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## MEMORANDUM

January 16, 2023

To: From: Subject:	Greg Seidel, P.E. – The Balmoral Group Bronce Stephenson – The Balmoral Group Jonathan Williamson, ACIP – Dewberry Engineers Jason Cornell Noise Study Report Addendum CFX Project #429-309 PD&E Study SR 429 / Binion Road Interchange Orange County
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The October 2022 Traffic Noise Study Report documented the analysis conducted as part of the PD&E Study. At that time, the selected alternative included a roundabout intersection for Binion Road and Boy Scout Road. After finalizing the report, the roundabout intersection has been replaced with a signalized intersection. A roundabout is still an option presented in the engineering documentation.

The recommended noise barriers were analyzed to abate traffic noise from SR 429. Thus, the change in the intersection design is not anticipated to change the outcome of the barrier results.

The Traffic Noise Study will be re-evaluaed during the project's Design Phase at which time the signalized intersection will be incorporated into the analysis.





SR 429 INTERCHANGE WITH BINION ROAD (RE-ALIGNED BOY SCOUT ROAD SIGNAL ALTERNATIVE)



## **Traffic Noise Study Report**

## **Daniel Webster Western Beltway**

SR 429 / Binion Road Interchange Project Development and Environment (PD&E) Study Orange County, Florida CFX Project No: 429-309

> Prepared For: Central Florida Expressway Authority



Prepared By: Environmental Transportation Planning, LLC Ponte Vedra Beach, FL

> In Association With: Dewberry Engineers, Inc. Orlando, FL

> > October 2022



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### **1.0 INTRODUCTION**

The Daniel Webster Western Beltway (SR 429) is a 23-mile long, limited-access toll road that extends from Interstate 4 in Osceola County to US 441 in Orange County. Expansion of the Beltway's capacity is underway from Tilden Road to the north of SR 414. The Central Florida Expressway Authority (CFX) is now conducting a Project Development and Environment (PD&E) Study to evaluate a proposed half interchange expressway connection from Binion Road to SR 429. The new interchange and other improvements will provide enhanced access and mobility to southwest Apopka.

#### **1.1 Project Limits**

The study area runs along the vicinity of Binion Road and Boy Scout Road at SR 429. The project study area is illustrated in **Figure 1**.

#### **1.2** Purpose and Need

#### <u>Purpose</u>

A new interchange connection between SR 429 and Binion Road has been identified as a need to provide enhanced access and mobility to southwest Apopka from SR 429 in the vicinity of Binion Road. Currently, vehicles in the vicinity of Binion Road must enter or exit SR 429 by traveling approximately three miles north to just north of US 441 at the SR 429 Connector Road interchange or travel approximately three miles south to the interchange at Ocoee Apopka Road. Therefore, this PD&E Study will analyze and evaluate a proposed half interchange (northbound on-ramp and southbound off-ramp) expressway connection from Binion Road to SR 429. Additional purposes for the project include improved emergency vehicle access to the hospital and supporting economic development.

#### Need

Six project needs serve as justification for the proposed improvements. These needs are to 1) Provide system linkage; 2) Provide regional connectivity and mobility; 3) Support social and economic needs; 4) Provide consistency with Local and Regional Plans; 5) Accommodate and provide for multi-modal transportation options; and 6) Design a safe intersection at Binion Road & Boy Scout Road.

#### <u>Environment</u>

Environmental analyses are a critical component of any PD&E study. When evaluating new infrastructure, the potential environmental effects are studied, with multiple evaluations covering the spectrum of natural and human-centered environments.

The objective of this Traffic Noise Study Report is to summarize the traffic noise analysis conducted for the PD&E's preferred build alternative. The analysis identifies the noise sensitive





receptors within the study corridor and evaluates the noise levels predicted to occur due to the proposed project. Sites and communities not specifically identified in **Appendix D** are 1) not within the project limits or 2) are located too far from the adjacent roadways under study to be considered noise sensitive.

#### **1.3 Build Alternative**

The PD&E's preferred build alternative is illustrated in **Appendix A**. Additional engineering detail can be found in the project's Preliminary Engineering Report (PER).

#### **1.4 No-Build Alternative**

Consistent with FDOT guidelines, this analysis also considers an alternative that assesses what would happen to the environment in the future if this proposed project was not built. This alternative called the No-Build Alternative consists of the existing roadways within the study area, programmed improvements to existing facilities, and routine maintenance improvements to these facilities. While the No-Build Alternative does not meet project needs, it provides a baseline condition to compare and measure the proposed project's effects.





#### Figure 1: Project Location Map



## 2.0 METHODOLOGY

The traffic noise study conducted for this project is consistent with *Code of Federal Regulations* (C.F.R.), Title 23, § 772; Chapter 335, Section 335.17, *Florida Statutes*; Part II, Chapter 18 of the Florida Department of Transportation's (FDOT) *Project Development and Environment Manual*; and Federal Highway Administration's (FHWA) traffic noise analysis guidelines contained in *FHWA-HEP-10-025*. The FHWA Traffic Noise Model (TNM) - version 2.5 was used to predict traffic noise levels for this project. The analysis evaluated noise levels for the existing condition and the 2045 No-Build and Build Alternatives.

Noise receptor coordinates used in the TNM are located in exterior areas where frequent human use may occur, usually at the edge of the residential structure closest to the project roadways, unless the analyst's professional judgment determines otherwise.

Project engineering design files were used to determine the design alternative's location for input into TNM. Roadway elevation data for the study was obtained from the project engineering team. Data for the noise receptors and cross streets were obtained from the United States Geological Survey digital elevation models<sup>1</sup>. Additional receptor elevation data was gleaned from the approved final development plans for the two residential communities adjacent to SR 429.

