CENTRAL FLORIDA EXPRESSWAY AUTHORITY

Final Location Hydraulics Report July 2018

SR 408 Eastern Extension PD&E Study



PROFESSIONAL ENGINEER CERTIFICATE

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with Metric Engineering, Inc. and I have reviewed or approved the evaluation, findings, opinions and conclusions as reported for:

PROJECT:

SR-408 Eastern Extension PD&E Study

FINANCIAL PROJECT NUMBER:

Orange County

CFX-Project No. 408-254

CLIENT:

LOCATION:

Central Florida Expressway Authority

This Location Hydraulics Report (LHR) provides the results of a summary of data collection efforts, and limited calculation for the proposed cross drains and floodplain evaluations prepared for the conceptual analyses for the Project Development and Environment Study for SR-408 Eastern Extension project. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of hydrologic analysis and hydraulic engineering as applied through professional judgment and experience. This document is for planning purposes only and is not to replace any effort required for the final design.

Florida Registered Engineer:

Name: Chandra S Raman, P.E.

Registration Number: FL # 58740

Signature: Chanderlemon Date: 7/24/18







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ACRONYMS

- PD&E Project Development and Environment
- LHR Location Hydraulics Report
- BHR Bridge Hydraulics Report
- PSR Pond Siting Report
- CFX Central Florida Expressway Authority
- SJRWMD St. Johns River Water Management District
- IDF Intensity-Duration-Frequency
- **BMP Best Management Practices**
- MSSW Management and Storage of Surface Waters
- FIRM Flood Insurance Rate Map
- FPL Florida Power & Light Company
- SR State Road



EXECUTIVE SUMMARY

The purpose of the SR-408 Eastern Extension Project Development and Environment (PD&E) study is to develop a proposed improvement strategy that is technically sound, environmentally sensitive and publicly acceptable. As with every PD&E Study, emphasis has been placed on the development, evaluation and documentation of detailed engineering and environmental studies including data collection, conceptual design, environmental analyses, project documentation and the preparation of a Location Hydraulics Report (LHR). The project is located in Orange County, Florida.

The Central Florida Expressway Authority (CFX) is presently evaluating the potential to expand SR-408 from its current eastern terminus at SR-50, locally known as East Colonial Drive, to SR-520 in northeast Orange County. This new seven-mile eastern extension of SR-408 would constitute the first stage towards providing a west-east high-speed corridor with future connectivity to I-95; enhancing safety, capacity and mobility for the region and CFX's customers. After a comprehensive evaluation process of various typical sections, horizontal alignment combinations, and public involvement efforts, a recommended alignment was selected.

The proposed SR-408 Eastern Extension project is divided into three segments based on the land use characteristics. Segment 1 is more urban in nature and exhibits a higher traffic demand than Segments 2 and 3. Segment 1 is from the beginning of the SR-50/SR-408 interchange to Avalon Park Boulevard. Segments 2 and 3, beginning east of Avalon Park Boulevard to SR-520 at the east end of the study area, exhibit more of a rural tendency.

The purpose of this LHR is to identify and discuss the proposed cross drains throughout the project corridor. There are fourteen new cross drains identified for this project. The cross drains were sized appropriately using HY-8 program to minimize the impacts to flood elevations and limits of the floodplain. The cross drain analysis indicates the proposed structures will be able maintain hydraulic connectivity within the tributaries, wetlands or floodplains that the project crosses without significant increase in the existing flood elevation. Thus, the project will not affect existing flood heights or floodplain limits. This project will not cause significant change in the potential for interruption or termination of emergency service or emergency evacuation routes in the surrounding areas. Therefore, it has been determined that the encroachment due to the proposed roadway is not significant.

1.0 INTRODUCTION

The vision of this enhanced west-east corridor has been documented in prior concept studies prepared by CFX, including the SR-408 Eastern Extension Concept Development and Evaluation Study completed in 2008. The limits of this study generally extend from the current terminus of SR-408 at SR-50 to the vicinity of the SR-50/SR-520 intersection. The project location and vicinity are shown in **Appendix-A**. The proposed Typical Sections



for Segment 1 and Segment 2/3 are provided in **Appendix-D**. The SR-408 Eastern Extension is one piece of Florida's Strategic transportation investments to support future growth and create connections between global trade activities, from the Orlando International Airport and the University of Central Florida to Cape Canaveral.

SR-50 is located within the project vicinity and is classified as a major arterial facility. SR-50 provides an important connectivity function between the east Orlando area to the west, and I-95 just south of Titusville to the east. As traffic continues to grow within the study area due to the projected development, it is essential to maintain adequate mobility for the region. A new expressway facility will not only improve mobility but significantly reduce the existing exposure to at-grade conflict points associated with traffic signals and local access issues. In summary, the proposed SR-408 Eastern Extension will greatly enhance Central Florida's regional expressway needs and provide the initial phase of the ultimate vision of an expressway connection from Orlando to I-95.

This report discusses and analyzes proposed cross drains throughout the project corridor. The proposed corridor impacts wetlands and floodplains, therefore the placement of cross drains is crucial to maintain the natural flow. A description of each proposed cross drain is located in Section 4.1 of this report. Exhibits showing proposed cross drains within wetlands and floodplains are in **Appendix-E**. Based on an assumed profile, the proposed culverts are shown along the existing ground based on a 1' contour tin file (**Appendix-F**).

2.0 CROSS DRAIN ANALYSIS METHODOLOGY AND DESIGN CRITERIA

The proposed project alignment is a new corridor. There are no existing cross drains along the proposed project corridor; therefore, the project will consist of all new cross drains. Cross drains were located strategically along the proposed SR-408 Eastern Extension corridor to maintain flow connectivity within the impacted wetlands, floodplains, and Econ River tributaries. There are a total of fourteen cross drains proposed along this new corridor. The flow rates for cross drains 1 through 4 were obtained from the Big Econ River Basin Stormwater Management Master Plan (**Appendix-I**). In accordance with the FDOT Drainage Design Guide for designing culverts, the Rational Method was used to conduct hydrologic analysis for cross drains 5 through 9. The Rational Method was used because the delineated drainage areas for each cross drain were less than 600 acres. Drainage areas were delineated by using a one foot Lidar contour map (St. Johns River Water Management District), existing drainage maps from SR-50 projects, and drainage maps from land development projects along the project corridor. The flow rates for cross drains 10 through 13 were obtained from the Bithlo Area Stormwater Management Master Plan (**Appendix-J**).



2.1 Contributing Flow Determination

Rational Method

- The Rational Method procedures require calculating a peak basin flow rate from the basin characteristics.
- The composite runoff coefficient was calculated based on the percentage of land use for residential, commercial, flat lawns, and woods/wetland areas per the FDOT Hydrology Handbook.
- Time of concentration was calculated using the TR-55 Method.
- The intensity for each storm event was calculated from the FDOT Intensity-Duration-Frequency (IDF) curve for Zone 7.
- The composite coefficient is only designed for a storm period of 10 years. Storm frequency factors were used to adjust the composite runoff coefficient for 25, 50, and 100 year storm events (**Appendix-H**, **Table B-5**).
- Frequency Factor for Return Period 500 year runoff coefficient is not provided in the FDOT Hydrology Handbook; therefore, a log-log graph was created in order to interpolate the peak discharge.
- The Rational Method should only be used for areas up to 600 acres.

2.2 Floodplains/Floodways Criteria

- The proposed project may not cause a net reduction in flood storage within the 10-year floodplain.
- Structures shall cause no more than a one-tenth (0.1) of a flood increase in the 100-year flood elevation 500-feet upstream.
- Proposed construction shall not cause a reduction in flood conveyance capabilities.
- Best Management Practices (BMP's) shall be employed to minimize velocity to avoid undue erosion.
- The design of encroachments shall be consistent with standards established by FEMA.

2.3 Culvert Design Criteria

The following criteria was drawn from the 2018 FDOT Drainage Manual. The following table provides the required storm events to be analyzed for each cross drain per the FDOT Drainage Manual and the FDOT Drainage Design Guide.

Storm Event Frequency	Definitions
50-Year	Design Flood Event
100-Year	Base Flood Event
500-Year	Greatest Flood Event

Table-1 Storm Frequency Criteria

- All cross drains, if applicable, shall be designed to have sufficient hydraulic capacity to convey the 50-year (Design Frequency) storm event. In accordance with the FDOT Drainage Manual, mainline interstate culverts should be designed for a frequency of 50 years (**Appendix-H**). All culverts shall be analyzed for the base flood (100 year).
- Backwater shall not significantly change land use values unless flood rights are purchased.
- The headwater for design frequency conditions shall be kept at or below the travel lanes.
- The highest tailwater elevation, which can reasonably be expected to occur coincident with the design storm event, shall be used (typically, crown of pipe is used at the outlet).
- The minimum culvert size is 18" or its equivalent size.
- The design of all cross culverts shall comply with the guidelines set forth in the FDOT Drainage Manual, Chapter 4.
- The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.

The criteria listed above was collected from the following applicable sources:

- FDOT Drainage Design Guide Culvert Design (January 2018)
- FDOT Drainage Manual (January 2018)
- FHWA Code of Federal Regulation 23 CFR 650A
- SJRWMD Management and Storage of Surface Waters (MSSW) Permit Information Manual (October 2013)

2.4 Culvert Sizing

All cross drains were sized for a 100-year storm event even though the FDOT design criteria specifies a 50-year Design Frequency. The Big Econ River Basin Stormwater Management Master Plan and Bithlo Area Stormwater Management Master Plan only provided flows and stages for 5-year, 10-year, 25-year, and 100-year. The 50-year and 500-year flows were interpolated by a log-log graph. Since stages were not provided for the 50-year storm event, the 100-year flows and stages were used instead. The calculated 100-year backwater stage elevation from the HY-8 analysis was compared with the existing 100-year flood stage. Culvert trial sizes were determined by using the Manning's Equation. The trial sizes were used to perform HY-8 analysis. While performing the overtopping analysis, the cross drains were appropriately sized to conform with the floodplain criteria in Section 2.2 of this report.



