A-010	22-22S-32E	38	24	6thSt. culvert (near BCC pond)
				<u></u>		
Drop St	ructures					
26	DA-241A	NA-241	16-22S-32E	24	24	From perimeter ditch SW of Pond A-2
27	DA-241B	NA-241	16-22S-32E	15	15	From perimeter ditch NW of Pond A-2
28	DA-243A	NA-243	16-22S-32E	15	15	From perimeter ditch SE of Pond A-2
29	DA-243B	NA-243	16-22S-32E	15	15	From perimeter ditch east of Pond A-2
30	DA-243C	NA-243	16-22S-32E	15	15	From perimeter ditch NE of Pond A-2
31	DN4-035A	NN4-035	22-22S-32E	24	24	From depression west of C.R. 13 into Channel N4
32	DN4-035B	NN4-035	22-22\$-32E	24	24	From depression west of C.R. 13 into Channel N4
Other						
33	-	NA-140	22-22\$-32E	-		Pond A-1
34	_	NA-240	16-22S-32E	_		Pond A-2
35		NA-250	16-22S-32E			Pond A-3
H 33		110.000	.0-220-021			

Wetland at Channel B/BA confluence

Wetland (Pond KE-1)

Wetland north of Hollister Rd.

Wetland south of Hollister Rd.

39

36 37

38

22-22\$-32E

22-22S-32E

15-22S-32E

15-22S-32E

NB-080

NN-060

NBB-030

NC-050

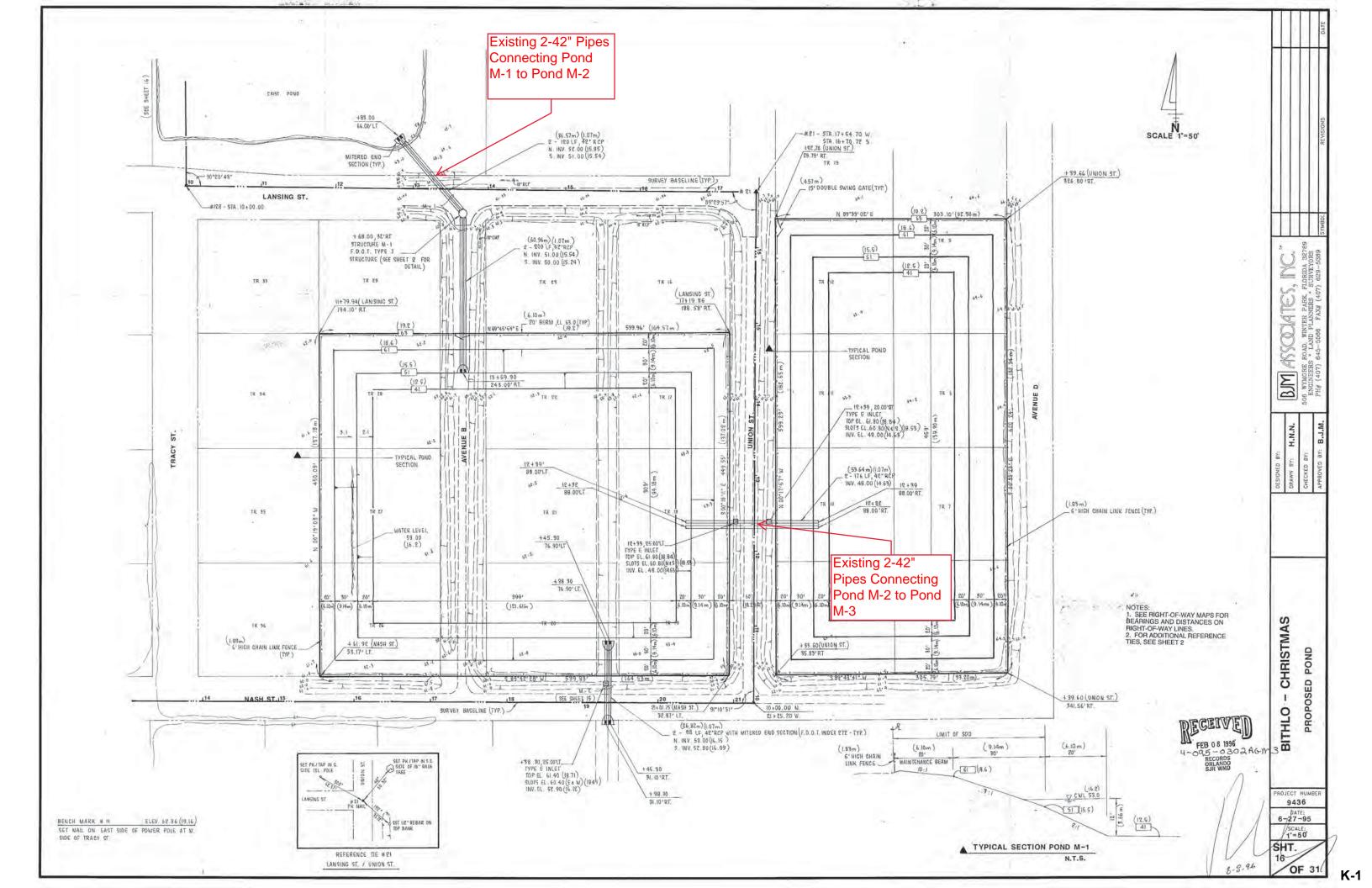
^{1.} The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 3.1)
2. Detailed structure information for culverts, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.

Table 3.2 Maximum Stages and Flows at Selected Locations in the Bithlo Proper Sub-System (Current and Project Conditions).

					Annual Event			Annual Control	/ear Event				Year Event				Year Event		100-Year Storm Event			
	- N		Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	Tent	Pro	oject
LOC	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
Channel	A															L CARLLE	10 -		Toler.	4.5		
1	NA-015	Power Easement, N.	40.2	325	40.2	322	40.5	492	40.5	489	40.7	620	40.7	615	41.5	762	41.5	744	42.8	1027	42.8	1005
2	NA-060	Seminole Trl., W.	48.2	256	48.2	253	48.6	377	48.6	372	48.8	465	48.8	458	49.1	564	49.1	549	49.5	719	49.4	697
2	NA-070	Seminole Trl., E.	48.4	253	48.4	250	49.6	373	49.6	369	50.5	461	50.4	454	50.7	556	50.7	541	50.9	703	50.9	682
3	NA-110	SR 50, N.	57.0	204	57.0	204	58.3	310	58.3	310	59.04	379	59.05	380	59.5	425	59.5	425	60.3	499	60.3	499
4	NA-115	Old Cheney Hwy., N.	57.1	192	57.1	191	58.4	295	58.4	290	59.2	373	59.2	369	60.0	395	60.0	393	61.0	446	61.0	447
m ./C	NA-130	CR 13, W.	60.1	182	60.1	182	60.4	280	60.4	280	60.6	345	60.6	345	60.9	386	60.9	387	61.5	446	61.5	447
33	NA-140	Pond A-1	60.3	10	60.3	10	60.8	15	60.8	15	61.1	22	61.1	22	61.4	27	61,4	27	62.0	34	62.0	34
5	NA-220	Belvedere Rd., N.	65.6	58	65.6	58	66.6	80	66.6	80	66.9	81	66.9	81	67.3	83	67.3	83	68.4	91	68.4	91
6	NA-230	Just S. of Pond A-2	67.1	56	67.1	56	67.9	87	67.9	87	68.2	93	68.2	93	68.4	90	68.4	90	68.8	106	68.8	106
34	NA-240	Pond A-2	67.6	56	67.6	56	68.7	86	68.7	86	69.2	91	69.2	91	69.6	86	69.6	86	69.9	74	69.9	74
35	NA-250	Pond A-3	68.6	-11	68.6	- 11	69.3	29	69.3	29	69.8	34	69.8	34	70.4	38	70.4	38	71.3	42	71.3	42
Channel	AA								22,000		23.0						13.1		* 1.0		77.0	
7	NAA-020	Belvedere Rd., W.	63.2	12	60.9	14	64.1	14	61.6	22	64.3	22	62.0	25	64.5	31	63.0	35	64.6	52	64.3	53
Channel	AB	- Construction of the cons	2 UT 11																			
8	NAB-030	Belvedere Rd., W.	63.5	9	63.3	20	64.5	14	63.3	20	64.6	20	63.8	20	64.6	24	64.4	22	64.7	31	64.6	31
Channel	T 12 12 22 23 23	100 100 V A 100 A 2	77.250						- A	328			. = = 1									
9	NB-010	Wetland, E. of CR 13	60.3	142	60.3	142	60.8	206	60.8	206	61.1	249	61,1	249	61.3	270	61.3	271	62.0	296	62.0	297
10	NB-040	Sixth St., E.	64.9	76	64.9	76	65.3	79	65.3	79	65.7	82	65.7	82	66.2	91	66.2	91	66.7	98	66.7	98
11	NB-070	Belvedere Rd., N.	66.6	59	66.6	59	67.3	64	67.3	64	68.2	71	68.2	71	68.8	79	68.8	79	69.3	85	69.3	85
•	NB-080	Channel B/BA confluence	67.5	50	67.5	50	68.0	62	68.0	62	68.6	73	68.6	73	69.0	84	69.0	84	69.4	98	69.4	98
Channel	ВА												E	4 7 71			1 -		12			-
12	NBA-010	Eighth St., W.	68.3	12	68.3	12	68.8	13	68.8	13	69.0	11	69.0	11	69.1	10	69.1	10	69.4	10	69.4	10
12	NBA-020	Eighth St., E.	68.5	29	68.5	29	69.1	32	69.1	32	69.2	49	69.2	49	69.2	71	69.2	71	69.4	105	69.4	105
13	NBA-040	Tenth St., W.	68.5	16	68.5	16	69.1	23	69.1	23	69.2	24	69.2	24	69.3	25	69.3	25	69.5	26	69.5	26
14	NBA-060	East Orlando Rd., W.	66.2	2	66.2	2	66.3	3	66.3	3	66.4	4	66.4	4	66.4	4	66.4	4	66.5	5	66.5	5

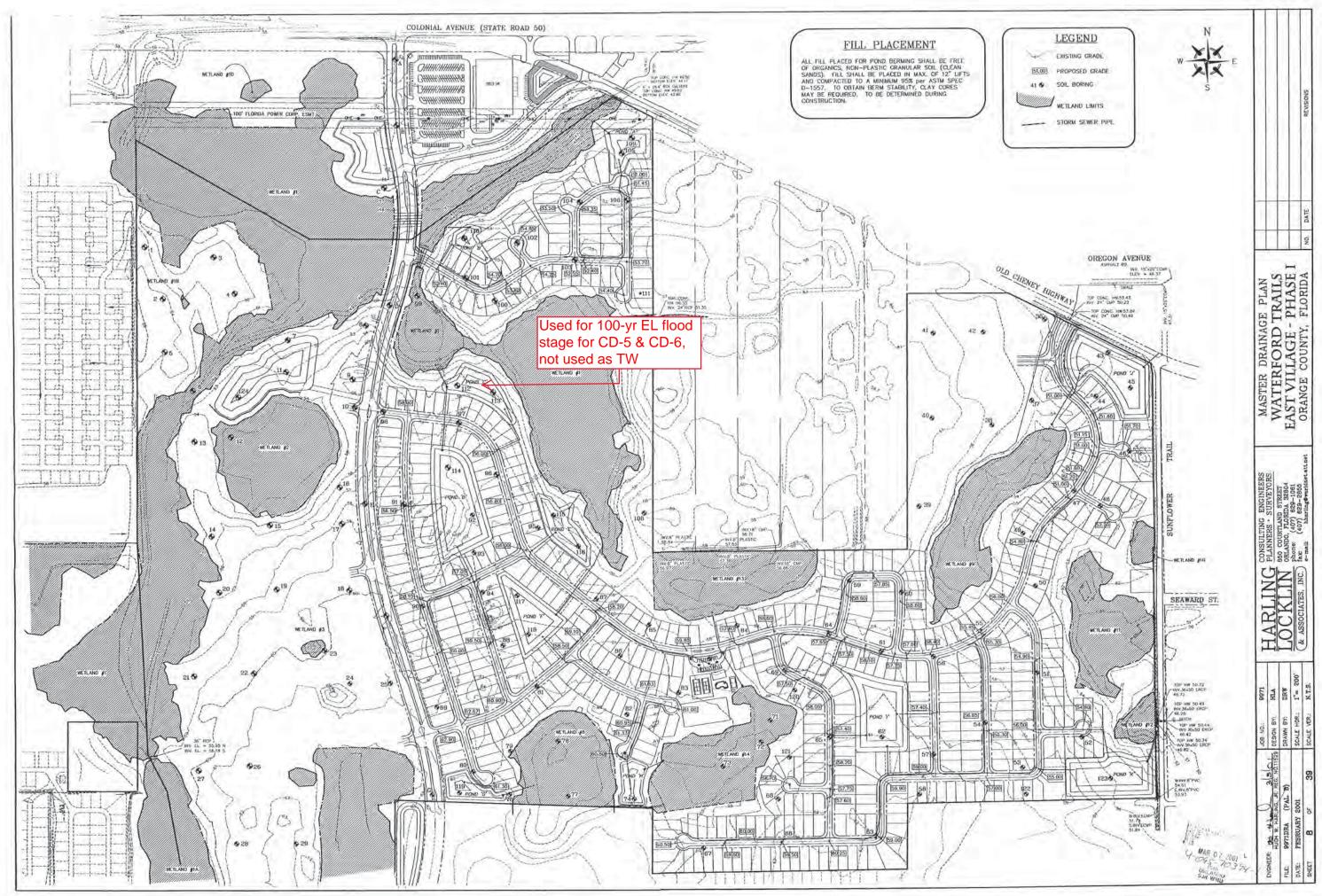
Appendix: K

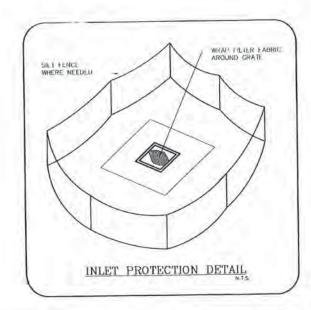
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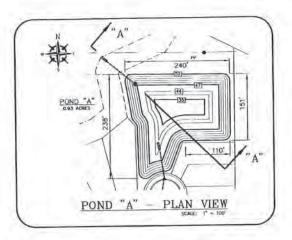


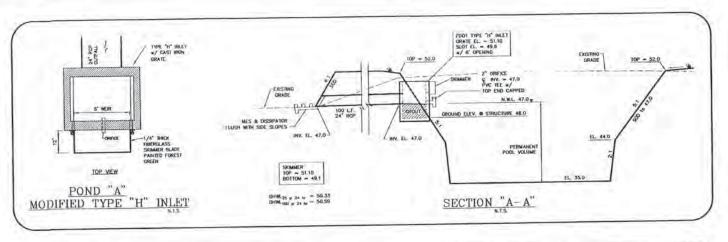
Appendix: L

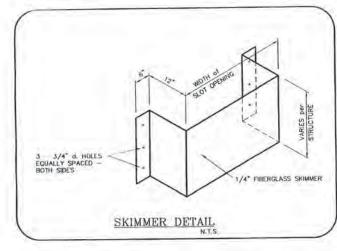
Excerpt from Harling Locklin & Associates, Inc. Waterford Trails Plans & Avalon Park Blvd

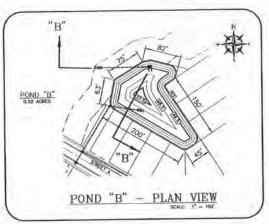


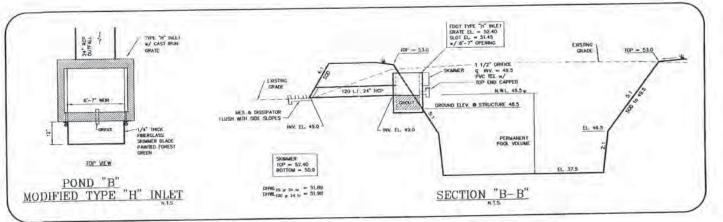


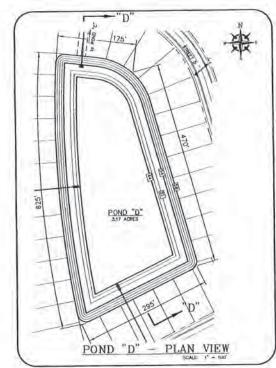


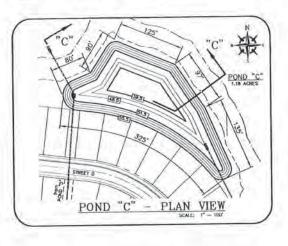


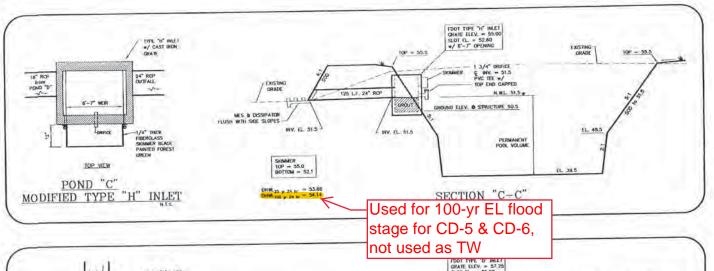


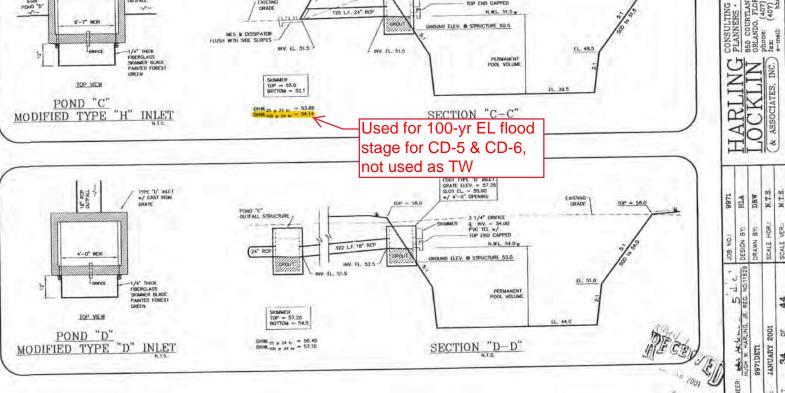




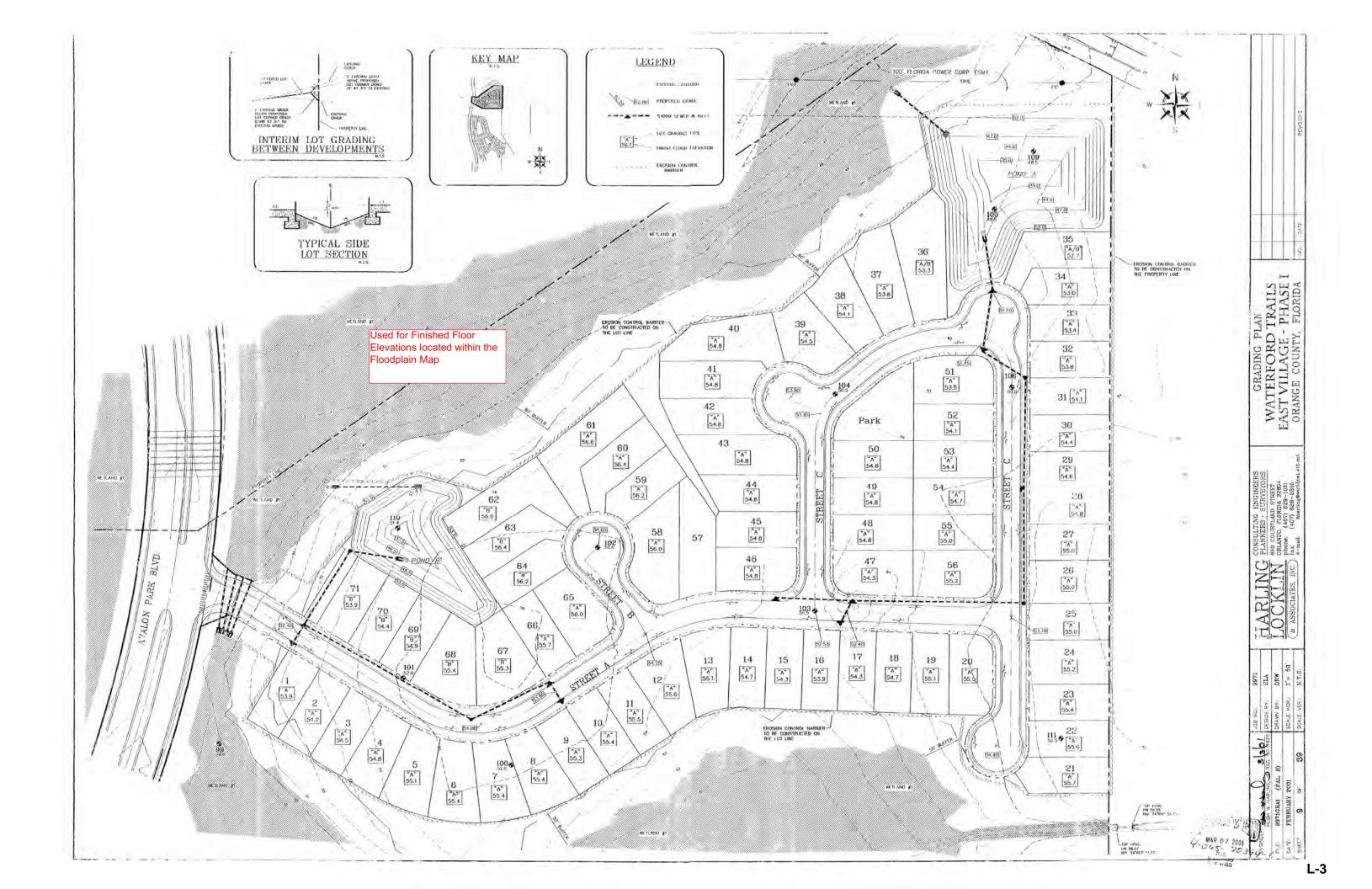


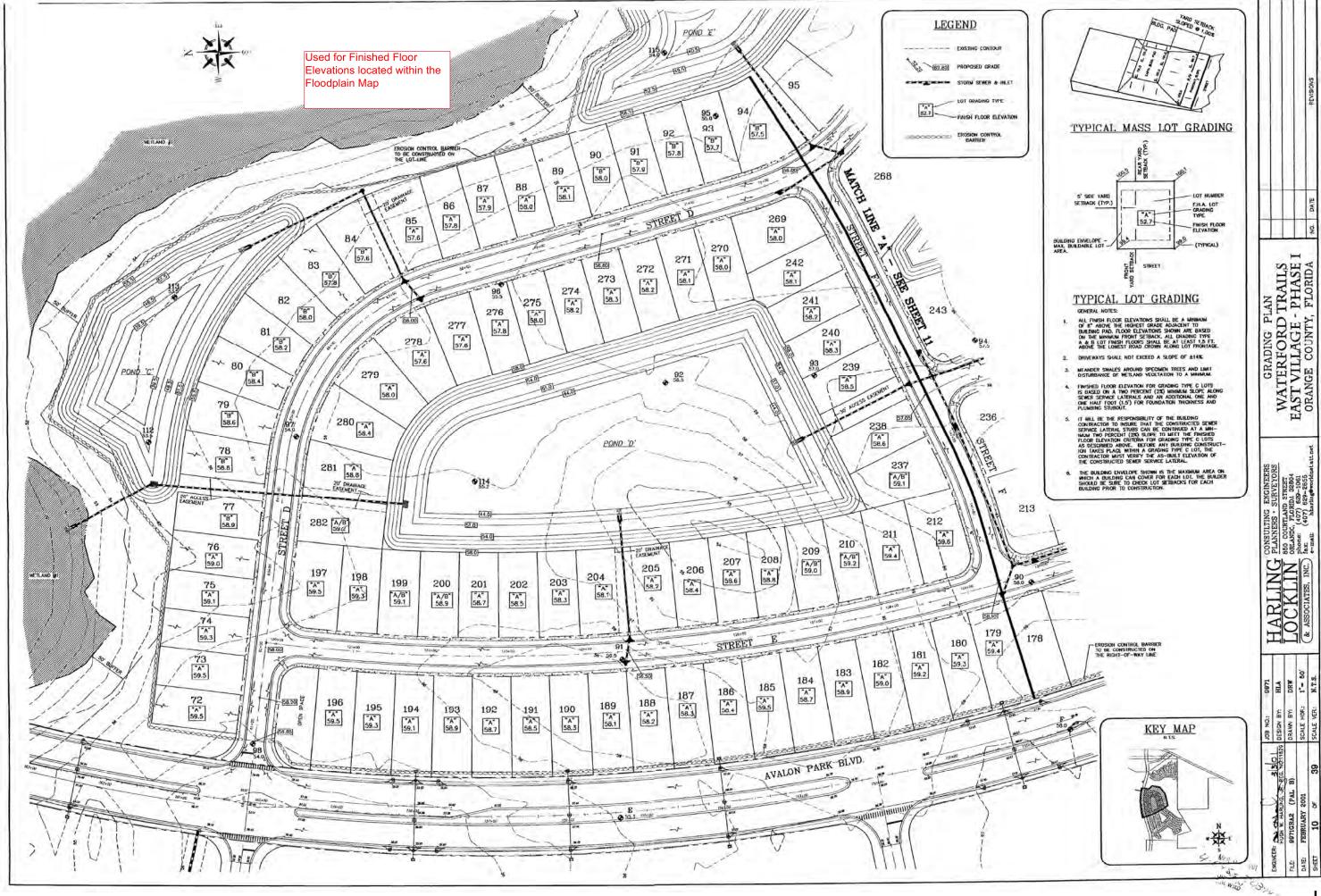


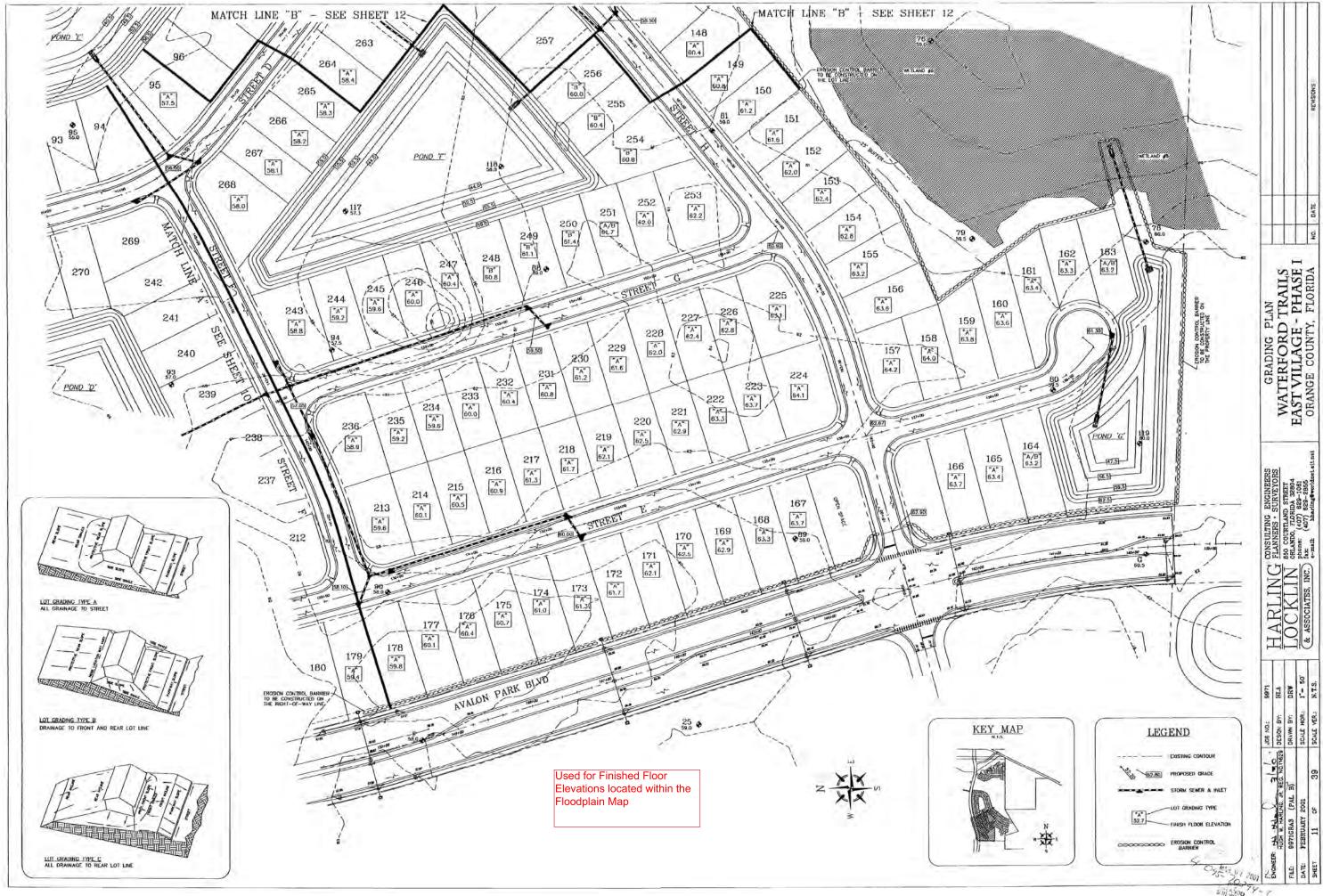


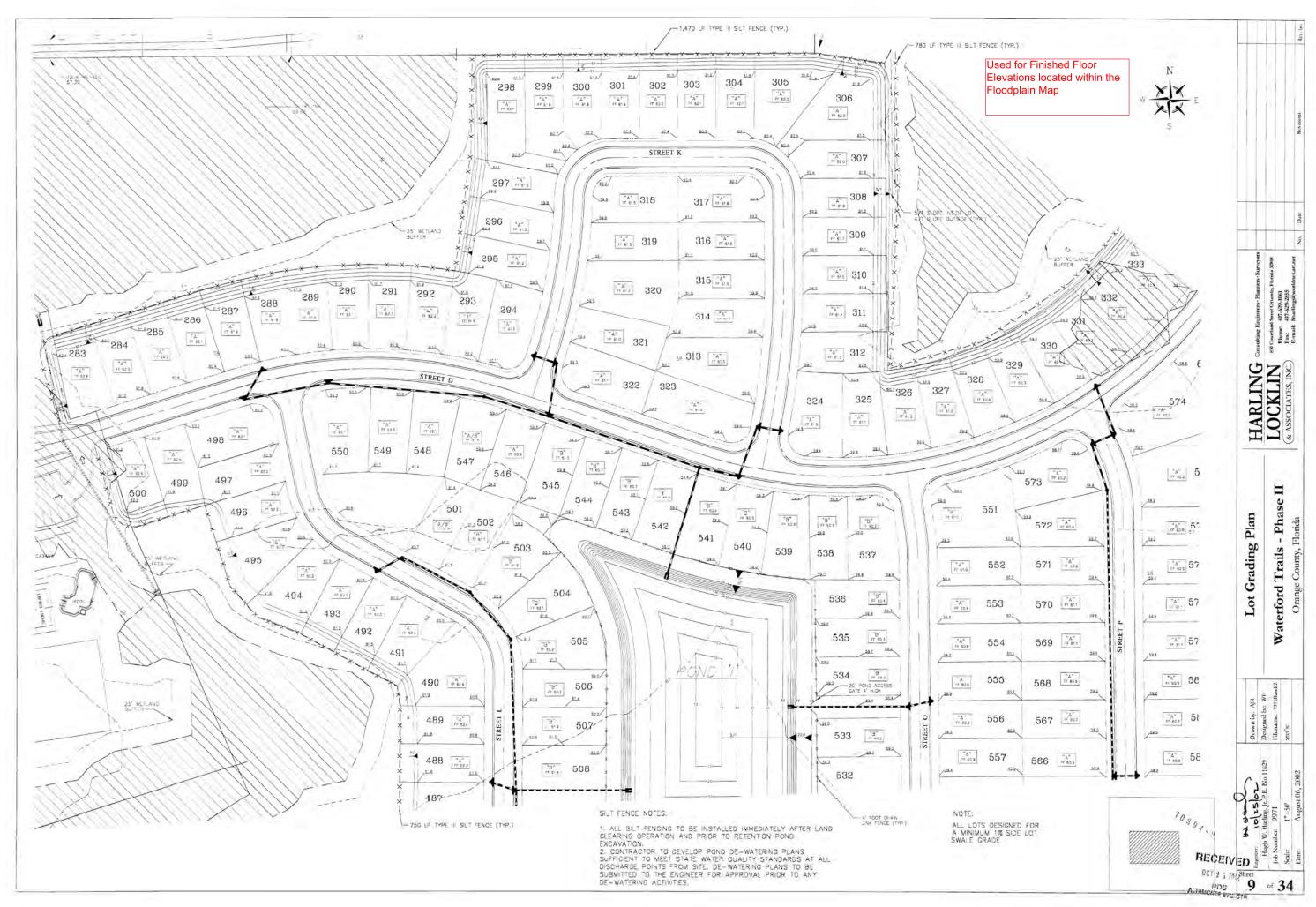


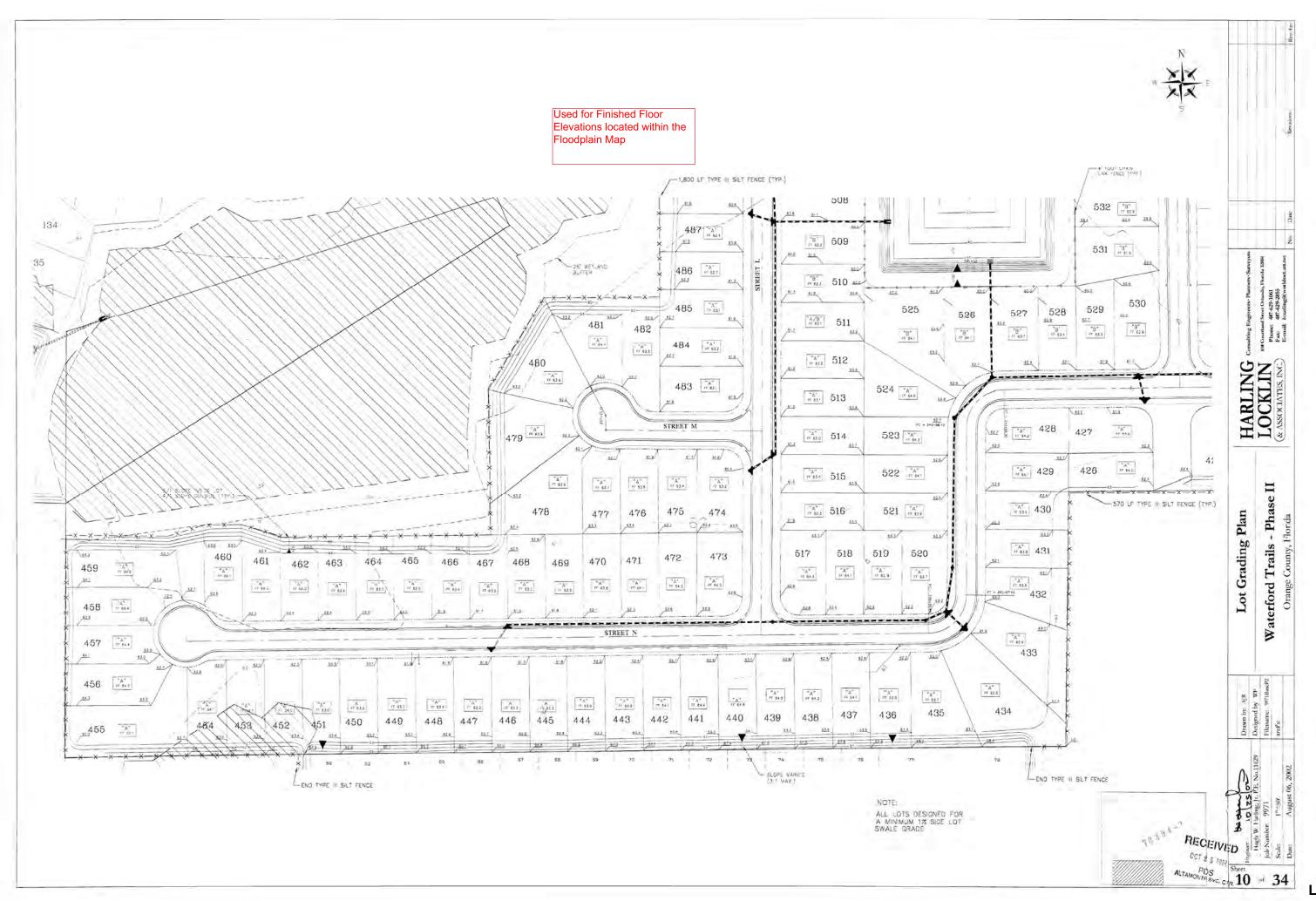
STORMWATER DETAIL SHEET
WATERFORD TRAILS
EAST VILLAGE - PHASE
ORANGE COUNTY, FLORIDA