### 2.1 NOISE METRICS

Noise is typically defined as unwanted sound. Traffic noise is a combination of noises produced by the engine, exhaust, and tires and is never constant. The noise metric used to describe this combination of noise is called "Leq." This metric allows for the fluctuations of daily traffic noise to be analyzed in terms of steady noise levels with the same acoustic energy, and thus, is the level of constant sound. Constant sound is quantified by a meter that measures units called decibels (dB). For highway traffic noise, an adjustment or weighting of the high and low-pitched sounds is applied to approximate how an average person hears. These adjusted sounds are called "A-weighted decibels" and are expressed as "dB(A)."

### **2.2 TRAFFIC DATA**

Traffic noise is heavily dependent on traffic volume and speed, with the amount of noise generated by traffic increasing as the vehicle speed and number of vehicles increase. Characteristics contributing to the 2045 Design Year's highest traffic noise levels were used to predict project noise levels. Worst-case noise conditions occur with the maximum traffic traveling at the posted speed and represent a Level of Service (LOS) C operating condition. However, if the traffic analysis indicates the roadway will operate below LOS C, the project's Demand peak-hour directional traffic volumes are used per Chapter 18 of the FDOT PD&E Manual. Traffic volumes and speeds used in the analysis are included in **Appendix B**.

<sup>&</sup>lt;sup>1</sup> USGS, https://apps.nationalmap.gov/lidar-explorer/#/



#### 2.3 NOISE ABATEMENT CRITERIA

Land use plays an important role in traffic noise analyses. To determine which land uses are "noise sensitive," this noise impact analysis used the FHWA Noise Abatement Criteria (NAC). **Table 1** shows these criteria are divided into individual land use activity categories. The FDOT has established noise levels at which noise abatement must be considered for each of these categories, referred to in this report as the FDOT NAC. Another criterion for determining project impacts that warrant abatement consideration occurs when project noise levels are below the NAC but show a substantial increase (15.0 dB(A) or more) over existing levels.

Hourl	-	ghted Sou els (dB(A)		
Activity	Activity	/ Leq(h) <sup>1</sup>	Evaluation	Description of Activity Category
Category	FHWA	FDOT	Location	
A	57.0	56.0	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need; and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose.
B <sup>2</sup>	67.0	66.0	Exterior	Residential.
C <sup>2</sup>	67.0	66.0	Exterior	Active sports areas, amphitheaters, auditoriums, campgrounds, cemeteries, daycare centers, hospitals, libraries, medical facilities, parks, picnic areas, golf courses, places of worship, playgrounds, public meeting rooms, public/nonprofit institutional structures, radio studios, recording studios, recreational areas, Section 4(f) sites, schools, television studios, trails, and trail crossings.
D	52.0	51.0	Interior	Auditoriums, daycare centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public/nonprofit institutional structures, radio studios, recording studios, schools, and television studios.
E <sup>2</sup>	72.0	71.0	Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties, or activities not included in A-D or F.
F	-	-	-	Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing.
G	-	- 23 CER Part 7	-	Undeveloped lands that are not permitted.

#### Table 1: Noise Abatement Criteria

(Based on Table 1 of 23 CFR Part 772)

<sup>1</sup> The Leq(h) Activity Criteria values are for impact determination only and are not design standards for noise abatement measures.

<sup>2</sup> Includes undeveloped lands permitted for this activity category.



An illustration of typical exterior and interior noises and their corresponding sound level is presented in **Table 2**. This table gives the reader a better understanding of the noise levels discussed herein. In Florida, noise levels that reach 66.0 dB(A) at Activity Category B and C land use require noise abatement consideration. A 71.0 dB(A) noise level is required for an Activity Category E land use to be impacted by traffic noise.

Common Outdoor Activity	dB(A)	Inside Activity
Jet Flyover at 1,000 ft. Gas Lawn Mower at 3 ft.	110	Rock Band
Diesel Truck at 50 ft. (at50 mph) Busy Urban Area Daytime	90 80	Food Blender at 3 ft. Garbage Disposal at 3 ft.
Gas Mower at 100 ft. Commercial Area Heavy Traffic at 300 ft.	70 60	Vacuum Cleaner at 10 ft. Normal Speech at 3 ft. Large Business Office
Quiet Urban Daytime Quiet Urban Nighttime Quiet Suburban Nighttime	50 40	Dishwasher Next Room Theater, Large Conference Room (Background)
Quiet Rural Nighttime	30 20	Library Bedroom at Night
	10	
Lowest Threshold of Human Hearing	0	Lowest Threshold of Human Hearing

#### Table 2: Comparative Sound Levels

Source: California Dept. of Transportation Technical Noise Supplement, Oct. 1998, Pg. 18

#### 2.4 Noise Abatement Measures

When traffic noise impacts are identified, noise abatement must be considered. The potential abatement alternatives include traffic management techniques, alternative roadway alignments, buffer zones, and noise barriers. The most common type of noise abatement measure is the construction of a noise barrier that reduces traffic noise by blocking the sound path between the roadway and the adjacent noise receptor.



Consistent with the FDOT PD&E Manual – Chapter 18, the following factors must be evaluated to determine if a noise barrier is considered feasible and reasonable:

- To be considered acoustically feasible, the barrier must reduce traffic-related noise levels by at least 5.0 dB(A) for at least two impacted receptors. Receptors that receive the 5.0 dB(A) reduction, or higher, are defined as "benefited" by FDOT. Consequently, noise barriers are not evaluated for isolated and single receptors.
- To be considered acoustically reasonable, the noise barrier must achieve the FDOT noise reduction design goal of 7.0 dB(A) for at least one benefited receptor.
- The cost per benefited receptor (CBPR) is calculated by multiplying the barrier's total square footage by \$30. Per Chapter 18, \$30 per/ft<sup>2</sup> is the statewide average used to determine cost reasonableness regardless of barrier type (shoulder/traffic railing mounted, right-of-way post/panel, etc.) To be considered cost reasonable, the total cost of a barrier that meets all acoustical criteria should not exceed the cost of \$42,000 per benefited receptor.