Manning's Equation

- The pipe length was measured from R/W to R/W for each cross drain.
- The change in flow line elevation from upstream to downstream was assumed to be 0.50 ft.
- Manning's "n" value of 0.012 was used.
- The 100-year flow rate for each cross drain was used.

HY-8

- The trial culvert size from the Manning's equation was used for the HY-8 analysis.
- The culvert size was adjusted to maintain backwater stage elevations below the 100-year stage elevation.
- The 10-year flow was the minimum flow, 50-year flow was the design flow, and 100-year flow was the maximum flow.
- The crown of the pipe/top of box culvert or existing SR-50 cross drain DHW elevations were used as the constant tailwater elevations.

3.0 EXISTING CONDITIONS

3.1 Soil Data

The NRCS Soil Survey of Orange County published by United States Department of Agriculture (USDA) has been reviewed for the project. The soil survey map and soil types found throughout the proposed corridor are shown in the complete NRCS USDA Soil Survey located in **Appendix-C**. In general, the superficial soils consist of fine sands, muck and poorly drained soil. The groundwater is at a depth of 0'-3.5' below the existing ground. Refer to **Table-2** below for the most occurring soils within the project area.

Soil No.	Orange County USDA Soil Name	Depth to Water Table	Hydrologic Soil Group
3	Basinger Fine Sand	0	A/D
15	Felda Fine Sand	0 to 6	A/D
20	Immokalee Fine Sand	6 to 12	B/D
34	Pomello Fine Sand	24 to 42	A
37	St. Johns Fine Sand	6 to 12	B/D
42	Sanibel Muck	0	A/D
44	Smyrna-Smyrna, Wet, Fine Sand	6 to 18	A/D
51	Wabasso Fine Sand	6 to 18	B/D
53	Wauberg Fine Sand	0 to 6	D
54	Zolfo Fine Sand	24 to 42	A

Table-2 USDA NRCS Soil Survey Information



3.2 Land Use

The existing land use along the proposed SR-408 Eastern Extension corridor consists mostly of residential developments, commercial properties, and undeveloped areas. The residential areas consist of both multi-family and single-family residences. There are a few commercial properties along the proposed corridor as well. The undeveloped areas are mostly wetlands and upland forests with conservation easements. Please refer to **Appendix-A** for a Land Use map.

3.3 Existing Cross Drains

Considering this is a new alignment, there are not any existing cross drains or bridge structures for review. However, existing cross drains upstream and downstream of the proposed alignment were taken into consideration to maintain functionality and to verify the recommended improvements do not adversely impact the overall drainage function. Refer to **Table-3** for existing SR-50 cross drain information. The SR-50 Straight Line Diagram is in **Appendix-N** and identifies each SR-50 cross drain. The culvert size and 50-Year DHW elevations were obtained from the construction plans in **Appendix-P**, **Appendix-Q**, and **Appendix-R**. There is no evidence of scour or sedimentation of any existing cross drains along SR-50. Refer to **Appendix-S** for photos of the existing SR-50 cross drains.

Cross Drain ID	Pipe Description	50-Year DHW EL (ft)	Date of Construction
SR-50 CD-1	2-8'x6' CBC	58.57	2012
SR-50 CD-2	2-24" RCP	53.53	2012
SR-50 CD-3	2-12.95'x8.5' CBC	50.04	2012
SR-50 CD-4	1-30" RCP	54.68	2012
SR-50 CD-5	3-10'x6' CBC	43.70	1960
SR-50 CD-6	3-36" RCP	59.10	1960
SR-50 CD-7	1-4'x4' CBC & 1- 54" RCP Jointed	59.10	1960
SR-50 CD-8	1-30" RCP	66.50	1960
SR-50 CD-9	1-8'x7' CBC	54.80	1960
SR-50 CD-10	1-10'x4' CBC	60.80	1960
SR-50 CD-11	1-24" RCP	61.60	1960

Table-3 Existing SR-50 Cross Drain General Information



4.0 **PROPOSED CONDITIONS**

The project corridor will cross through residential homes, commercial businesses, wetlands, wooded areas, and Econ River tributaries. Most tributaries west of the Econ River which cross the proposed SR-408 Eastern Extension corridor flow north and eventually into the Econ River. There is one slough, where UCF is located north of SR-50, which flows south into one of the Econ River tributaries and ultimately flows north to the Econ River. All tributaries east of the Econ River, which cross the proposed SR-408 Eastern Extension corridor, flow south and ultimately flow into the Econ River. Refer to the Drainage Basin Map located on **Page-17**.

4.1 **Proposed Cross Drains**

The roadway geometry is limited in order to minimize impacts and meet the requirements for the proposed design speed. Different interchange layouts and considerations were made to provide alternative conceptual designs. Fourteen cross drain locations were selected once the alignment and the most effective interchange layouts were identified. The proposed cross drain locations were also chosen based on the natural flow of the land from the surrounding floodplains and wetlands. The proposed SR-408 Eastern Extension corridor will have floodplain impacts along most of the corridor. These floodplain impacts will be mitigated by routing this volume to the project's proposed storm water management facilities, and roadside swales. Refer to **Table-4** for calculated culvert size, flow direction, and floodplain status. Refer to **Table-5** for flood data and **Table-6** for 100-year flows, 100-year stage elevations, tailwater elevations, and backwater stage elevations. Refer to **Appendix-G** for proposed cross drain calculations and HY-8 analyses.



Cross Drain ID	Pipe Description	Flow Direction	Receiving Water Body	Within Floodplain (Yes/No)
			Unnamed	
CD-1	3-11'x5' CBC	North	Tributary(1)	Yes (Zone A)
			Unnamed	
CD-2	4-10'x5' CBC	South	Tributary(1)	Yes (Zone A)
			Unnamed	
CD-3	3-11'x7' CBC	North	Tributary(1)	Yes (Zone A)
			Unnamed	
CD-3A	1-30" RCP	South	Tributary(2)	Yes (Zone A)
			Unnamed	
CD-4	2-8'x4' CBC	North	Tributary(2)	Yes (Zone A)
CD-5	2-72" RCP	North	Floodplain	Yes (Zone A)
CD-6	2-72" RCP	North	Floodplain	Yes (Zone A)
CD-7	2-48" RCP	South	Wetland	Yes (Zone X)
CD-8	1-10'x5' CBC	South	Wetland	Yes (Zone X)
CD-9	1-72" RCP	South	Floodplain	Yes (Zone AE)
CD-10	2-6'x4' CBC	South	Channel E	Yes (Zone AE)
CD-11	2-24" RCP	South	Channel K	Yes (Zone A)
CD-12	2-8'x4' CBC	South	Channel KE	Yes (Zone A)
CD-13	1-48" RCP	South	Channel M	Yes (Zone X)

Table-4 Proposed SR-408 Cross Drain General Information



Structure	Proposed Size		Design Flood 50-Yr Storm Event		Base Flood 100-Yr Storm Event		Overtopping Flood			Overtopping
Number	Size	Length (ft)	Discharge (cfs)	Stage (ft)	Discharge (cfs)	Stage (ft)	Discharge (cfs)	Stage (ft)	Storm Frequency	EL (II)
CD-1	3-11'x5' CBC	485	1160.00	51.97	1322.00	52.45	4902.10	88.87	>500 Yr	88.87
CD-2	4-10'x5' CBC	302	1499.00	51.91	1690.00	52.41	5709.63	85.27	>500 Yr	85.27
CD-3	3-11'x7' CBC	400	1770.00	52.05	2000.00	52.51	6240.70	80.88	>500 Yr	80.88
CD-3A	1-30" RCP	303	5.76	57.88	7.69	57.95	84.31	75.41	>500 Yr	75.41
CD-4	2-8'x4' CBC	456	427.00	52.03	496.00	52.95	1727.16	82.31	>500 Yr	82.31
CD-5	2-72" RCP	374	226.00	51.51	312.00	52.46	1603.28	84.25	>500 Yr	84.25
CD-6	2-72" RCP	427	190.00	52.10	259.00	52.91	1588.91	84.64	>500 Yr	84.64
CD-7	2-48" RCP	129	165.00	61.86	231.00	63.17	384.40	68.47	<500 Yr	68.47
CD-8	1-10'x5' CBC	447	223.00	54.27	309.00	54.96	1356.63	84.68	>500 Yr	84.68
CD-9	1-72" RCP	300	153.00	43.51	212.00	44.45	532.70	54.79	>500 Yr	54.79
CD-10	2-6'x4' CBC	310	353.00	44.11	398.00	44.69	896.98	55.97	>500 Yr	55.97
CD-11	2-24" RCP	395	21.00	58.98	24.00	59.28	107.98	83.94	>500 Yr	83.94
CD-12	2-8'x4' CBC	522	373.00	54.57	409.00	54.89	1405.58	75.36	>500 Yr	75.36
CD-13	1-48" RCP	325	42.00	56.50	51.00	56.73	173.94	64.50	>500 Yr	64.50

Table-5 Flood Data Summary Table

** The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.



Cross Drain	HY-8 Cross Drain Size	100-Year Flow (cfs)	Existing Ground EL (ft)	Tailwater EL (fft)	Existing 100- Year EL (ft)*	Backwater Stage Based on HY-8
			(11)		(11)	(11)
CD-1	3-11'x5' CBC	1322	51.00	50.04	52.70 ¹	52.45
CD-2	4-10'x5' CBC	1690	49.38	50.04	52.70 ¹	52.41
CD-3	3-11'x7' CBC	2000	45.00	50.04	52.70 ¹	52.51
CD-3A	1-30" RCP	7.69	57.71	57.80	58.00	57.95
CD-4	2-8'x4' CBC	496	49.00	50.40	53.70 ¹	52.95
CD-5	2-72" RCP	312	49.00	49.73	53.04 ³	52.46
CD-6	2-72" RCP	259	51.00	49.73	53.04 ³	52.91
CD-7	2-48" RCP	231	57.40	60.50	63.56	63.17
CD-8	1-10'x5' CBC	309	48.51	53.51	55.03	54.96
CD-9	1-72" RCP	212	37.50	42.50	45.00	44.45
CD-10	2-6'x4' CBC	398	38.00	42.00	45.40 ²	44.69
CD-11	2-24" RCP	24	58.00	58.00	59.50 ²	59.28
CD-12	2-8'x4' CBC	409	51.00	53.00	55.50 ²	54.89
CD-13	1-48" RCP	51	55.00	56.00	57.10 ²	56.73

Table-6 Summary of Proposed SR-408 Cross Drains (HY-8 Analysis)

* The existing 100-year elevations from the sources listed below were converted from NGVD to NAVD by subtracting 1.1 ft.