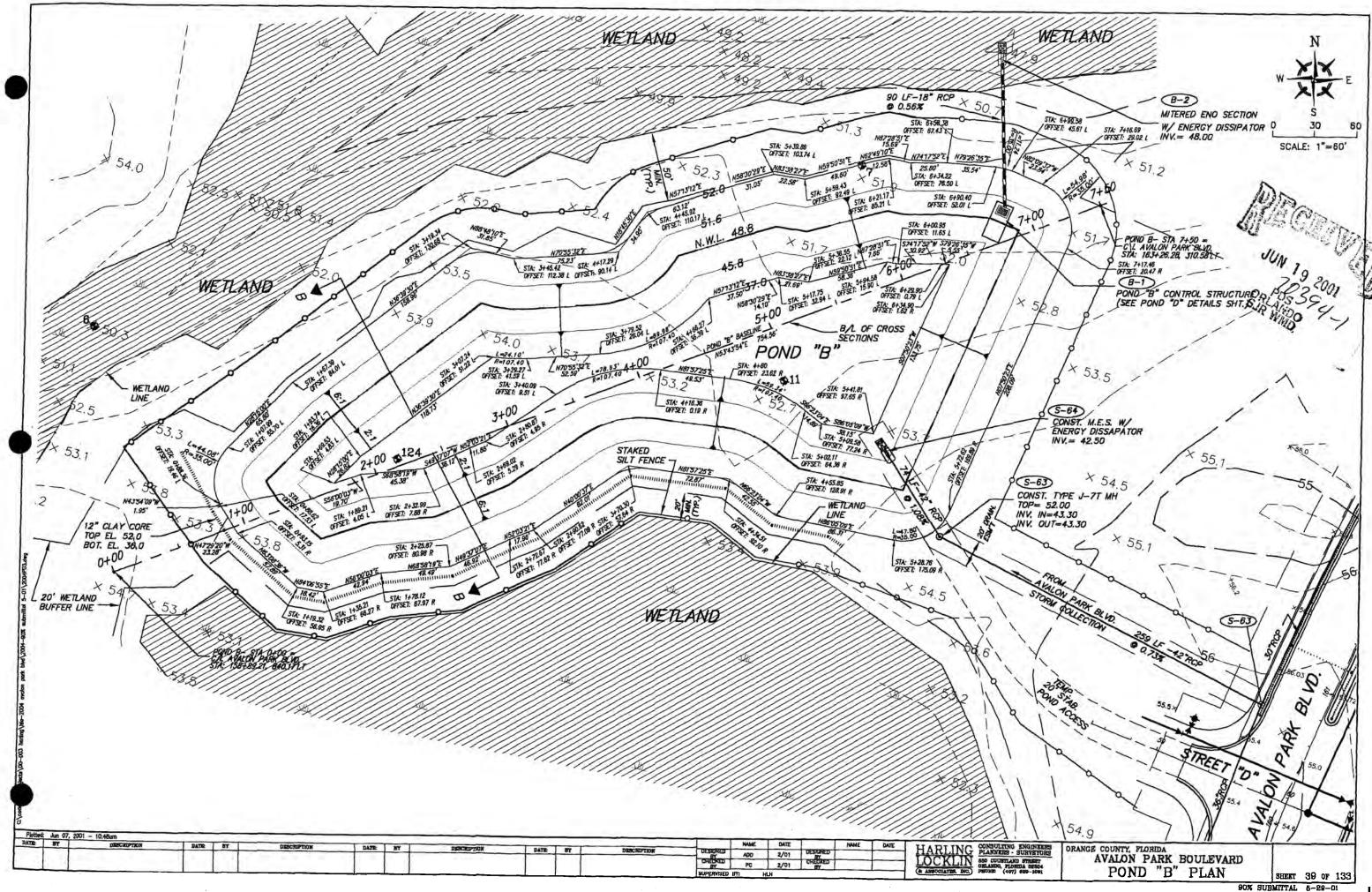


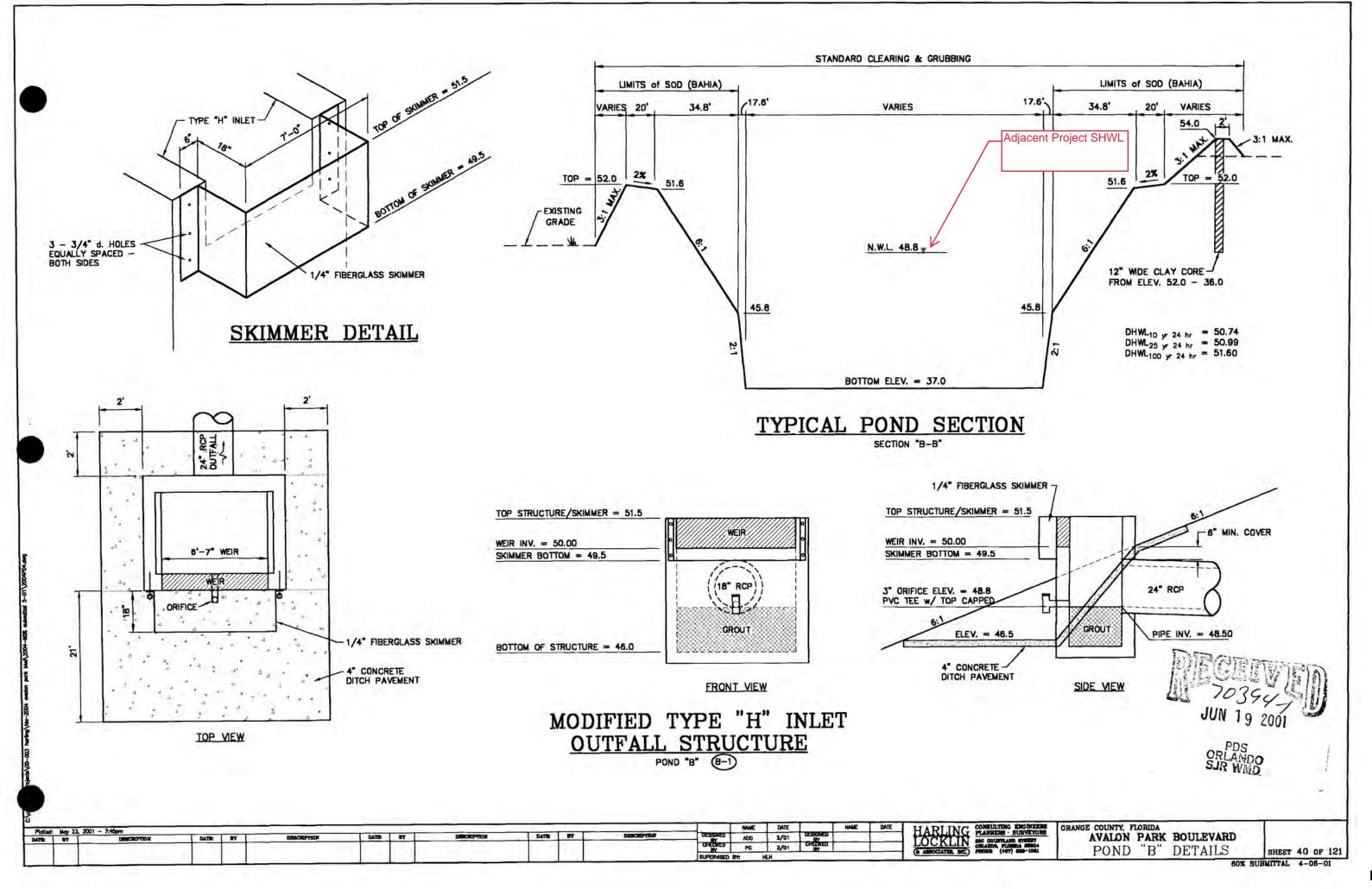


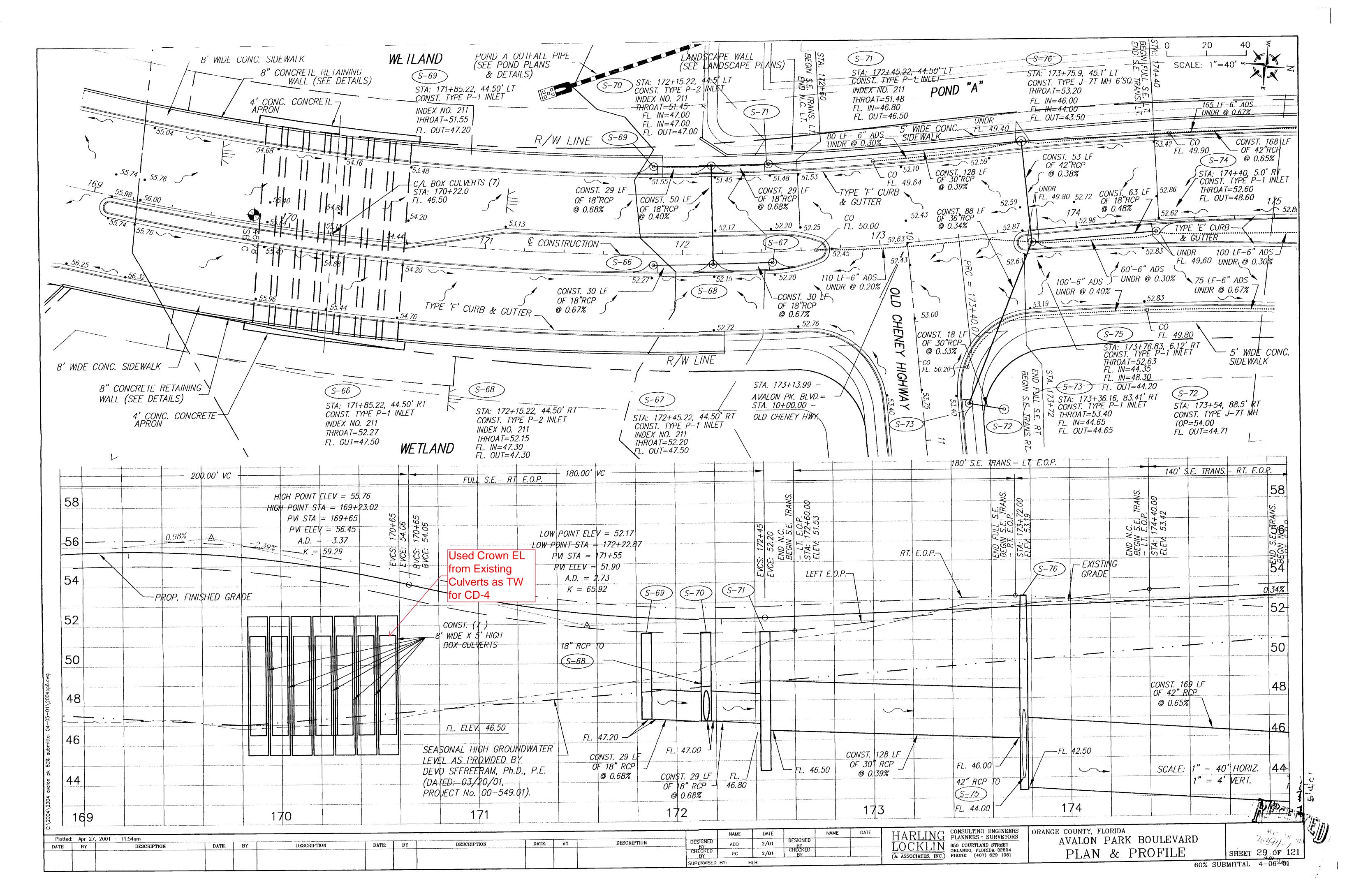


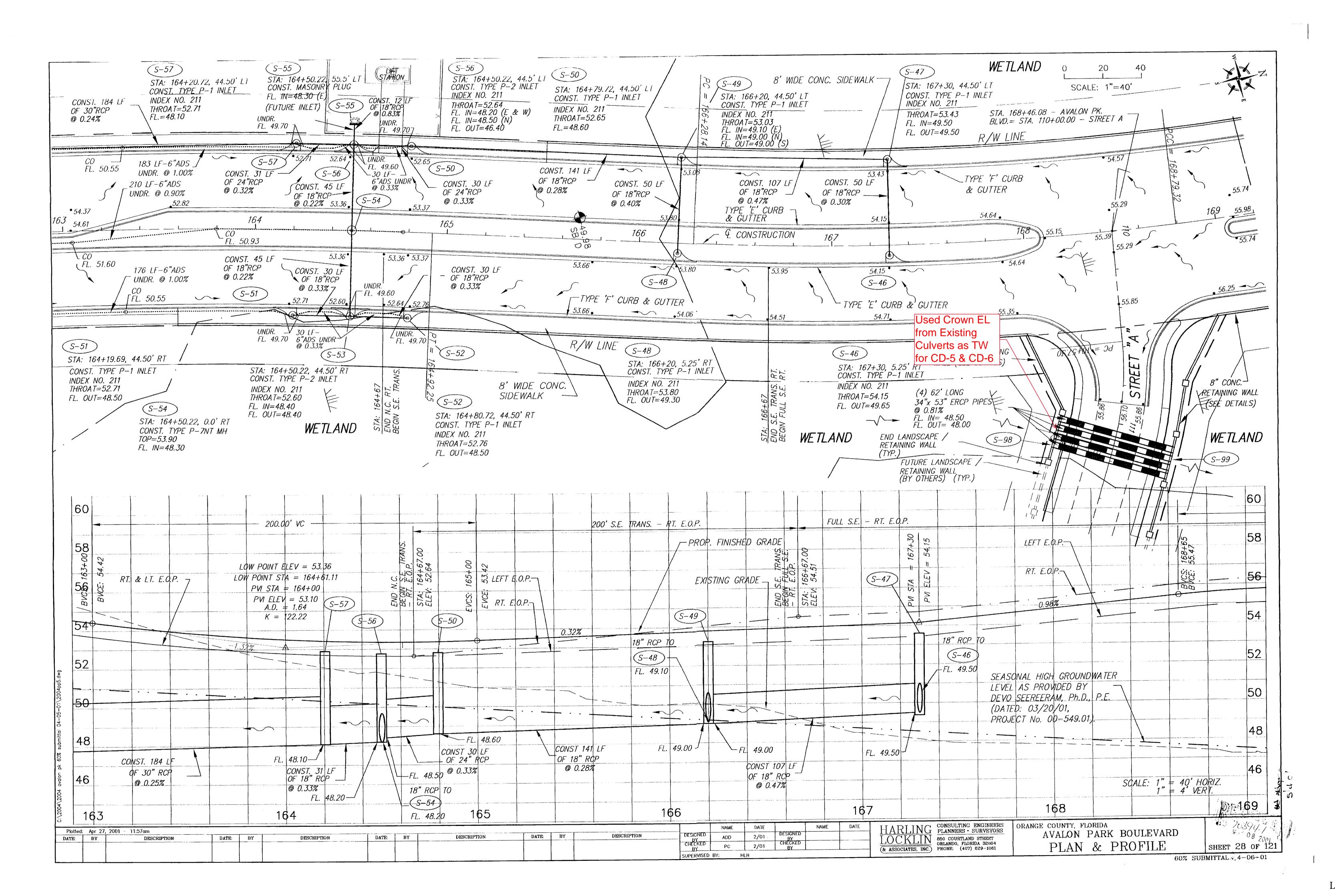








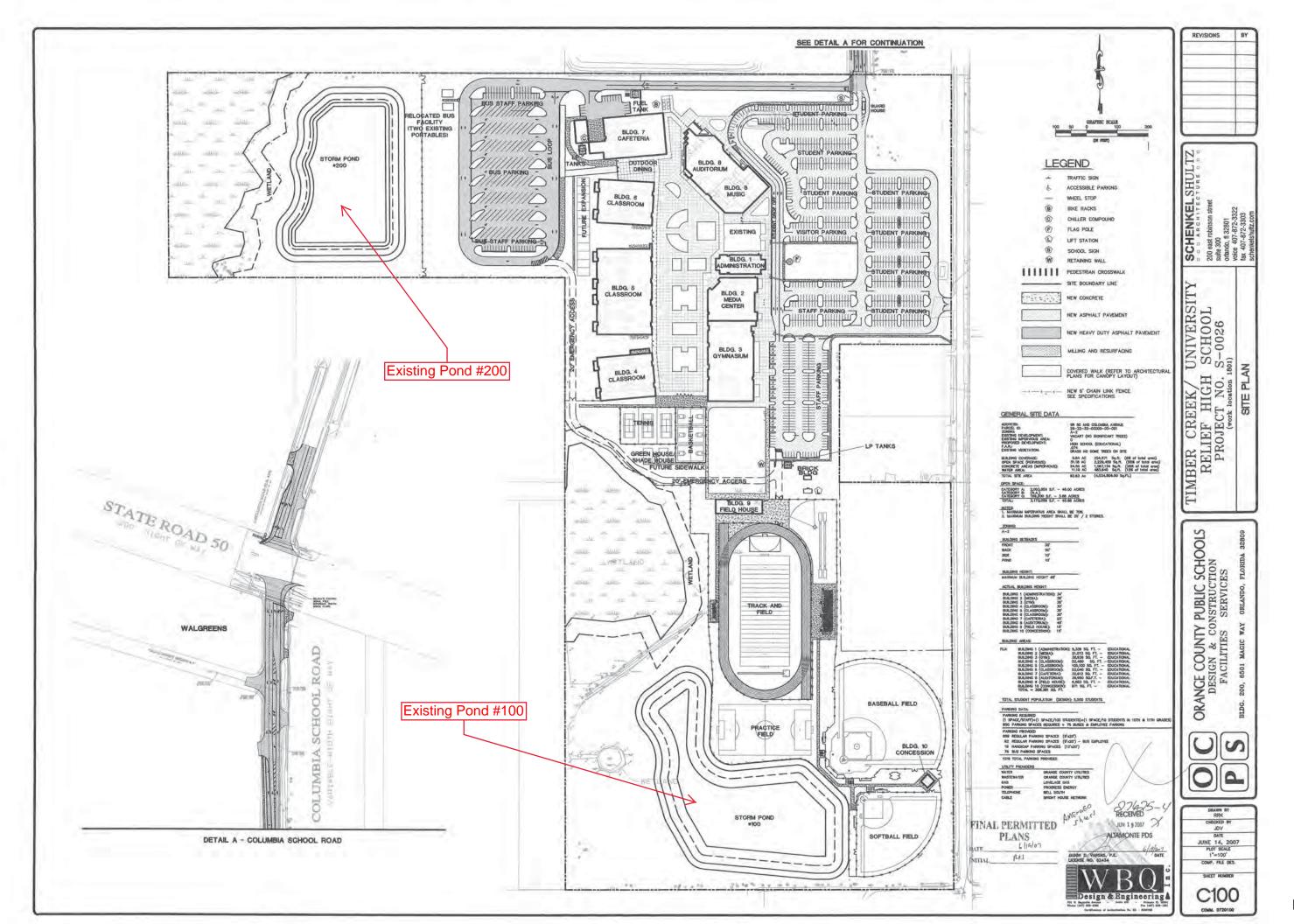


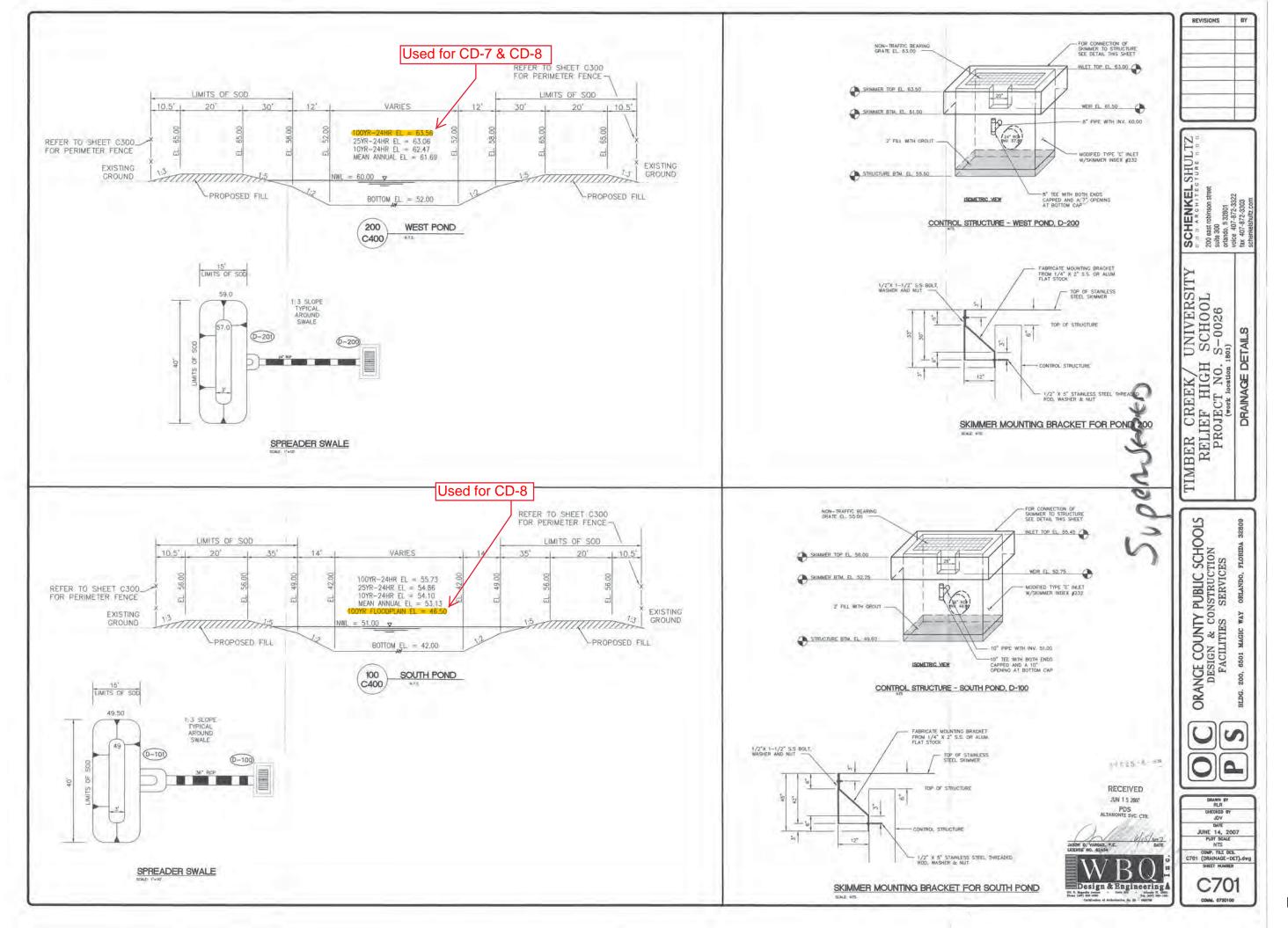


Appendix: M

Excerpt from Orange County Public Schools

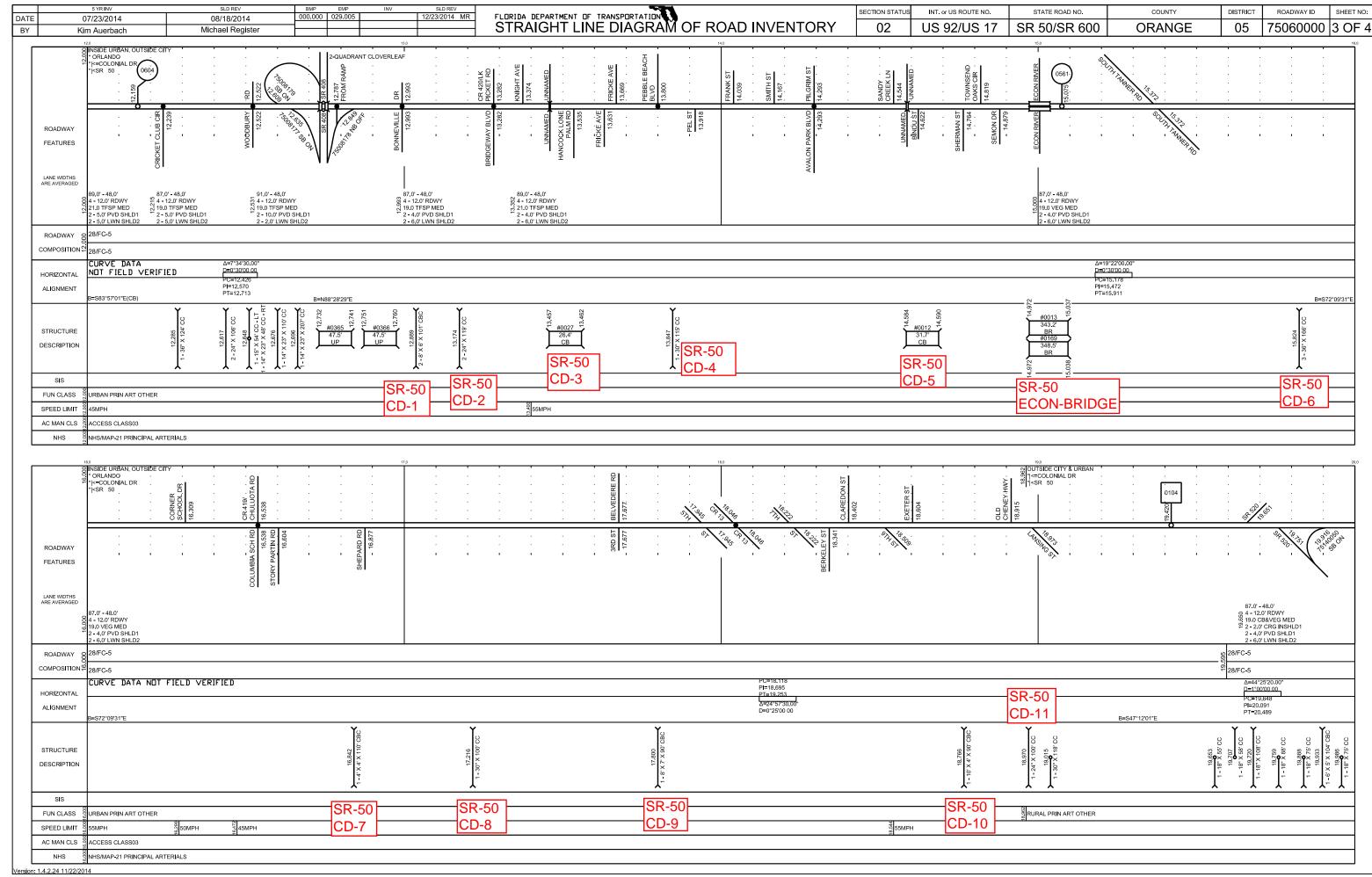
Timber Creek High School Construction Plans