In some locations, noise barriers may provide a benefit to non-impacted residences. Due to design considerations or aesthetics, CFX may propose noise barriers exceeding cost reasonableness limits. An example would be extending a noise barrier to maintain community continuity (i.e., avoiding terminating a noise barrier in the middle of a community).

Consistent with the FDOT Design Manual, Section 264<sup>2</sup>, noise barrier heights are limited as follows:

- Noise barriers on bridge and retaining wall structures are limited to a maximum height of 8 feet; unless otherwise specified;
- Shoulder-mounted noise barriers at the edge of shoulder pavement are limited to a maximum height of 14 feet; and
- Non-shoulder mounted noise barriers (i.e., post and panel) located outside the clear recovery zone are limited to a maximum height of 22 feet. If a non-shoulder barrier is placed within the clear recovery zone, it must be shielded.

Other factors must also be considered when evaluating a barrier's feasibility, including accessibility, sight distance, and aesthetics. Accessibility refers to the ingress and egress to properties that would be affected by the construction of a noise barrier. Sight distance is a safety issue related to drivers' ability to see far enough in each direction to enter the roadway safely. Aesthetics refers to the noise barrier's physical appearance from both the highway and affected property sides.

<sup>&</sup>lt;sup>2</sup> FDOT, FDOT Design Manual

### **3.0 TRAFFIC NOISE ANALYSIS**

#### 3.1 Identification of Noise Sensitive Sites

Using **Table 1** as a guide, the noise sensitive land uses analyzed within the study corridor fall under Activity Category B and C. The Category C land uses are associated with the Binion Reserve playground and the Ivy Trails pedestrian trail.

No land uses in the study corridor warrant an Activity Category A analysis. Analysis of interior (Activity Category D) noise levels was not required for this project as all Category C locations have areas of exterior use. A search of building permits for potentially noise sensitive Category G (undeveloped) and non noise sensitive Category F lands within the study area did not identify any active permits for future buildings that would be considered noise sensitive. Another search will be conducted during the final design process. Any noise sensitive land permitted between the time of this report and the approval of the Project Environmental Impact Report will be analyzed for project noise impacts if warranted.

#### 3.2 Model Validation

Existing noise levels are measured in the project corridor to confirm if traffic is the primary noise source. These field measurements are also required to verify the accuracy of the TNM before it can be used to predict noise levels. A series of three 10-minute measurements were taken on September 16, 2022, using an Extech Instruments Model 407780 Type 2 Integrating Sound Level Meter. The sound level meter, calibrated at 114.0 dB(A) with an Extech Instruments Model 407766 calibrator, was adjusted to the A-weighted frequency scale, which approximates the frequency sensitivity of the human ear. Traffic data, including vehicle volumes, speeds by type, and meteorological conditions, were recorded during each measurement session. The data collection effort also recorded the travel speed for each type of vehicle using a Bushnell Speedster handheld radar gun.

One location within the study corridor was selected to undergo a series of three 10-minute measurements. The validation site, illustrated on page **D-2 in Appendix D**, was selected for measurement because it presented a clear view of free-flow traffic conditions on SR 429. No unusual noise events occurred during this location's three 10-minute monitoring sessions. The weather during the monitoring session was 77°, 97% humidity, under clear skies with a mild breeze ranging from 2 to 5 m.p.h.

Validation of TNM occurs when the model-predicted noise levels are within three decibels of the field-measured levels. Since all noise levels in this analysis are based on one hour, each of the 10-minute sessions field-recorded traffic volumes was adjusted upward by a factor of "6" to reflect hourly traffic flow. Once adjusted, these volumes were input into the noise prediction model. As shown in **Table 3**, TNM predicted within the 3.0-decibel acceptance range for each 10-minute session. Consequently, the model is acceptable for predicting noise levels for this project.



			FIE	LD TRAF	FIC COUN	T: 9/16/	2022				
Session	#1: 9:38 AN	Л									
	Car	S	Medium	Trucks	Heavy T	rucks	Buse	es	Moto	cycles	
SR 429	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	
SB	168	57	9	51	19	50	0	0	0	0	
NB	147	54	15	51	19	50	0	0	0	0	
	F	ield Mea	surement	(dB(A)):	68.6						
		TNM	Prediction	(dB(A)):	69.9						
			Va	ariance:	1.3						
Session	#2: 9:50 AN	Л									
SR 429	Car	s	Medium	Trucks	Heavy T	rucks	Buse	es	Motorcycles		
	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	
SB	169	55	18	51	26	50	0	0	1	52	
NB	144	53	11	51	20	50	0	0	0	0	
	F	ield Mea	surement	(dB(A)):	68.0						
		TNM	Prediction	(dB(A)):	69.9						
			Va	ariance:	1.9						
Session	#3: 10:02 A	M									
SR 429	Car	S	Medium	Trucks	Heavy T	rucks	Buse	es	Motorcycles		
	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	Volume	Avg. Speed	
SB	168	53	19	51	27	50	0	0	0	0	
NB	113	53	14	51	22	50	0	0	1	53	
	F	ield Mea	surement	(dB(A)):	69.1						
		TNM	Prediction	(dB(A)):	70.2						
			Va	ariance:	1.1						



#### **3.3 Predicted Noise Levels**

Traffic on SR 429 is the dominant noise source within the project's evaluation area. For this project, 53 sites were analyzed for project-related impacts. The noise analysis divided the project corridor into three Noise Study Areas (NSA).

The 2022 existing condition and 2045 No-Build and Build Alternative noise analysis results discussed in this section are also presented in a noise impact comparison matrix in **Appendix C.** A summary of the results is provided in **Table 3**.

Four residential (Category B) receptors and one Category C Special Use site currently experience noise levels that meet or exceed the FDOT 66.0 dB(A) NAC. Predicted noise levels for the No-Build Alternative meet or exceed the NAC at nine Category B and one Category C receptor. By comparison, the Build Alternative is predicted to meet or exceed the NAC at 18 residential receptors and the same Category C site, with an average 3.1 dB(A) increase in noise over the existing condition. The greatest increase over existing is 4.9 dB(A); thus, none of the noise increases are considered substantial (defined as 15 dB(A) or higher).