¹ Big Econ Stormwater Management Master Plan (Appendix-I)

² Bithlo Area Stormwater Management Master Plan (Appendix-J)

³ Waterford Trails Construction Plans from Harling Locklin & Associates, Inc. (Appendix-L)

** The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.



The proposed alignment will impact wetlands; therefore, CD-1 was strategically placed to maintain the flow connectivity between wetlands and the Econ River tributary that flows south through proposed CD-2 and then north through proposed CD-3. The culvert will convey runoff from one side of the road to the other while replicating the natural flow of the tributary. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 1322 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL015X, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.45 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 3-11'x5' concrete box culverts.

CD-2

CD-2 was proposed in order to maintain flow connectivity of the existing slough, which drains from the north to the south into a tributary. The tributary flows north through proposed CD-3 and drains into the Econ River. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 1690 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL020C, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.41 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 4-10'x5' concrete box culverts.

CD-3

CD-3 maintains flow connectivity to a tributary, which flows north into the Econ River. The 50-Year DHW elevation of 50.04 ft from SR-50 CD-3 (**Table-3**) was used as the tailwater for this cross drain. The 100-year elevation of 52.70 ft and 100-year flow of 2000 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEWL030C, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.51 ft from HY-8 analysis is less than the existing 100-year flood elevation of 52.70 ft. The proposed culvert sizes from the HY-8 analysis are 3-11'x7' concrete box culverts.

CD-3A

The basin area is approximately 2.35 acres. A time of concentration of 10 minutes was assumed. The crown of the pipe was used as the tailwater. The DHW elevation of 58.00 ft was obtained from SJRWMD Permit 100527 (**Appendix-X**). The calculated backwater stage elevation of 57.95 ft from HY-8 analysis is less than the existing 100-year flood elevation of 58.00 ft; therefore. The 100-year flow of 7.69 cfs was calculated using the Rational Method. The proposed culvert size from the HY-8 analysis are 1-30" RCP. The culvert will convey runoff from the wetlands that are severed by the proposed corridor, which flows southeast to the tributary that flows north and drains into the Econ River.



The culverts will maintain flow connectivity to a tributary, which flows north into the Econ River. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.70 ft and the 100-year flow of 496 cfs from the Big Econ River Basin Stormwater Management Master Plan (Model ID: BEBE195X, **Appendix-I**) were used to size this cross drain. The calculated backwater stage elevation of 52.95 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.70 ft. The proposed culvert sizes from the HY-8 analysis are 2-8'x4' concrete box culverts.

CD-5

The basin area is approximately 109.03 acres. A time of concentration of 1.39 hours was calculated for this basin area using the TR-55 method. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.04 ft was obtained from SJRWMD Permit 70394-1 (**Appendix-L**). The calculated backwater stage elevation of 52.46 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.04 ft. The 100-year flow of 312 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-72" pipes. The culvert will convey runoff from the wetlands to the tributary which flows north and drains into the Econ River. There is forty-six feet of space from the edge of the proposed ramp to the right-of-way line; therefore, a by-pass swale can be constructed in order to provide flow connectivity from CD-5 to CD-6 (**Appendix-E**, **Page-E3**). In addition to the one foot contour map, two drainage maps (**Appendix-O** and **Appendix-R**) were used to determine the basin area.

CD-6

CD-6 will maintain flow connectivity between the wetlands that will be severed by the proposed SR-408 Eastern Extension alignment. The runoff from the wetlands flows north and drains into the Econ River. The basin area is approximately 119.01 acres. The time of concentration was calculated for this basin area using the TR-55 method. The total time of concentration for this basin area is 1.44 hours. The elevation from the top of the box culvert was used as the tailwater. The 100-year elevation of 53.04 ft was obtained from SJRWMD Permit 70394-1 (**Appendix-L**). The calculated backwater stage elevation of 52.91 ft from HY-8 analysis is less than the existing 100-year flood elevation of 53.04 ft. The 100-Year flow of 259 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-72" pipes. There is forty-six feet of space from the edge of the proposed ramp to the right-of-way line; therefore, a by-pass swale can be constructed in order to provide flow connectivity from CD-5 to CD-6 (**Appendix-E**, **Page-E3**). In addition to the one foot contour map, a regional drainage map (**Appendix-O**) was used to determine to the basin area.



CD-7 will provide flow connectivity between wetlands that will be severed by the proposed CR 419 (Chuluota Road) corridor. The runoff flows south through proposed CD-8 and drains into the Econ River. The basin area is approximately 77.95 acres. A time of concentration of 1.54 hours was calculated for this basin area using the TR-55 method. The crown of pipe was used as the tailwater. The 100-year elevation of 63.56 ft was obtained from SJRWMD Permit #27625-4 (**Appendix-M**). The calculated backwater stage elevation of 63.17 ft from HY-8 analysis is less than the existing 100-year flood elevation of 63.56 ft. The 100-year flow of 231 cfs was calculated using the Rational Method. The proposed culvert sizes from the HY-8 analysis are 2-48" RCP. A one foot contour map was used to delineate the basin area for this cross drain. This basin area consists of single-family residential homes, several commercial businesses located on SR-50, several ponds, and woodland areas.

CD-8

The culvert will convey runoff from the severed wetlands to the tributary which flows south and drains into the Econ River. The total basin area for CD-8 is 121.44 acres and consists of two basin areas, which includes the basin area for CD-7. The time of concentration was calculated for this basin area using the TR-55 method. The total time of concentration calculated for this basin area is 1.68 hours. The elevation from the top of the box culvert used as the tailwater. The 100-year elevation of 55.03 ft was averaged from two 100-year elevations of 63.56 ft from existing Pond 200 and 46.50 ft from existing Pond 100 (SJRWMD Permit #27625-4, **Appendix-M**). CD-8 is located between existing Pond 200 and existing Pond 100. The calculated backwater stage elevation of 54.96 ft from HY-8 analysis is less than the existing 100-year flood elevation of 55.03 ft. The 100-year flow of 309 cfs was calculated using the Rational Method. The proposed culvert size from the HY-8 analysis is a single 10'x5' concrete box culvert. A one foot contour map was used to delineate the basin area for this cross drain. This basin area consists of single-family residential homes, several commercial businesses located on SR-50, several ponds, and woodland areas.

CD-9

The basin area is approximately 75.82 acres. A time of concentration of 1.66 hours was calculated for this basin area using the TR-55 method. The calculated flow rate for a 100-year storm event is 212 cfs. The 100-year flood elevation of 45.00 ft was obtained from the FEMA Flood Map (**Appendix-B**). The top of the box culvert was used as the tailwater for this culvert. The calculated backwater stage elevation of 44.45 ft from HY-8 analysis is less than the existing 100-year flood elevation of 45.00 ft. The proposed culvert size from the HY-8 analysis is a single 72" RCP. The culvert will convey runoff from the wetlands to the tributary which flows south and drains into the Econ River. A one foot contour map was used to delineate the basin area for this cross drain.



CD-10 will maintain flow connectivity from Channel E that flows south into the Econ River. The proposed alignment interrupts the natural flow of Channel E; therefore, culverts will be strategically placed where the proposed corridor and the channel intersect. The elevation from the top of the box culvert was used as the tailwater. The 100-year stage elevation of 45.40 ft and 100-Year flow of 398 cfs for Channel E (Node ID: NE-020, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 44.69 ft from HY-8 analysis is less than the existing 100-year flood elevation of 45.40 ft. The proposed culvert sizes from the HY-8 analysis are 2-6'x4' concrete box culverts.

CD-11

CD-11 will provide flow connectivity between a wetland and Channel K that will be severed by the proposed SR-408 Eastern Extension corridor. The proposed cross drain location is on an existing wetland that is east of CR13. The crown of pipe was used as the tailwater. The proposed location of CD-11 lies directly on a Wetland East of CR13 (Node ID: NK-130, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan. The wetland has a 100-year stage elevation of 59.50 ft and a 100-year flow of 24 cfs, which were used to size this cross drain. The calculated backwater stage elevation of 59.28 ft from HY-8 analysis is less than the existing 100-year flood elevation of 59.50 ft. The proposed culvert sizes from the HY-8 analysis are 2-24" pipes.

CD-12

The new alignment interrupts the natural flow of Channel KE. To maintain the natural flow connectivity of Channel KE, concrete box culverts will be strategically placed where the proposed roadway and channel intersect. The culverts will convey runoff from one side of the road to the other as it flows south towards the Econ River. The elevation from the top of the box culvert was used as the tailwater. The 100-year stage elevation of 55.50 ft and 100-Year flow of 409 cfs for Channel KE (Node ID: NKE-080, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 55.50 ft. The proposed culvert sizes from the HY-8 analysis are 2-8'x4' concrete box culverts. The existing upstream pipe size is a single 10'x4' concrete box culvert, therefore, the calculated culvert sizes of 2-8'x4' CBC are larger than the existing upstream culvert and will not restrict flow.