Appendix: N

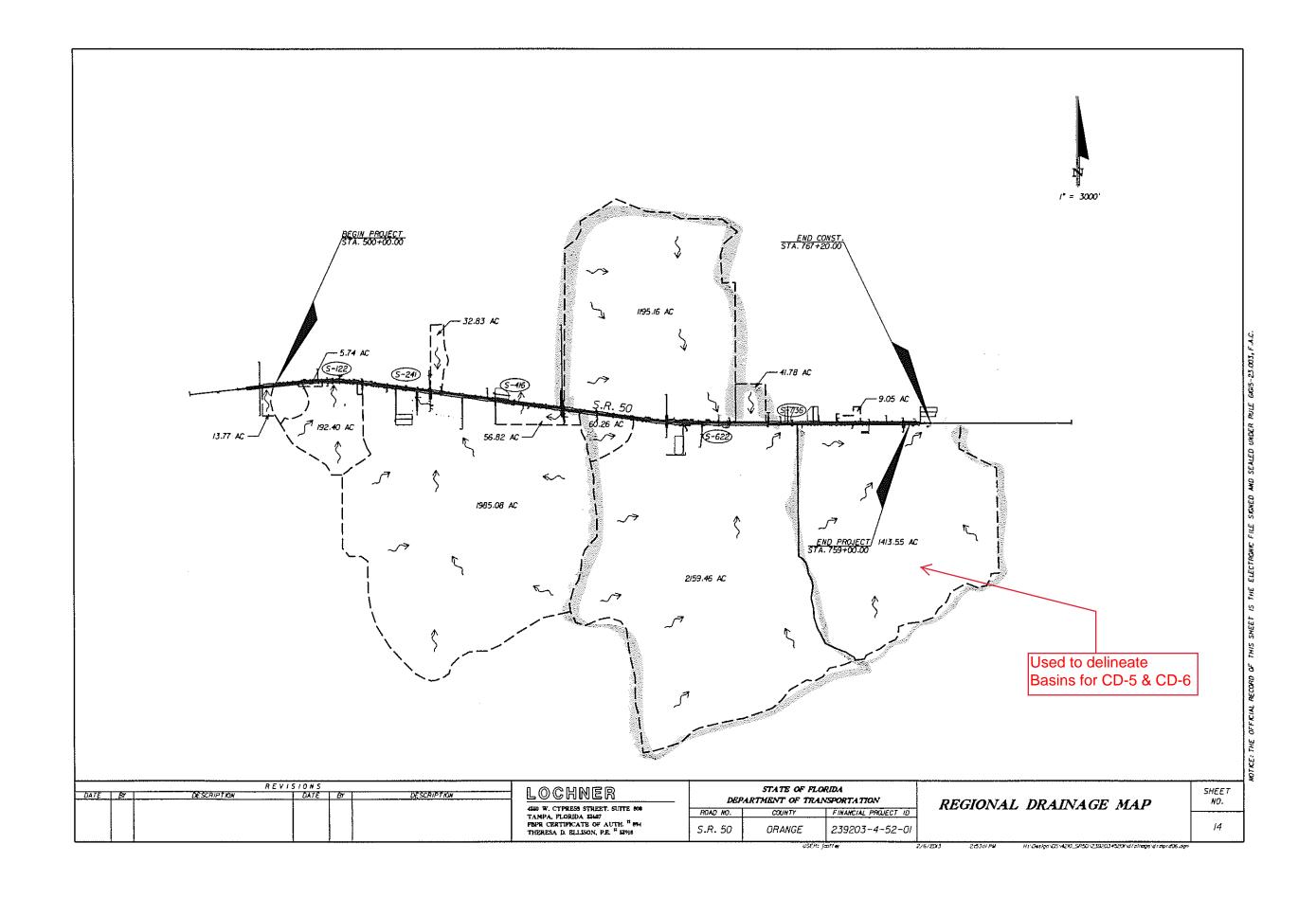
SR-50 Straight Line Diagram



Appendix: O

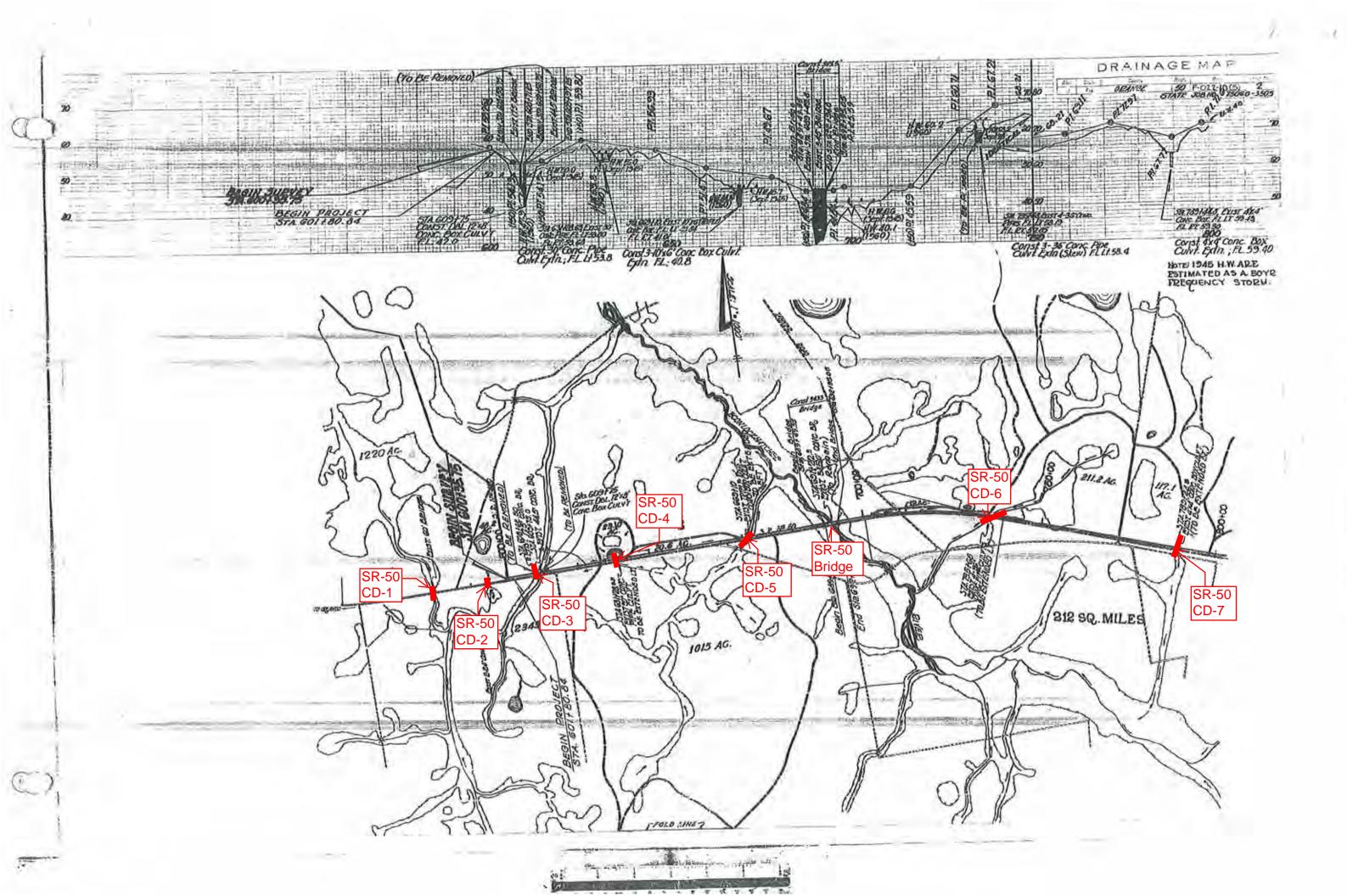
Excerpt from Lochner

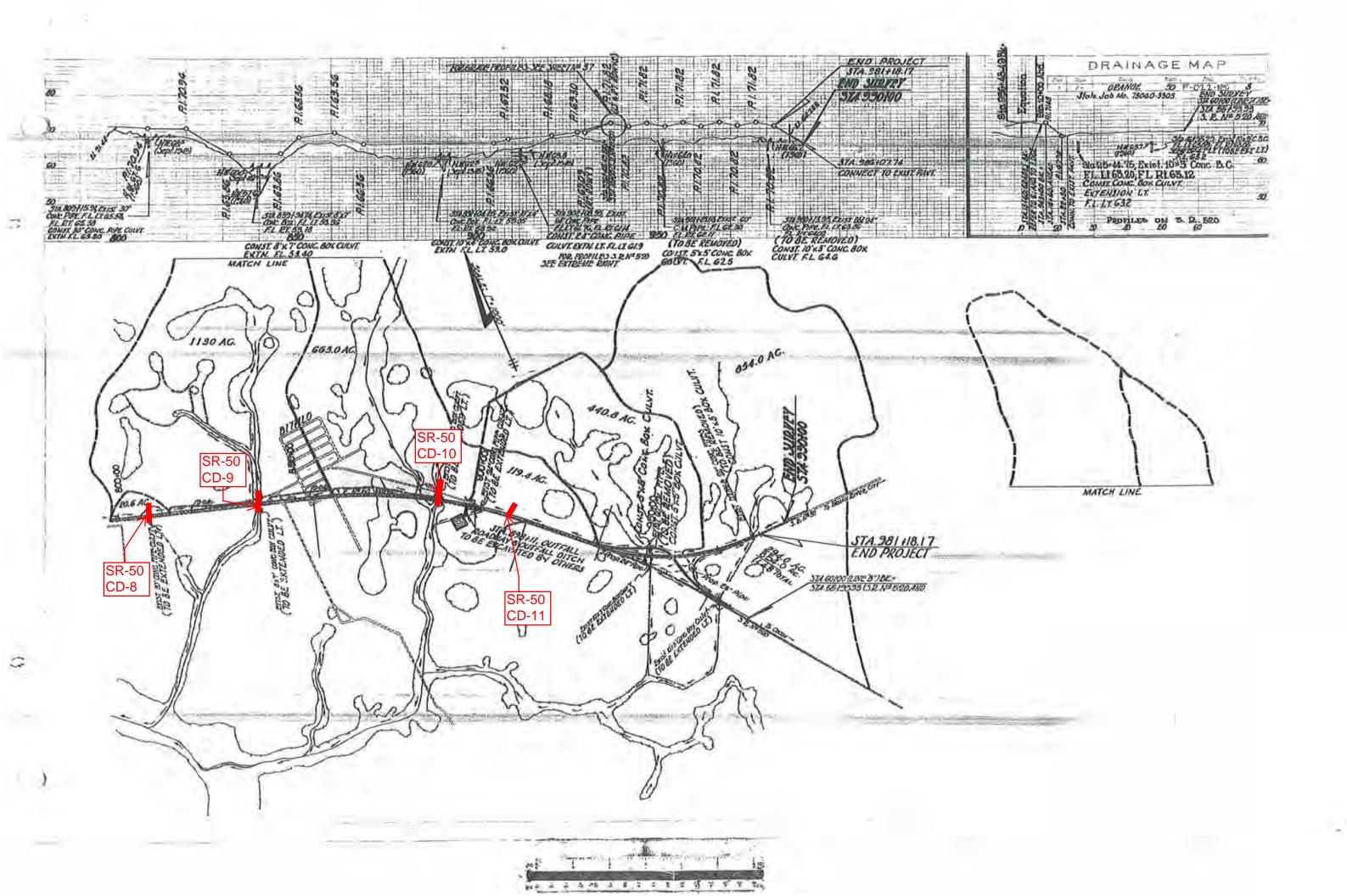
Regional Drainage Map

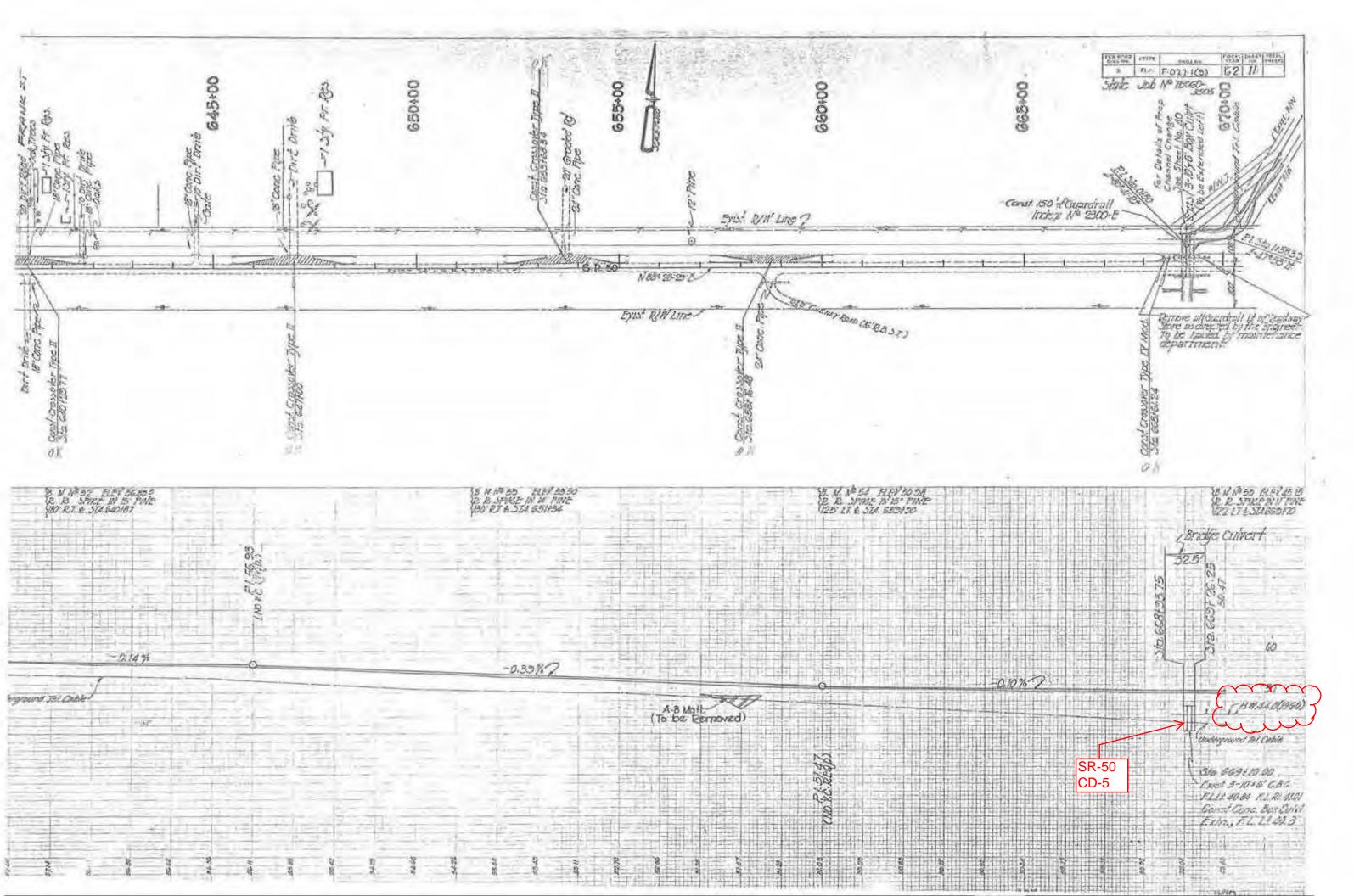


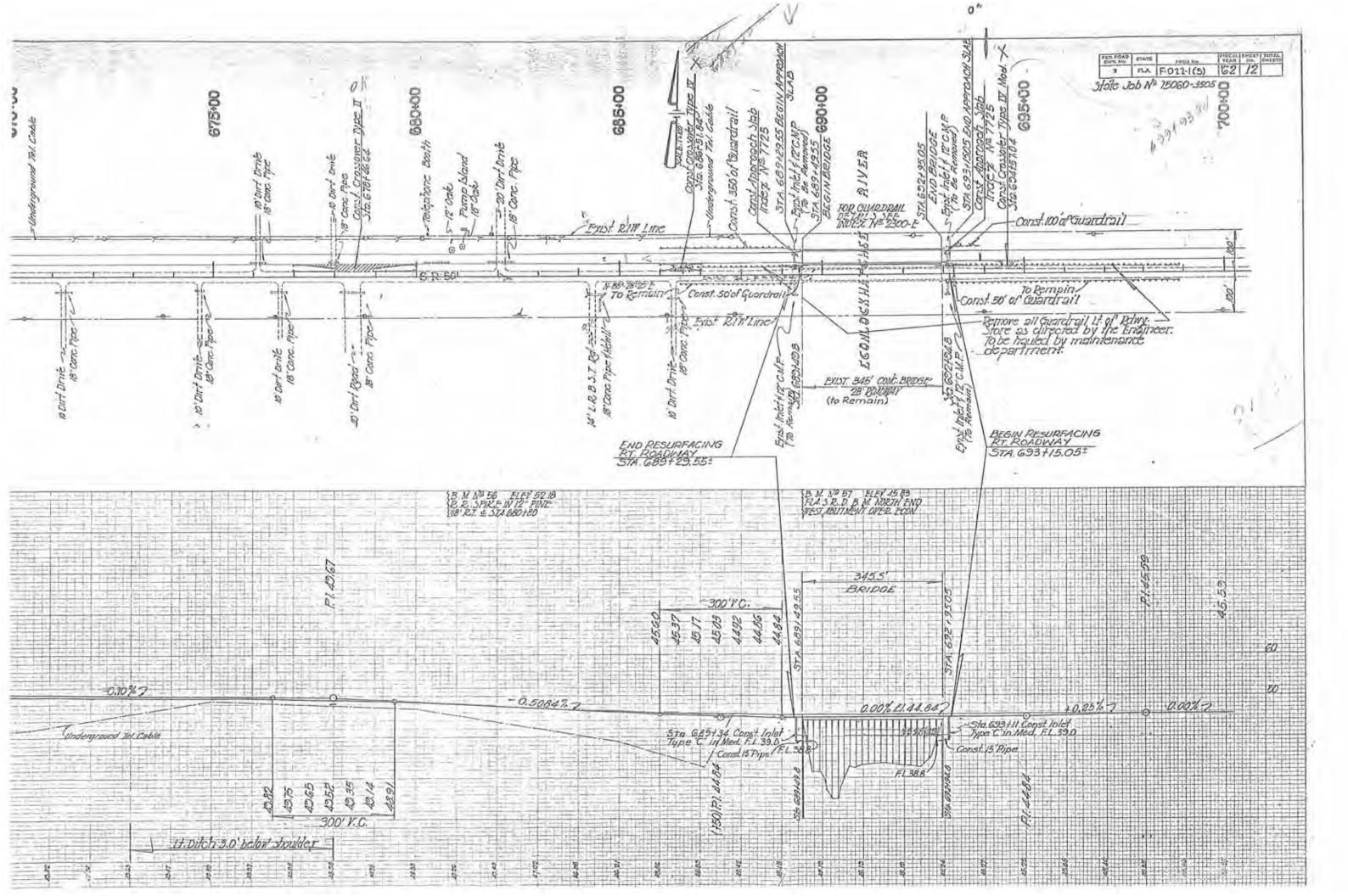
Appendix: P

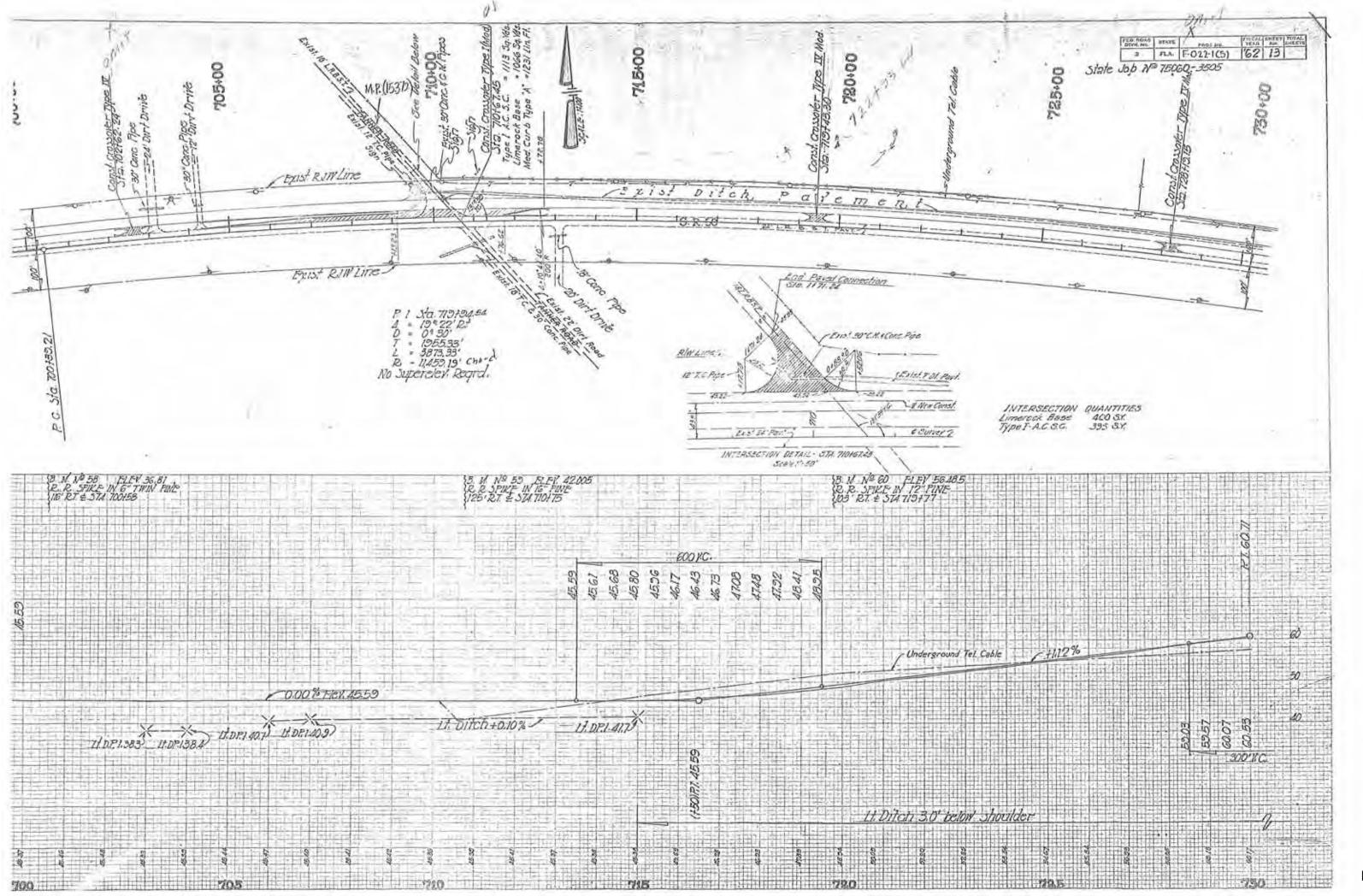
Excerpt from SR-50
Original Construction Plans