When discussing noise level increases, the general rule that applies to perception is:

- A 3 dB(A) increase is barely perceptible to most people.
- A 5 dB(A) increase is noticeable to most people.
- A 10 dB(A) increase is perceived as twice as loud and considered a doubling noise.

A discussion of each NSA and the corresponding impact and abatement analysis is provided in the following sections. A set of project aerials illustrating the NSA's and analyzed sites is included in **Appendix D**.

Noise	Activity	2022 Existing	2045 No-Build	2045 Build	Average Increase Over	
Sensitive Area	Category	# of receptors	Existing			
	В	n/a	n/a	n/a		
NSA 1 (undeveloped)	С	n/a	n/a	n/a	n/a	
(4.14010.00004)	Subtotal	n/a	n/a	n/a		
	В	0	0	0		
NSA 2	С	0	0	0	1.3 dB(A)	
	Subtotal	0	0	0		
	В	4	9	9		
NSA 3 Binion Reserve	С	0	0	0	3.5 dB(A)	
	Subtotal	4	9	9		
	В	0	0	9		
NSA 3 Ivy Trails	С	1	1	1	3.8 dB(A)	
ivy rialio	Subtotal	1	1	10		
	Project Totals	5	10	19	3.1 dB(A)	

#### Table 4: Impact Analysis Summary

### 3.3.1 Noise Study Area 1

NSA 1 comprises the area south of Boy Scout Road and east of Binion road. As of the date of this report, the site is undeveloped. A search was conducted to determine the plans for this area and whether or not active building permits are in place. The future development is referred to as The Ridge. Mass grading plans have been submitted to the St. Johns River Water Management District (SJRMWD). However, no active building/structure permits have been issued by the City of Apopka. Because there are currently no noise sensitive sites built or permitted, this area was not analyzed for noise impacts. This NSA is illustrated in **Appendix D: Page D-1**.

#### 3.3.2 Noise Study Area 2

Across from NSA 1, north of Boy Scout Road, is NSA 2, which consists of scattered single-family residences. The residences, represented by receptors 2-1 through 2-10, are not part of a named subdivision.

Currently, the average noise level for these receptors is 55.8 dB(A), with the highest noise level being 59.8 dB(A) at receptor 2-10, which is located closest to the Binion Road / Boy Scout Road intersection. None of the sites currently meet or exceed their 66.0 dB(A) FDOT NAC, nor are they



predicted to do so under the No-Build alternative. Once the project is built, the overall traffic noise levels increase by an average of 1.3 dB(A), with the average project-related noise level predicted to be 57.1 dB(A). Receptor 2-2 has the highest build-related noise level, 63.7 dB(A), which is a 3.3 dB(A) increase over the existing condition. None of the increases over existing are considered substantial, and none of the sites are predicted to exceed the NAC. Abatement evaluation for this NSA is not required.

#### 3.3.3 Noise Study Area 3

NSA 3 comprises the area east of SR 429 from the project beginning limits (Binion Road) to the project ending limits (Lust Road). Within this NSA, two residential developments are in various stages of construction – Binion Reserve and Ivy Trails. The two developments and their associated noise sensitive sites are illustrated in **Appendix D: Page D-2**.

#### **Binion Reserve**

Binion Reserve is a new residential development located in the northeast quadrant of the proposed SR 429 / Binion Road interchange. The residences within the development are under various stages of construction, with many homes nearest to Binion Road being completely constructed or very near completion. Numerous sites immediately adjacent to SR 429 are under active construction. The majority of the sites are at a higher elevation than SR 429 with the sites located at the southern end having the greatest elevation differences. All home sites fronting SR 429, the future ramps, and the Binion Road / Boy Scout Road intersection were included in the analysis.

The homes are represented by receptors 3-1 through 3-25. The single Category C site, the neighborhood playground, is represented by receptor SLU1. The development's six-foot-tall privacy wall was included in the analysis.

Currently, the average noise level for the Binion Reserve sites is 60.7 dB(A), with the highest noise level being 70.5 dB(A) at receptor 3-16. Currently, sites 3-11 and 3-15 through 3-17 are affected by traffic noise. Under the No-Build alternative, nine sites represented by receptors 3-10 through 3-18 are predicted to meet or exceed the FDOT NAC. Once the project is built, the overall traffic noise levels increase by an average of 3.5 dB(A), with the average project-related noise level predicted to be 64.2 dB(A). Receptor 3-16 has the highest predicted build noise level (74.0 dB(A)). None of the increases over existing are considered substantial.

Because the predicted noise levels meet or exceed the 66.0 dB(A) FDOT NAC, they are considered impacted. Noise abatement was considered to mitigate these impacts, as summarized in **Section 3.2.4.1**.



#### Ivy Trails

Ivy Trails is a new residential development located north of Binion Reserve. Site development is nearing completion, with building/structure construction imminent. The home sites are represented by receptors 3-26 through 3-42. The single Category C site, the neighborhood pedestrian walking trail, is represented by receptor SLU2. All home sites fronting SR 429 were included in the analysis.

Currently, the average noise level for the Ivy Trails home sites and the trail is 61.3 dB(A). The highest noise level (66.0 dB(A)) occurs at receptor SLU2. The trail is the only site currently affected by traffic noise and is also the only site predicted to meet or exceed the FDOT NAC under the No-Build alternative. The average noise level predicted for the No-Build is 64.4 dB(A). Once the project is built, the overall traffic noise levels increase by an average of 3.8 dB(A), with the average project-related noise level predicted to be 65.0 dB(A). The highest noise level within Ivy Trails continues to be attributed to the trail (67.8 dBA), while the highest noise level for the homes sites is 66.4 dB(A) at receptors 3-30 and 3-31. None of the increases over existing are considered substantial, and none of the sites are predicted to exceed the NAC.