CD-13

The new alignment interrupts the natural flow of Channel M. To maintain the natural flow of Channel M, CD-13 will be strategically placed where the proposed roadway and channel intersect. This pipe will convey runoff from Channel M to the existing pond M-1. The crown of pipe was used as the tailwater. The 100-year stage elevation of 57.10 ft and 100-Year flow of 51 cfs for Channel M (Node ID: NM-070, **Appendix-J**) from the Bithlo Area Stormwater Management Master Plan were used to size this cross drain. The calculated backwater stage elevation of 56.73 ft from HY-8 analysis is less than the



existing 100-year flood elevation of 57.10 ft. The proposed culvert size from HY-8 is a single 48" pipe. Pond M-1 will also be modified due to the proposed alignment. Please refer to **Appendix-K** for oversized drawings of pond M-1.

4.2 Floodplain Impacts

The project will impact the 100-year floodplain in three different ways:

- 1) Longitudinal roadway widening impacts resulting from filling the floodplain areas associated with Econ River and its tributaries.
- 2) Impact due to proposed pond locations in floodplain.
- 3) Impact due to proposed cross drains in floodplain.

The longitudinal impact due to the recommended SR-408 Eastern Extension alignment cannot be avoided. During the final design phase of the project, every effort should be taken to minimize floodplain impacts. During the design phase, floodplain impacts should be mitigated by routing to proposed stormwater management facilities and roadside swales. Also, a Bridge Hydraulics Report (BHR) will be prepared during the design phase to document the hydraulic impacts of the recommended SR-408 Eastern Extension alignment.

The FEMA's Flood Insurance Rate Map (FIRM) for Orange County shows that a portion of the project lies within the 100-year floodplain areas Zone AE (100 year Base flood elevations are provided) and Zone A (100 year base flood elevations are not provided, areas with 1% change of flooding). Most of the project lies within flood Zone X (Areas of minimal flood hazard and above the 500-year flood zone). FEMA Map No. 12095C0280F, 129095C0285F, 12095C0295F and 12095C0315F, provide flood information for the project. Floodplain impact will occur throughout the project corridor and includes the Econ River and its tributaries. Please refer to **Appendix-A** for a FEMA exhibit and **Appendix-B** for a FEMA Flood Insurance Rate Map.

The total floodplain impact due to roadway fill for the entire proposed project corridor is 100.28 ac-ft. Available compensation in the proposed stormwater ponds and floodplain compensation ponds are 107.47 ac-ft. Please refer to Table-7 in the PSR for a summary of floodplain impacts and compensation. The dredge and fill volume are based on limited information available during the PD&E study. A detail evaluation has to be done during the final design. Based on the preliminary evaluation the project will provide more floodplain compensation than the impact. Therefore, a cup for cup compensation is provided by the project.

Two floodplain compensation pond sites were identified for this project in Basin 11C. The pond sites are Pond 11C3 and Pond 11C4. Both Pond 11C3 and Pond 11C4 are selected as the recommended floodplain compensation ponds. Beside this two floodplain compensation ponds, several stormwater ponds located adjacent to floodplains will also provide floodplain compensation. Please refer to Table-7 in the PSR. At certain segments of the project, for example at Basin 11C, the roadway profile is low enough to provide





floodplain compensation in the swales; this option should be evaluated during the design phase.

Runoff from within the corridor will be collected and conveyed to stormwater management facilities; therefore, reducing the overall impact to the remaining floodplains. The preliminary hydraulic evaluation indicates the flood elevation and limits will not change significantly; therefore, it is assumed that the project will not have a significant impact and the encroachment will be minimal.

4.3 **Project Classification**

The floodplain is in a medium density, semi-urbanized area and the encroachments are classified as "minimal". Minimal encroachment of a floodplain occurs when there is floodplain involvement, but the impacts on human life, transportation facilities, and natural and beneficial floodplain values are not significant and can be resolved with minimal efforts. Normally, these minimal efforts to address the impacts will consist of applying the FDOT drainage design standards and following the Water Management procedures to achieve results that will not increase or significantly change the flood elevation and the floodplain limits.

4.4 Flooding History and Maintenance Concern

In a phone interview with FDOT maintenance staff at the Oviedo Operations Center on 7/8/2016; there are no areas of flooding concern along the SR-50 corridor. The staff member Mike Danos mentioned that there have been no reports of flooding or overtopping within the SR-50 corridor. The proposed SR-408 Eastern Extension alignment is located just south of SR-50. Due to the close proximity of the proposed SR-408 Eastern Extension project to existing SR-50, flooding history of SR-50 will be used as a comparison for this project. Future investigation regarding flooding concerns at the proposed SR-408 Eastern Extension project corridor should be conducted during the final design.

5.0 BRIDGE HYDRAULICS EVALUATION

Bridges are proposed at the Econ River and at a major Econ River Tributary (Channel A) just east of the FPL Transmission Line (Sta. 660+00). Both proposed bridges will maintain flow conveyance in the Econ River and its major tributary. Bridge Hydraulic Reports for these proposed bridges shall be prepared during the design phase. The proposed Econ River Bridge will span over the river without impacting the floodplain or wetland. Please refer to the Bridge Analysis Report for the determination of bridge length, span and the pier locations. There is minimal impact to the floodplain due to the bridge piers. Refer to the Drainage Basin Map on Page-17, Econ River Basin Map on Page-18, Floodplain and Wetland Exhibits in Appendix-E, and Bridge Profiles in Appendix-F. The flows and stages in Table-7 for the Econ River Bridge were obtained from the Big Econ River Stormwater Management Master Plan (Model ID: BEBE160X, Appendix-I). The flows and stages in Table-7 for the Econ River Tributary Bridge were obtained from the Bithlo



Area Stormwater Management Master Plan (Node ID: NA-060, **Appendix-J**). The Econ River Tributary Bridge will need to account for additional runoff from a small area between Station 649+50 to 651+00. It is assumed that the proposed bridge over the Econ River will not increase the flood stage or the flood limits. Minor floodplain impacts are anticipated due to the bridge pier placement. Overall, insignificant impacts are anticipated at the Econ River. During the design phase, a FEMA No-Rise Certification should be assessed.

Bridge	100-Year	100-Year	Bridge Low	Existing	Bridge	Bridge
Structure	Flow	EL	Member EL	Ground EL	Clearance	Length
	(cfs)	(ft)	(ft)	(ft)	(ft)	(ft)
Econ River	10360	42.20	74.41	31.00	42.20	3820
Econ River						
Tributary						
(Channel A)	697	48.30	63.41	40.00	16.87	300

6.0 CONCLUSION

The purpose of this report was to determine potential cross drain locations along the proposed SR-408 Eastern Extension project corridor to reduce impacts to floodplains and wetlands. The proposed alignment will cross through residences, commercial businesses, wetlands, Econ River tributaries, and wooded areas. These proposed cross drain locations were chosen based on maintaining the natural flow of the land from the surrounding floodplains, wetlands, and Econ River tributaries. Fourteen potential cross drains were selected and analyzed for this project. The 100-year flow rates for cross drains 1 through 4 were obtained from the Big Econ River Basin Stormwater Management Master Plan. The 100-year flow rates for cross drains 10 through 13 were obtained from the Bithlo Area Stormwater Management Master Plan. The Rational Method was used to determine the flow for cross drains 5 through 9. Each cross drain was designed for a 100year storm event, in order to compare the 100-year backwater elevation with the 100-year existing flood elevation. Manning's Equation was used to determine trial sizes for each culvert. The trial sizes were used to perform the HY-8 analysis. The floodplains will be impacted due to longitudinal roadway widening and proposed pond locations. By following FDOT design standards and water management procedures, the proposed cross drains will have minimal impacts on the existing floodplains and wetlands. The purpose is to achieve results which do not increase or significantly change existing flood elevations or floodplain limits. The proposed cross drains located within floodplains will have minor volumetric impacts, and insignificant impact to flood stage and flood limits. The final design team should verify the proposed culvert sizes and their locations, based on the final roadway geometry and profile. BHR's for the Econ River Bridge and the Econ River Tributary Bridge should be provided during the design phase. The flows and tailwater elevations used in this report are based on preliminary information. The culvert design will need to be reviewed for flows and tailwater elevations during the final design.





Appendix: A

Exhibits:

- Project Location Map
- FEMA Flood Insurance Rate Map
- Soil Survey
- USGS Quadrangle Map
- Existing Land Use Map



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- Preferred Alternative Proposed Alignment
- Preferred Alternative Proposed R/W

0 0.25 0.5 1

CFX Project Number: 408-254 Orange County, FL

Exhibit 1. **Project Location** A-1





A-2



0 0.25 0.5

D

1

CFX Project Number: 408-254 Orange County, FL

CD-11

Existing SR-50 CD-10 1-10'x4'CBC

Existing SR-50 CD-11 1-24" RCP

End Project

Existing 2-42" RCP

0

Exhibit 3. Soil Survey A-3







A-5

Appendix: B

FEMA Flood Insurance Rate Map

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood elevation information. Accordingly, flood elevation data presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or flood/plain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this unerdetion. for this jurisdiction

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The **projection** used in the preparation of this map was State Plane Florida East FIPS Zone 0901. The **horizontal datum** was NAD33, GR31980 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical **datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1923 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <u>http://www.ngs.nosa.gov/</u> or contact the National Geodetic Survey at the following art/tress:

Spatial Reference System Divisio National Geodetic Survey, NOAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

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Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1.09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.89	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	+1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wekiva River	-0.88	-1.01	-0.94	0.07



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Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	+1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1.01	0.09
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Reedy Creek	-0.86	-0.89	-0.88	0.02
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Wekiva River	-0.88	-1.01	-0.94	0.07



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Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	+1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wekiva River	-0.88	-1.01	-0.94	0.07



possible updated of additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance range purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation tata presented in the FIS report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0° North American Vertical Datum of 1988 (NAVD 86). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Sillwater Elevations table in the Flood Insurance Study report for this jurisdiction. Elevations shown in the Summary of Sillwater Elevations table should be used for construction and/or floodplaim management purposes when they are higher than the elevations shown on the FIRM.