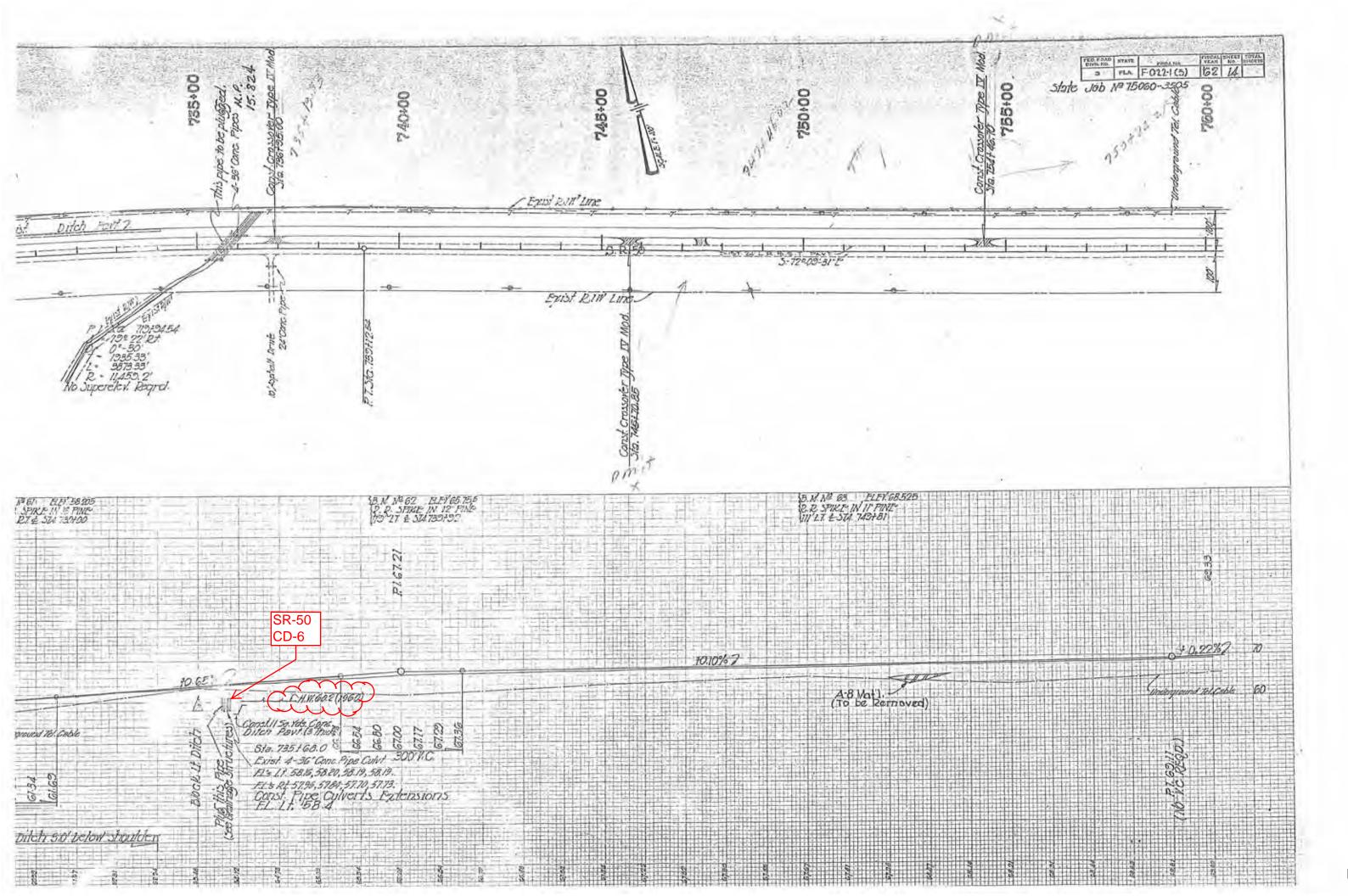


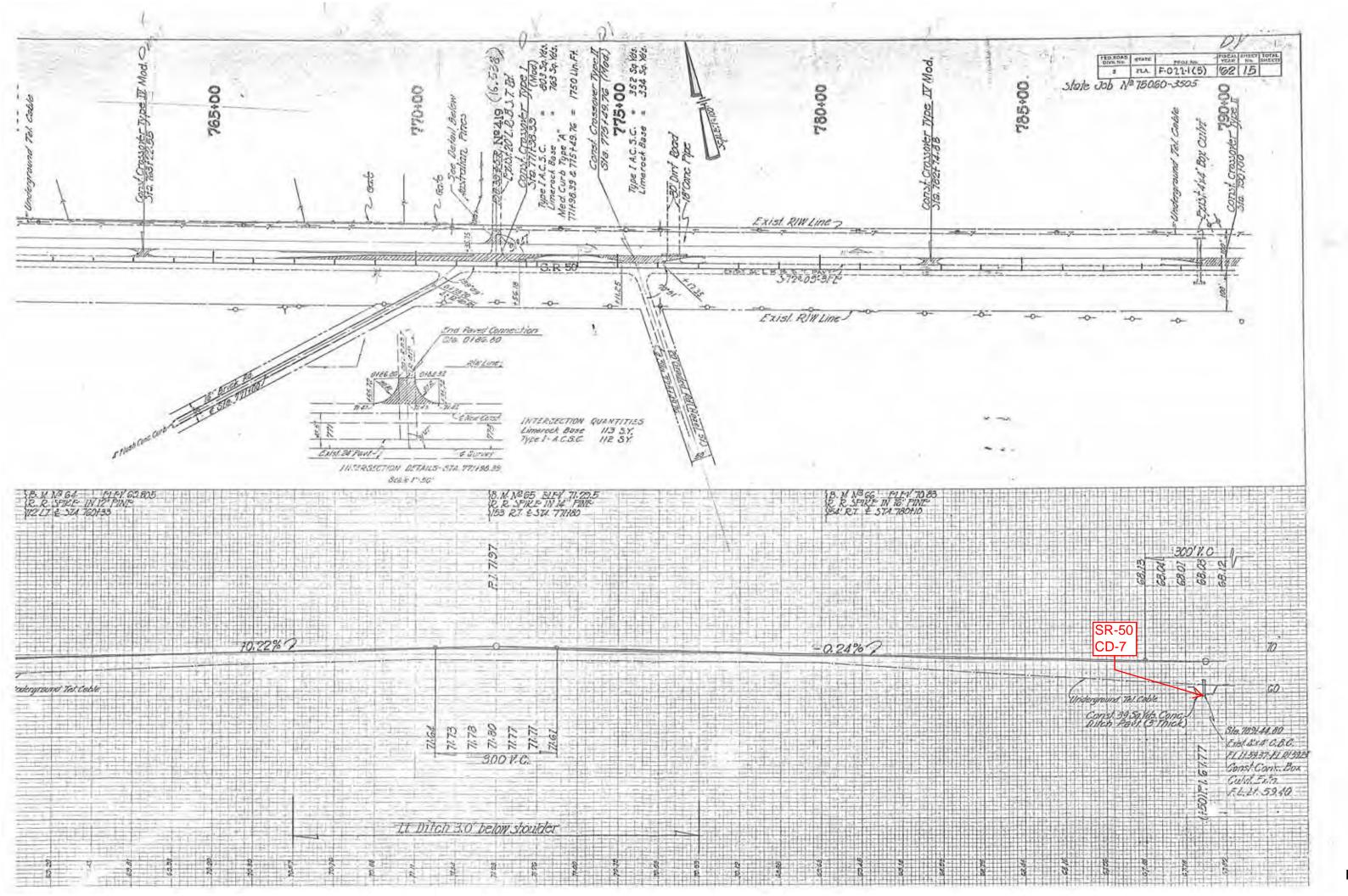


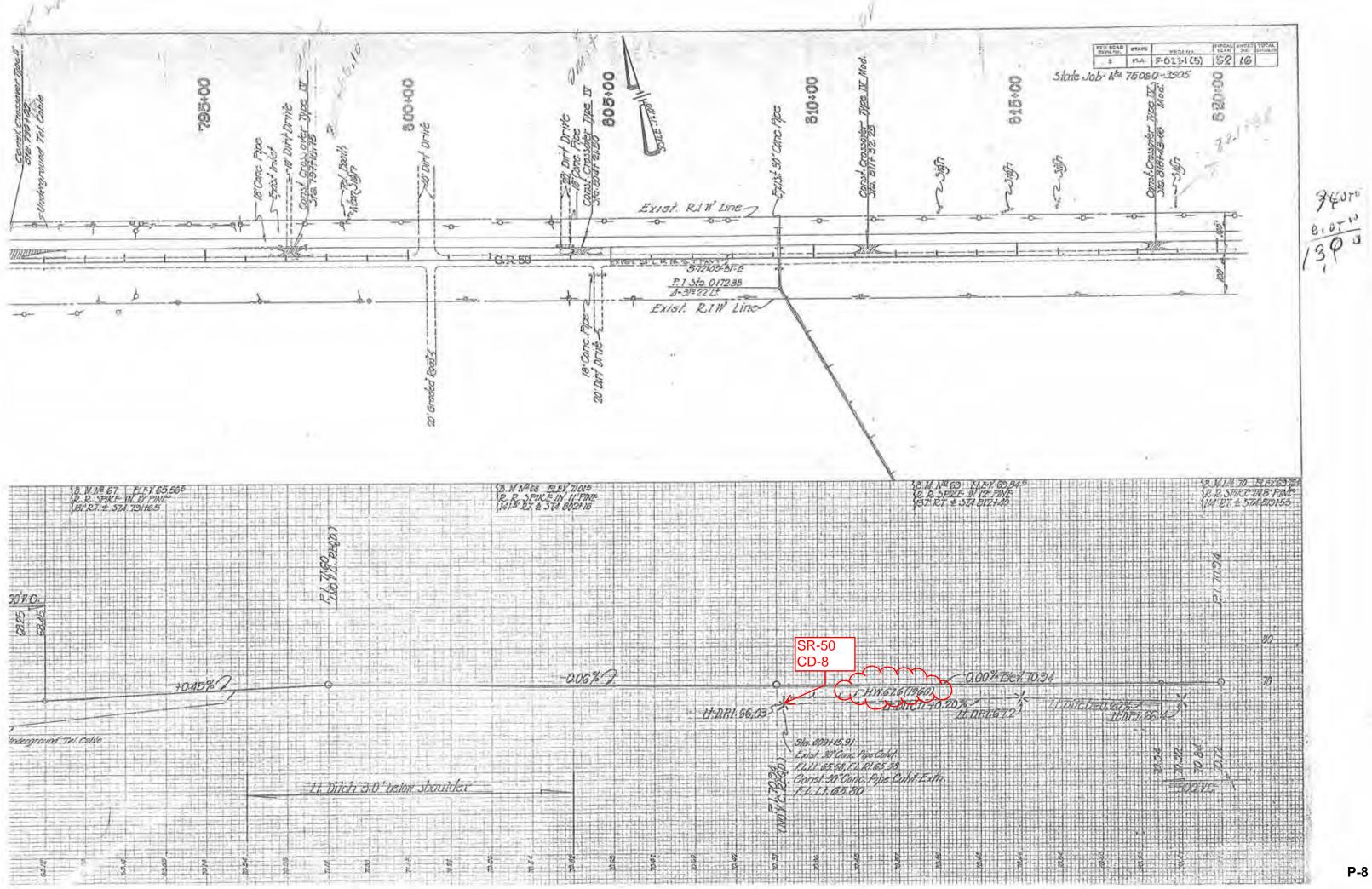


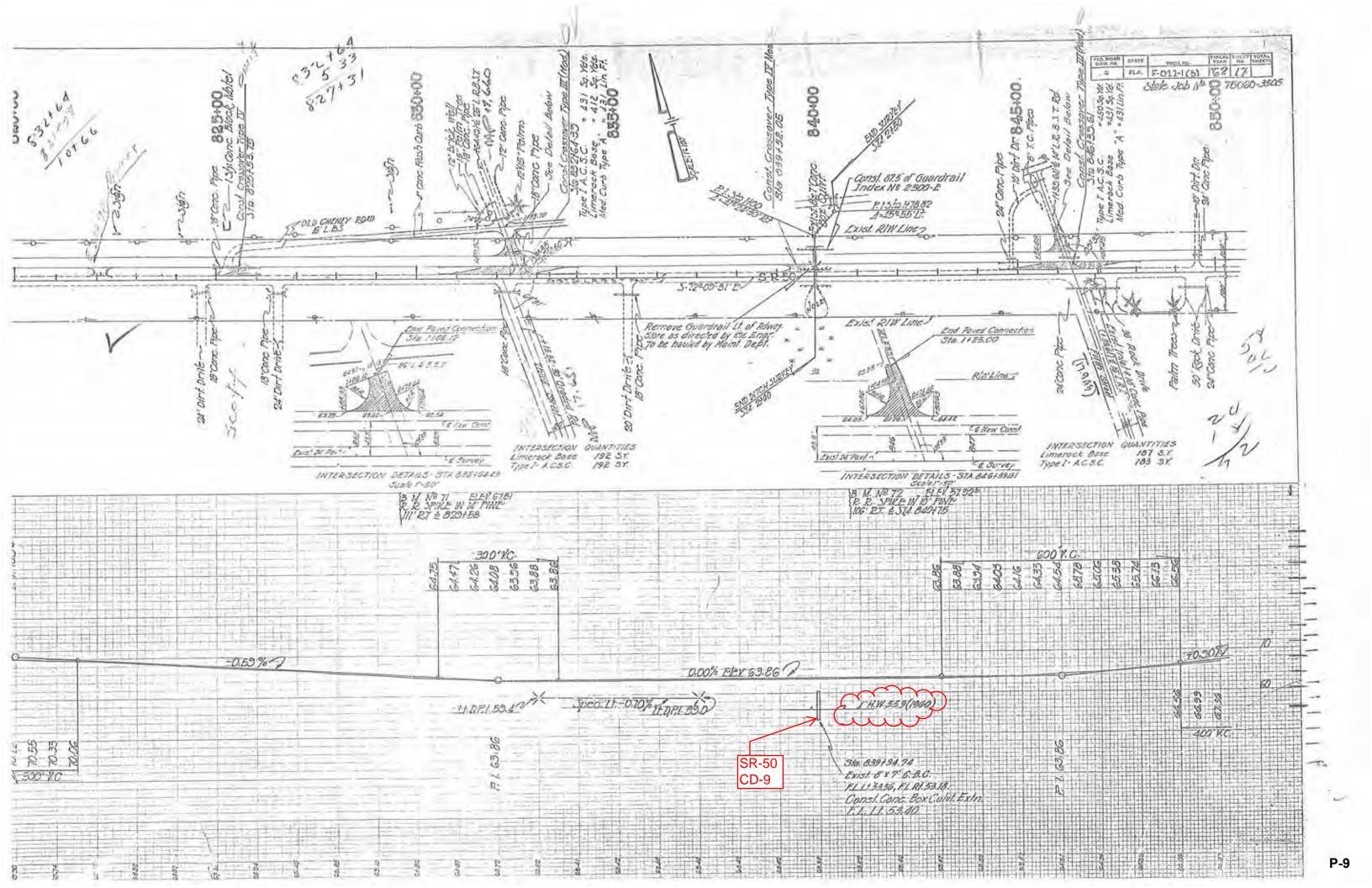


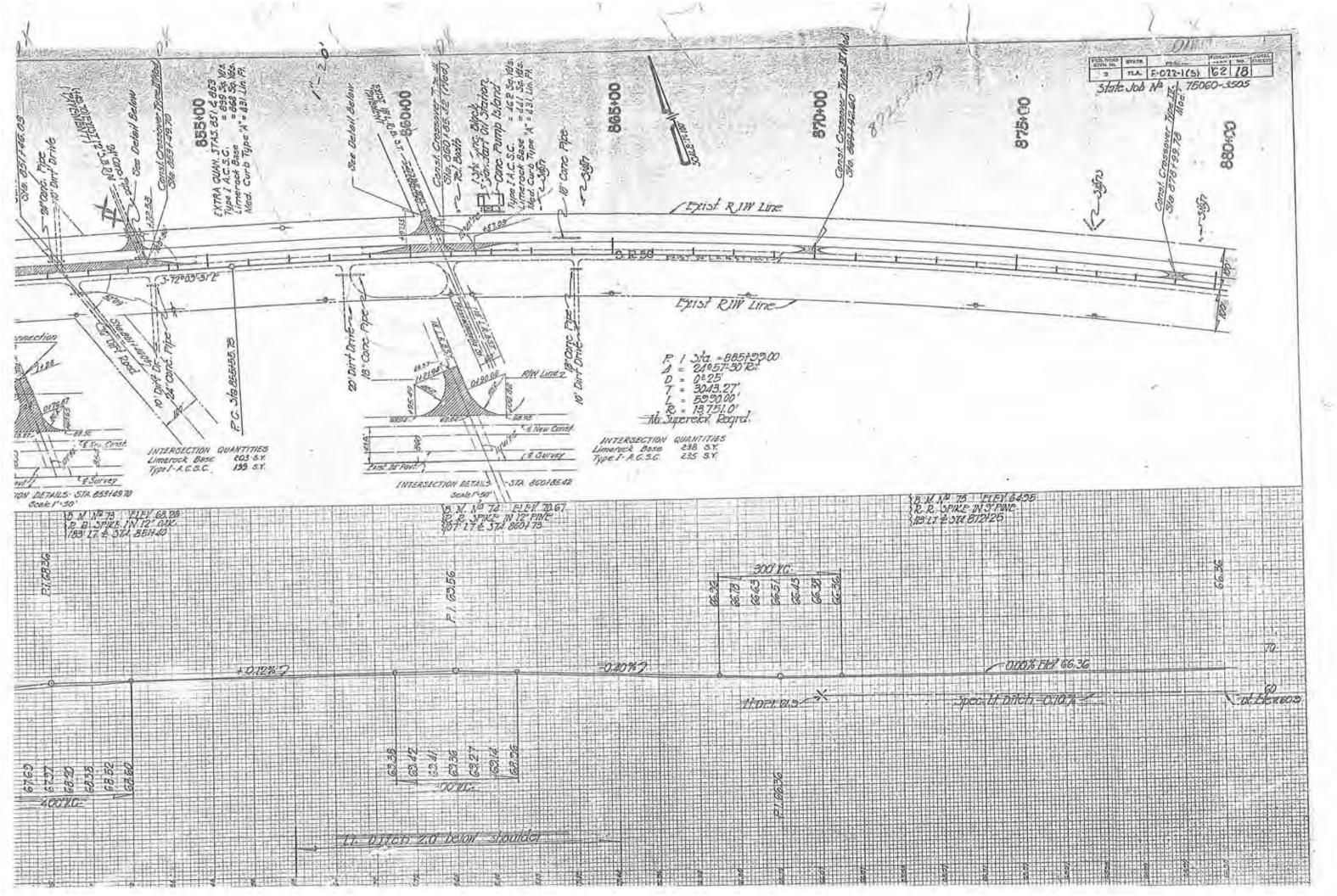


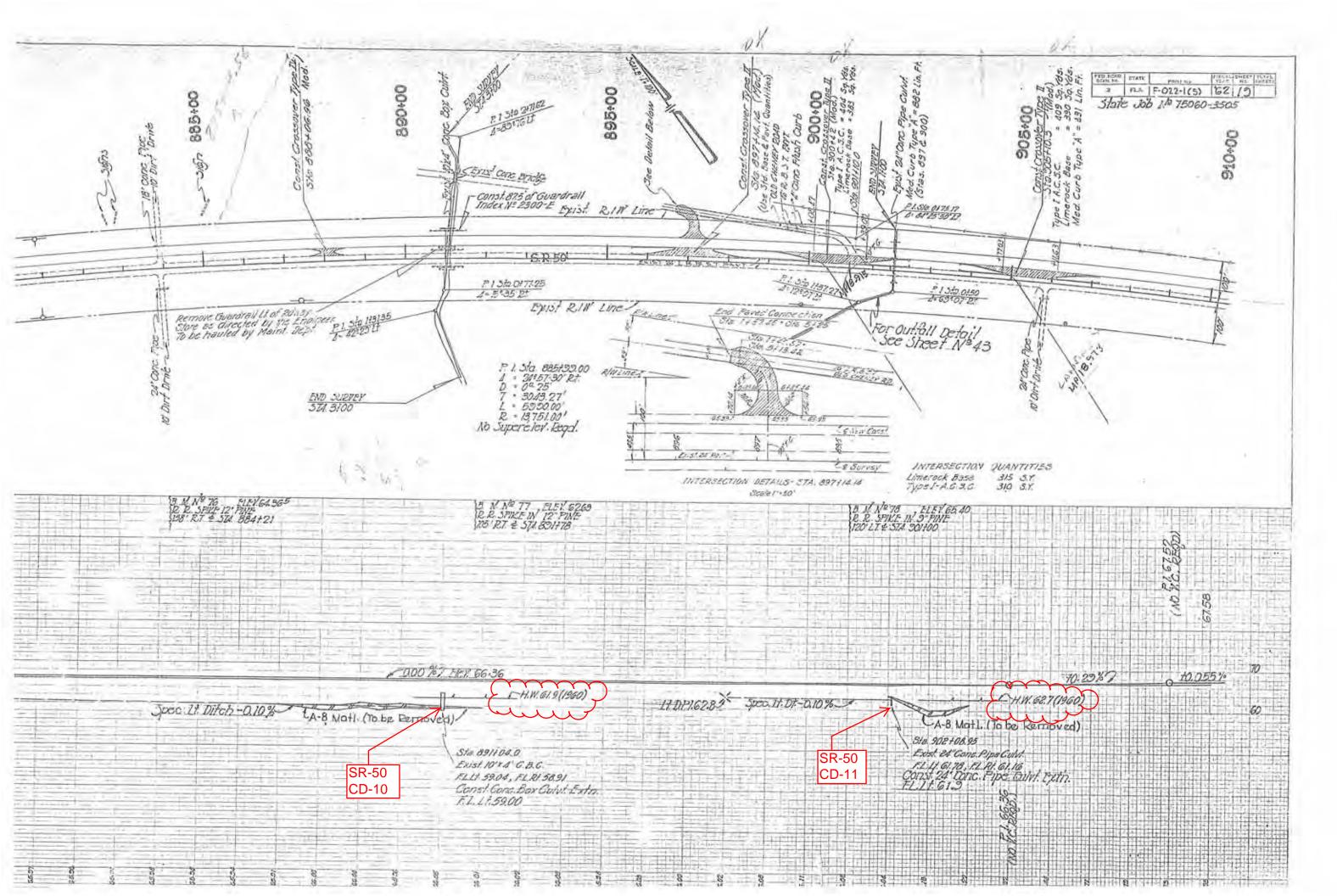


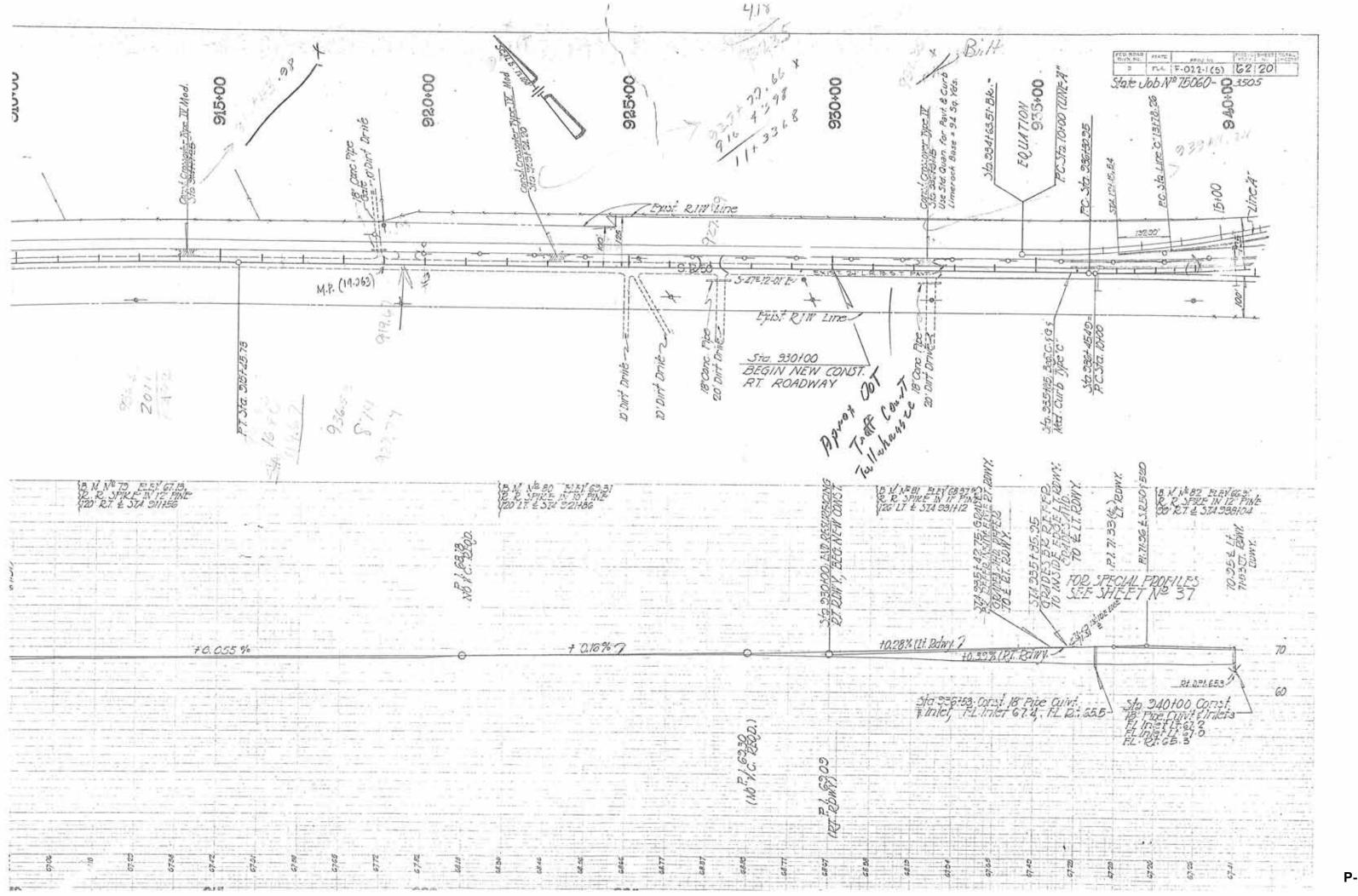


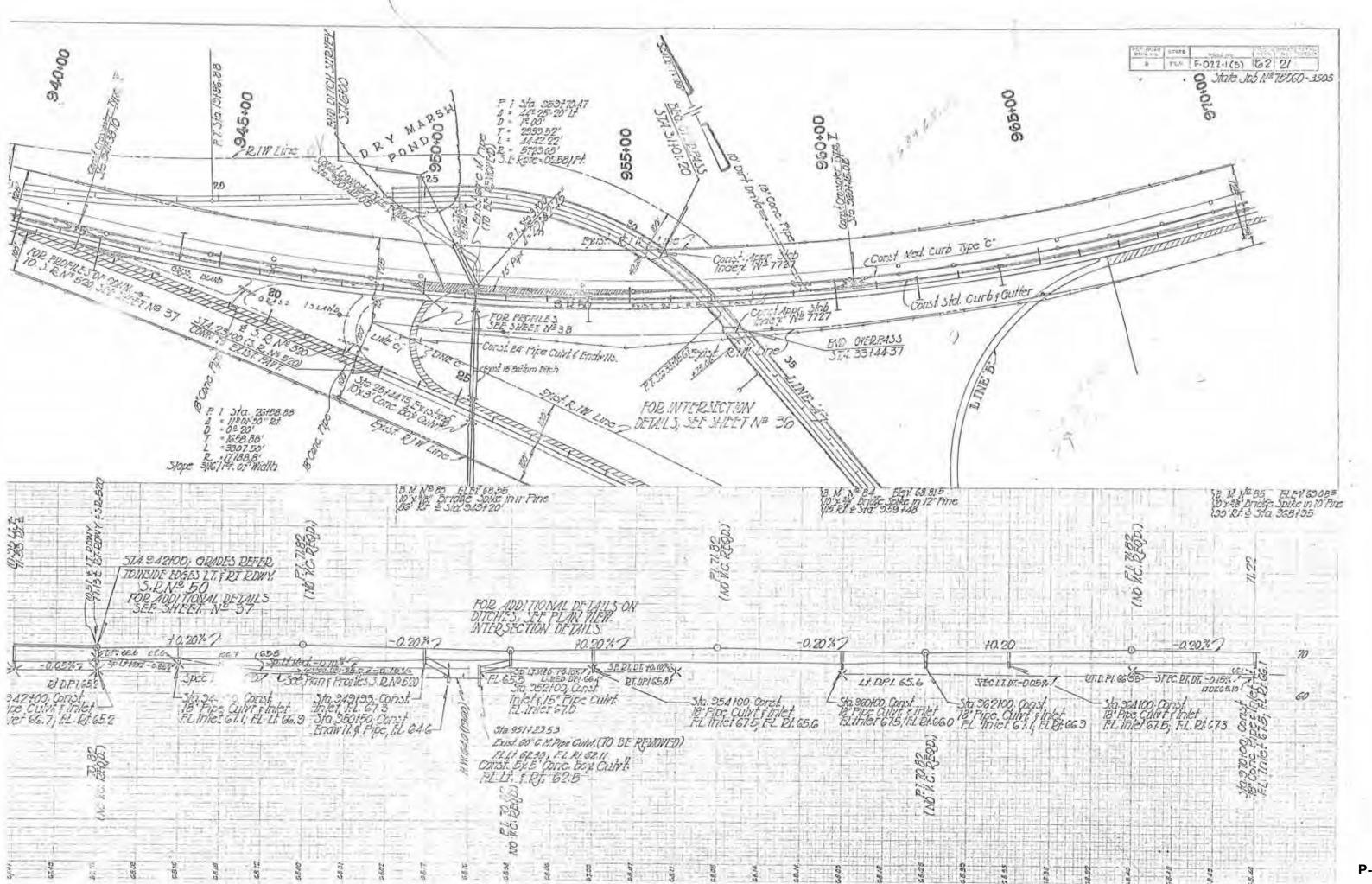












Appendix: Q

Excerpt from Lochner SR-50 Widening Construction Plans

COMPONENTS OF CONTRACT PLANS SET

ROADWAY PLANS SIGNING AND PAVEMENT MARKING PLANS SIGNALIZATION PLANS ITS PLANS

A DETAILED INDEX APPEARS ON THE KEY SHEET OF EACH COMPONENT

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION

CONTRACT PLANS

FINANCIAL PROJECT ID 239203-4-52-01

ORANGE COUNTY (75060)

LOCATION OF PROJECT BRIDGE CULVERT 750833 /BEGIN STA.710+00.05 END STA.710+26.55 FND PROJECT STA. 759+00.00

PENSACOLA

ROADWAY SHOP DRAWINGS TO BE SUBMITTED TO:

JOHN N. BOX P.E. NO. 41832 H.W. LOCHNER INC. 13577 FEATHER SOUND DR. SUITE 600 CLEARWATER, FLORIDA 33762

PIERCE

I AUDERDALE

PLANS PREPARED BY:

LOCHNER

H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 13577 FEATHER SOUND DR., SUITE 600 CLEARWATER, FLORIDA 33762 VENDOR NO. 36-233881 CONTRACT NO. C-7461 C.A. 894

NOTE: THE SCALE OF THESE PLANS MAY HAVE CHANGED DUE TO REPRODUCTION.

PLANS UPDATE PERMIT SUBMITTAL SEPTEMBER 2012

STATE ROAD NO. 50 SHEET NO. SHEET DESCRIPTION KFY SHFFT TO SANFORD TO OVIEDO NOTES TO REVIEWER BRIDGE CULVERT 750832 SUMMARY OF PAY ITEMS BEGIN STA. 556+57.26 II - 12 DRAINAGE MAP END STA. 556+90.61 15 - 33 TYPICAL SECTIONS -34 - 48 SUMMARY OF QUANTITIES 49 - 52 BRIDGE CULVERT DETAILS -53 - 63 REPORT OF BORINGS 64 - 78 SUMMARY OF DRAINAGE STRUCTURES OPTIONAL MATERIAL TABULATION BEGIN PROJECT GENERAL NOTES 81 - 82 PROJECT LAYOUT STA. 500+00.00 83 - 85 REFERENCE TIES MP 9.467 120 - 125 ROADWAY PLAN-PROFILES -126 - 150 SIDE STREET PROFILES -151 - 154 RAMP TERMINAL DETAILS TO ORLANDO -155 - 158 INTERSECTION DETAILS -159 - 330 DRAINAGE STRUCTURES Miles POND DETAILS 338 - 340 DRAINAGE DETAILS TO TITUSVILLE SPECIAL DETAILS INTERCHANGE CROSS SECTION PATTERN SHEET ROADWAY SOIL SURVEY 602 - 605 CROSS SECTIONS -629 - 630 DRIVEWAY SECTIONS -631 - 664 STORMWATER POLLUTION PREVENTION PLAN--665 - 772 TRAFFIC CONTROL PLANS 773 - 818 UTILITY ADJUSTMENTS -819 - 828 CRITICAL TEMPORARY SHEET PILE WALL DETAILS -829 - 830 CONCRETE ENDWALL DETAILS -30-E -31-E EQUATION: STA. 684+57.21 & CONST. (BK.) = STA. 684+58.35 € CONST. (AH.) = TO KISSIMMEE STA. 684+58.35 ₽ SURVEY (AH.)

GOVERNING STANDARDS AND SPECIFICATIONS: FLORIDA DEPARTMENT OF TRANSPORTATION. DESIGN STANDARDS DATED 2010, AND SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION DATED 2010, AS AMENDED BY CONTRACT DOCUMENTS.

APPLICABLE DESIGN STANDARDS MODIFICATIONS: 7-1-2013

FOR DESIGN STANDARDS MODIFICATIONS CLICK ON "DESIGN STANDARDS" AT THE FOLLOWING WEB SITE: http://www.dot.state.fl.us/rddesign/

REVISIONS

PROJECT LENGTH IS BASED ON & CONSTRUCTION *I F NGTH* 0F PROJECT LINEAR FEET MILES ROADWAY 25,898.86 4.905 BRIDGES NΔ NA NET LENGTH OF PROJECT 25,898.86 4.905 EXCEPTIONS NΑ NΔ GROSS LENGTH OF PROJECT 25,898.86 4.905 FDOT PROJECT MANAGER: CHRISTOPHER L. DABSON, P.E.

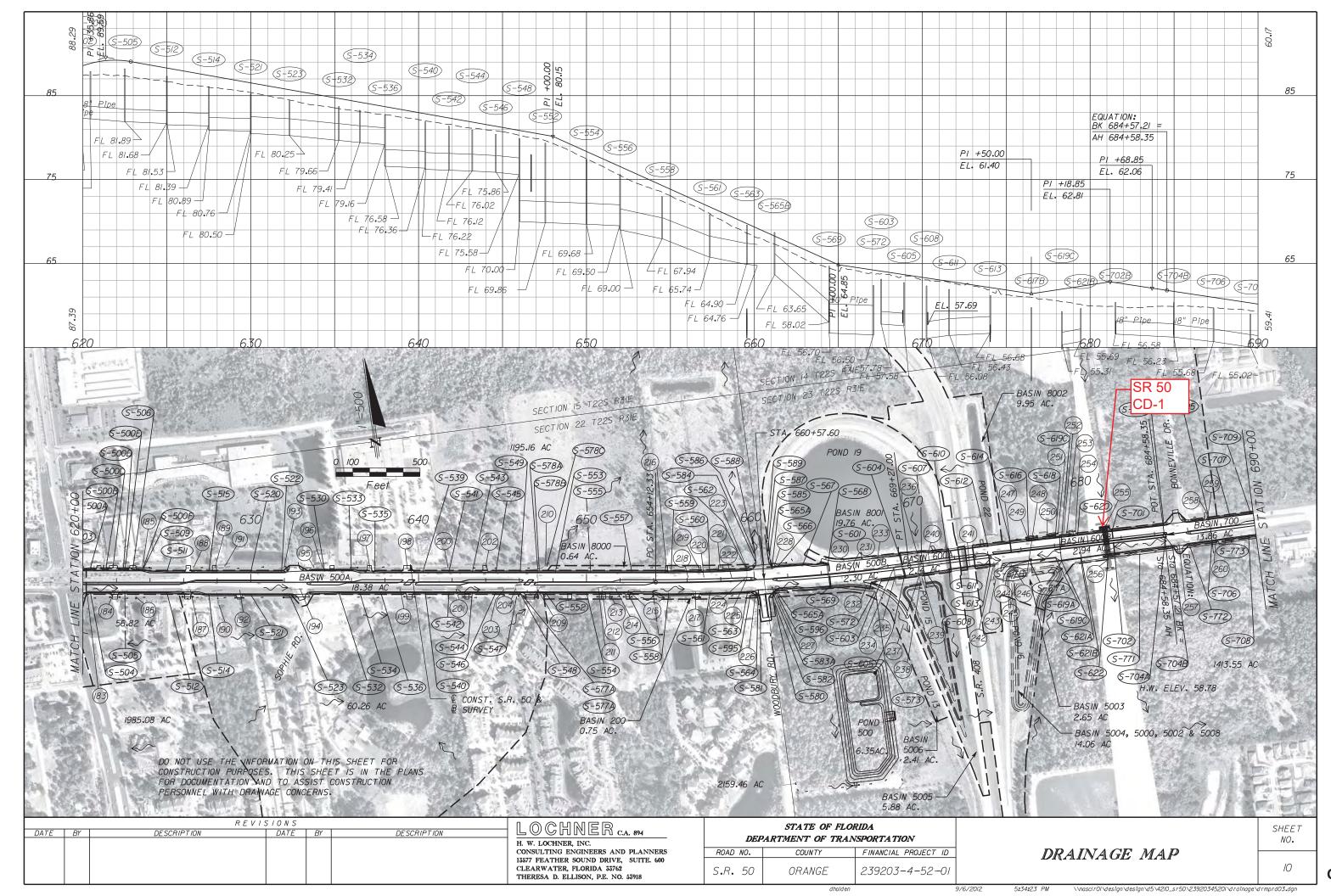
KEY SHEET REVISIONS

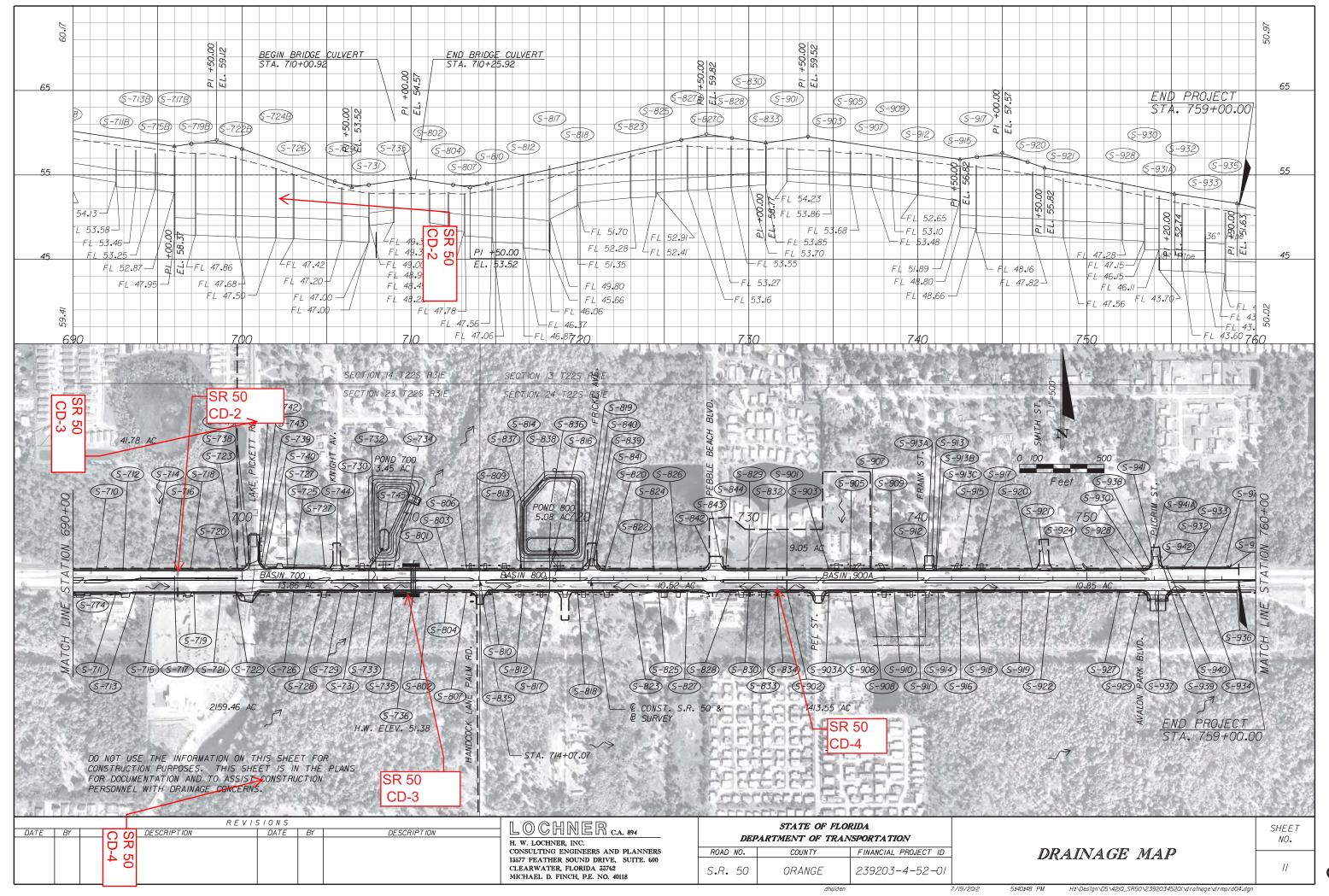
ROADWAY PLANS ENGINEER OF RECORD (E.O.R.): JOHN N. BOX, P.E. P.E. NO.: 41832 FISCAL SHEET

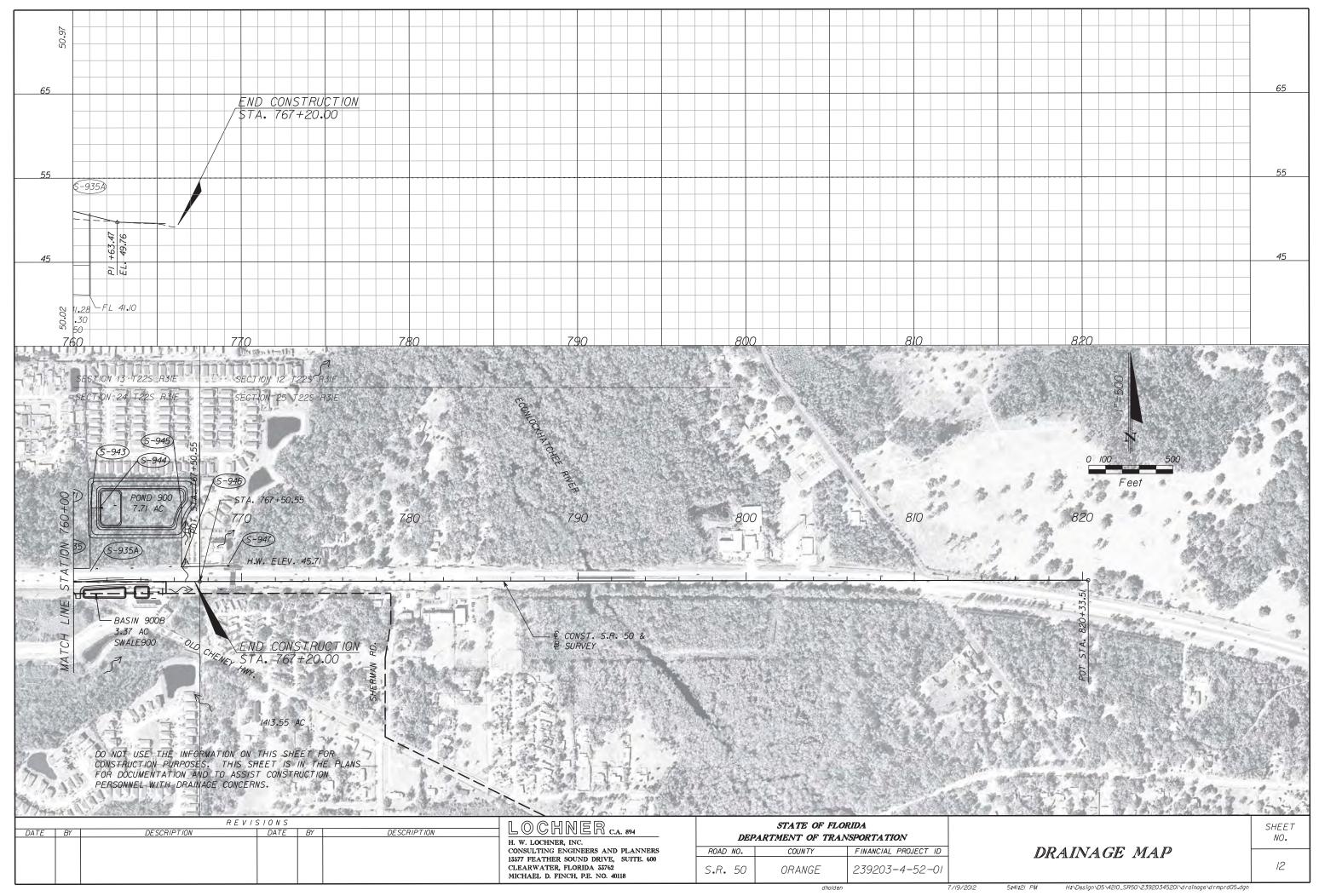
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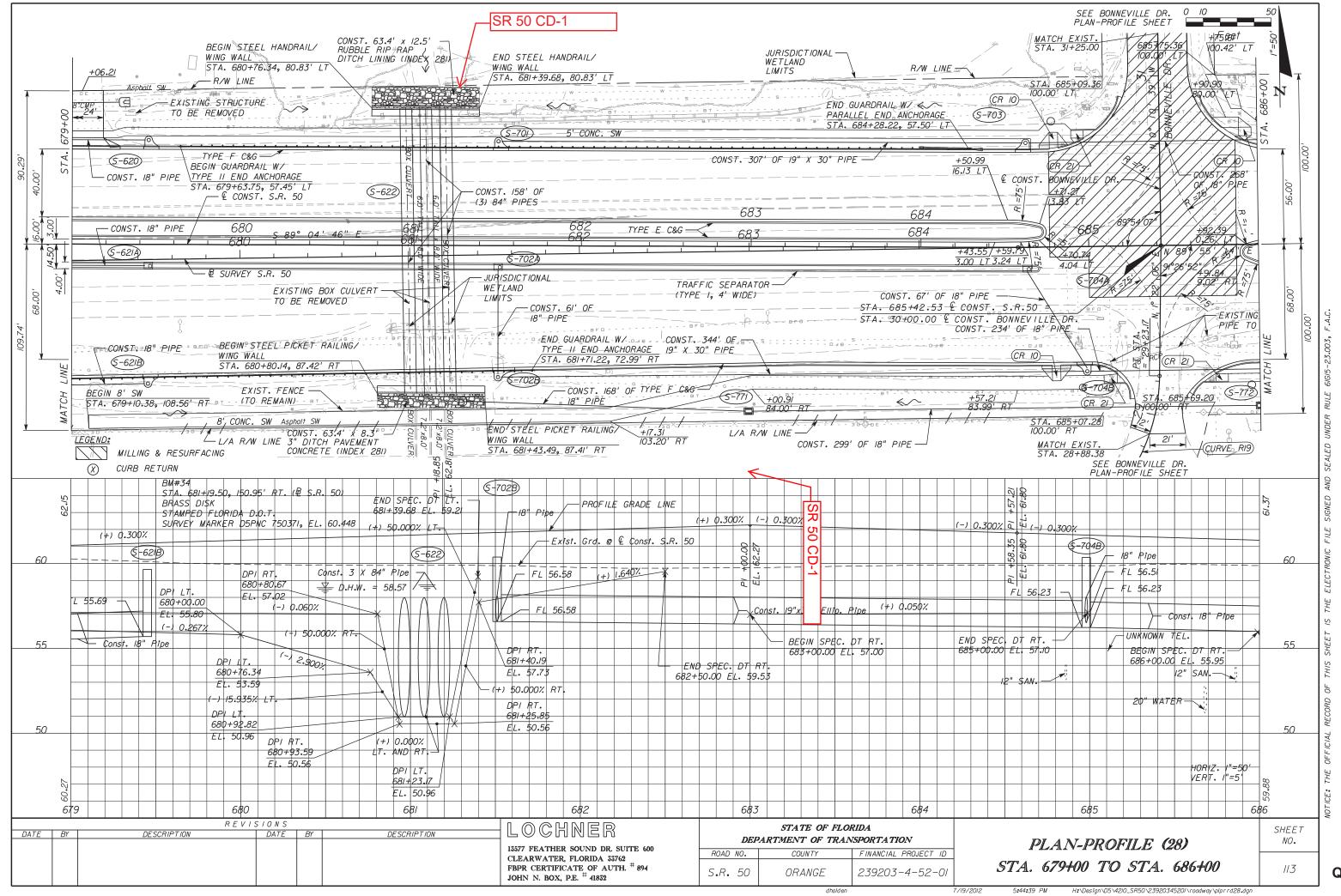
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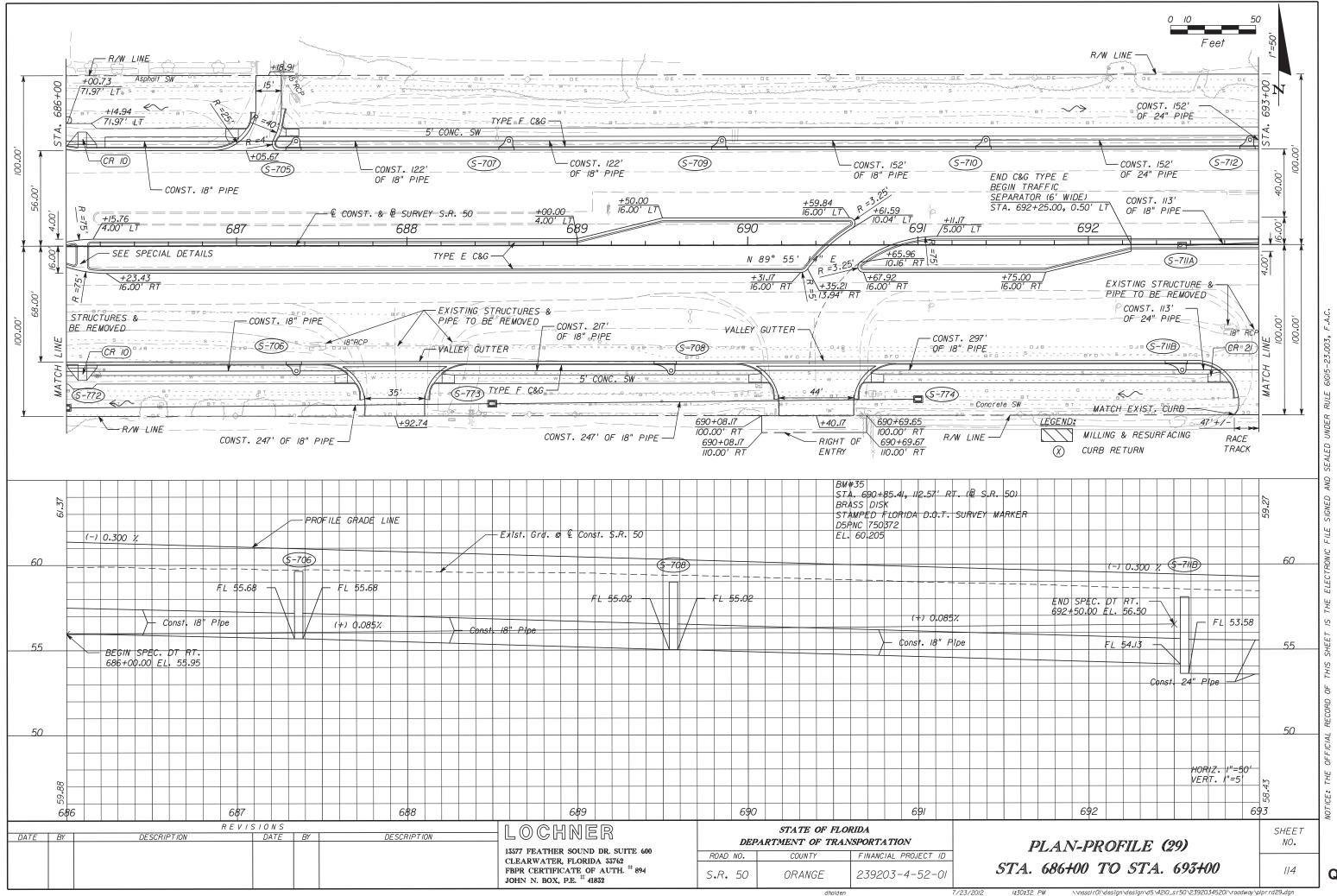
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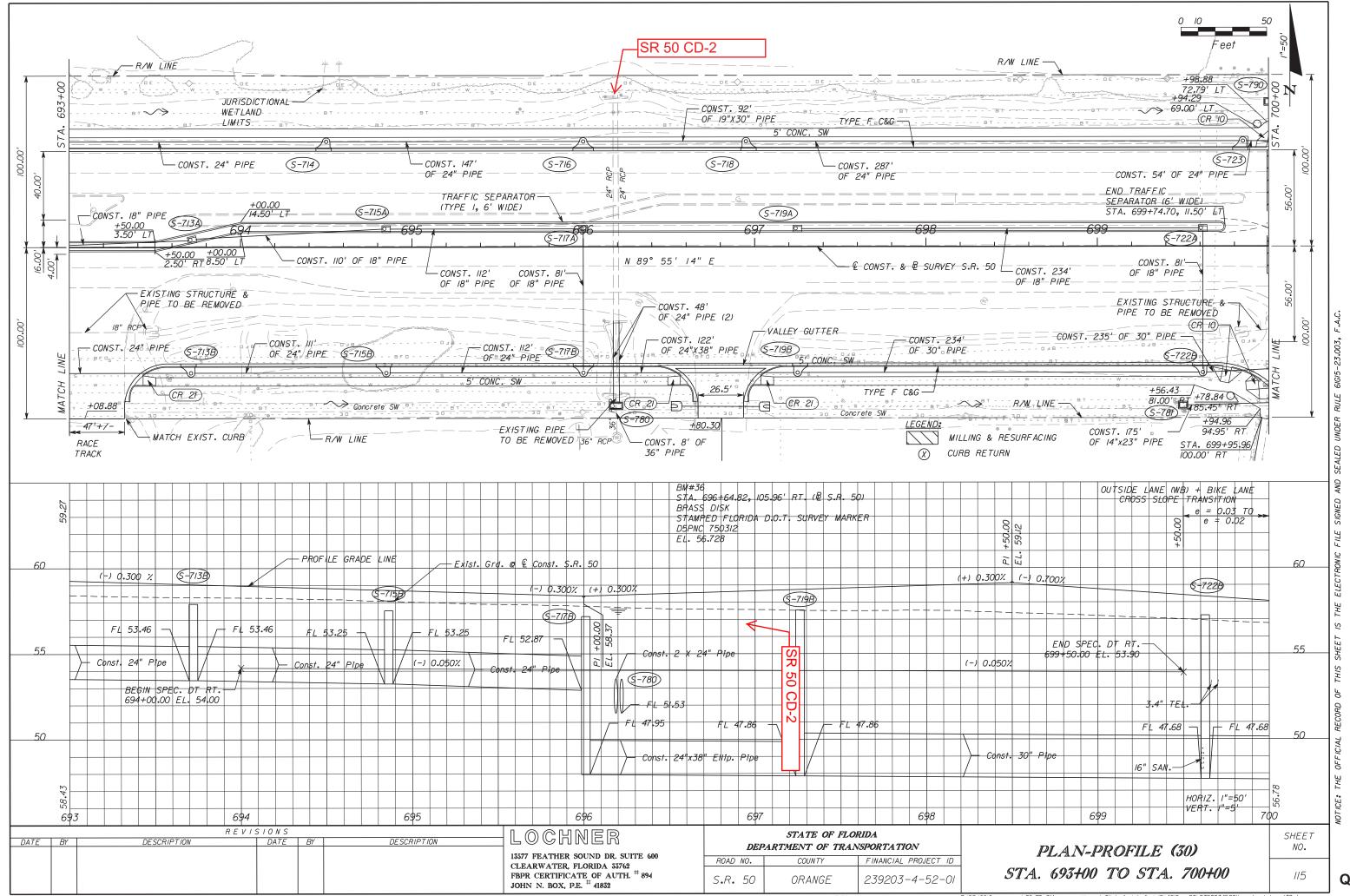