Because the predicted noise levels meet or exceed the 66.0 dB(A) FDOT NAC, they are considered impacted. Noise abatement was considered to mitigate these impacts, as summarized in **Section 3.2.4.1**.

#### 3.2.4.1 Noise Barrier NB1

Three scenarios were evaluated to determine potential abatement options for the 18 impacted home sites and the pedestrian trail in NSA 3. The following options were analyzed to provide noise reduction to the sites within Binion Reserve and Ivy Trails from an acoustic and cost perspective. The analyzed options are summarized in **Table 5** and illustrated in **Appendix E**.

- <u>Option 1</u> This option was evaluated as a single noise barrier.
  - This option includes a maximum height barrier (14 feet tall) located at the edge of the northbound entry ramp and mainline shoulder edge of pavement. The approximate stationing is 1571+00 to 600+00.
  - This 2,903-foot-long barrier can benefit 24 residences (16 impacted and eight non-impacted) and the trail.
  - $\circ~$  This option provides an average noise reduction of 7.0 dB(A) and a maximum reduction of 11.9 dB(A).
  - However, with an estimated cost of \$1,219,260, the Cost Per Benefited Receptor (CPBR) is \$50,803, which is over the FDOT cost-reasonableness guideline of \$42,000 per benefited receptor.



- <u>Option 2</u> This option was evaluated as a single noise barrier.
  - This option includes a maximum height barrier in the same location as Option 1 but with a reduced length. The approximate stationing is 1576+20 to 600+00.
  - This 2,385-foot-long barrier can benefit 24 residences (16 impacted and eight non-impacted) and the trail.
  - $\circ~$  This option provides an average noise reduction of 7.0 dB(A) and a maximum reduction of 11.9 dB(A).
  - The estimated cost for this option is \$1,001,700, and it has a \$41,738 CPBR, which is within FDOT cost-reasonableness guidelines.
- Option 3 This option was evaluated as a two-segment noise barrier system.
  - This option was evaluated to further reduce the length of the maximum height shoulder barrier but add in a second segment located approximately 10 feet from the CFX right-of-way (ROW) line.
    - Segment 1: 14-foot-tall tall shoulder barrier with a total length of 2,005 feet; approximate stationing is 1580+00 to 600+00.
    - Segment 2: ROW barrier with a total length of 604 feet; stepped to account for the change in topography from south to north
      - Step 1 10' tall sta. 1575+00 to 1576+00
      - Step 2 12' tall sta. 1576+00 to 1577+00
      - Step 3 14' tall sta. 1577+00 to 1579+00
      - Step 4 16' tall sta. 1579+00 to 1581+00
  - $\circ~$  This barrier system can benefit 26 residences (all 18 impacted and eight non-impacted) and the trail.
  - $\circ~$  This option provides an average noise reduction of 7.1 dB(A) and a maximum reduction of 12.1 dB(A).
  - The estimated cost for this option is \$1,089,720, with a \$41,912 CPBR, which is within FDOT cost-reasonableness guidelines.

Barrier NB1 Option 2 and Option 3 meet all FDOT acoustic and cost-reasonableness criteria and are recommended for further consideration during the final design process.

Table 5: Noise Barrier NB1	<b>Evaluation Summary</b>
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	NSA 3: Barrier NB1 Evaluation Summary															
Evaluated Barrier Options					Number of	Number of Impacted Sites Within a Noise Reduction Range			Number of Benefited Sites <sup>*1</sup>					Gentreen	Recommended	
Option	Barrier Type/Location	Height (feet) <sup>*6</sup>	Length (feet)	Approx. Station	Impacted Residential Sites	5-5.9 dB(A)	6-6.9 dB(A)	≥ 7.0 dB(A) <sup>*2</sup>	Impacted	Other *3	Total	Avg / Max Reduction dB(A)	Total Estimated Cost <sup>*4</sup>	Cost per Benefited Receptor *5	for further consideration in final design?	
Option 1	Shoulder	14	2,903	1571 to 600		4	7	5	16	8	24	7.0/11.9	\$ 1,219,260	\$ 50,803	No	
Option 2	Shoulder	14	2,385	1576+20 to 600	18		4	7	5	16	8	24	7.0/11.9	\$ 1,001,700	\$ 41,738	Yes
	Shoulder	14	2,005	1580 to 600		18			18	8	26	7.1/12.1	\$ 1,089,720			
Option 3	ROW - step 1	10	100	1575 to 1576												
two- segment system	ROW - step 2	12	101	1576 to 1577		3	3 8	7						\$ 41,912	Yes	
(stepped)	ROW -step 3	14	203	1577 to 1579												
	ROW - step 4	16	200	1579 to 1581												

\*1 = Minimum of 5.0 dB(A) required to be considered benefited by noise barrier.

\*2 = FDOT Noise Reduction Design Goal is 7.0 dB(A) at a minimum of 1 benefited receptor.

\*3 = Refers to non-impacted noise-sensitive sites.

\*4 = Based on FDOT Statewide average of \$30 per square foot.

\*5 = FDOT Reasonable Cost Guideline is \$42,000.

\*6 = 8-ft max on MSE/Bridge; 14-ft max on shoulder; 22-ft max at ROW or offset from shoulder.



### 4.0 CONCLUSION

Five sites (4 Category B and one Category C) are currently affected by traffic noise. The noise levels associated with the 2045 No-Build Alternative are predicted to meet or exceed the 66.0 dB(A) FDOT NAC at nine Category B residences and one Category C site.

Once the widening project is built, the overall traffic noise levels will increase by an average of 3.1 dB(A), with the average project-related noise level, predicted to be 63.2 dB(A). The 2050 Build Alternative's noise levels are predicted to meet or exceed the 66.0 dB(A) FDOT NAC at 18 Category B and one Category C receptor. The highest noise level is predicted to be 74.0 dB(A) in NSA 3. None of the increases are considered substantial (i.e., 15 dB(A) or more over existing levels).