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by **flood control** structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was State Plane Florida East PIPS Zone 0901. The **horizontal datum** was NAD83, GRS1960 spheroid Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical **datum**. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at <u>http://www.ngs.noaa.gov/</u> or contact the National Geodetic Survey at the following address:

Spatial Reference System Division National Geodetic Survey, NCAA Silver Spring Metro Center 1315 East-West Highway Silver Spring, Maryland 20910 (301) 713-3191

To obtain current elevation, description, and/or location information for **bench marks** shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713-3242 or visit its website at http://www.ngs.ncaa.gov/.

Base map information shown on this FIRM was provided in digital format by Orange County, Florida.

This map reflects more detailed and up-to-date **stream channel configurations** than those shown on the previous FIRM for this jurisdiction. The floodplains and floodways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables in the Flood Insurance Study report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed **Map Index** for an overview map of the county showing the layout of map panels, community map repository addresses, and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

Contact the FEMA Map Service Center at 1-800-358-9616 for information on available products associated with this FIRM. Available products may include previously associated leafters of Map Change, a Flood Insurance Sludy report, and/or digital versions of this map. The FEMA Map Service Center may also be reached by Fax at 1-800-358-9620 and its website at <u>Hitm/Jwww.msc.fema.gov/</u>.

Watershed Name	Minimum Conversion	Maximum Conversion	Average Conversion	Maximum Offset
Big Econlockhatchee River	-1.03	-1.15	-1,09	0.06
Boggy Creek	-0.91	-1.01	-0.96	0.05
Cypress Creek	-0.87	-0.91	-0.89	0.02
Howell Branch	-0.96	-1.05	-0.98	0.07
Lake Apopka	-0.87	-0.97	-0.91	0.06
Lake Hart	-0.97	-1.07	+1.02	0.05
Little Econlockhatchee River	-0.92	-1.07	-1.01	0.09
Little Wekiva River	-0.91	-1.02	-0.95	0.07
Reedy Creek	-0.86	-0.89	-0.88	0.02
Shingle Creek	-0.88	-0.95	-0.91	0.04
St. Johns River	-1.08	-1.33	-1.19	0.14
Wekiva River	-0.88	-1.01	-0.94	0.07





Appendix: C

USDA NRCS Soil Report


USDA United States Department of Agriculture

Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Orange County, Florida

SR 408 Soil Data



May 27, 2016



Custom Soil Resource Report Soil Map



MAP LEGEND				MAP INFORMATION	
Area of Interest (AOI)		000	Spoil Area	The soil surveys that comprise your AOI were mapped at 1:20,000.	
	Area of Interest (AOI)	۵	Stony Spot	Please rely on the har scale on each man sheet for man	
Soils	Coil Mon Linit Dolygono	00	Very Stony Spot	measurements.	
	Soil Map Unit Polygons	Ŷ	Wet Spot	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: http://websoilsurvey.nrcs.usda.gov	
~	Soil Map Unit Lines	\triangle	Other		
Soil Map Unit Points			Special Line Features	Coordinate System: Web Mercator (EPSG:3857)	
Special (0)	Blowout	Water Features		Maps from the Web Soil Survey are based on the Web Mercator	
M	Borrow Pit	\sim	Streams and Canals	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accura calculations of distance or area are required.	
<u>س</u>	Clav Spot	Transport	tation		
~	Closed Depression	+++	Rails		
Ň	Gravel Pit	~	Interstate Highways	This product is generated from the USDA-NRCS certified data as	
6.15	Gravelly Spot	~	US Routes	the version date(s) listed below.	
 A	Landfill	~		Soil Survey Area: Orange County Florida	
A	Lava Flow	Local Roads		Survey Area Data: Version 12, Nov 19, 2015	
1.	Marsh or swamp	Backgrou	Aerial Photography	Soil map units are labeled (as space allows) for map scales 1:50, or larger.	
	Mine or Quarry	No.			
6	Miscellaneous Water			Deta(a) social images were photographed. Mar 12, 2011. Est	
õ	Perennial Water			20, 2015	
Š	Rock Outcrop				
Ť	Saline Spot	2 Shot		The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifti of map unit boundaries may be evident	
•.•	Sandy Spot				
	Severely Eroded Spot			or map unit boundaries may be evident.	
6	Sinkhole				
à	Slide or Slip				
Ŕ	Sodic Spot				

Map Unit Legend

Orange County, Florida (FL095)						
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI			
1	Arents, nearly level	16.4	0.1%			
2	Archbold fine sand, 0 to 5 percent slopes	73.1	0.4%			
3	Basinger fine sand, depressional, 0 to 1 percent slopes	1,106.2	6.2%			
15	Felda fine sand, frequently flooded	1,060.0	5.9%			
16	Floridana fine sand, frequently flooded	1.5	0.0%			
17	Floridana mucky fine sand, depressional	13.6	0.1%			
20	Immokalee fine sand	754.8	4.2%			
22	Lochloosa fine sand	57.6	0.3%			
23	Malabar fine sand	7.3	0.0%			
26	Ona fine sand	193.0	1.1%			
27	Ona-Urban land complex	4.8	0.0%			
30	Pineda fine sand	28.5	0.2%			
33	Pits	13.4	0.1%			
34	Pomello fine sand, 0 to 5 percent slopes	986.4	5.5%			
35	Pomello-Urban land complex, 0 to 5 percent slopes	19.4	0.1%			
37	St. Johns fine sand	920.5	5.2%			
38	St. Lucie fine sand, 0 to 5 percent slopes	34.7	0.2%			
39	St. Lucie-Urban land complex, 0 to 5 percent slopes	29.9	0.2%			
40	Samsula muck	145.3	0.8%			
42	Sanibel muck	1,496.8	8.4%			
44	Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes	9,067.4	50.9%			
45	Smyrna-Urban land complex	80.9	0.5%			
46	Tavares fine sand, 0 to 5 percent slopes	11.6	0.1%			
51	Wabasso fine sand, 0 to 2 percent slopes	669.4	3.8%			
53	Wauberg fine sand	26.8	0.2%			
54	Zolfo fine sand, 0 to 2 percent slopes	717.2	4.0%			
55	Zolfo-Urban land complex	11.2	0.1%			
99	Water	277.9	1.6%			
Totals for Area of Interest		17,825.4	100.0%			

3-Basinger fine sand, depressional, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2v16v Elevation: 0 to 160 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Basinger, depressional, and similar soils: 90 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Basinger, Depressional

Setting

Landform: Depressions on marine terraces, drainageways on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 14 inches: fine sand Bh/E - 14 to 36 inches: fine sand Cg - 36 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 20.00 in/hr)

Depth to water table: About 0 inches Frequency of flooding: None Frequency of ponding: Frequent Calcium carbonate, maximum in profile: 1 percent Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0 Available water storage in profile: Low (about 5.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL) Hydric soil rating: Yes

Minor Components

Smyrna, hydric

Percent of map unit: 5 percent

Landform: - error in exists on -

Landform position (three-dimensional): Tread, talf

Down-slope shape: Convex

Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy

soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: Yes

Samsula, muck

Percent of map unit: 3 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Tread, dip, talf Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Freshwater Marshes and Ponds (R155XY010FL), Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes Floridana, hydric

Percent of map unit: 2 percent Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Cypress Woodlands (MCV026CA), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL) Hydric soil rating: Yes

20—Immokalee fine sand

Map Unit Setting

National map unit symbol: bv7n Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Immokalee, non-hydric, and similar soils: 82 percent Immokalee, hydric, and similar soils: 10 percent Minor components: 8 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Immokalee, Non-hydric

Setting

Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand E - 5 to 35 inches: fine sand Bh - 35 to 67 inches: fine sand C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 6 to 12 inches
Frequency of flooding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Description of Immokalee, Hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 5 inches: fine sand

E - 5 to 35 inches: fine sand

Bh - 35 to 67 inches: fine sand

C - 67 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: B/D Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: Yes

Minor Components

Pineda

Percent of map unit: 4 percent
Landform: Flats on marine terraces
Landform position (three-dimensional): Talf
Down-slope shape: Linear
Across-slope shape: Linear
Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

Wabasso

Percent of map unit: 4 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

34—Pomello fine sand, 0 to 5 percent slopes

Map Unit Setting

National map unit symbol: 2v16y Elevation: 0 to 180 feet Mean annual precipitation: 44 to 52 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 342 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Pomello and similar soils: 95 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Pomello

Setting

Landform: Knolls on marine terraces, ridges on marine terraces Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Interfluve, riser Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 47 inches: fine sand Bh - 47 to 58 inches: fine sand Bw - 58 to 65 inches: fine sand C - 65 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 5 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 24 to 42 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6s Hydrologic Soil Group: A Other vegetative classification: Sand Pine Scrub (R155XY001FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL) Hydric soil rating: No

Minor Components

Smyrna

Percent of map unit: 3 percent Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Tavares

Percent of map unit: 1 percent
Landform: Ridges on marine terraces, flats on marine terraces
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Linear
Ecological site: Longleaf Pine-Turkey Oak Hills (R154XY002FL)
Other vegetative classification: Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL)
Hydric soil rating: No

Bulow

Percent of map unit: 1 percent
Landform: Ridges on marine terraces
Landform position (three-dimensional): Interfluve
Down-slope shape: Convex
Across-slope shape: Linear
Other vegetative classification: Sandy over loamy soils on knolls and ridges of mesic uplands (G155XB211FL)
Hydric soil rating: No

37—St. Johns fine sand

Map Unit Setting

National map unit symbol: bv87 Elevation: 30 to 150 feet Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

St. johns, non-hydric, and similar soils: 60 percent *St. johns, hydric, and similar soils:* 30 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of St. Johns, Non-hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)
Depth to water table: About 6 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: B/D

Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)

Hydric soil rating: No

Description of St. Johns, Hydric

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 12 inches: fine sand E - 12 to 24 inches: fine sand Bh - 24 to 44 inches: fine sand C - 44 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 1.98 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.2 inches)

Interpretive groups

Land capability classification (irrigated): None specified
Land capability classification (nonirrigated): 3w
Hydrologic Soil Group: B/D
Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 5 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Immokalee, non-hydric

Percent of map unit: 5 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

42—Sanibel muck

Map Unit Setting

National map unit symbol: bv8f Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Sanibel, undrained, and similar soils: 65 percent Sanibel, drained, and similar soils: 25 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Sanibel, Undrained

Setting

Landform: Marshes on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck *A - 11 to 15 inches:* fine sand *C - 15 to 80 inches:* fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 7w Hydrologic Soil Group: A/D Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL)

Hydric soil rating: Yes

Description of Sanibel, Drained

Setting

Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Parent material: Thin organic material over sandy marine deposits

Typical profile

Oa - 0 to 11 inches: muck *A - 11 to 15 inches:* fine sand *C - 15 to 80 inches:* fine sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 0 to 24 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Moderate (about 7.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

Minor Components

Hontoon, undrained

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

Samsula

Percent of map unit: 5 percent Landform: Depressions on marine terraces Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Organic soils in depressions and on flood plains (G155XB645FL) Hydric soil rating: Yes

44—Smyrna-Smyrna, wet, fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2v171 Elevation: 0 to 150 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Smyrna, non-hydric, and similar soils: 76 percent *Smyrna, hydric, and similar soils:* 20 percent *Minor components:* 4 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Smyrna, Non-hydric

Setting

Landform: Flatwoods on marine terraces, flats on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 17 inches: fine sand Bh - 17 to 27 inches: loamy fine sand C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Description of Smyrna, Hydric

Setting

Landform: Flats on marine terraces, flatwoods on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 4 inches: fine sand

E - 4 to 17 inches: fine sand

Bh - 17 to 27 inches: loamy fine sand

C - 27 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 6.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 3.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: Yes

Minor Components

Basinger, depressional

Percent of map unit: 2 percent Landform: Depressions on marine terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Concave Other vegetative classification: Sandy soils on stream terraces, flood plains, or in depressions (G155XB145FL) Hydric soil rating: Yes

Pomona, non-hydric

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces Landform position (two-dimensional): Backslope Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Eaugallie, hydric

Percent of map unit: 1 percent Landform: Flatwoods on marine terraces, flats on marine terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Dip Down-slope shape: Linear Across-slope shape: Linear

Other vegetative classification: South Florida Flatwoods (R154XY003FL), Sandy soils on flats of mesic or hydric lowlands (G154XB141FL)

Hydric soil rating: Yes

Across-slope shape: Linear

Other vegetative classification: North Florida Flatwoods (R154XY004FL), Sandy soils on rises and knolls of mesic uplands (G155XB131FL)

Hydric soil rating: No

51—Wabasso fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2svzg Elevation: 0 to 130 feet Mean annual precipitation: 38 to 62 inches Mean annual air temperature: 68 to 77 degrees F Frost-free period: 300 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Wabasso and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wabasso

Setting

Landform: Flatwoods on flats on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits over loamy marine deposits

Typical profile

A - 0 to 4 inches: fine sand E - 4 to 16 inches: fine sand Bh - 16 to 28 inches: fine sand E' - 28 to 32 inches: fine sand Btg - 32 to 48 inches: fine sandy loam Cg - 48 to 80 inches: loamy fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: 12 to 63 inches to strongly contrasting textural stratification
Natural drainage class: Poorly drained
Runoff class: High
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: About 6 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum in profile: 5 percent

Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0

Available water storage in profile: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A/D Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Minor Components

Basinger

Percent of map unit: 4 percent
Landform: Drainageways on flatwoods on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Convex, linear, concave
Across-slope shape: Linear, convex, concave
Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Felda

Percent of map unit: 4 percent
Landform: Flatwoods on drainageways on marine terraces
Landform position (three-dimensional): Tread, dip, talf
Down-slope shape: Linear
Across-slope shape: Concave, linear
Ecological site: Slough (R155XY011FL)
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on stream terraces, flood plains, or in depressions (G155XB245FL)
Hydric soil rating: Yes

Riviera

Percent of map unit: 4 percent
Landform: Flatwoods on drainageways on marine terraces
Landform position (three-dimensional): Tread, talf, dip
Down-slope shape: Linear, convex
Across-slope shape: Concave, linear
Ecological site: Slough (R155XY011FL)
Other vegetative classification: Slough (R155XY011FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G156AC241FL)
Hydric soil rating: Yes

Boca

Percent of map unit: 3 percent
Landform: Flatwoods on marine terraces
Landform position (three-dimensional): Tread, talf
Down-slope shape: Convex
Across-slope shape: Linear
Ecological site: South Florida Flatwoods (R155XY003FL)
Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)
Hydric soil rating: Yes

53—Wauberg fine sand

Map Unit Setting

National map unit symbol: bv8t Mean annual precipitation: 45 to 53 inches Mean annual air temperature: 70 to 77 degrees F Frost-free period: 350 to 365 days Farmland classification: Not prime farmland

Map Unit Composition

Wauberg and similar soils: 94 percent Minor components: 6 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Wauberg

Setting

Landform: Flats on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy and loamy marine deposits

Typical profile

- A 0 to 8 inches: fine sand
- E 8 to 28 inches: fine sand
- B 28 to 60 inches: sandy clay loam
- C 60 to 80 inches: sandy clay

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.06 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Sodium adsorption ratio, maximum in profile: 4.0
Available water storage in profile: Low (about 5.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: D Other vegetative classification: Sandy over loamy soils on flats of hydric or mesic lowlands (G155XB241FL)

Hydric soil rating: Yes

Minor Components

Wabasso

Percent of map unit: 6 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

54—Zolfo fine sand, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2w0q1 Elevation: 30 to 160 feet Mean annual precipitation: 44 to 56 inches Mean annual air temperature: 68 to 75 degrees F Frost-free period: 324 to 365 days Farmland classification: Farmland of unique importance

Map Unit Composition

Zolfo and similar soils: 88 percent *Minor components:* 12 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Zolfo

Setting

Landform: Rises on marine terraces, knolls on marine terraces Landform position (two-dimensional): Summit, footslope Landform position (three-dimensional): Interfluve, side slope, riser Down-slope shape: Convex Across-slope shape: Linear Parent material: Sandy marine deposits

Typical profile

A - 0 to 6 inches: fine sand E - 6 to 53 inches: fine sand Bh - 53 to 80 inches: fine sand

Properties and qualities

Slope: 0 to 2 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Somewhat poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr)

Depth to water table: About 24 to 42 inches Frequency of flooding: None Frequency of ponding: None Salinity, maximum in profile: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm) Sodium adsorption ratio, maximum in profile: 4.0 Available water storage in profile: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A Other vegetative classification: North Florida Flatwoods (R154XY004FL), South Florida Flatwoods (R154XY003FL), Sandy soils on rises and knolls of mesic uplands (G154XB131FL) Hydric soil rating: No

Minor Components

Myakka

Percent of map unit: 4 percent Landform: Flatwoods on marine terraces Landform position (three-dimensional): Tread, talf Down-slope shape: Convex Across-slope shape: Linear Other vegetative classification: South Florida Flatwoods (R155XY003FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL) Hydric soil rating: No

Tavares

Percent of map unit: 3 percent

Landform: Ridges on marine terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Interfluve, tread, rise

Down-slope shape: Linear, convex

Across-slope shape: Linear

Other vegetative classification: Longleaf Pine-Turkey Oak Hills (R154XY002FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL) *Hydric soil rating:* No

Millhopper

Percent of map unit: 3 percent

Landform: Ridges on marine terraces, knolls on marine terraces, flatwoods on marine terraces

Landform position (two-dimensional): Shoulder, summit

Landform position (three-dimensional): Interfluve

Down-slope shape: Convex, concave

Across-slope shape: Linear

Other vegetative classification: Upland Hardwood Hammock (R154XY008FL), Sandy soils on rises, knolls, and ridges of mesic uplands (G154XB121FL) *Hydric soil rating:* No

Lochloosa

Percent of map unit: 1 percent Landform: Rises on marine terraces Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex

Across-slope shape: Linear Other vegetative classification: Sandy over loamy soils on rises and knolls of mesic uplands (G155XB231FL) Hydric soil rating: No

Malabar

Percent of map unit: 1 percent
Landform: Drainageways on marine terraces
Landform position (three-dimensional): Dip
Down-slope shape: Linear, convex
Across-slope shape: Concave, linear
Other vegetative classification: Slough (R155XY011FL), Sandy soils on flats of mesic or hydric lowlands (G155XB141FL)
Hydric soil rating: Yes

Appendix: D

SR-408 Typical Section





Appendix: E

Cross Drain Exhibits

Cross Drains Site Maps



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Proposed Cross Drains Within Floodplains




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Proposed Cross Drains Within Wetlands



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Appendix: F

Cross Drain and Bridge Profiles





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Appendix: G

Cross Drain Hydraulic Analysis

Cross Drain 1

CD-1 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-1.