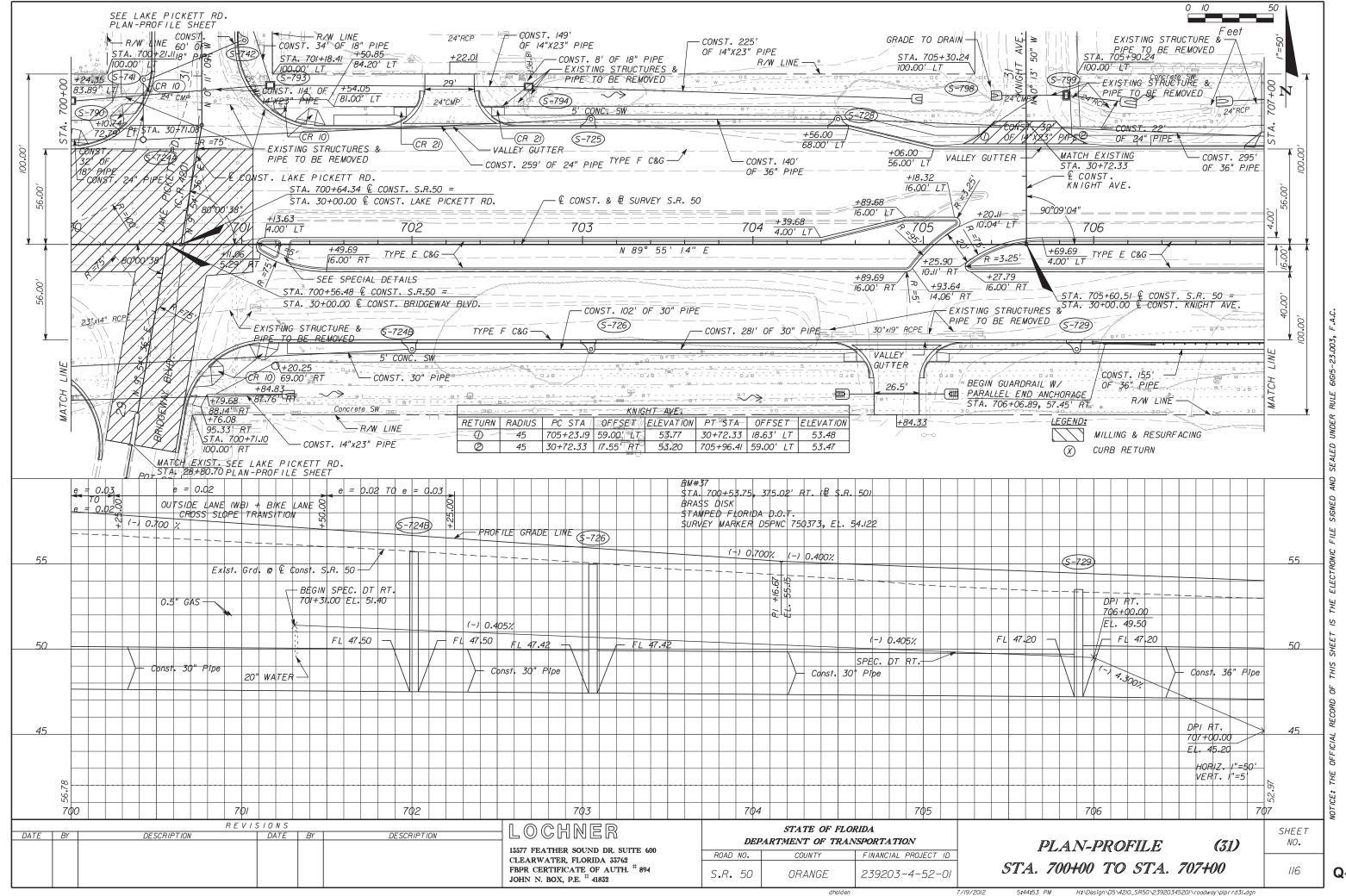


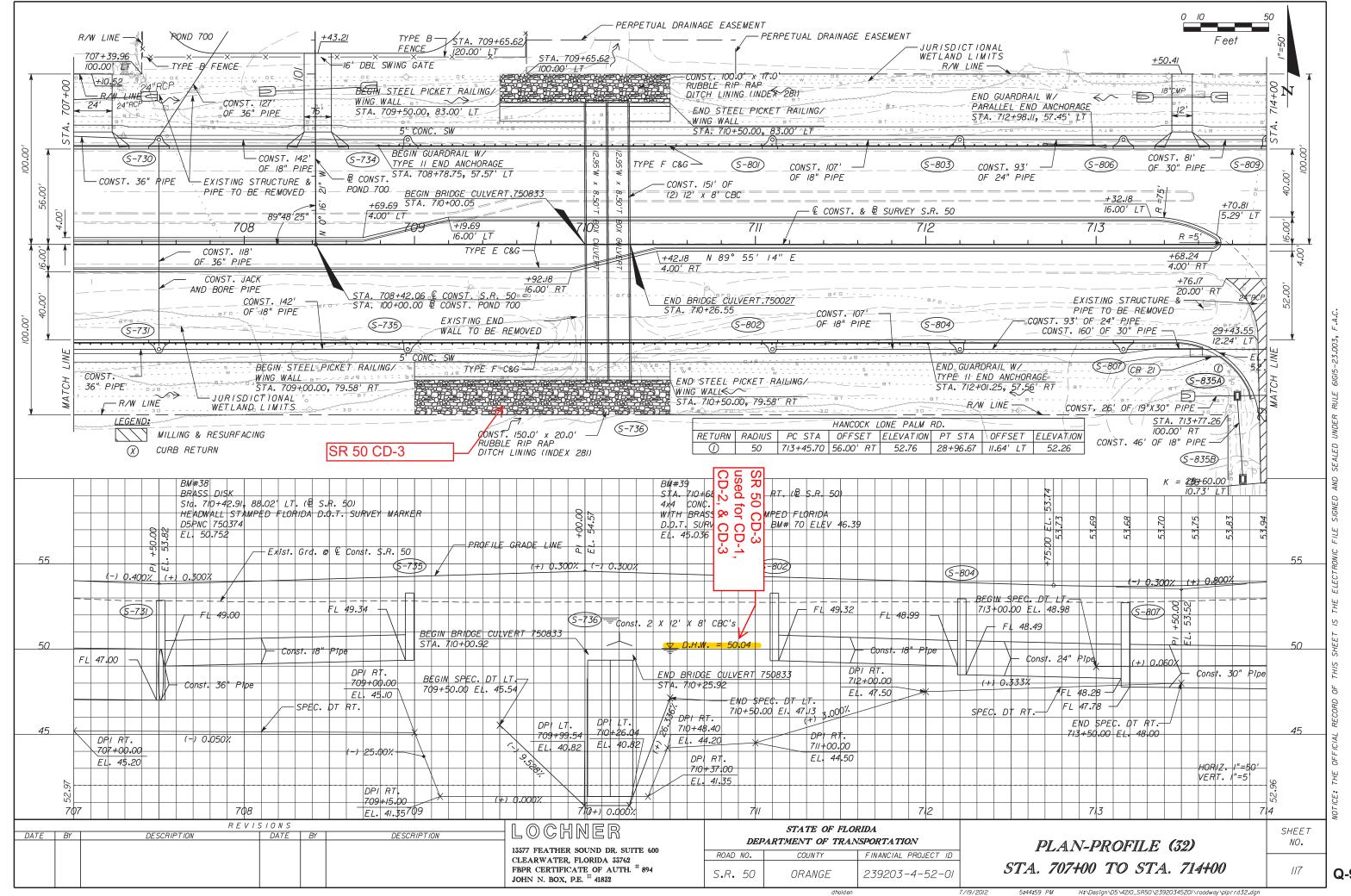


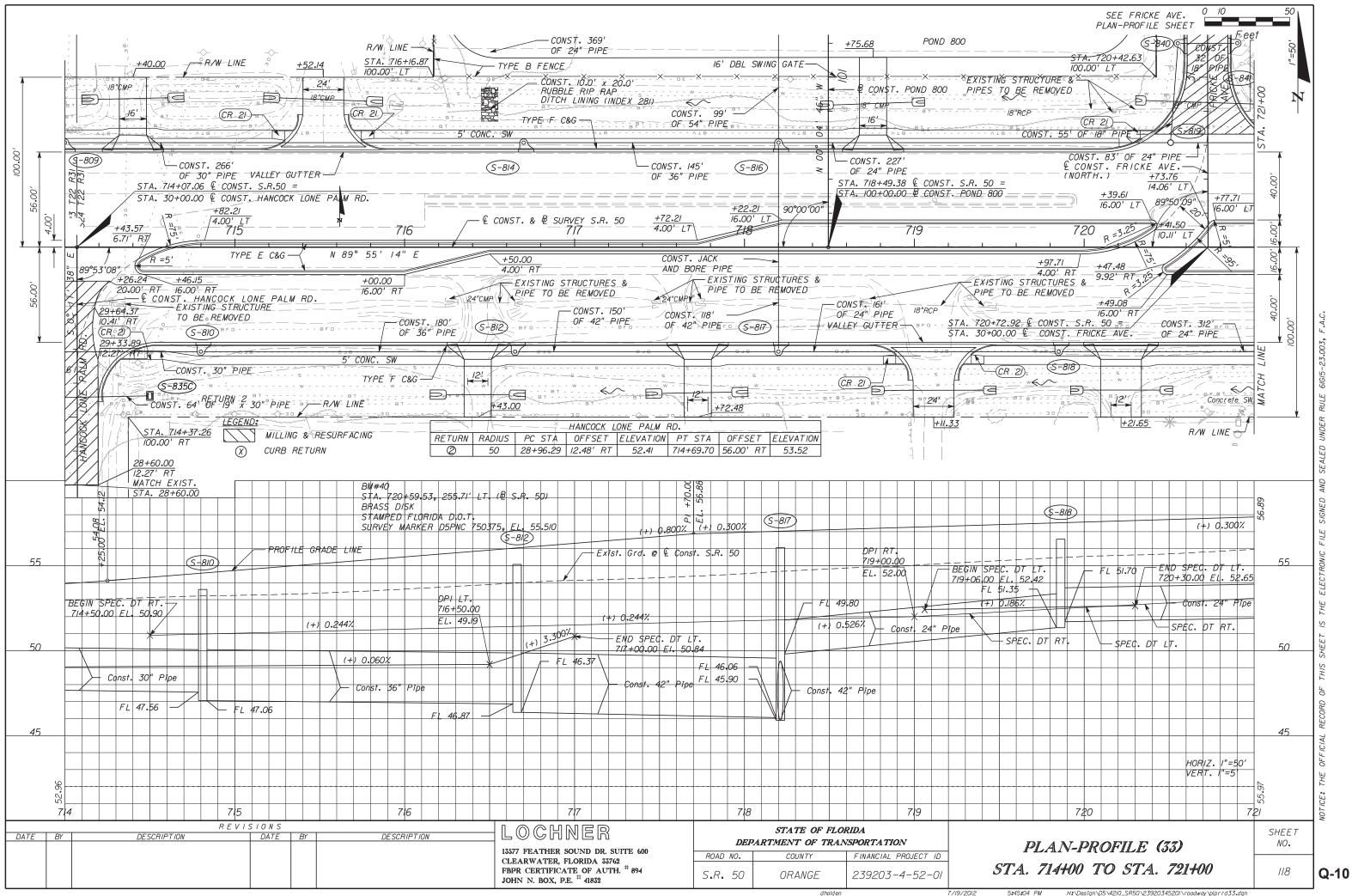


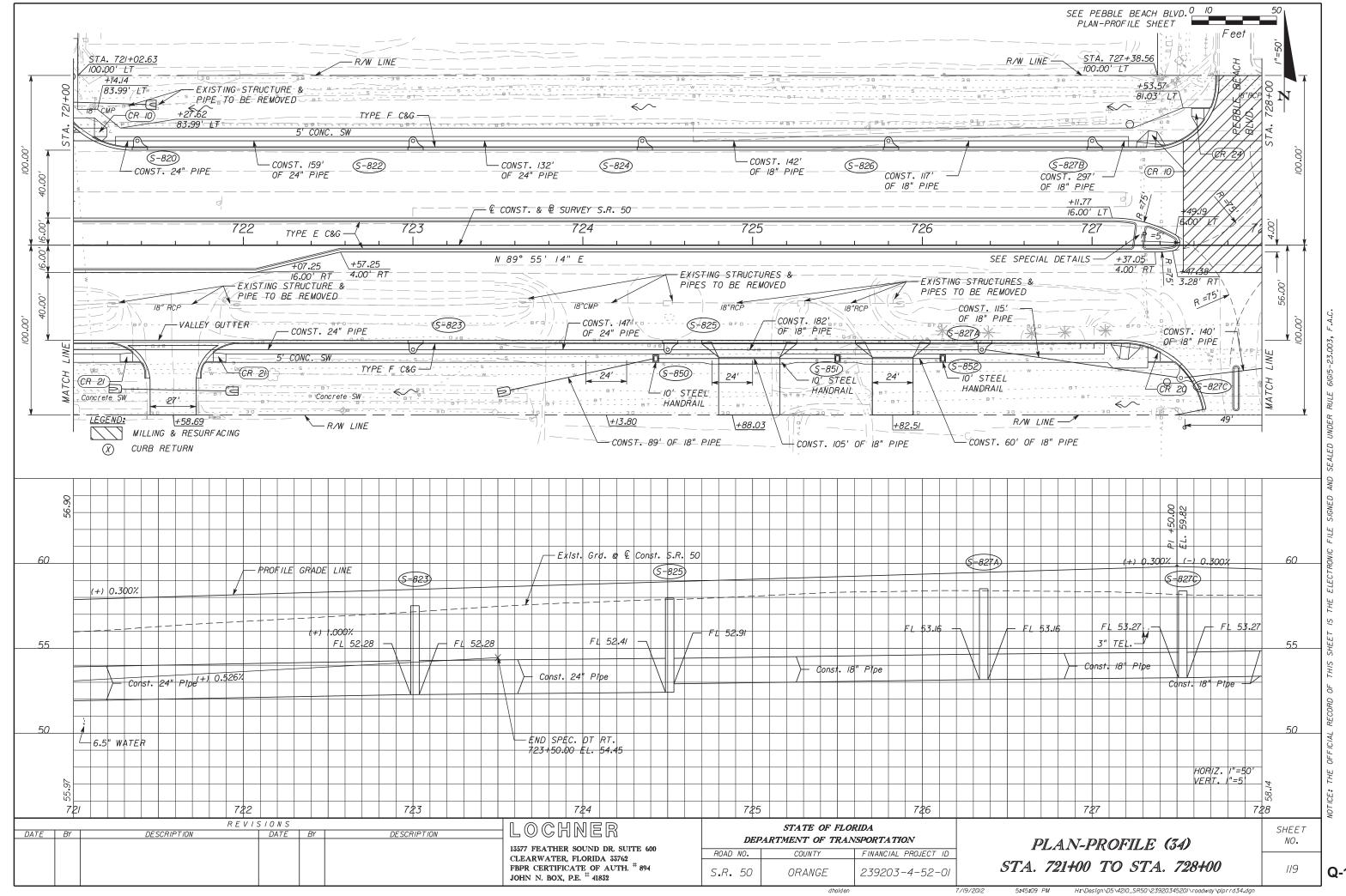


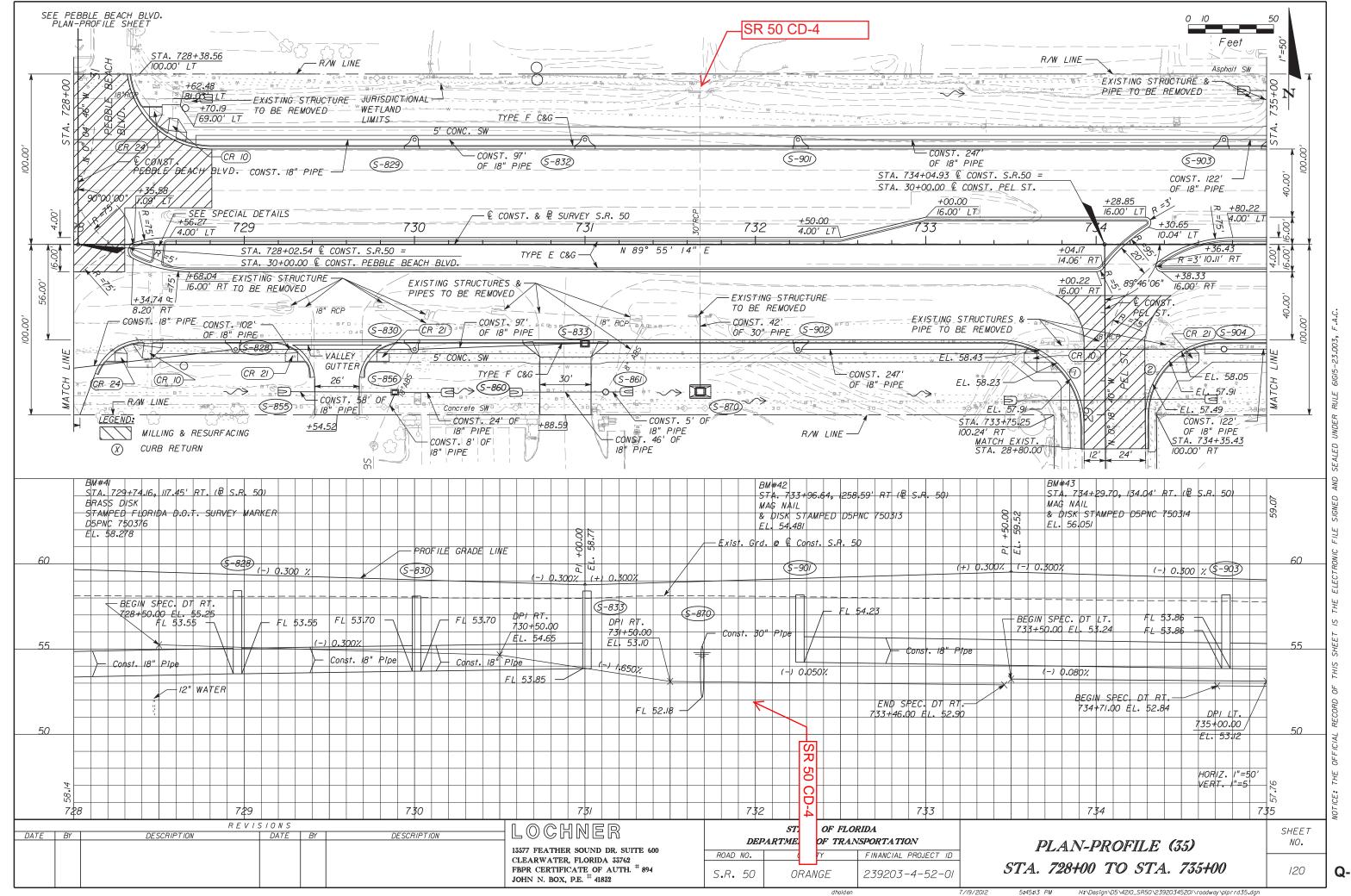


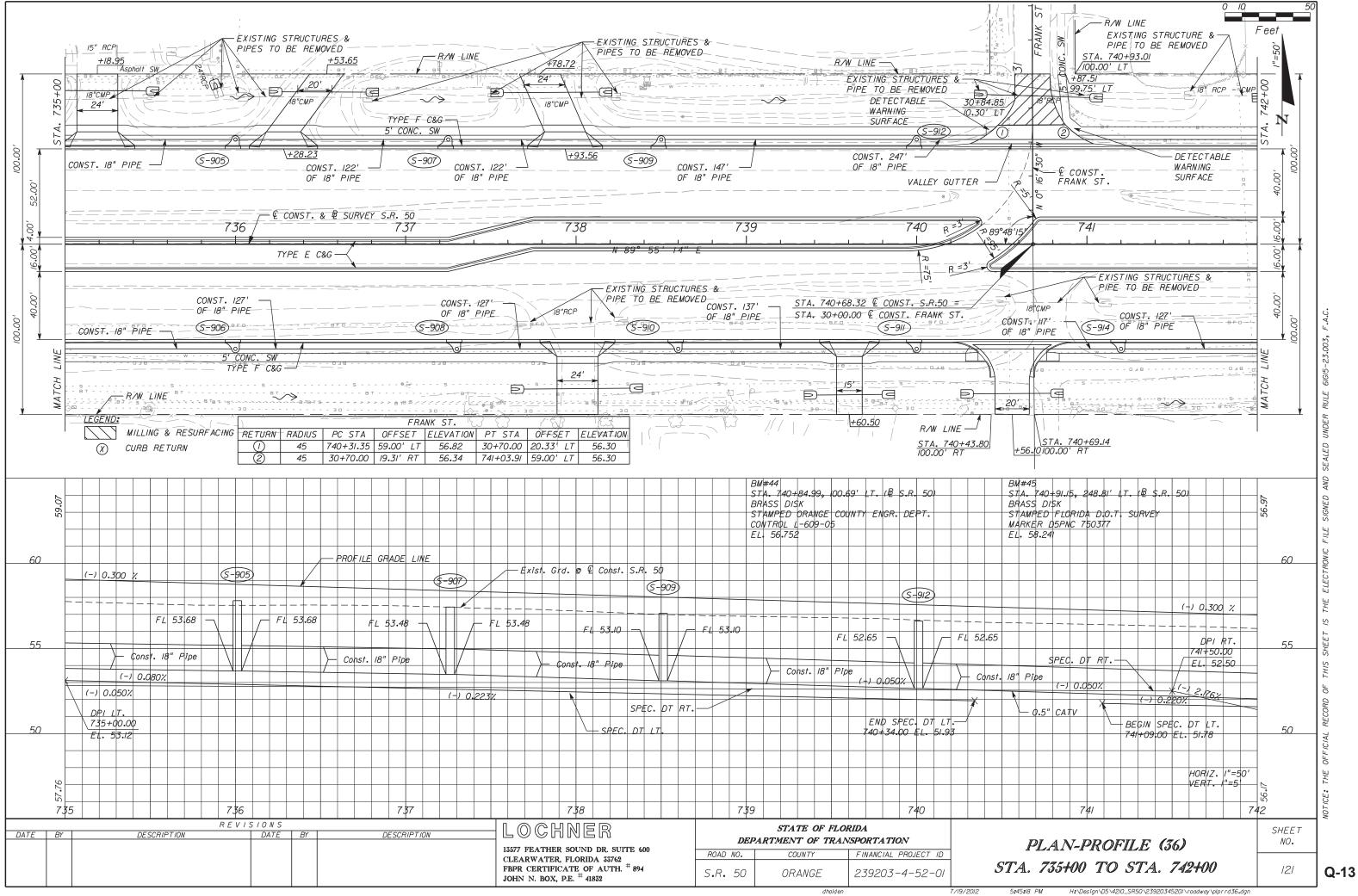


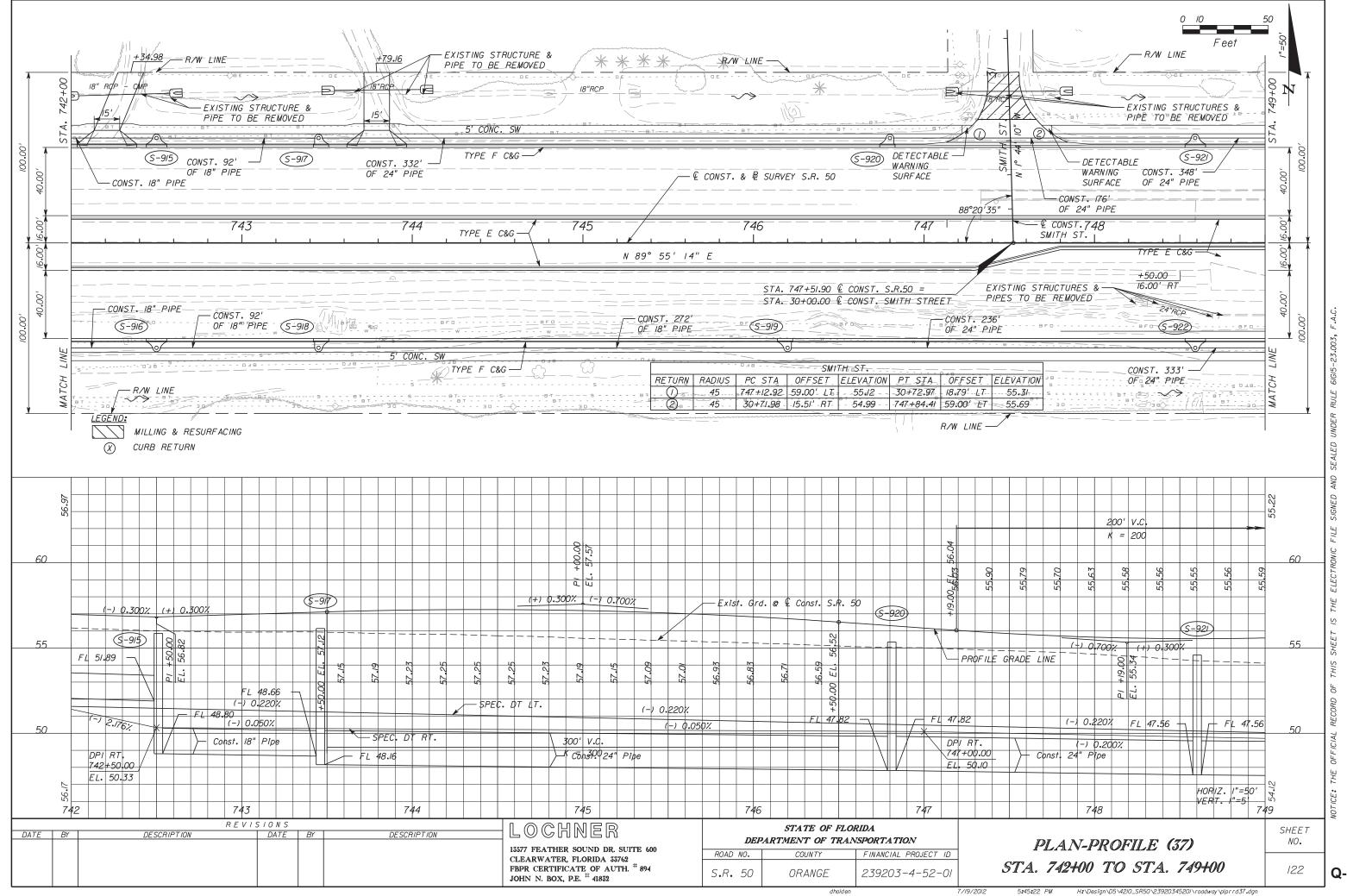


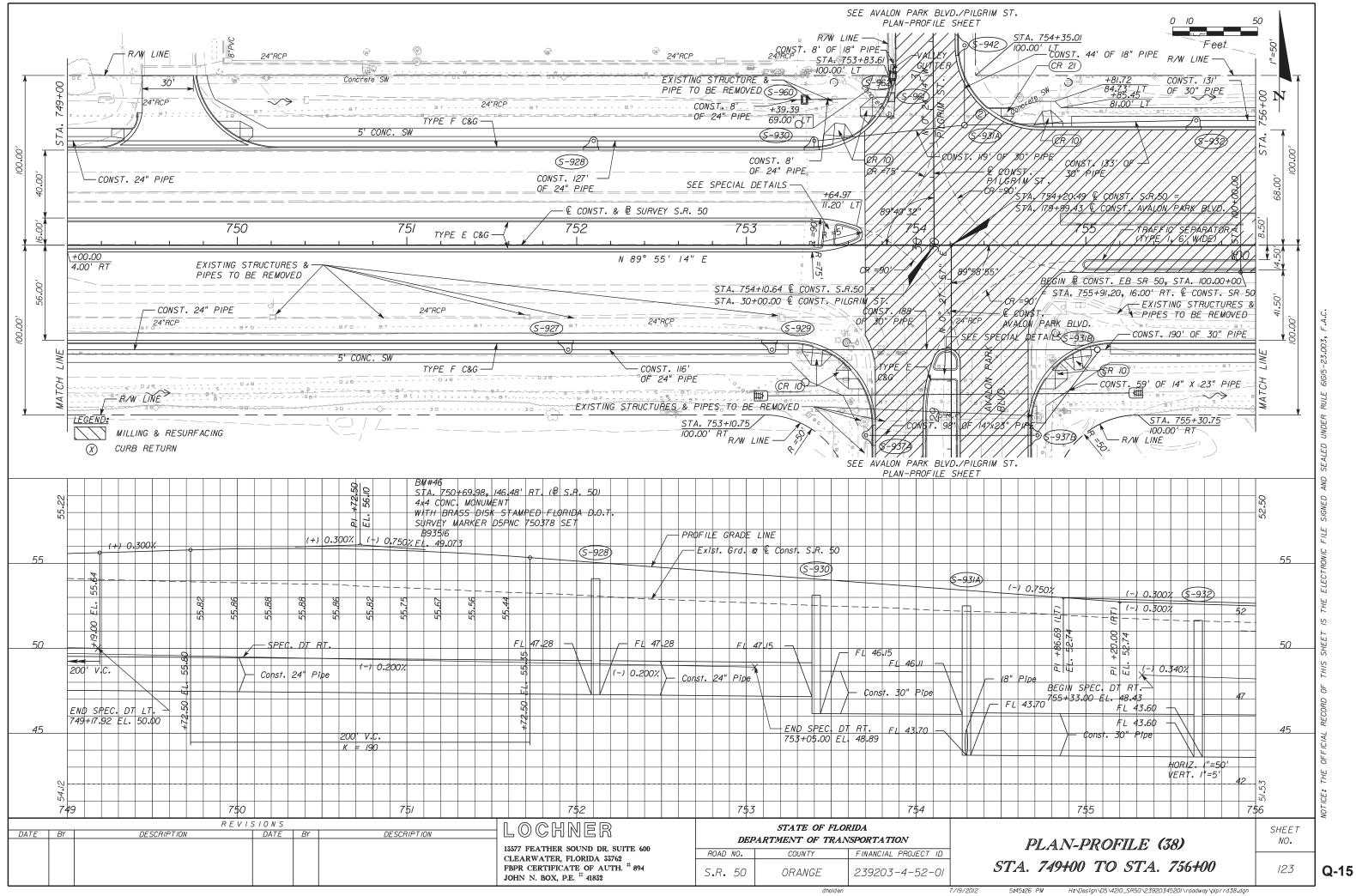


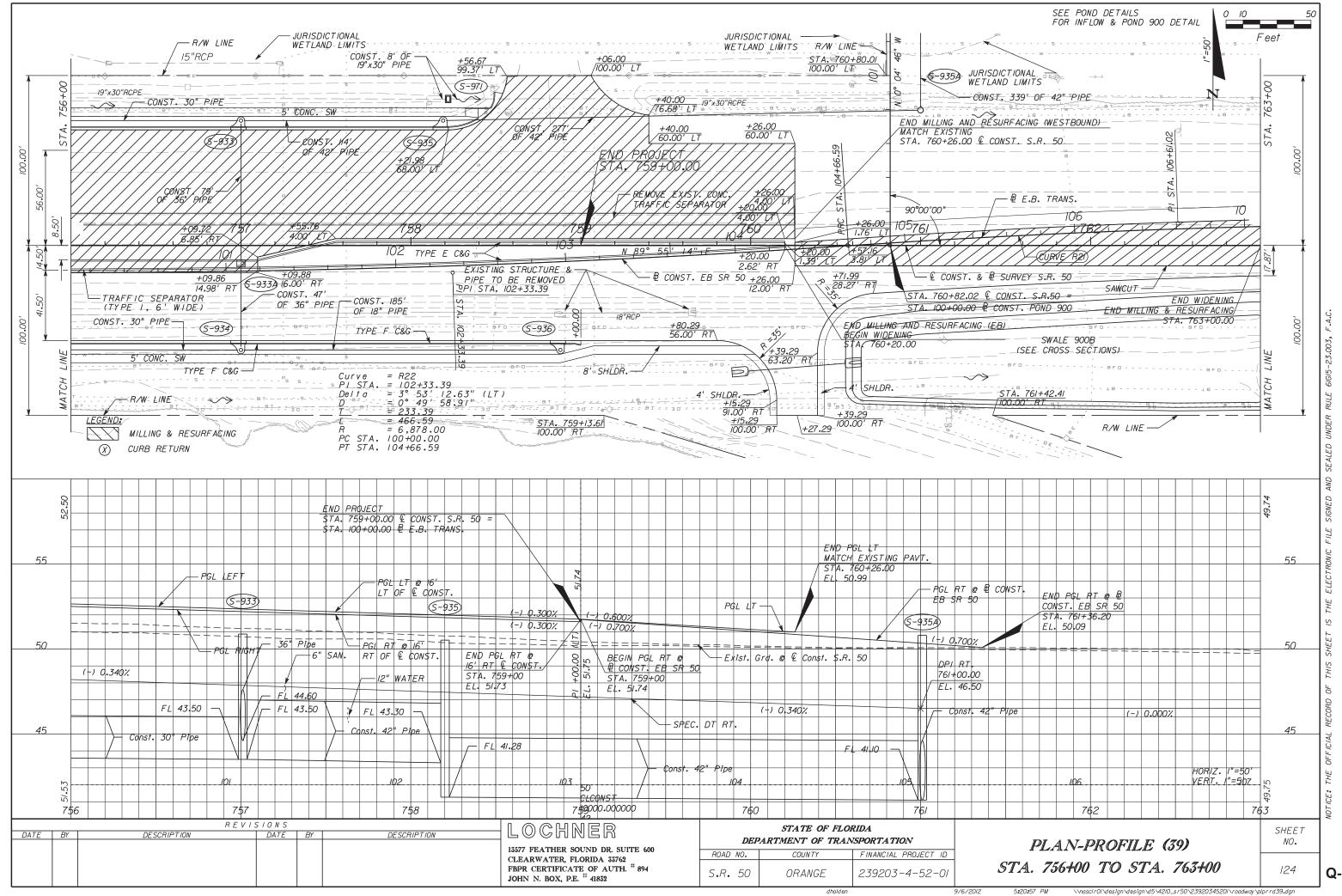


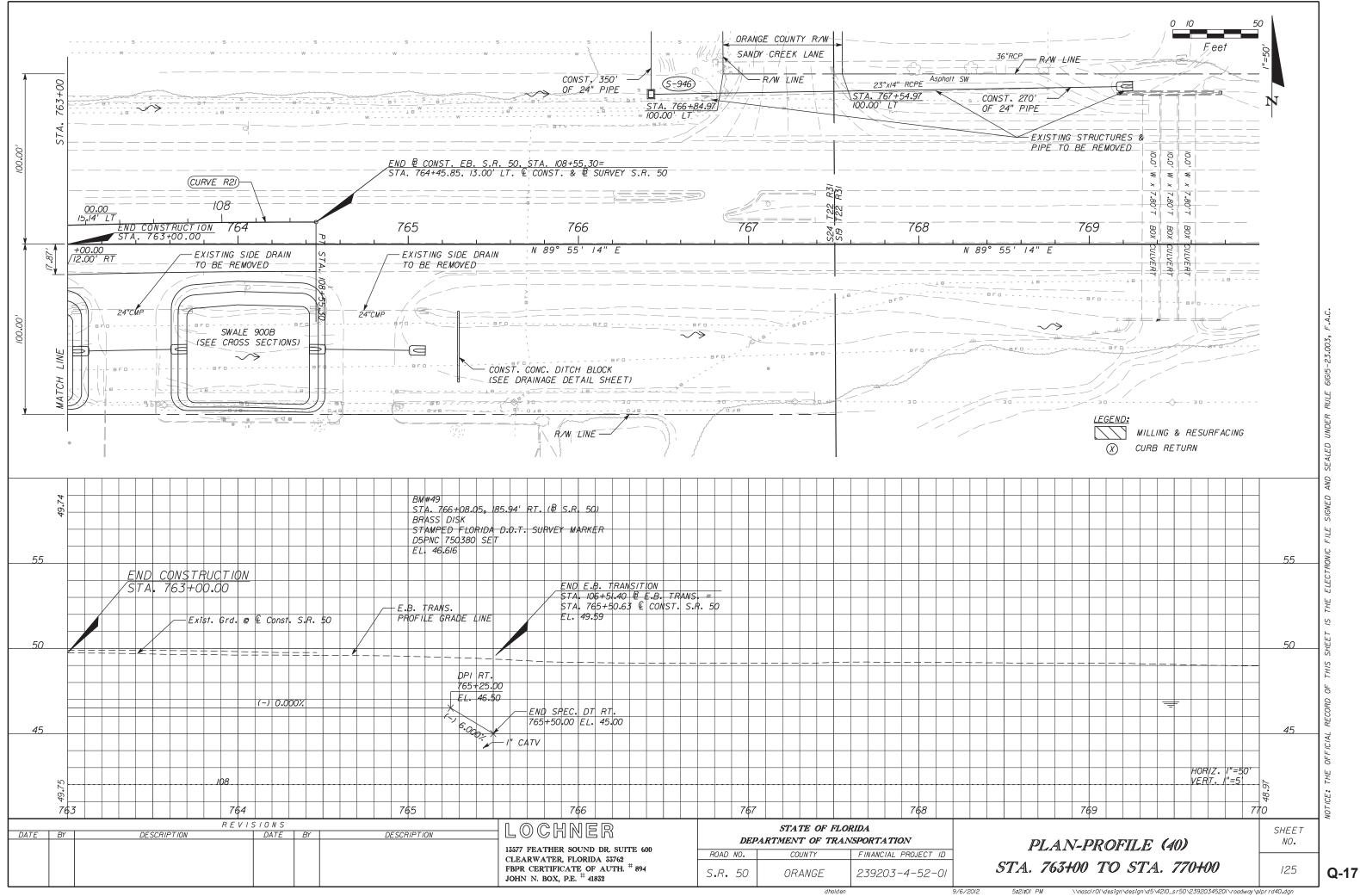






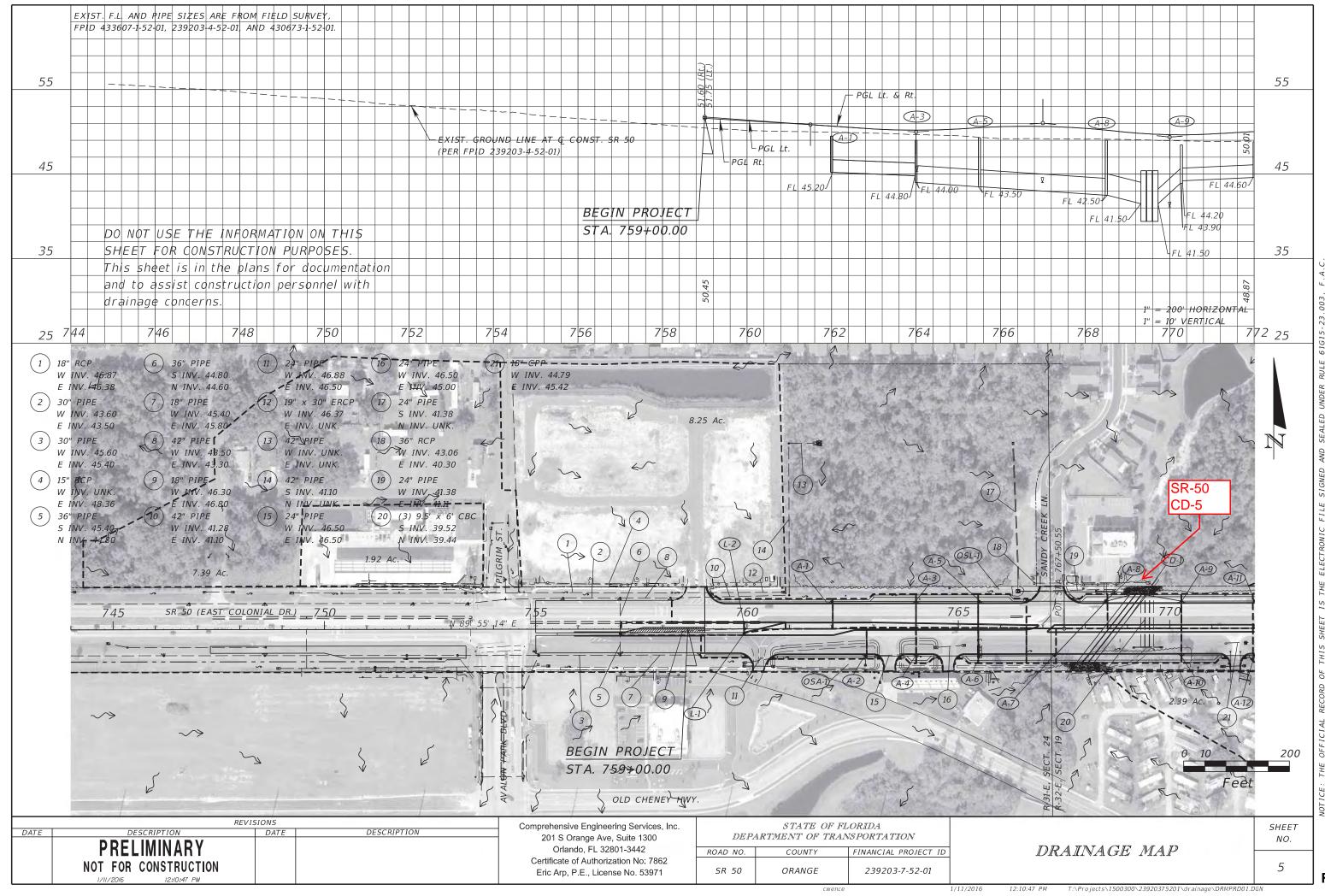


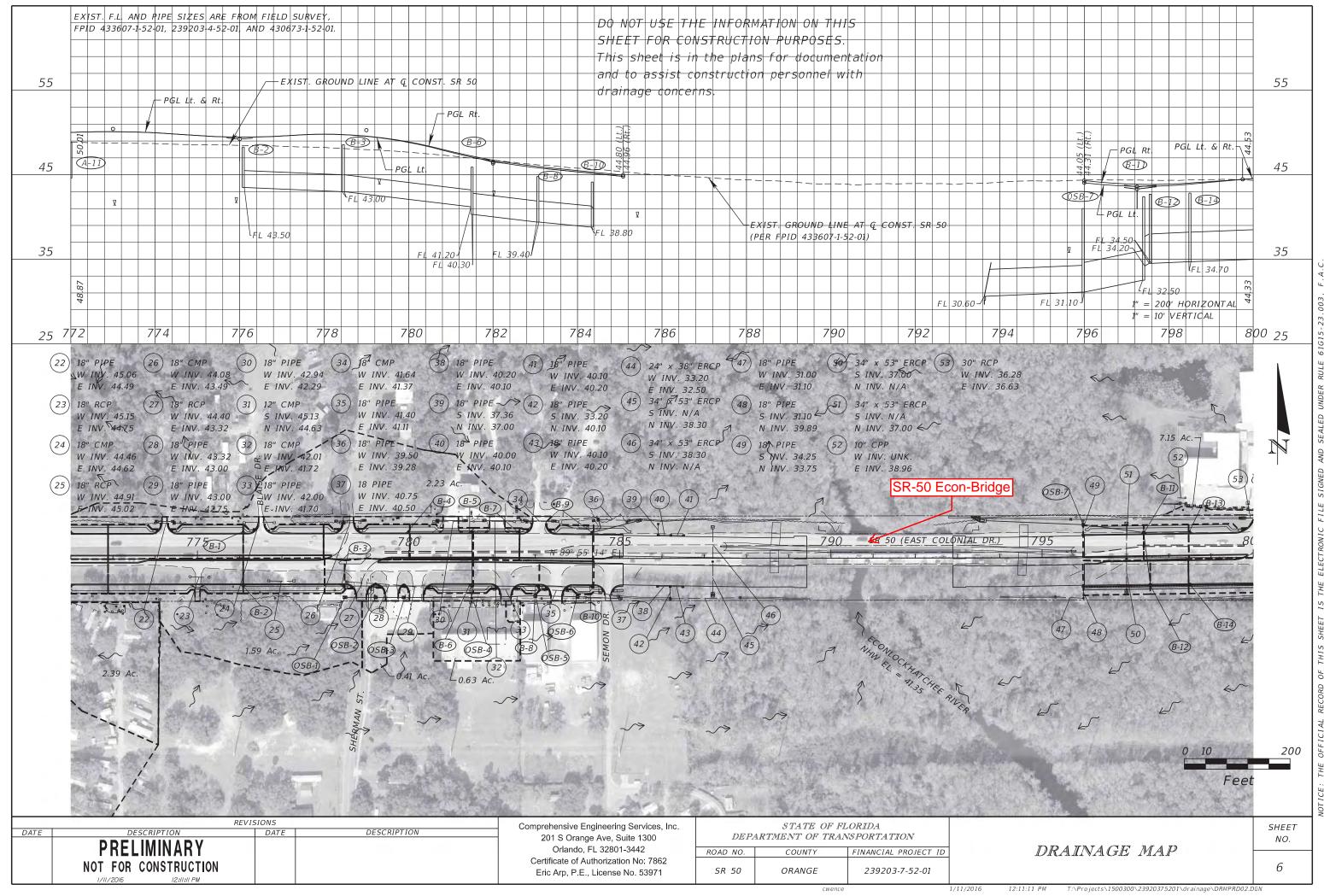


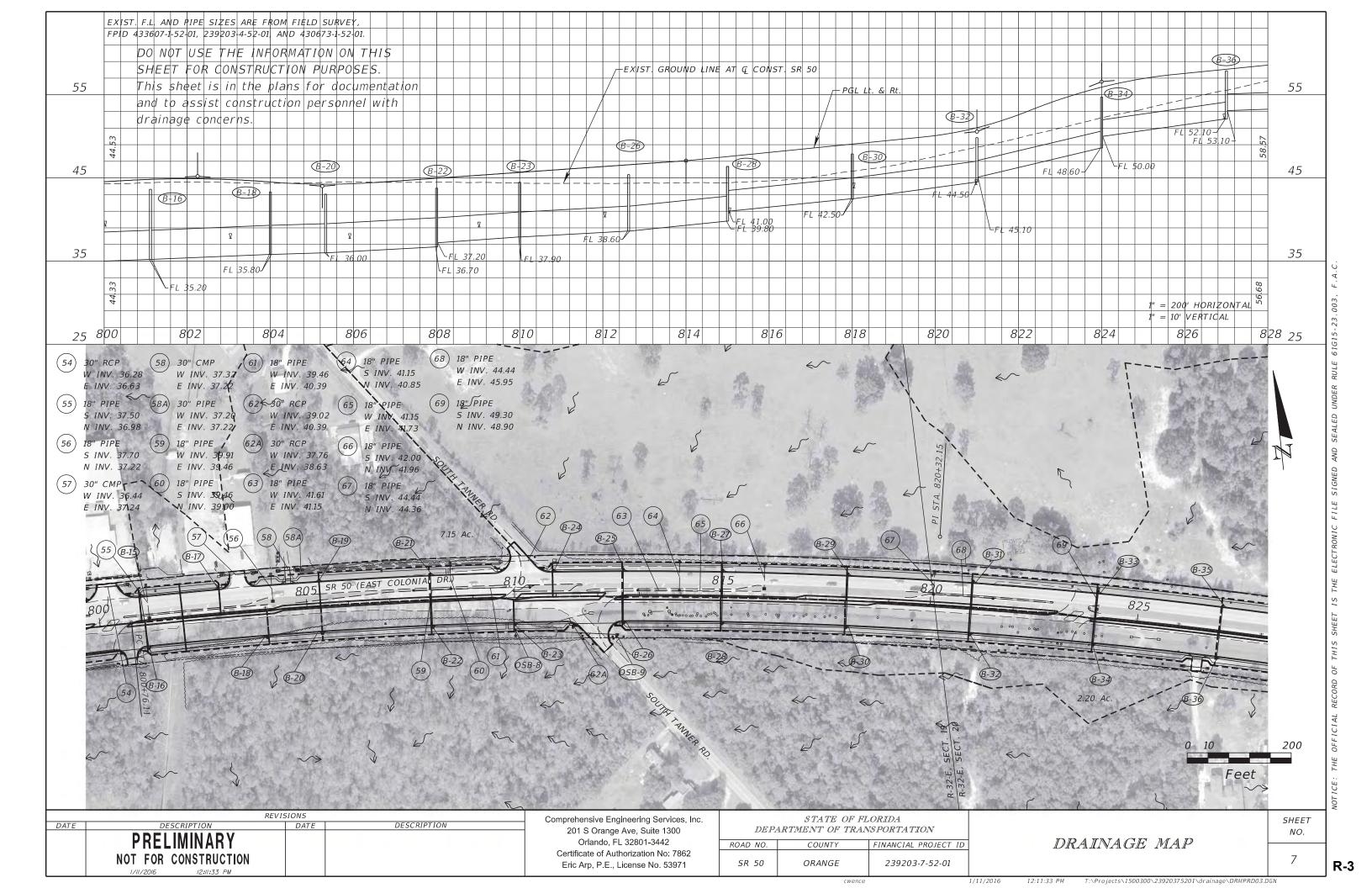


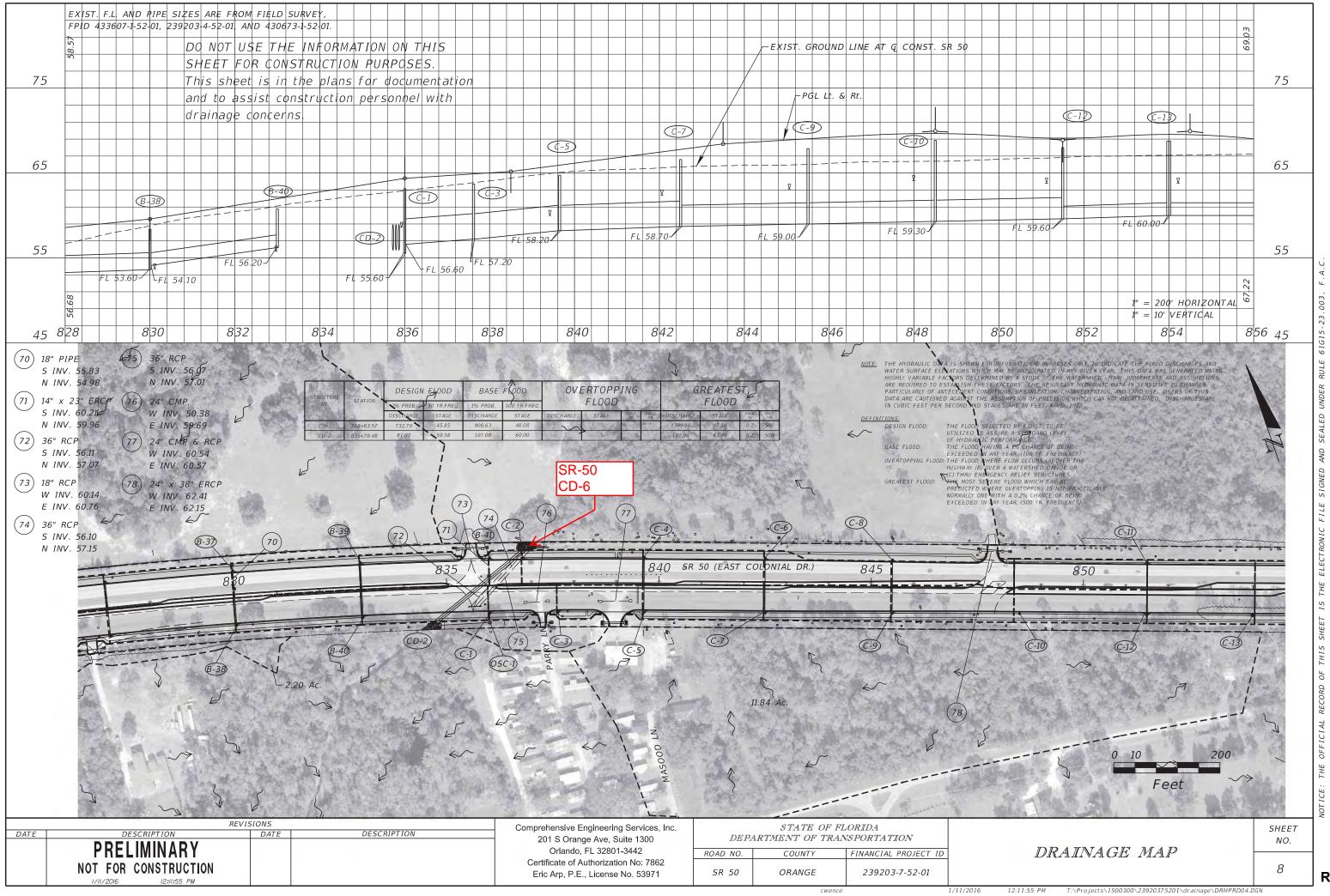
Appendix: R

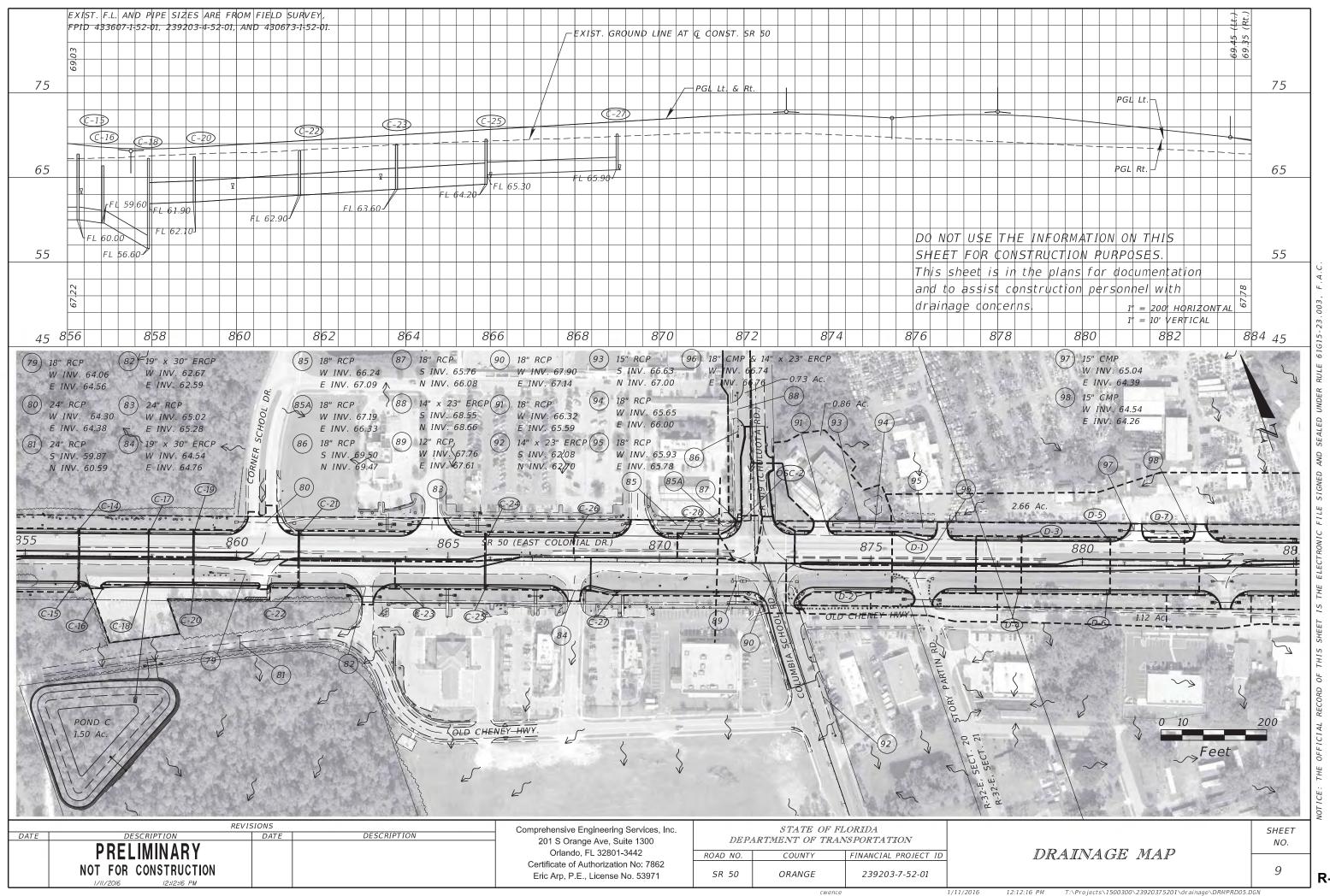
Excerpt from Comprehensive Engineering Services, Inc.
SR-50 Widening Construction Plans