As required, noise abatement consideration was given to all 19 impacted sites. Noise Barrier NB1 was evaluated to mitigate the impacts. Of the three analyzed options, Option 2 and Option 3 were found to meet all FDOT acoustic and cost criteria. Thus, the two options, summarized in **Table 6,** are recommended for further consideration in the project's final design phase.

Noise Study Area	Impacted Development	Barrier ID   Barrier Location		Estimated Barrier Cost <sup>*1</sup>	Recommended for Further Evaluation?		
		NB1 Option 2	14	2,385	Shoulder	\$1,001,700	Yes
NSA 3	Binion Reseve Ivy Trails	NB1	14	2,005	Shoulder	\$1,089,720	Vec
		Option3	10/12/14/16	604	ROW	Ş <b>1</b> ,089,720	Yes

#### Table 6: Project #429-309 Noise Barrier Recommendations

\*1 = Based on FDOT Statewide average of \$30 per square foot.

\*2 = 8-ft max on MSE/Bridge; 14-ft max on shoulder; 22-ft max at ROW or offset from shoulder.



### 4.1 Statement of Likelihood

The Central Florida Expressway Authority is committed to the construction of feasible and reasonable noise abatement measures identified in **Table 6**, contingent upon the following conditions:

- Final recommendations on the construction of abatement measures are determined during the project's final design and through the public involvement process.
- Detailed noise analyses during the final design process support the need, feasibility, and reasonableness of providing abatement.
- Cost analysis indicates that the cost of the noise barrier(s) will not exceed the cost reasonable criterion.
- Community input supporting types, heights, and locations of the noise barrier(s) is provided to CFX.
- Safety and engineering aspects as related to the roadway user and the adjacent property owner have been reviewed, and any conflicts or issues resolved.

### **5.0 CONSTRUCTION NOISE AND VIBRATION IMPACTS**

Construction of the proposed roadway improvements is not expected to have significant vibration or construction noise impacts. Applying the FDOT Standard Specifications for Road and Bridge Construction is anticipated to minimize or eliminate most of the potential short-term noise and vibration impacts.

Should any construction noise or vibration issues arise during construction, the Project Engineer, in concert with the CFX Noise Specialist and the Contractor, will investigate additional methods of controlling these impacts.

### 6.0 COMMUNITY COORDINATION

#### 6.1 Noise Impact Contours

To aid in promoting land use compatibility, a copy of this report, which provides information that can be used to protect future land development from becoming incompatible with anticipated traffic noise levels, will be made available for use by Orange County and City of Apopka officials. In addition, generalized noise impact contours for the Build Alternative have been developed, identifying the distances between the Build Alternative and the location where traffic noise levels approach the NAC for Activity Categories A, B, C, and E. The contour distances provided in **Table 7** do not account for any reduction in noise levels that may be provided by berms, privacy walls, or intervening structures. These distances also do not account for any increase in noise levels caused by a variation in the noise path, increased roadway elevation, or increased elevation of a



noise sensitive site (e.g., second-floor patio). To minimize the potential for incompatible land use, future noise sensitive land uses should be located beyond these distances.

Impact Contours										
	Corresponding	Distance to EOP <sup>*2</sup>								
Activity Category *1	Noise Abatement Criterion	SR 429	Binion Road	Boy Scout Road						
Category A	56 dB(A)	585 ft	145 ft	145 ft						
Category B and C	66 dB(A)	235 ft	45 ft	45 ft						
Category E	71 dB(A)	140 ft	10 ft	10 ft						

#### **Table 7: Critical Distance Impact Contours**

\*1 Activity Categories as defined in 23 CFR 772.

\*2 Distance to the nearest edge of pavement.

#### 6.2 Public Meetings

A public meeting will be held for this project. Any comments received during the public meeting comment period about the PD&E Study in general, as well as those pertinent to the noise analysis, will be documented under separate cover.

During the final design process, CFX will hold a Sound Wall Information Meeting (SWIM) in which the proposed noise barrier(s) and other pertinent project construction-related information will be presented to the public. To aid in the decision-making process, CFX will directly solicit the opinions of the property owners and renters found to benefit (e.g., receive a minimum 5 dB(A) reduction in noise) from the proposed noise barrier. The solicitation of viewpoints will be conducted as part of the SWIM and mailed survey. The CFX SWIM process and survey results for this project will be documented under separate cover.



## 7.0 REFERENCES

- FHWA. *Code of Federal Regulations*, Title 23 Part 772, "Procedures for Abatement of Highway Traffic Noise and Construction Noise." July 13, 2010.
- FHWA. *Highway Traffic Noise: Analysis and Abatement Guidance, FHWA-HEP-10-025.* December 2011.
- FHWA. *Recommended Best Practices for the Use of the FHWA Traffic Noise Model (TNM.* December 8, 2015.
- FDOT. A+ Plus Aerial Photo Look-Up System. 2022.
- FDOT. FDOT Design Manual
- FDOT. Project Development and Environment Manual: Part II, Chapter 18. Effective July 1, 2020.
- FDOT. Standard Specifications for Road and Bridge Construction.
- FDOT. Traffic Noise Modeling and Analysis Practitioners Handbook. December 2018.
- Google Earth, @2022 Google. Imagery and elevation data.
- Section 335.17, Florida Statutes. State Highway Construction; Means of Noise Abatement. 2012.
- USGS. National Map 2022; https://apps.nationalmap.gov/lidar-explorer/#/.