Flow Rate 10 =	873 ft ³ /s
Flow Rate 25 =	1013 ft ³ /s
Flow Rate 50 =	1160 ft ³ /s
Flow Rate 100 =	1322 ft ³ /s
Flow Rate 500 =	1760 ft ³ /s
Pipe Length =	485 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	13.66 ft
D =	163.95 in
A =	146.60 ft ²
Proposed Size =	3-11'x5' CBC



CD-1 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 873 cfs Design Flow: 1160 cfs Maximum Flow: 1322 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-1 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.20	873.00	873.00	0.00	1
51.31	917.90	917.90	0.00	1
51.79	962.80	962.80	0.00	1
51.87	1007.70	1007.70	0.00	1
51.72	1052.60	1052.60	0.00	1
51.79	1097.50	1097.50	0.00	1
51.92	1142.40	1142.40	0.00	1
51.97	1160.00	1160.00	0.00	1
52.18	1232.20	1232.20	0.00	1
52.31	1277.10	1277.10	0.00	1
52.45	1322.00	1322.00	0.00	1
88.87	4902.10	4902.10	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-1

Rating Curve Plot for Crossing: CD-1



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
873.00	873.00	51.20	4.724	5.199	7-M1t	3.751	2.791	4.540	4.040	5.827	0.000
917.90	917.90	51.31	4.890	5.312	7-M1t	3.889	2.886	4.540	4.040	6.127	0.000
962.80	962.80	51.79	5.057	5.793	7-M2t	5.000	2.979	4.540	4.040	6.426	0.000
1007.70	1007.70	51.87	5.224	5.869	7-M2t	5.000	3.071	4.540	4.040	6.726	0.000
1052.60	1052.60	51.72	5.392	5.722	3-M2t	5.000	3.161	4.540	4.040	7.026	0.000
1097.50	1097.50	51.79	5.562	5.793	3-M2t	5.000	3.251	4.540	4.040	7.325	0.000
1142.40	1142.40	51.92	5.734	5.919	3-M2t	5.000	3.339	4.540	4.040	7.625	0.000
1160.00	1160.00	51.97	5.802	5.970	3-M2t	5.000	3.373	4.540	4.040	7.743	0.000
1232.20	1232.20	52.18	6.085	6.177	3-M2t	5.000	3.512	4.540	4.040	8.225	0.000
1277.10	1277.10	52.31	6.266	6.308	3-M2t	5.000	3.596	4.540	4.040	8.524	0.000
1322.00	1322.00	52.45	6.449	6.440	3-M2t	5.000	3.680	4.540	4.040	8.824	0.000

Table 2 - Culvert Summary Table: CD-1

Straight Culvert

Inlet Elevation (invert): 46.00 ft, Outlet Elevation (invert): 45.50 ft

Culvert Length: 485.00 ft, Culvert Slope: 0.0010

Culvert Performance Curve Plot: CD-1





Water Surface Profile Plot for Culvert: CD-1

Site Data - CD-1

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 46.00 ft Outlet Station: 485.00 ft Outlet Elevation: 45.50 ft Number of Barrels: 3

Culvert Data Summary - CD-1

Barrel Shape: Concrete Box Barrel Span: 11.00 ft Barrel Rise: 5.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-1)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
873.00	50.04	4.04
917.90	50.04	4.04
962.80	50.04	4.04
1007.70	50.04	4.04
1052.60	50.04	4.04
1097.50	50.04	4.04
1142.40	50.04	4.04
1160.00	50.04	4.04
1232.20	50.04	4.04
1277.10	50.04	4.04
1322.00	50.04	4.04

Tailwater Channel Data - CD-1

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 50.04 ft

Roadway Data for Crossing: CD-1

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 88.87 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 2

CD-2 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-2.

Flow Rate 10 =	1136 ft ³ /s
Flow Rate 25 =	1325 ft ³ /s
Flow Rate 50 =	1499 ft ³ /s
Flow Rate 100 =	1690 ft ³ /s
Flow Rate 500 =	2233 ft ³ /s
Pipe Length =	302 ft
Change in FL Elevation from Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	13.71 ft

D =	13./1 π
D =	164.48 in
A =	147.56 ft ²
Proposed Size =	4-10'x5' CBC



CD-2 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 1136 cfs Design Flow: 1499 cfs Maximum Flow: 1690 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-2 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.06	1136.00	1136.00	0.00	1
51.16	1191.40	1191.40	0.00	1
51.27	1246.80	1246.80	0.00	1
51.40	1302.20	1302.20	0.00	1
51.57	1357.60	1357.60	0.00	1
51.70	1413.00	1413.00	0.00	1
51.83	1468.40	1468.40	0.00	1
51.91	1499.00	1499.00	0.00	1
52.11	1579.20	1579.20	0.00	1
52.26	1634.60	1634.60	0.00	1
52.41	1690.00	1690.00	0.00	1
85.27	5709.63	5709.63	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-2

Rating Curve Plot for Crossing: CD-2



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
1136.00	1136.00	51.06	4.960	5.557	3-M1f	3.393	2.926	5.000	4.540	5.680	0.000
1191.40	1191.40	51.16	5.130	5.659	3-M1f	3.511	3.020	5.000	4.540	5.957	0.000
1246.80	1246.80	51.27	5.301	5.770	3-M1f	3.629	3.113	5.000	4.540	6.234	0.000
1302.20	1302.20	51.40	5.473	5.895	3-M1f	3.745	3.205	5.000	4.540	6.511	0.000
1357.60	1357.60	51.57	5.647	6.071	3-M1f	3.860	3.295	5.000	4.540	6.788	0.000
1413.00	1413.00	51.70	5.823	6.197	4-FFf	3.974	3.384	5.000	4.540	7.065	0.000
1468.40	1468.40	51.83	6.002	6.330	4-FFf	5.000	3.472	5.000	4.540	7.342	0.000
1499.00	1499.00	51.91	6.102	6.405	4-FFf	5.000	3.520	5.000	4.540	7.495	0.000
1579.20	1579.20	52.11	6.369	6.610	4-FFf	5.000	3.644	5.000	4.540	7.896	0.000
1634.60	1634.60	52.26	6.558	6.758	4-FFf	5.000	3.729	5.000	4.540	8.173	0.000
1690.00	1690.00	52.41	6.751	6.911	4-FFf	5.000	3.813	5.000	4.540	8.450	0.000

Table 2 - Culvert Summary Table: CD-2

Straight Culvert

Inlet Elevation (invert): 45.50 ft, Outlet Elevation (invert): 45.00 ft

Culvert Length: 302.00 ft, Culvert Slope: 0.0017

Culvert Performance Curve Plot: CD-2



Water Surface Profile Plot for Culvert: CD-2



Site Data - CD-2

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 45.50 ft Outlet Station: 302.00 ft Outlet Elevation: 45.00 ft Number of Barrels: 4

Culvert Data Summary - CD-2

Barrel Shape: Concrete Box Barrel Span: 10.00 ft Barrel Rise: 5.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-2)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
1136.00	50.04	4.54
1191.40	50.04	4.54
1246.80	50.04	4.54
1302.20	50.04	4.54
1357.60	50.04	4.54
1413.00	50.04	4.54
1468.40	50.04	4.54
1499.00	50.04	4.54
1579.20	50.04	4.54
1634.60	50.04	4.54
1690.00	50.04	4.54

Tailwater Channel Data - CD-2

Tailwater Channel Option:Enter Constant Tailwater ElevationConstant Tailwater Elevation:50.04 ft

Roadway Data for Crossing: CD-2

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 85.27 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 3

CD-3 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-3.

3-11'x7' CBC

Flow Rate 10 =	1354 ft ³ /s
Flow Rate 25 =	1549 ft ³ /s
Flow Rate 50 =	1770 ft ³ /s
Flow Rate 100 =	2000 ft ³ /s
Flow Rate 500 =	2624 ft ³ /s
Pipe Length =	400 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	15.39 ft
D =	184.69 in
A =	186.04 ft ²

Proposed Size =



CD-3 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 1354 cfs Design Flow: 1770 cfs Maximum Flow: 2000 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-3 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.24	1354.00	1354.00	0.00	1
51.36	1418.60	1418.60	0.00	1
51.47	1483.20	1483.20	0.00	1
51.60	1547.80	1547.80	0.00	1
51.72	1612.40	1612.40	0.00	1
51.85	1677.00	1677.00	0.00	1
51.99	1741.60	1741.60	0.00	1
52.05	1770.00	1770.00	0.00	1
52.26	1870.80	1870.80	0.00	1
52.41	1935.40	1935.40	0.00	1
52.51	2000.00	2000.00	0.00	1
80.88	6240.70	6240.70	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-3

Rating Curve Plot for Crossing: CD-3



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
1354.00	1354.00	51.24	6.323	7.243	7-M1t	4.816	3.739	6.540	6.040	6.274	0.000
1418.60	1418.60	51.36	6.526	7.356	7-M1t	4.985	3.857	6.540	6.040	6.573	0.000
1483.20	1483.20	51.47	6.729	7.474	7-M1t	5.153	3.973	6.540	6.040	6.872	0.000
1547.80	1547.80	51.60	6.931	7.596	7-M1t	5.320	4.088	6.540	6.040	7.172	0.000
1612.40	1612.40	51.72	7.134	7.723	7-M1t	5.486	4.201	6.540	6.040	7.471	0.000
1677.00	1677.00	51.85	7.337	7.853	7-M1t	5.651	4.312	6.540	6.040	7.770	0.000
1741.60	1741.60	51.99	7.542	7.986	7-M1t	5.815	4.423	6.540	6.040	8.070	0.000
1770.00	1770.00	52.05	7.633	8.046	7-M1t	5.886	4.470	6.540	6.040	8.201	0.000
1870.80	1870.80	52.26	7.957	8.264	7-M1t	6.140	4.639	6.540	6.040	8.668	0.000
1935.40	1935.40	52.41	8.168	8.407	7-M1t	6.301	4.745	6.540	6.040	8.968	0.000
2000.00	2000.00	52.51	8.381	8.512	7-M1t	6.462	4.850	6.540	6.040	9.267	0.000

Table 2 - Culvert Summary Table: CD-3

Straight Culvert

Inlet Elevation (invert): 44.00 ft, Outlet Elevation (invert): 43.50 ft

Culvert Length: 400.00 ft, Culvert Slope: 0.0013

Culvert Performance Curve Plot: CD-3



Water Surface Profile Plot for Culvert: CD-3



Site Data - CD-3

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 44.00 ft Outlet Station: 400.00 ft Outlet Elevation: 43.50 ft Number of Barrels: 3

Culvert Data Summary - CD-3

Barrel Shape: Concrete Box Barrel Span: 11.00 ft Barrel Rise: 7.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
1354.00	50.04	6.04
1418.60	50.04	6.04
1483.20	50.04	6.04
1547.80	50.04	6.04
1612.40	50.04	6.04
1677.00	50.04	6.04
1741.60	50.04	6.04
1770.00	50.04	6.04
1870.80	50.04	6.04
1935.40	50.04	6.04
2000.00	50.04	6.04

Tailwater Channel Data - CD-3

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 50.04 ft

Roadway Data for Crossing: CD-3

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 80.88 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 3A

CD-3A Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-3A.