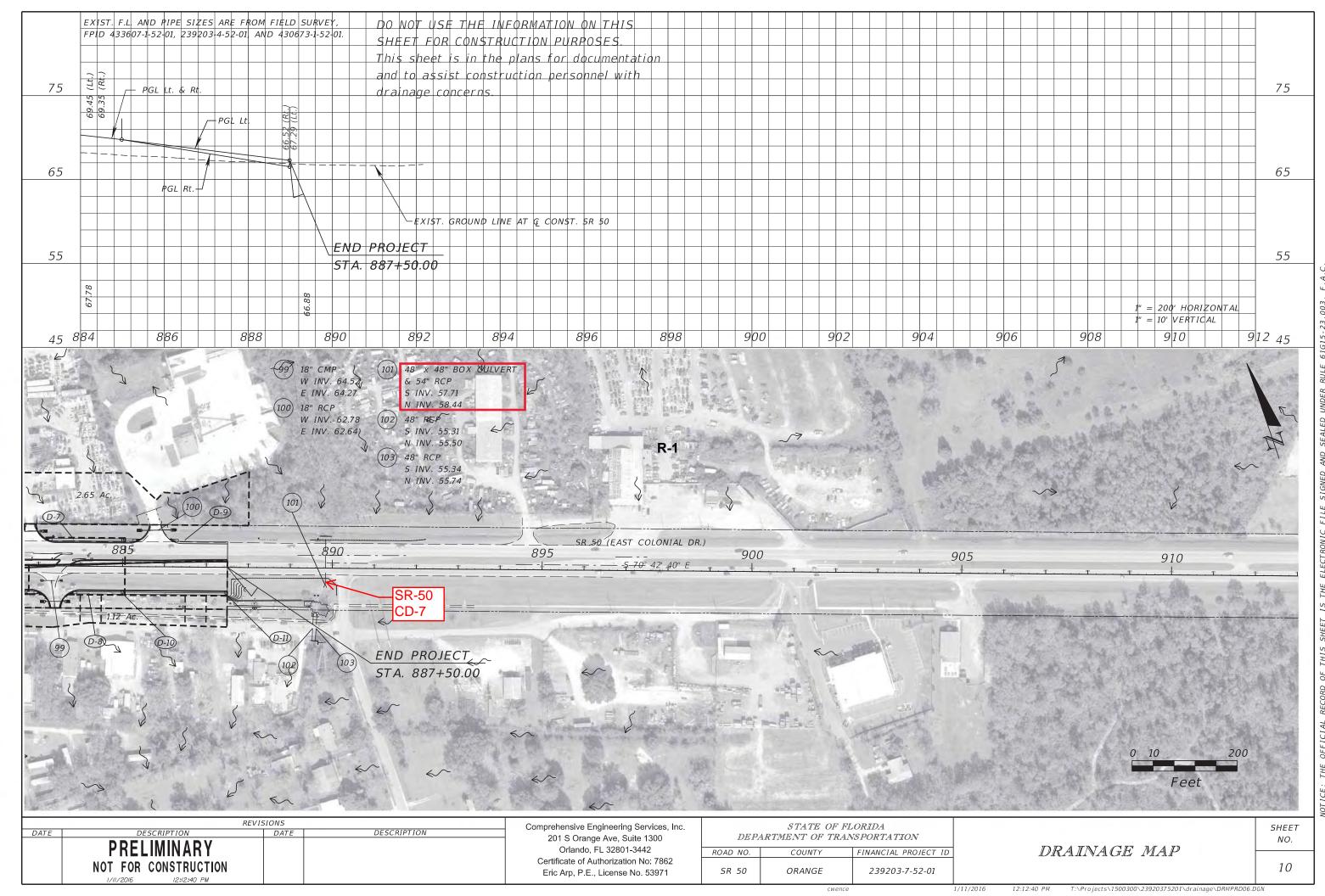




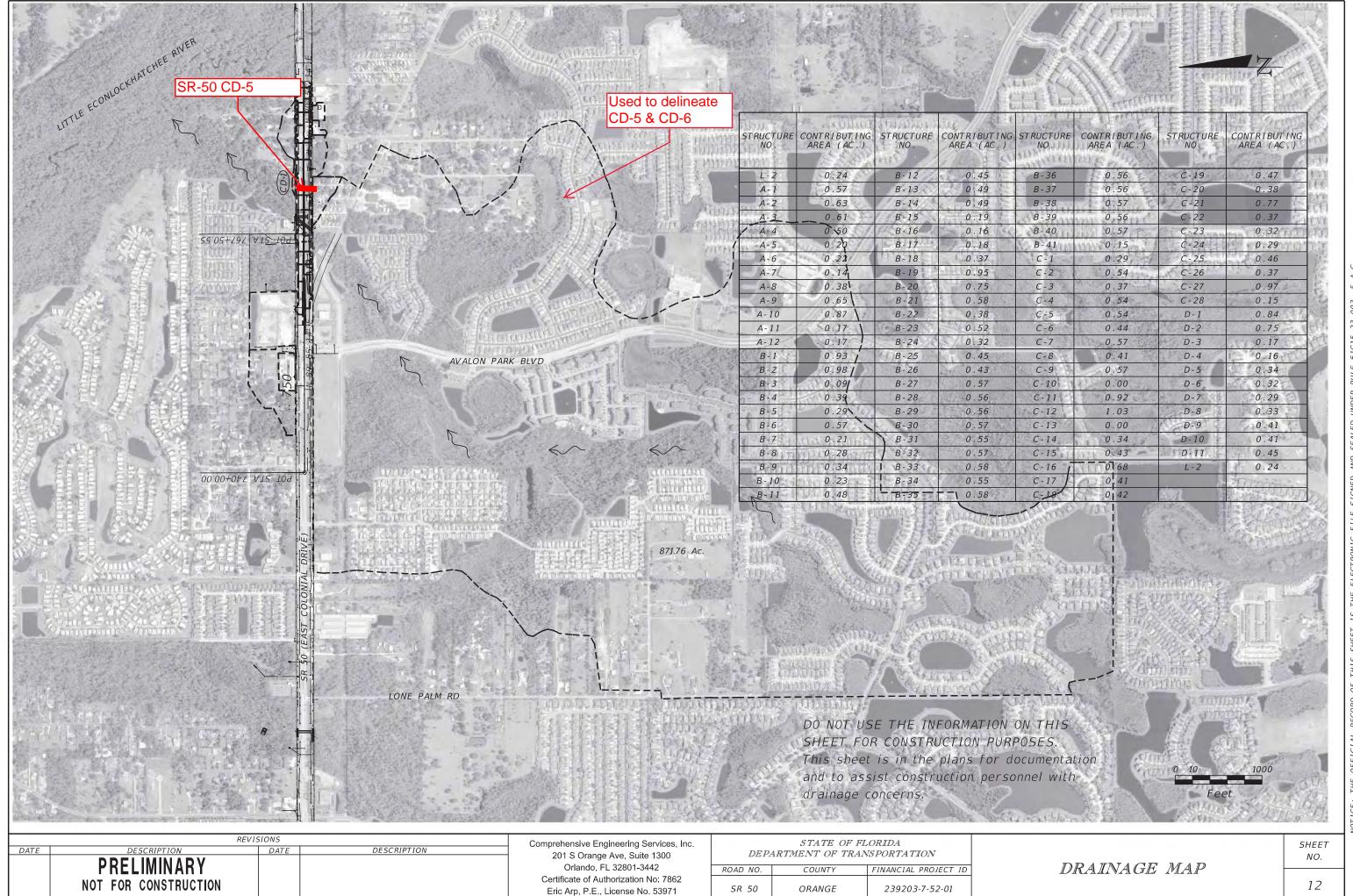






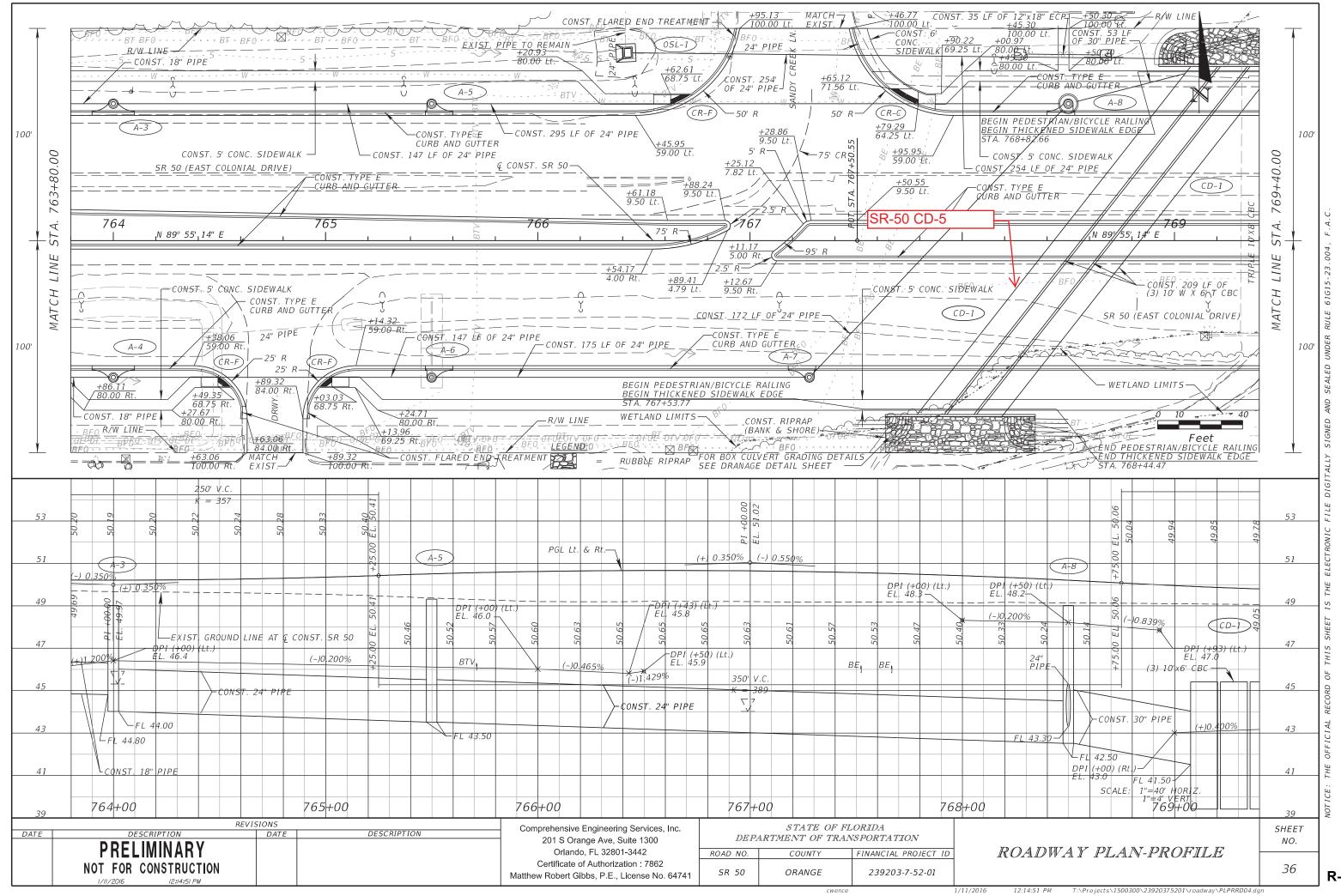


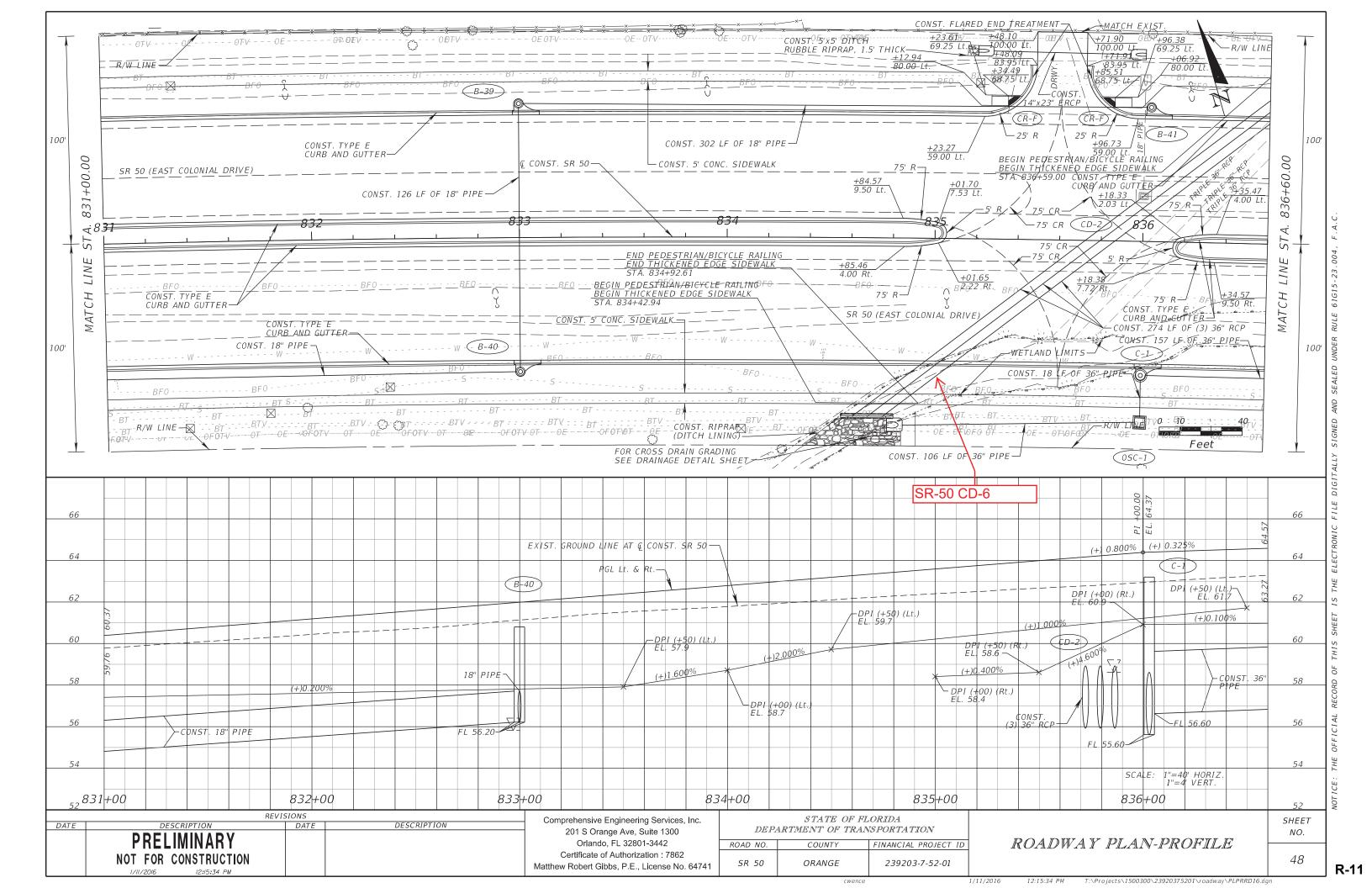


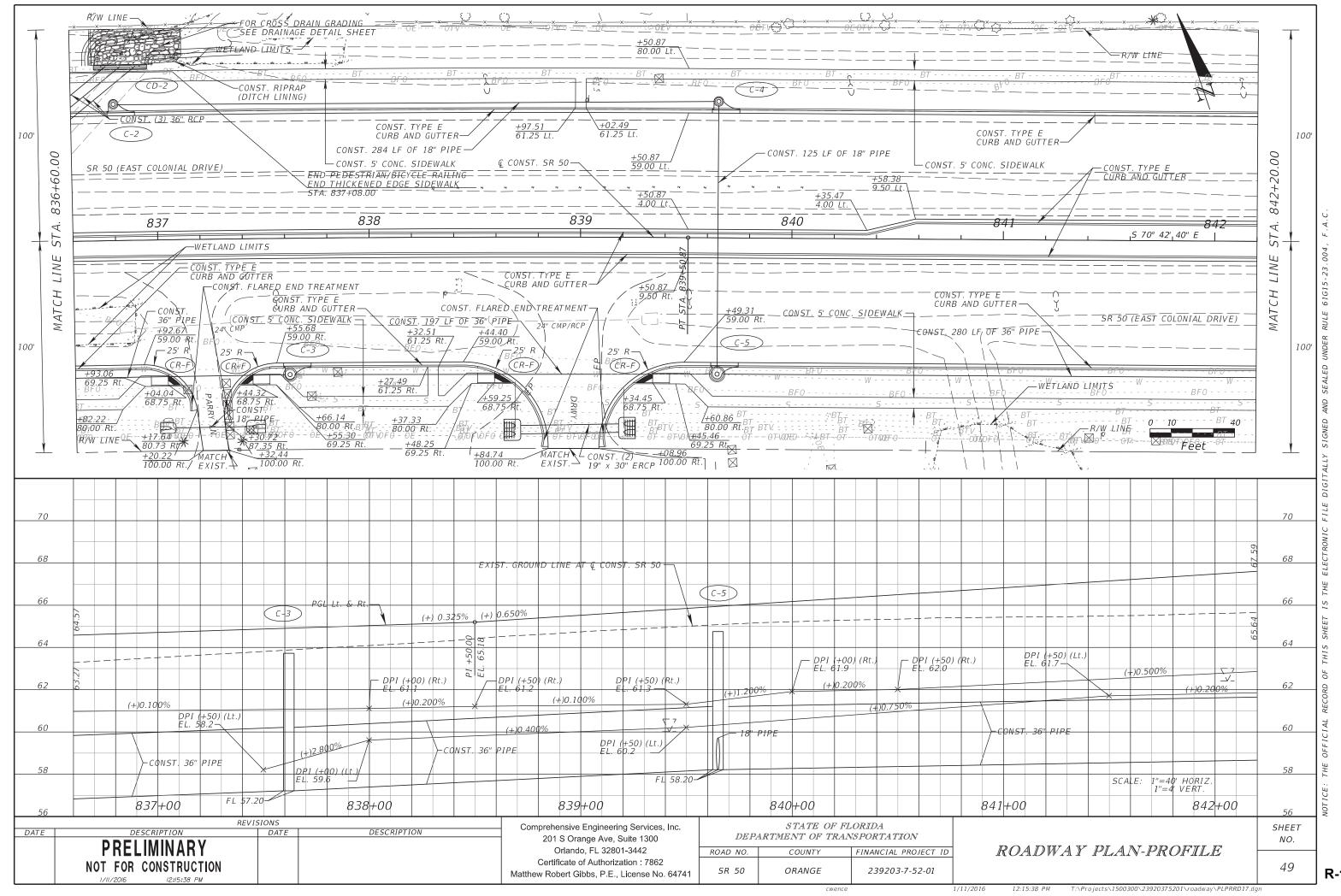


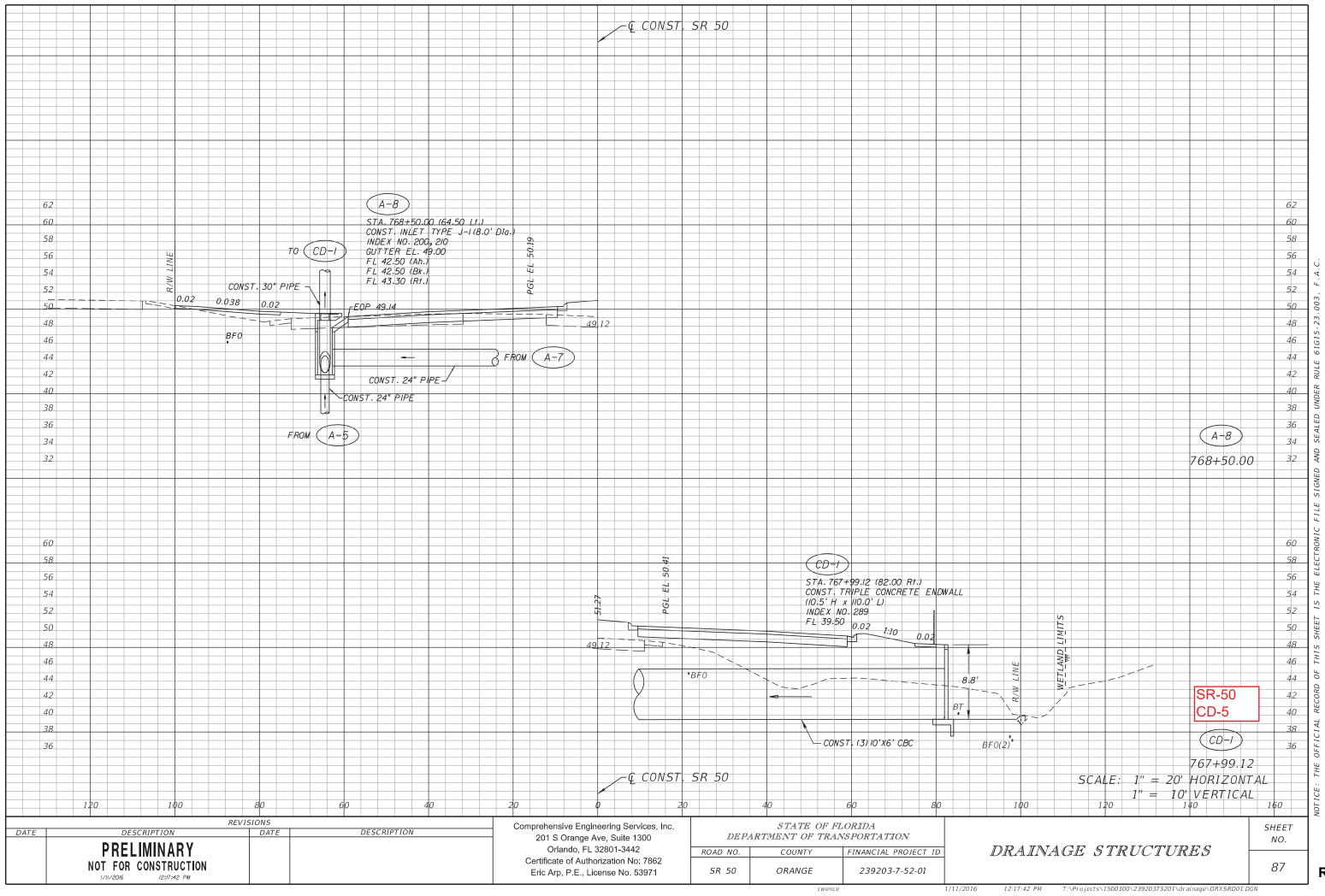


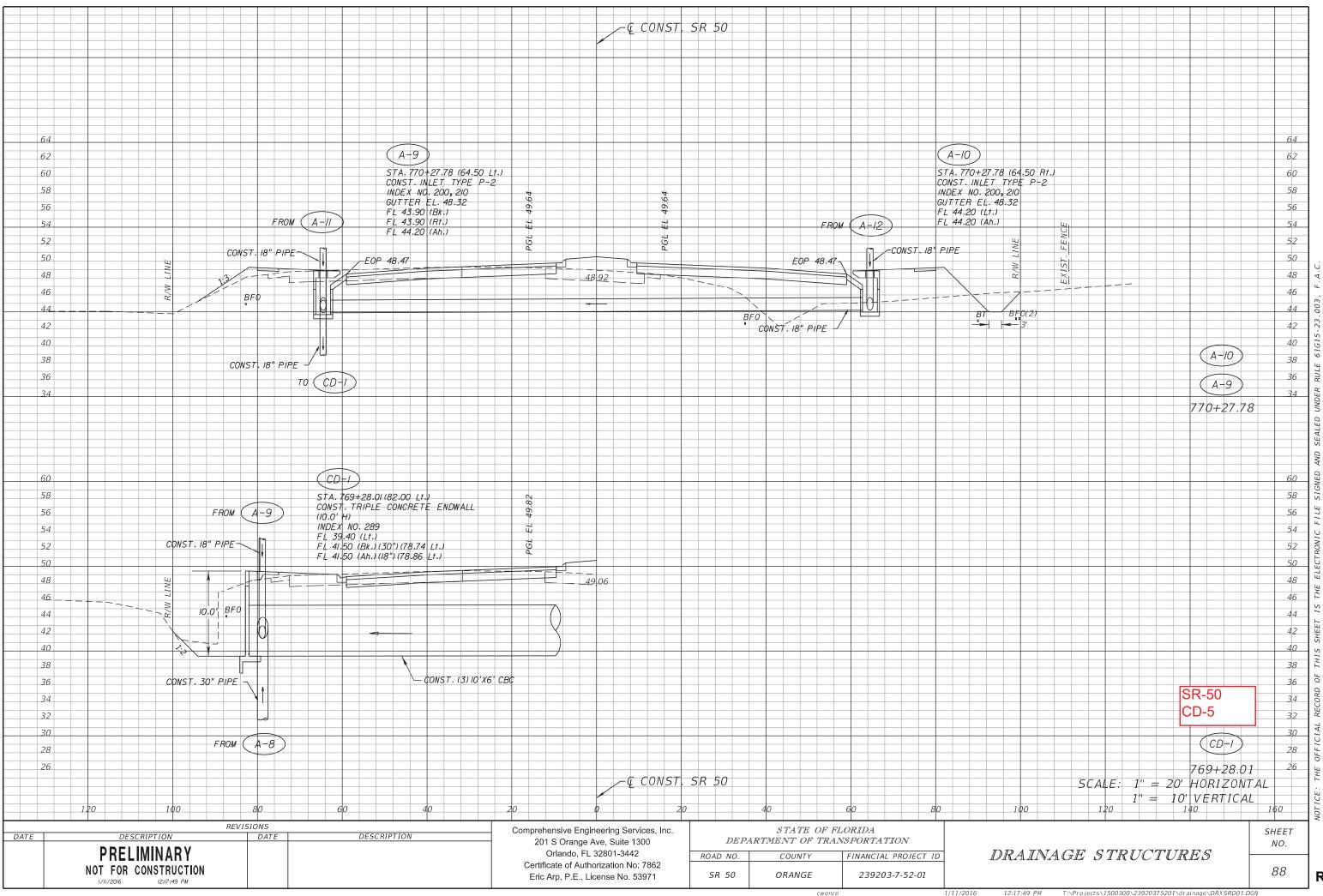
REVISIONS				ARCADIS	STATE OF FLORIDA						SHEET	
DATE	DESCRIPTION	DATE	DESCRIPTION	1650 Prudential Drive, Suite 400	DEPARTMENT OF TRANSPORTATION							
	PRELIMINARY			Jacksonville, Florida 32207			FINANCIAL PROJECT ID			DRAINAGE MAP		NO.
				T: 904 721 2991 F: 904 861 2450	NUAD NU.	COUNTY	FINANCIAL PROJECT ID	1	II II			
	NOT FOR CONSTRUCTION			Certificate of Authorization No. 7917	SR 50	ORANGE	239203-7-52-01					13
	1/11/2016 5:24:21 PM			Walter J. Nemecek, III, PE No. 58122								
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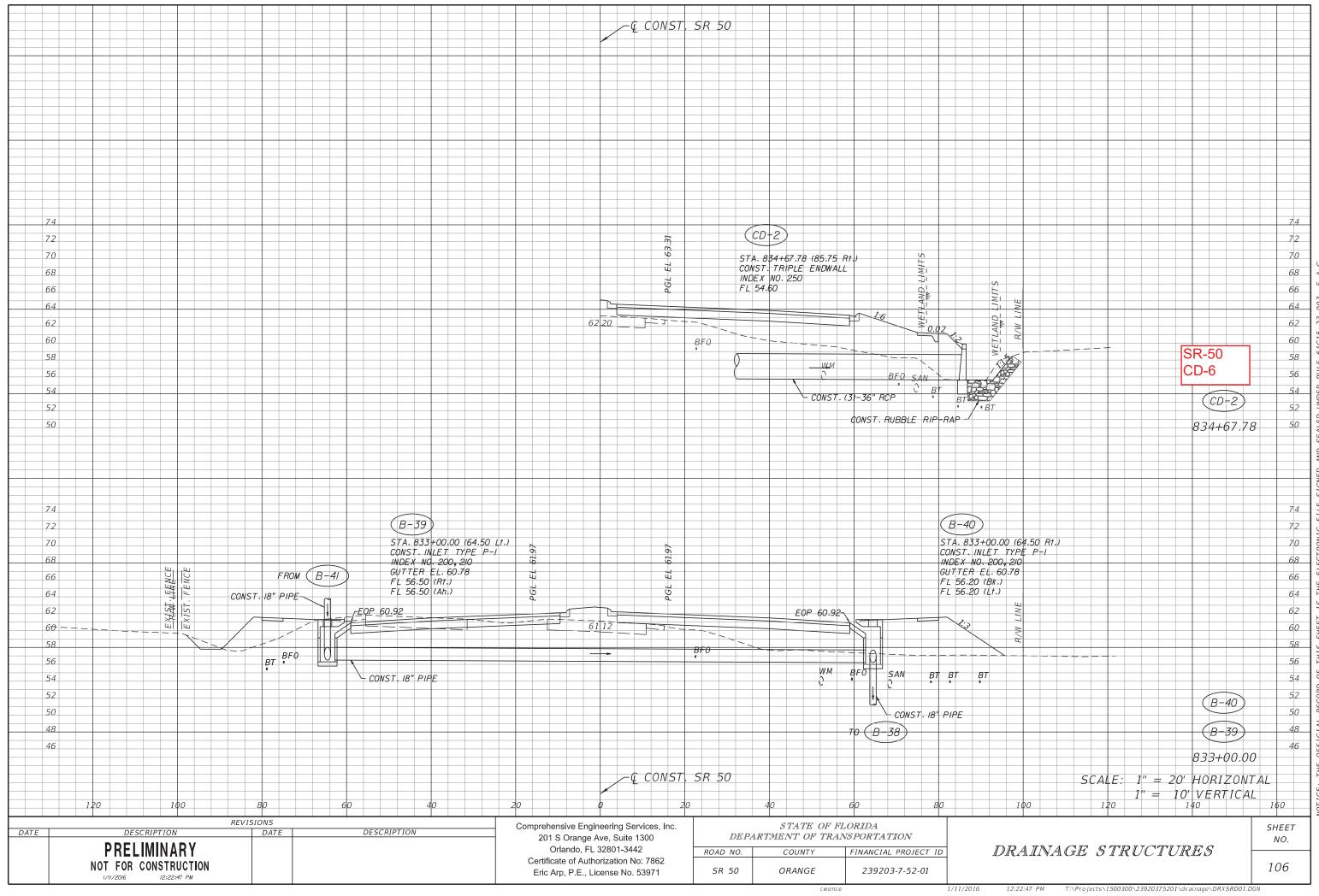


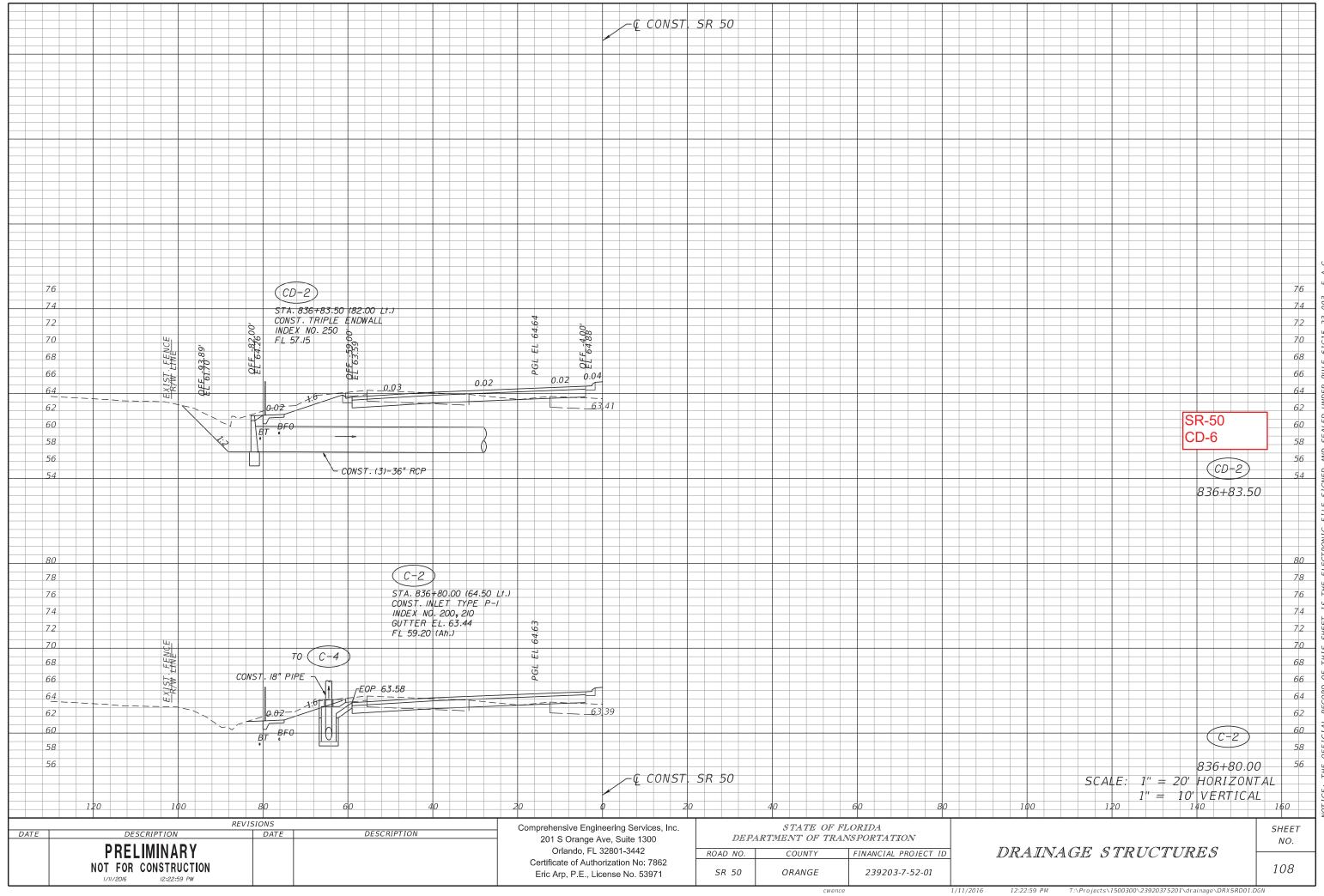












Appendix: S

SR-50 Field Visit Photos (May 2016)



SR 50- CD1 (2-8' x 6' CBC)
(Looking North Side of the Culvert)



SR 50- CD2 (2-24" RCP)
(North side of the Culvert)



SR 50-CD3 (2-12.95' x 8.5' CBC)
(South Side of the Culvert)



SR 50-CD4 (1-30" RCP)
(South Side of the Culvert)



SR 50-CD5(3-10'x6' CBC)
(South Side of the Culvert)



SR 50-CD6 (3-36" RCP)
(South side of the Culvert)



SR 50-CD7 (4' x 4' CBC & 1-54" RCP Jointed)
(South Side of the Culvert)



SR 50- CD8 (1-30" RCP)
(South side of the culvert)



SR 50- CD9 (1-8'x7' CBC)
(South Side of the Culvert)



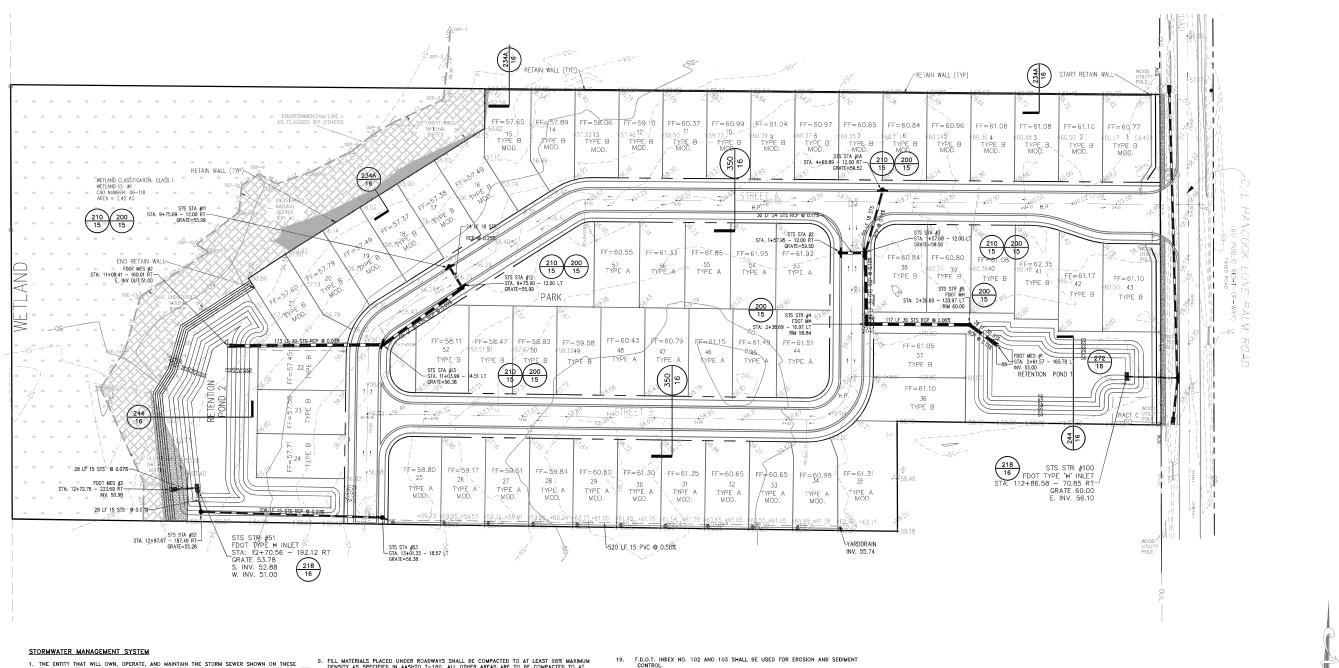
SR 50-CD10 (1-10'x4' CBC)
(South Side of the Culvert)



SR 50-CD11 (1-24" RCP)
(South Side of the Culvert)

Appendix: T

Excerpt from CAD Engineering and Design, Inc
Waterford Creek



- THE ENTITY THAT WILL OWN, OPERATE, AND MAINTAIN THE STORM SEWER SHOWN ON THESE PLANS IS MATTAMY-JACKSONVILLE PARTNERSHIP. THE CONTRACTOR SHALL BE EXPECTED TO MEET ALL THE REQUIREMENTS OF THE PERMITS OBTAINED.
- . THE CONTRACTOR SHALL PERFORM HIS OWN INVESTIGATIONS AND CALCULATIONS AS NECESSAR' TO ASSURE HIMSELF OF EARTHWORK QUANTITIES. THERE IS NO IMPLICATION THAT EARTHWORK BALANCES AND THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY IMPORT FILL NEEDED, OR FOR REMOVAL AND DISPOSAL OF EXCESS MATERIALS.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING THE NECESSARY TESTING TO ASSURE THAT THE PROPER COMPACTION HAS BEEN ACHIEVED ON THE SUBGRADE, BASE, AND ALL OTHER PERTINENT AREAS THAT HAVE BEEN COMPLETED. THE CONTRACTOR SHALL BEAR ALL COSTES ASSOCIATED WITH TESTING AND SHALL PROVIDE THE OWNER AND THE ENGINEER WITH COPIES OF THE CERTIFICATION OF COMPACTION FROM THE TESTING COMPANY.
- PRIOR TO BIO PREPARATION, THE CONTRACTOR MUST BECOME FAMILIAR WITH THE OVERALL SITE CONDITIONS AND PERFORM ADDITIONAL INVESTIGATIONS AS DETERMINED NECESSARY TO UNDERSTAND THE LIMIT AND DEPTH OF EXPECTED ORGANIC SLIT PEAT AREAS, ADEQUACY OF EXISTING MATERIALS AS FILL, DEWATERING REQUIREMENTS, CLEAN FILL REQUIRED FROM OFF-SITE ALL OF WHICH WILL AFFECT HIS PRICING, ANY DELAY, INCONVENIENCE, OR EXPENSE CAUSED TO THE CONTRACTOR DUE TO INADEQUATE INVESTIGATION OF EXISTING CONDITIONS SHALL BE INCIDENTAL TO THE CONTRACT, AND NO EXTRA COMPRISATION WILL BE ALLOWED. THE METRICAL STATE OF THE RECOUNTERED OF THE CONTRACT AND THE CONTRACT AN
- 5. IT IS THE CONTRACTOR'S RESPONSIBILITY TO DETERMINE EXISTING SITE CONDITIONS OF SOIL PRIOR TO N.T.P. TO DETERMINE IF ANY OFF-SITE MATERIALS WILL NEED TO BE IMPORTED TO ACHIEVE THE GRADES SPECIFIED ON THE PLANS.
- . THE CONTRACTOR SHALL NOTIFY THE OWNER AND ENGINEER WHEN ALL WORK IS LAID OUT (SURVEY STAKED), SO THAT A DETERMINATION MAY BE MADE OF SPECIFIC TREES TO BE REMOVED. A TREE REMOVAL PERMIT IS REQUIRED TO BE OBTAINED BY THE CONTRACTOR.
- 7. ALL FILL MATERIALS SHALL BE FREE OF MUCK, STUMPS, ROOTS, BRUSH, VEGETATIVE MATTER, RUBBISH, OR OTHER UNSUITABLE MATTER.
- 8. ALL MATERIALS EXCAVATED SHALL REMAIN THE PROPERTY OF THE OWNER AND SHALL BE STOCKPILED AT ON-SITE LOCATIONS AS SPECIFIED BY THE OWNER. MATERIALS SHALL BE STOCKPILED SEPARATELY AS TO USEABLE (MONORANIC) FILL STOCKPILES AND ORGANIC (MUCK) STOCKPILES IF MUCK IS ENCOUNTERED. CONTRACTOR SHALL BE RESPONSIBLE FOR THE REMOVAL OF ALL UNBUTTABLE FILM MATERIALS FROM THE SITE.

- 9. FILL MATERIALS PLACED UNDER ROADWAYS SHALL BE COMPACTED TO AT LEAST 98% MAXIMUM DENSITY AS SPECIFIED IN AASHTO T-180. ALL OTHER AREAS ARE TO BE COMPACTED TO AT LEAST 95% MAXIMUM DENSITY AS SPECIFIED IN ASHTOT T-180. FILL MATERIALS SHALL BE PLACED AND COMPACTED IN A MAXIMUM OF 12" LIFTS, REFER TO SOLIS REPORT FOR ADDITIONAL INFORMATION. THE CONTRACTOR SHALL PROVIDE THE CRIGINEER AND THE OWNER WITH ALL (PASSION AND FAILING) TESTING RESULTS. RESULTS SHALL BE PROVIDED ON A TIME AND REGULAR BASIS FROM TO CONTRACTOR'S PAY REQUEST SUBMITTALE.
- . GRADING SHOWN ON THESE PLANS IS PROVIDED TO THE CONTRACTOR TO EXPRESS THE GENERAL GRADING INTENT OF THE PROJECT. THE CONTRACTOR SHALL GRADE THE ENTIRE SITE TO PROVIDE POSITIVE PRAINAGE IN ALL AREAS. SMOOTH TRANSITIONS SHALL BE PROVIDED BETWEEN CONTOURS OR SPOT ELEVATIONS AS SHOWN ON THE PLANS TO ACCOMPLISH THE GRADING INTENT. ALL SLOPES SHALL BE STABILIZED IMMEDIATELY AFTER FIRAL GRADING HAS BEEN COMPLETED. CONTRACTOR SHALL NOTIFY OWNER AND ENGINEER A MINIMUM OF FORTY-EIGHT(48) HOURS PRIOR TO DEMOBLIZATION OF GRADING EQUIPMENT TO DETERMINE THAT THE GRADING INTENT HAS BEEN ACHIEVED.
- 12. ALL OTHER RELATED ITEMS REQUIRED FOR THE CONSTRUCTION OF THE STORM SEWER (OUTFALL PROTECTION, POLLUTION CONTROL, ETC.) ARE TO BE IN ACCORDANCE WITH DETAILS SHOWN ON THE CONSTRUCTION PLANS, FOOT ROADWAY AND TRAFFIC DESIGN STANDARDS, AND FDOT STANDARD SPECIFICATIONS FOR ROADWAY AND BRIDGE CONSTRUCTION (LATEST EDITION).
- 13. ALL PIPE CALL OUTS ARE MEASURED CENTERLINE TO CENTERLINE FOR MANHOLES AND INLETS. 14. ALL ON-SITE AREAS DISTURBED BY THE CONSTRUCTION SHALL BE STABILIZED WITH A SEED AND MULCH MIXTURE UNLESS OTHERWISE NOTED.
- 15. ALL OFF-SITE AREAS DISTURBED BY CONSTRUCTION SHALL BE SODDED WITH BAHLA

- 18. COORDINATE WITH LANDSCAPE CONTRACTOR TO ASSURE POND(S) ARE SODDED TO PREVENT

- FOR SOILS DATA, REFER TO REPORT PREPARED BY NODARSE & ASSOCIATES, INC. DATED JUNE 29, 2011.
- SITE GRADING, PAVING, AND DRAINAGE MATERIALS AND CONSTRUCTION SHALL CONFORM TO ORANGE COUNTY AND SJRWMD DEVELOPMENT STANDARDS AND SPECIFICATIONS.
- THE STORMWATER POND SIDE SLOPES SHALL BE CONSTRUCTED DURING THE EARLY STAGES OF CONSTRUCTION; SIDE SLOPES SHALL BE SODDED AND THE BOTTOM SEEDED. THESE AREAS SHOULD HAVE VEGETAINON ADDED AS SOON AS FEASIBLE.

PAVING & DRAINAGE NOTES:

- SIDEWALKS ARE TO BE CONSTRUCTED THE LENGTH OF FRONTAGE FOR TRACTS A & B AND ALONG HANCOCK LONE PALM ROAD AS PART OF THE INFRASTRUCTURE.
- THE MINIMUM GRADE FOR THE SUBDIVISION STREETS WITH MIAMI CURB SHALL BE TWENTY-FOUR HUNDREDTHS (.24%) PERCENT.
- WHERE BERMS ARE PROPOSED, THE DESIGN SHALL BE CERTIFIED BY THE GEOTECHNICAL ENGINEER.
- ALL ENVIRONMENTAL SWALES WILL BE OWNED AND MAINTAINED BY THE INDIVIDUAL LOT OWNER AND WILL BE CONSTRUCTED WITH THE INFRASTRUCTURE
- AN EROSION CONTROL PLAN IS BEING SUBMITTED AND WILL BE APPROVED BY THE COUNTY ENGINEER.
- 30. THE SIDEWALK AND APRON IN FRONT OF THE DETENTION PONDS & LIFTSTATION ARE 6" THICK AS SHOWN ON PLANS.