# **Appendix A:**

# Preferred Build Alternative Project Layout





# Appendix B:

# Noise Study Traffic Data

## Noise Analysis Traffic Data - SR 429 and Binion Road Interchange 2022 Existing Conditions

				Freeway Mainl									
Mainline Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	Standard K-factor	D-factor	Posted Spe (mph)
SR 429													
North of US 441 (Ponkan Mainline Plaza)	4	46,300	59,400	2,121	3,100	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
From US 441 to SR 414	6	53,300	89,000	2,449	4,650	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
South of SR 414	6	60,000	78,500	2,799	4,100	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
				SR 429 Ramp	os				R.				
SR 429 Ramp	Number of Lanes	One-Way AADT	One-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Operationa Speed (mph
US 441													
Southbound off	1	500	14,600	46	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound on	1	500	14,600	46	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Southbound on	2	4,000	29,400	369	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound off	2	4,000	29,400	369	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
SR 414													
Southbound off	2	9,650	25,800	1,008	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound on	2	9,650	25,800	1,008	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Southbound on	2	13,000	25,900	1,359	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound off	2	13,000	25,900	1,359	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
			Arter	ials and Cross	Streets								
Arterial Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Posted Spee (mph)
Binion Road													
North of Boy Scout Road	2	7,100	16,600	378	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	54.9%	40
South of Boy Scout Road	2	5,200	16,200	261	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	56.1%	40
Boy Scout Road													
East of Binion Road	2	4,700	15,700	220	740	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	52.2%	45

Number of lanes are obtained from field observations and aerial maps.
 Taffic data are obtained from the PD&E study traffic development effort.
 Peak hour demand and LOS C peak hour maximum service volumes are provided directionally.
 LOS C targets are based on the FDD7 2020 QualityLevel of Service Handbook tables, and adjusted for local conditions.
 LOS C AADTs are estimated using K and D factors and the design hour peak direction LOS C maximum service volumes.
 The vehicle classification factors are obtained from finde Taffic Online.
 Posted speed data are obtained by field observations.

## Noise Analysis Traffic Data - SR 429 and Binion Road Interchange 2045 No Build Conditions

			1.0	Freeway Mainl				16				-	
Mainline Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	Standard K-factor	D-factor	Posted Spee (mph)
SR 429													
North of US 441 (Ponkan Mainline Plaza)	4	108,200	59,400	5,610	3,100	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
From US 441 to SR 414	6	118,700	89,000	6,140	4,650	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
South of SR 414	8	115,700	118,700	5,980	6,200	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
				SR 429 Ramp	S				R.				
SR 429 Ramp	Number of Lanes	One-Way AADT	One-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Operational Speed (mph
US 441													
Southbound off	1	5,100	14,600	470	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound on	1	5,100	14,600	470	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Southbound on	2	10,350	29,400	950	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound off	2	10,350	29,400	950	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
SR 414													
Southbound off	2	24,100	25,800	2,520	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound on	2	24,100	25,800	2,520	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Southbound on	2	22,600	25,900	2,360	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound off	2	22,600	25,900	2,360	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
			Arter	ials and Cross	Streets								
Arterial Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Posted Spee (mph)
Binion Road													
North of Boy Scout Road	2	15,000	16,600	740	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	54.9%	40
South of Boy Scout Road	2	12,100	16,200	610	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	56.1%	40
Boy Scout Road													
East of Binion Road	2	10.000	15,700	470	740	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	52.2%	45
ADT: Annual Average Daily Traffic MT: Medium Truck		HT: Heavy Tr											

Number of lanes are obtained from field observations, aerial maps and planned projects information.
 Traffic data are obtained from the PD&E study traffic development effort.
 Peak hour demand and LOS C peak hour maximum service volumes are provided directionally.
 LOS C targets are based on the FDOT 2020 Quality/Level of Service Handbook tables, and adjusted for local conditions.
 LOS C AADTs are estimated using K and D factors and the design hour peak direction LOS C maximum service volumes.
 The vehicle classification factors are obtained from Finde Taffic Online.
 Posted speed data are obtained by field observations.

Noise Analysis Traffic Data - SR 429 and Binion Road Interch	ange
2045 Build Conditions	

				Freeway Mainl									
Mainline Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	Standard K-factor	D-factor	Posted Spee (mph)
SR 429													
North of US 441 (Ponkan Mainline Plaza)	4	108,400	59,400	5,630	3,100	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
From US 441 to Binion Road	6	120,900	89,000	6,240	4,650	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
From Binion Road to SR 414	8	116,300	118,700	6,030	6,200	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
South of SR 414	8	113,800	118,700	5,900	6,200	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	70
				SR 429 Ramp									
SR 429 Ramp	Number of Lanes	One-Way AADT	One-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Operational Speed (mph)
US 441													
Southbound off	1	4,100	14,600	380	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound on	1	4,100	14,600	380	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Southbound on	2	10,350	29,400	950	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Northbound off	2	10,350	29,400	950	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	8.7%	52.8%	45
Binion Road								~					
Southbound off	1	2,300	13,400	230	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	53.0%	45
Northbound on	1	2,300	13,400	230	1,350	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	53.0%	45
SR 414													
Southbound off	2	23,850	25,800	2,490	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound on	2	23,850	25,800	2,490	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Southbound on	2	22,600	25,900	2,360	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
Northbound off	2	22,600	25,900	2,360	2,700	2.00%	0.41%	1.55%	0.04%	0.01%	9.5%	55.0%	45
			Arter	ials and Cross									
Arterial Segment	Number of Lanes	Two-Way AADT	Two-Way LOS C AADT	Peak Hour Peak Direction	LOS C Peak Hour Peak Direction	Design Hr. % T	Design Hr. % MT	Design Hr. % HT	Design Hr. % Buses	Design Hr. % Motorcycles	K-factor	D-factor	Posted Speed (mph)
Binion Road													
North of Boy Scout Road	2	13,800	16,600	680	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	54.9%	40
South of Boy Scout Road	2	12,300	16,200	620	820	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	56.1%	40
Boy Scout Road													
East of Binion Road		10.600	15,700	500	740	4.00%	2.40%	1.47%	0.13%	0.21%	9.0%	52.2%	45

Number of lanes are obtained from field observations, aerial maps and planned projects information.
 Traffic data are obtained from the PD&E study traffic development effort.
 Peak hour demand and LOS C peak hour maximum service volumes are provided directionally.
 LOS C targets are based on the FDDT 2020 Quality/Level of Service Handbook tables, and adjusted for local conditions.
 LOS C AADTs are estimated using K and D factors and the design hour peak direction LOS C maximum service volumes.
 The vehicle classification factors are obtained from Finde Taffic Online.
 Posted speed data are obtained by field observations.



# Appendix C:

## **Noise Impact Comparison Matrix**



		Noise	Impact Co	mparison M	atrix		
Noise	e Sensitive Sites				d Noise Levels bise Level abov	• • • •	
Receptor ID	ceptor ID # Sites Impact Represented Criterion (dB(A))		2022 Existing	2045 No-Build Alternative	2045 Build Alternative	Build Change From Existing	Consider Abatement
NSA 1: South of	Boy Scout Road	d from Binio	n Road to pro	oject end - Illus	strated on Page	e D-1 - Appe	endix D
No noise sensiti							
	Boy Scout Road	d from Binio	n Road to pro	oject end - Illus	strated on Page	e D-1 - Appe	endix D
	e-family homes					[	
2-1	1	66.0	56.7	60.0	60.6	3.9	-
2-2	1	66.0	60.4	63.7	63.7	3.3	-
2-3	1	66.0	51.7	55.0	55.8	4.1	-
2-4	1	66.0	51.5	54.8	53.5	2.0	-
2-5	1	66.0	54.2	57.6	57.2	3.0	-
2-6	1	66.0	51.5	54.7	53.7	2.2	-
2-7	1	66.0	57.8	61.2	57.5	-0.3	-
2-8	1	66.0	57.9	61.3	56.0	-1.9	-
2-9	1	66.0	56.2	59.5	55.2	-1.0	-
2-10	1	66.0	59.8	63.1	57.5	-2.3	-
NSA Summary	10		55.8	59.1	57.1	1.3	0
	oad Interchang	e to Lust Ro	ad (east of S	R 429) - Illustrat	ted on Page D-	2 - Append	ix D
Binion Reserve							
3-1	1	66.0	60.0	63.0	62.4	2.4	-
3-2	1	66.0	58.1	61.1	60.3	2.2	_
3-3	1	66.0	55.8	58.8	58.0	2.2	_
3-4	1	66.0	53.6	56.7	55.9	2.3	-
3-5	1	66.0	54.4	57.7	57.2	2.8	-
3-6	1	66.0	57.7	60.9	61.1	3.4	-
3-7	1	66.0	59.2	62.4	62.6	3.4	-
3-8	1	66.0	60.3	63.5	63.9	3.6	-
3-9	1	66.0	62.0	65.2	65.7	3.7	-
3-10	1	66.0	62.9	66.1	66.7	3.8	Yes
3-11	1	66.0	66.3	69.4	70.0	3.7	Yes
3-12	1	66.0	64.8	67.9	68.6	3.8	Yes
3-13	1	66.0	64.5	67.5	68.0	3.5	Yes
3-14	1	66.0	64.1	67.1	67.5	3.4	Yes
3-15	1	66.0	68.8	71.8	72.3	3.5	Yes
3-16	1	66.0	70.5	73.5	74.0	3.5	Yes



	Noise Impact Comparison Matrix Predicted Noise Levels (dB(A))												
Nois	e Sensitive Sites			Predicted Noise Levels (dB(A)) Red = Noise Level above NAC									
Receptor ID	# Sites Represented	NAC Impact Criterion (dB(A))	2022 Existing	2045 No-Build Alternative	2045 Build Alternative	Build Change From Existing	Consider Abatement						
3-17	1	66.0	67.3	70.3	71.4	4.1	Yes						
3-18	1	66.0	63.5	66.7	68.4	4.9	Yes						
3-19	1	66.0	60.0	63.1	64.3	4.3	-						
3-20	1	66.0	60.4	63.5	64.5	4.1	-						
3-21	1	66.0	59.1	62.2	62.9	3.8	-						
3-22	1	66.0	57.9	61.0	61.7	3.8	-						
3-23	1	66.0	57.9	61.1	61.9	4.0	-						
3-24	1	66.0	55.9	59.1	59.8	3.9	-						
3-25	1	66.0	55.8	59.0	59.7	3.9	-						
SLU1	1	66.0	56.1	59.3	60.0	3.9	-						
Ivy Trails	•												
3-26	1	66.0	62.1	65.1	66.0	3.9	Yes						
3-27	1	66.0	62.1	65.1	66.0	3.9	Yes						
3-28	1	66.0	62.2	65.3	66.0	3.8	Yes						
3-29	1	66.0	62.4	65.5	66.2	3.8	Yes						
3-30	1	66.0	62.5	65.6	66.4	3.9	Yes						
3-31	1	66.0	62.4	65.5	66.4	4.0	Yes						
3-32	1	66.0	62.2	65.3	66.3	4.1	Yes						
3-33	1	66.0	61.9	65.0	66.3	4.4	Yes						
3-34	1	66.0	62.0	65.1	66.2	4.2	Yes						
3-35	1	66.0	61.7	64.9	65.3	3.6	-						
3-36	1	66.0	60.5	63.7	64.4	3.9	-						
3-37	1	66.0	58.8	62.0	62.7	3.9	-						
3-38	1	66.0	58.7	62.0	62.4	3.7	-						
3-39	1	66.0	59.0	62.3	62.8	3.8	-						
3-40	1	66.0	59.7	62.9	63.3	3.6	-						
3-41	1	66.0	59.3	62.6	63.2	3.9	-						
3-42	1	66.0	59.1	62.4	63.1	4.0	-						
Ivy Trails - Pede	estrian Trail												
SLU2	1	66.0	66.0	69.0	67.8	1.8	Yes						
NSA Summary	43		60.9	64.0	64.5	3.6	19						



# Appendix D:

# **Project Aerials**







SR 429 / Binion Road Interchange PD&E



# Appendix E:

## **Noise Barrier Maps**





SR 538 Poinciana Pkwy Extension CFX#538-234; 538-235