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SED FOR EROSION AND SEDIMENT			site or	٥,
ON SURVEY PREPARED BY W.C. ELLIOTT		4	<u>و</u> ا	;

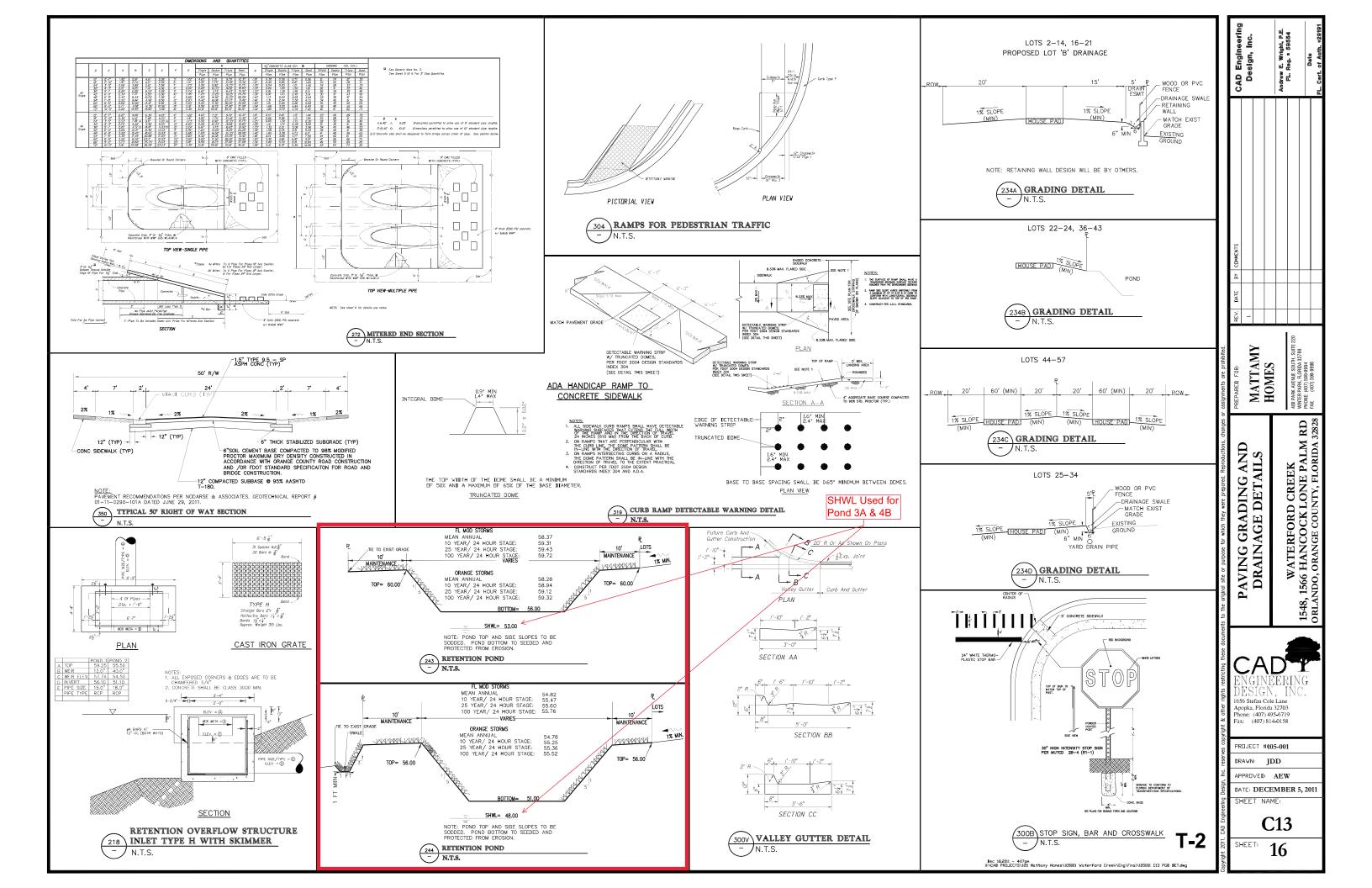


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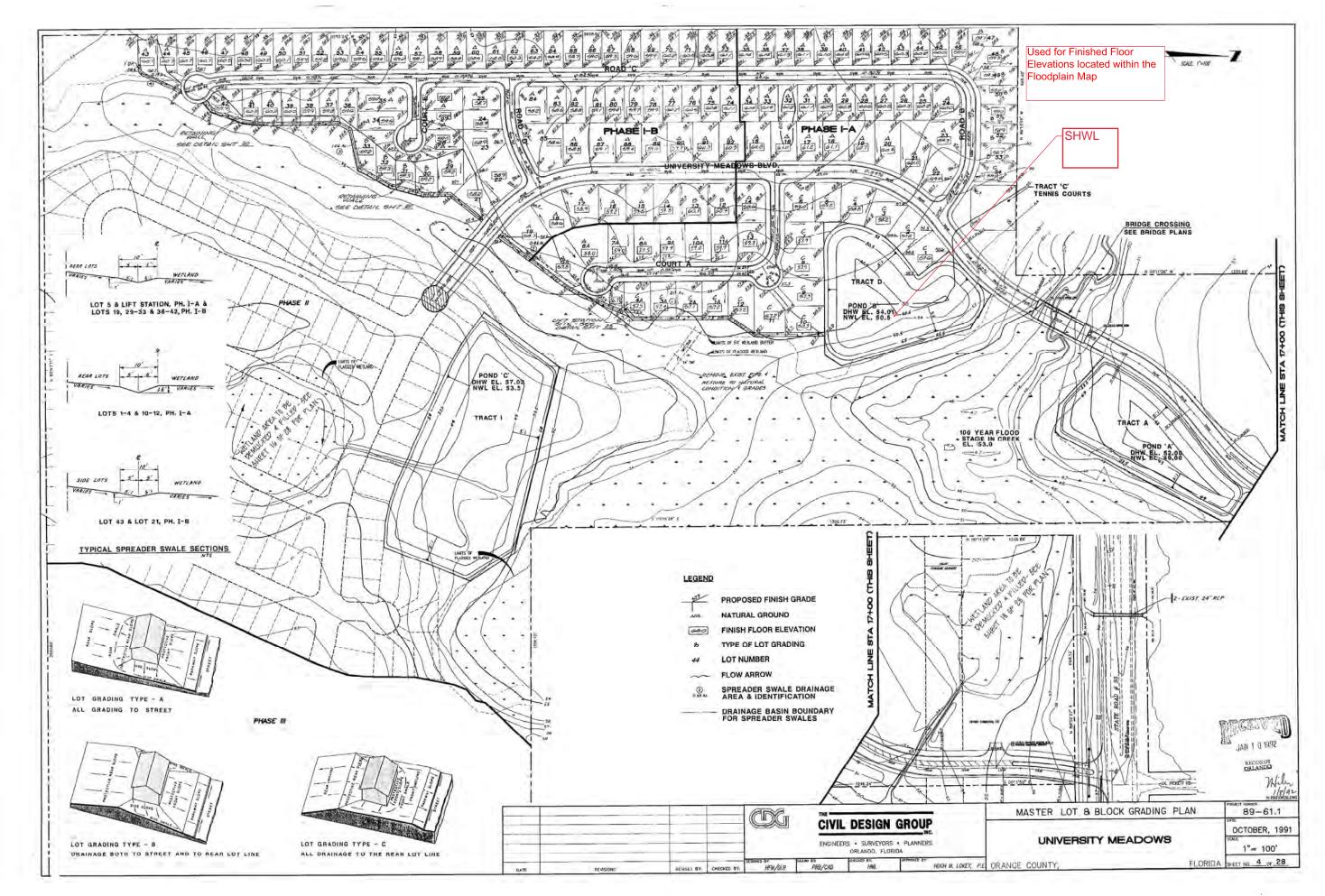
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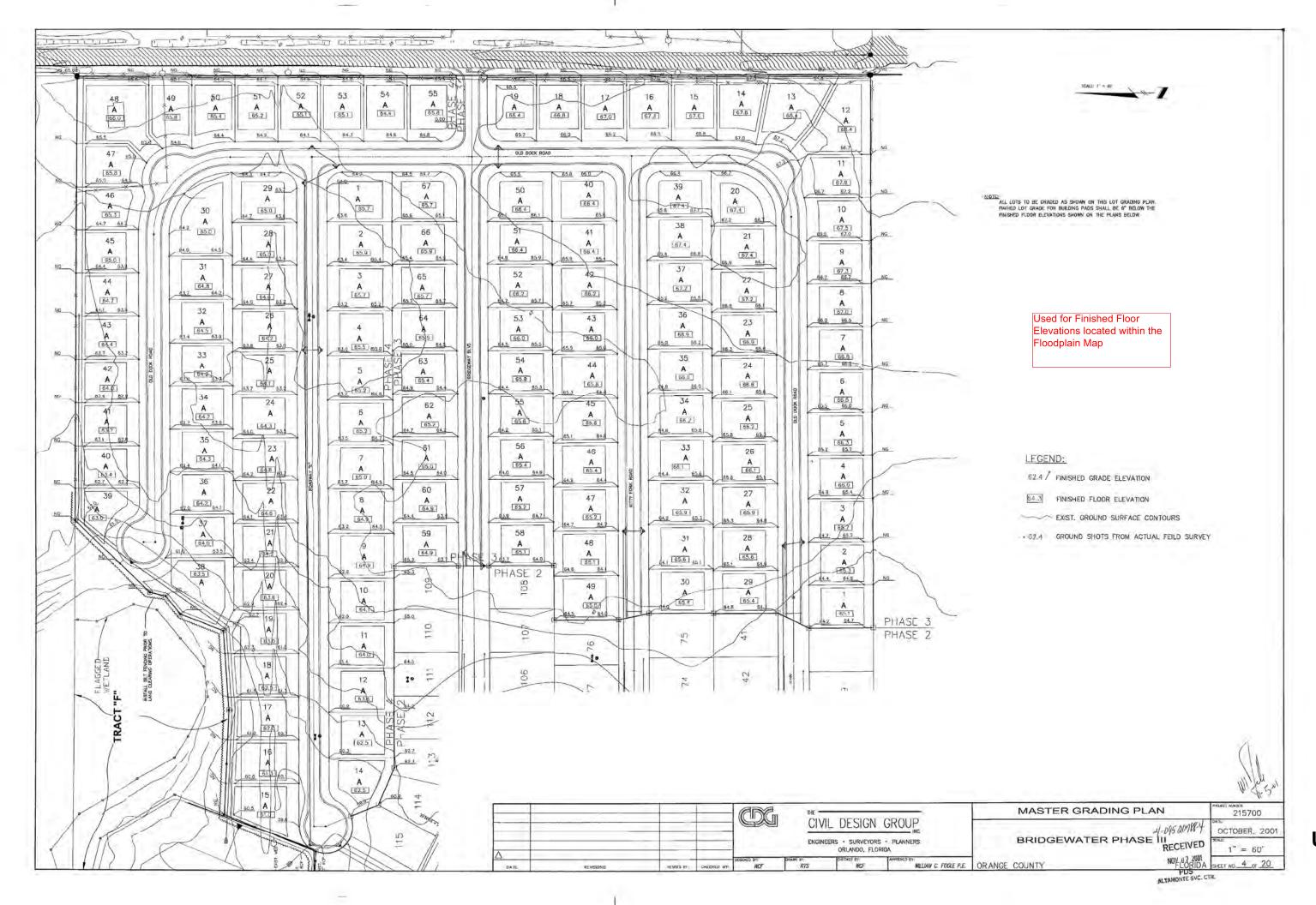
SCALE IN FEET



Appendix: U

Excerpt from The Civil Design Group
University Meadows & Bridgewater Plans

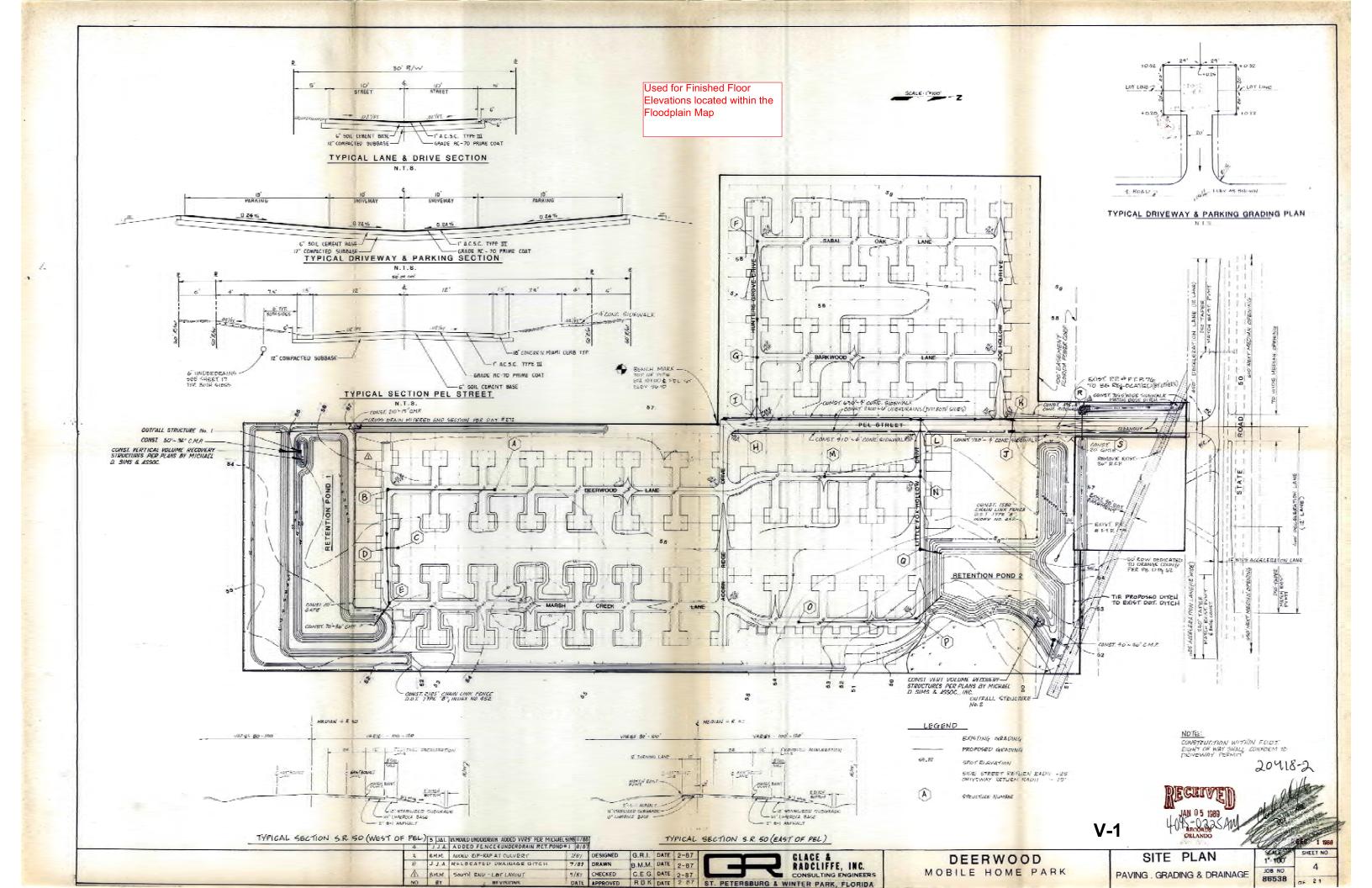




Appendix: V

Excerpt from Glace and Radcliffe, Inc.

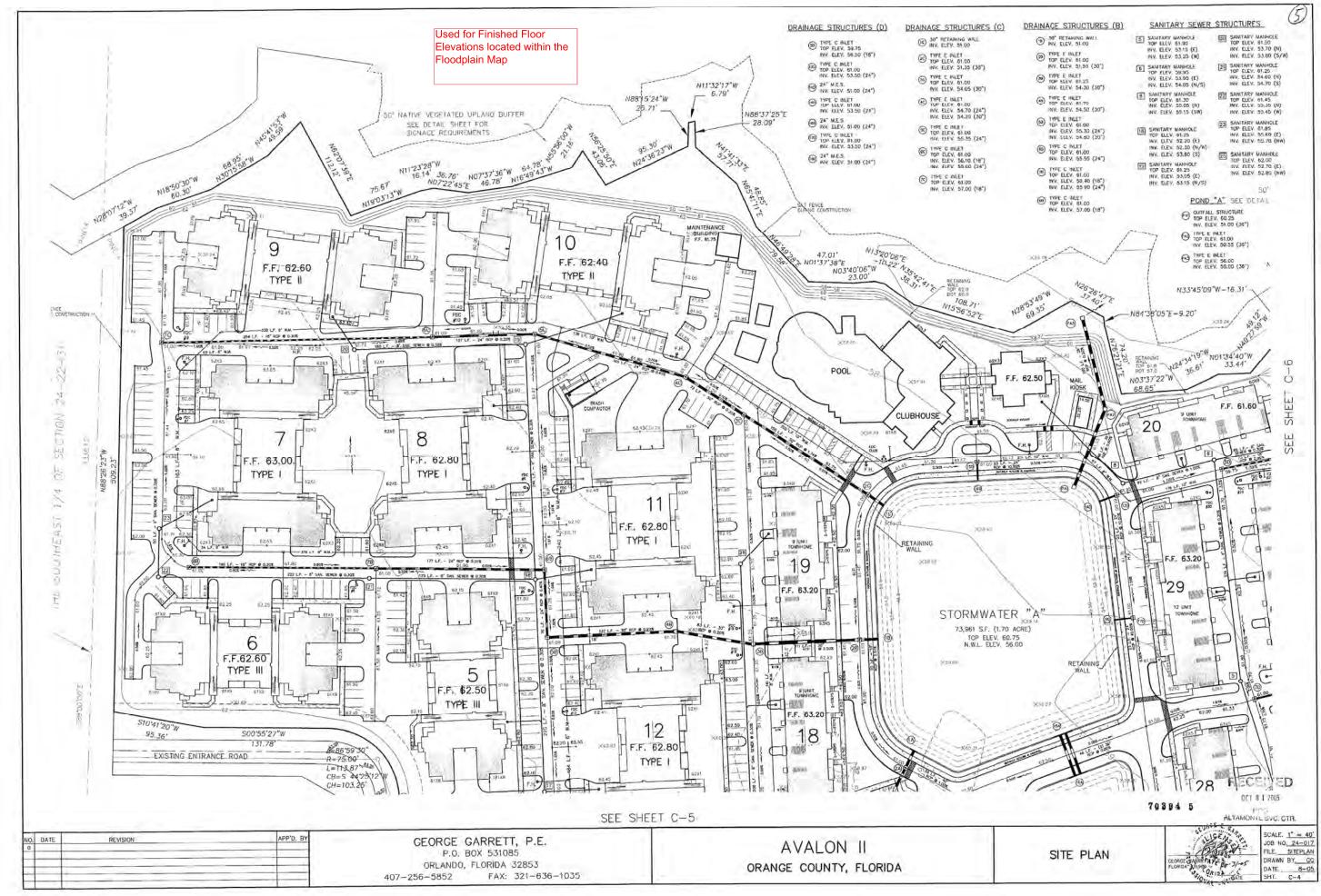
Deerwood Plans

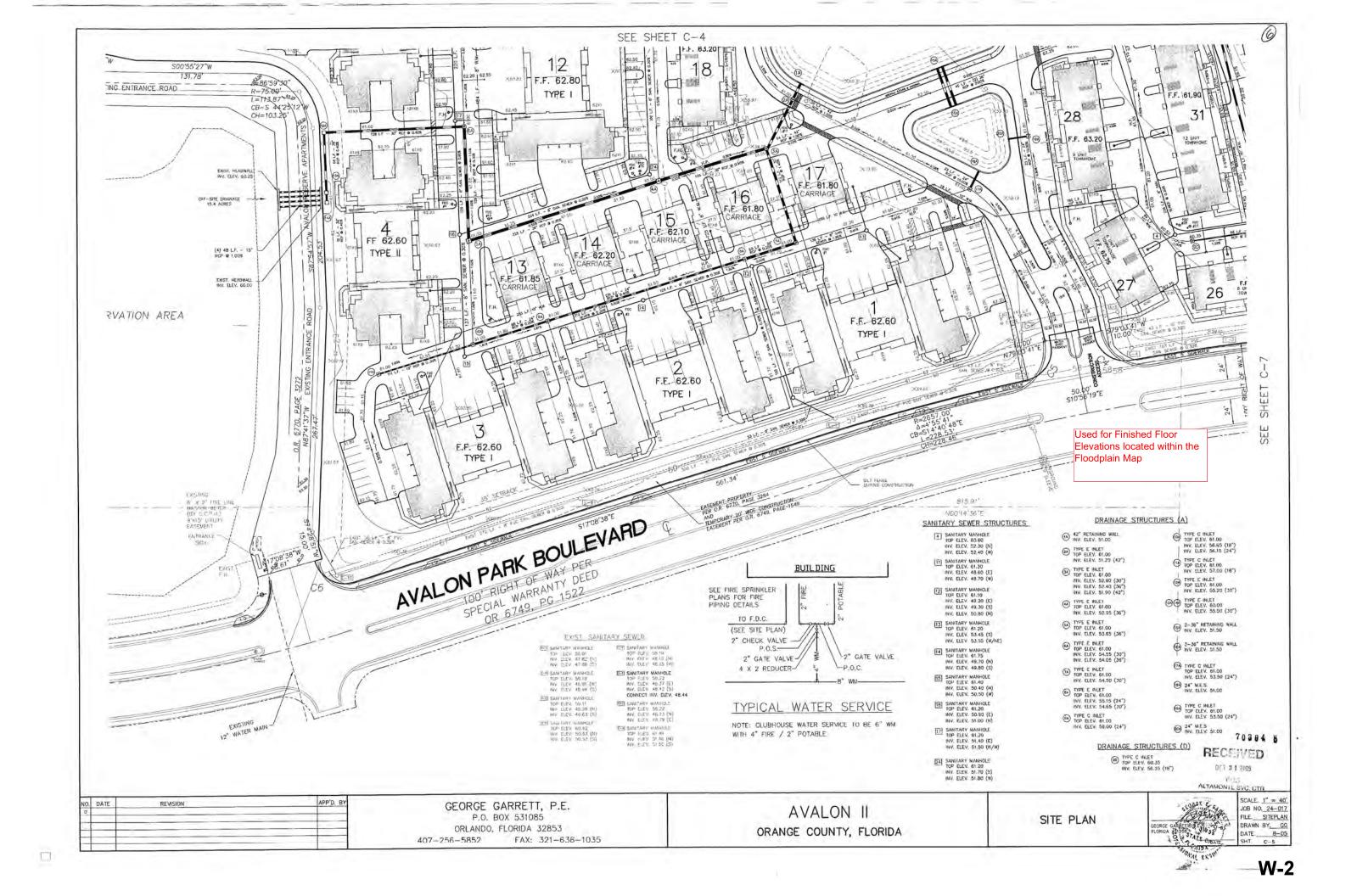


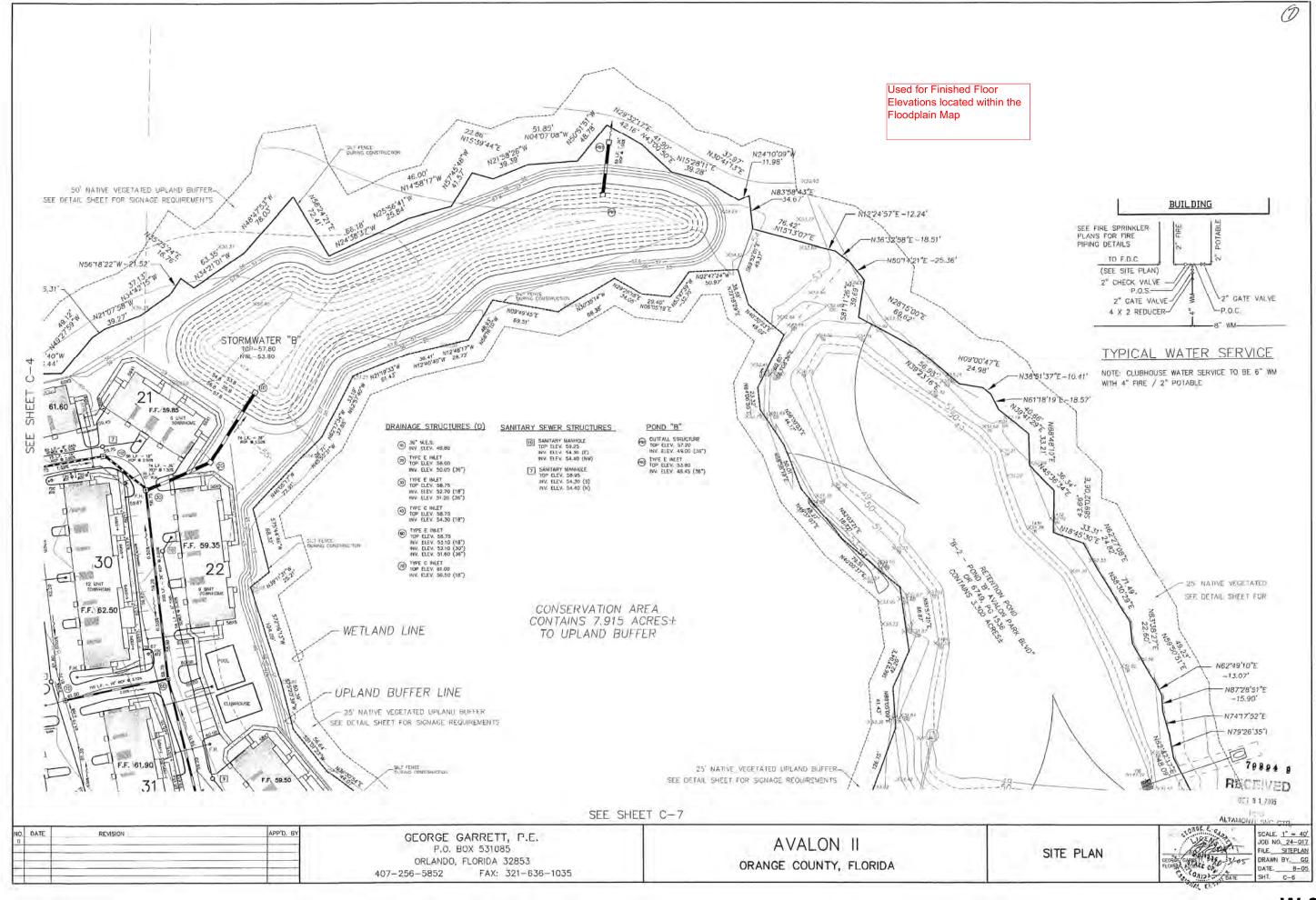
Appendix: W

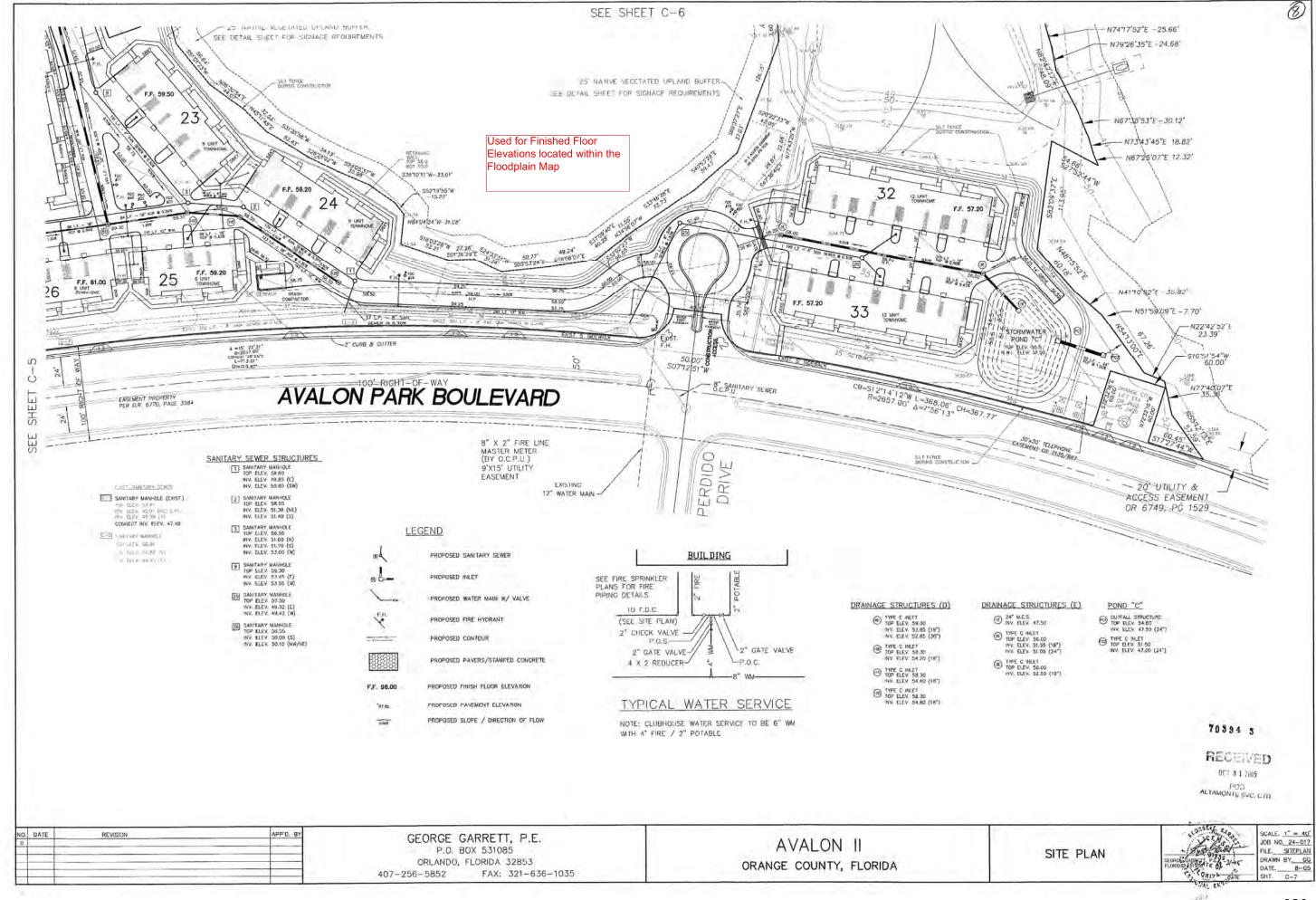
Excerpt from George Garrett, P.E.

Avalon II Plans





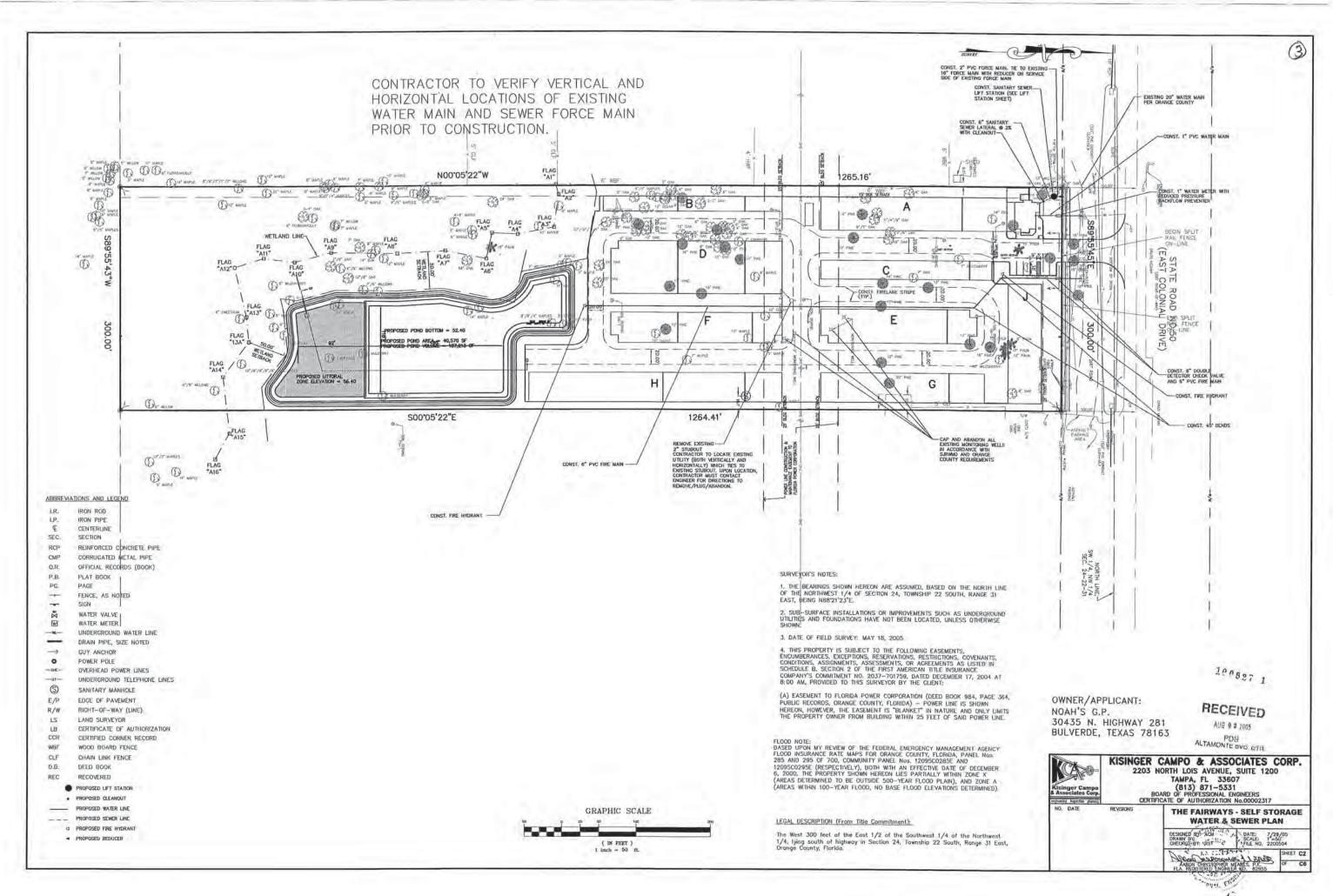




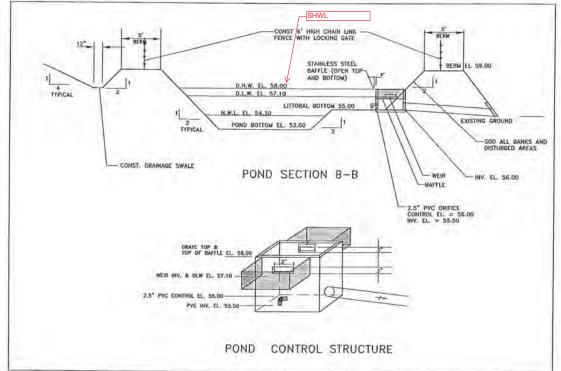
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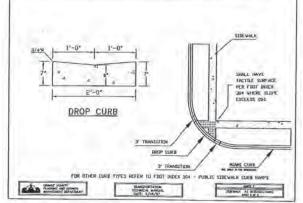
Excerpt from Kisinger Campo & Associates Corp.

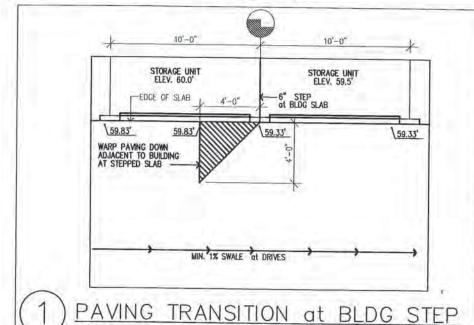
The Fairways – Self Storage











1. The dimensions and locations of the proposed buildings shown herean are approximate only. Do not utilize said measurements for building leyout. Refer to the Architectural drawings for exact building dimensions.

2. Land surveys, soils reports and legal descriptions were provided by others. The Engineer does not certify to the accuracy or completeness of some. The Large of these plans shall verify the accuracy of all soid information to the state of these plans shall verify the accuracy of all soid information.

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3. No constantiation is permitted in

ROAD AND DRAINAGE NOTES

1. All workmanship and malerials shall conform to fla. D.O.T. STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, 2004 edition and all Grange County Technical Manuals.

2. This drawing shows drainage and grading design to within 3 feet of the building(a) only and specifically excludes designs for structures, reliating walls, waterproofing and vertiliation. The Confractor shall coordinate with others to insure that support designs have been completed by other design professionals and that no conflicts exist with any other construction, particularly grading within 5 feet of the buildings. Order-executed prior to any other construction, with stormwater runoff directed to them.

Over-execution and burying any debtis beneath, the point is prohibited. It dewatering is required the Contractor shall be fine graded and sadded per the plan.

4. EROSION / SCUMENTATION CONTROL: The Contractor shall supply all erosion / sedimentation barriers (hay bales, all screens and so forth). To prevent sillation and excess quantities of earth from being transported either by natural drainage or vehicular traffic onto any adjacent properties, streets, storm sewers, waterwaye, conservation areas and so forth. The Contractor shall clean and restore and r

B. OPERATION & MAINTENANCE OF THE STORMWAITE MANAGEMENT SYSTEM:

(a) Regularly clean all pipes, welrs and intels.

(b) Maintoin all design elevations and dimensions in the pond.

(c) Repair oil areas affected by erosion immediately.

(d) Dry Ponds Mew, clean and power rake the pond bottom regularly.

(e) Wet Ponds Removal of native vegetation, including caltalls is prohibited. Removal includes dredging, the application of herbicides, infraculation of sors corp and cutting, Maintenance of the ponds shall include keeping structures free of any obstructions. The maintenance entity should address any questions regarding authorized activities within the well detention pand to SJRWMD.

7. The Contractor shall remove all existing asphall, trees being designated as being removed and other debris and dispose of some off site at an opproved dumping facility.

8. The Contractor shall stripe the parking lot and install concrete curb stops as indicated hereon.

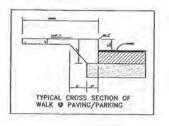
9. All inlets and grate tops shall be designed and furnished as H-20 load bearing. Grate tops must be traversible by bicycles and pedestrians.

Traffic Control Plan:

1. The Permittee shall conduct his operations such that there will be a minimum of interference with or interruption of traffic upon and along the roadway. This applies to both the initial installation and the confining maintenance and operation of facilities except in emergencies There shall be no inherterence with or interruption of traffic upon and along the roadway until a maintenance of traffic plan approved by the

South, and the installation of the facilities authorized by the Use Permit, the Permitlee shall at all times maintain flaggers, signs, lights, flares, barricades, and other safety devices as required by the applicable standards or as the County may reasonably deem necessary to properly protect fraffic upon the readway, and to warm and safeguard the public, work crews or County employees against injury or damage.

To work within County Right-of-way, submit a maintenance of traffic plan to Orange County Traffic

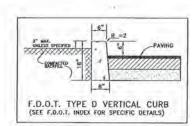


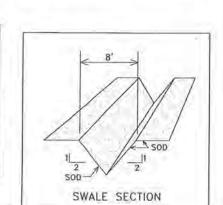
SILT SCREEN

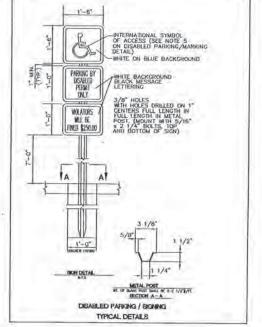
STAKE (2X2 MIN.)-

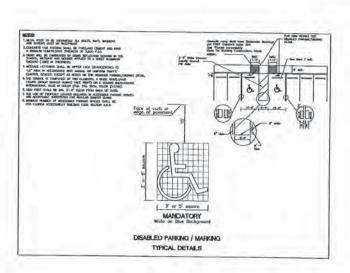
3'-0" MAX.

SILT SCREEN DETAIL









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PDS ALTAMONTE BVC, OTA



KISINGER CAMPO & ASSOCIATES CORP. 2203 NORTH LOIS AVENUE, SUITE 1200 TAMPA, FL 33607

(813) 871-5331 BOARD OF PROFESSIONAL ENGINEERS CERTIFICATE OF AUTHORIZATION No.00002317

THE FAIRWAYS - SELF STORAGE PAVING & DRAINAGE DETAILS

ARON CHROSTIPPER NO. 62955