1-30" RCP

Flow Rate 10 =	3.59 ft ³ /s
Flow Rate 25 =	4.38 ft ³ /s
Flow Rate 50 =	5.76 ft ³ /s
Flow Rate 100 =	7.69 ft ³ /s
Flow Rate 500 =	12.65 ft ³ /s
Pipe Length =	303 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	1.82 ft
D =	21.78 in
Α =	2.59 ft^2

Proposed Size =

CD-3A Rational Method									
Runoff Coefficient Calculations									
Land Use	Slope	Land Cover (%)	Runoff	Area (acre) - A	Product				
			Coefficient						
Residential	0-2%		0.45	0.00	0.00				
Commercial	0-2%	5	0.95	0.13	0.13				
Lawn flat 2%	0-2%	20	0.20	0.47	0.09				
Woods/Wetlands	0-2%	75	0.15	1.76	0.26				
		Total 2.35							
Composite Coefficient 0.21									
	Contributing	g Flow Rate for Va	rious Storm Fr	equency					
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q				
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)				
10-Year	1	0.1	7.4	0.21	3.59				
25-Year	1.1	0.04	8.2	0.23	4.38				
50-Year	1.2	0.02	9	0.27	5.76				
100-Year	1.25	0.01	9.6	0.34	7.69				
500-Year	-	0.002	-	-	12.65				
		Rational For	mula						
	Q = CIA								

**Time of Concentration was assumed to be 10 minutes for an area this small.

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-3A HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 3.59 cfs Design Flow: 5.76 cfs Maximum Flow: 7.69 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-3A Discharge (cfs)	Roadway Discharge (cfs)	Iterations
57.83	3.59	3.59	0.00	1
57.84	4.00	4.00	0.00	1
57.85	4.41	4.41	0.00	1
57.86	4.82	4.82	0.00	1
57.87	5.23	5.23	0.00	1
57.88	5.64	5.64	0.00	1
57.88	5.76	5.76	0.00	1
57.90	6.46	6.46	0.00	1
57.92	6.87	6.87	0.00	1
57.93	7.28	7.28	0.00	1
57.95	7.69	7.69	0.00	1
75.41	84.31	84.31	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-3A

Rating Curve Plot for Crossing: CD-3A



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
3.59	3.59	57.83	0.852	2.532	4-FFf	0.733	0.619	2.500	2.500	0.731	0.000
4.00	4.00	57.84	0.900	2.540	4-FFf	0.776	0.655	2.500	2.500	0.815	0.000
4.41	4.41	57.85	0.949	2.548	4-FFf	0.817	0.686	2.500	2.500	0.898	0.000
4.82	4.82	57.86	0.994	2.558	4-FFf	0.856	0.719	2.500	2.500	0.982	0.000
5.23	5.23	57.87	1.038	2.568	4-FFf	0.894	0.751	2.500	2.500	1.065	0.000
5.64	5.64	57.88	1.080	2.579	4-FFf	0.931	0.782	2.500	2.500	1.149	0.000
5.76	5.76	57.88	1.092	2.582	4-FFf	0.942	0.790	2.500	2.500	1.173	0.000
6.46	6.46	57.90	1.161	2.603	4-FFf	1.003	0.839	2.500	2.500	1.316	0.000
6.87	6.87	57.92	1.201	2.617	4-FFf	1.038	0.864	2.500	2.500	1.400	0.000
7.28	7.28	57.93	1.238	2.631	4-FFf	1.072	0.891	2.500	2.500	1.483	0.000
7.69	7.69	57.95	1.280	2.647	4-FFf	1.106	0.918	2.500	2.500	1.567	0.000

Table 2 - Culvert Summary Table: CD-3A

Straight Culvert

Inlet Elevation (invert): 55.30 ft, Outlet Elevation (invert): 54.80 ft

Culvert Length: 300.00 ft, Culvert Slope: 0.0017

Culvert Performance Curve Plot: CD-3A





Water Surface Profile Plot for Culvert: CD-3A

Site Data - CD-3A

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 55.30 ft Outlet Station: 300.00 ft Outlet Elevation: 54.80 ft Number of Barrels: 1

Culvert Data Summary - CD-3A

Barrel Shape: Circular Barrel Diameter: 2.50 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None
Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
3.59	57.80	2.50
4.00	57.80	2.50
4.41	57.80	2.50
4.82	57.80	2.50
5.23	57.80	2.50
5.64	57.80	2.50
5.76	57.80	2.50
6.46	57.80	2.50
6.87	57.80	2.50
7.28	57.80	2.50
7.69	57.80	2.50

Table 3 - Downstream Channel Rating Curve (Crossing: CD-3A)

Tailwater Channel Data - CD-3A

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 57.80 ft

Roadway Data for Crossing: CD-3A

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 75.41 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 4

CD-4 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Big Econ Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-4.

2-8'x4' CBC

Flow Rate 10 =	301 ft ³ /s
Flow Rate 25 =	370 ft ³ /s
Flow Rate 50 =	427 ft ³ /s
Flow Rate 100 =	496 ft ³ /s
Flow Rate 500 =	702 ft ³ /s
Pipe Length =	456 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	9.35 ft
D =	112.21 in
A =	68.67 ft ²

Proposed Size =



CD-4 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 301 cfs

Design Flow: 427 cfs

Maximum Flow: 496 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-4

Headwater Elevation (ft)	Total Discharge (cfs)	CD-4 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.27	301.00	301.00	0.00	1
51.38	320.50	320.50	0.00	1
51.49	340.00	340.00	0.00	1
51.61	359.50	359.50	0.00	1
51.72	379.00	379.00	0.00	1
51.84	398.50	398.50	0.00	1
51.97	418.00	418.00	0.00	1
52.03	427.00	427.00	0.00	1
52.46	457.00	457.00	0.00	1
52.72	476.50	476.50	0.00	1
52.95	496.00	496.00	0.00	1
82.31	1727.16	1727.16	0.00	Overtopping

Rating Curve Plot for Crossing: CD-4



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
301.00	301.00	51.27	3.763	4.273	7-M1t	3.061	2.223	3.900	3.400	4.824	0.000
320.50	320.50	51.38	3.930	4.380	7-M1t	3.204	2.318	3.900	3.400	5.136	0.000
340.00	340.00	51.49	4.096	4.491	7-M1t	3.346	2.412	3.900	3.400	5.449	0.000
359.50	359.50	51.61	4.265	4.606	7-M1t	3.487	2.503	3.900	3.400	5.761	0.000
379.00	379.00	51.72	4.434	4.724	7-M1t	3.626	2.593	3.900	3.400	6.074	0.000
398.50	398.50	51.84	4.606	4.844	7-M1t	3.764	2.681	3.900	3.400	6.386	0.000
418.00	418.00	51.97	4.782	4.968	3-M2t	4.000	2.767	3.900	3.400	6.699	0.000
427.00	427.00	52.03	4.864	5.025	3-M2t	4.000	2.807	3.900	3.400	6.843	0.000
457.00	457.00	52.46	5.144	5.464	7-M2t	4.000	2.937	3.900	3.400	7.324	0.000
476.50	476.50	52.72	5.331	5.717	7-M2t	4.000	3.020	3.900	3.400	7.636	0.000
496.00	496.00	52.95	5.524	5.954	7-M2t	4.000	3.102	3.900	3.400	7.949	0.000

Table 2 - Culvert Summary Table: CD-4

Straight Culvert

Inlet Elevation (invert): 47.00 ft, Outlet Elevation (invert): 46.50 ft

Culvert Length: 456.00 ft, Culvert Slope: 0.0011

Culvert Performance Curve Plot: CD-4



Water Surface Profile Plot for Culvert: CD-4



Site Data - CD-4

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 47.00 ft Outlet Station: 456.00 ft Outlet Elevation: 46.50 ft Number of Barrels: 2

Culvert Data Summary - CD-4

Barrel Shape: Concrete Box Barrel Span: 8.00 ft Barrel Rise: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-4)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
301.00	50.40	3.40
320.50	50.40	3.40
340.00	50.40	3.40
359.50	50.40	3.40
379.00	50.40	3.40
398.50	50.40	3.40
418.00	50.40	3.40
427.00	50.40	3.40
457.00	50.40	3.40
476.50	50.40	3.40
496.00	50.40	3.40

Tailwater Channel Data - CD-4

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 50.40 ft

Roadway Data for Crossing: CD-4

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 82.31 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 5

CD-5 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-5.

Flow Rate 10 =	134 ft ³ /s
Flow Rate 25 =	171 ft ³ /s
Flow Rate 50 =	226 ft ³ /s
Flow Rate 100 =	312 ft ³ /s
Flow Rate 500 =	541 ft ³ /s
Pipe Length =	374 ft
Change in FL Elevation from	0 50 ft
opstream to bownstream -	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	7.58 ft
D =	90.92 in
A =	45.08 ft ²
Proposed Size =	2-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: LOCATION : BASIN NAME:	STATE ROAD NO. 408 EAS ORANGE COUNTY CD-5	TERN EXTENSI	ON	1	NUMBER: FILE:	
C	ONDITIONS	COMPUTE		Water Resour	ces Group	Date
Pre-Development	X	T⊡dc	X	Computed By	KS	09/05/17
Post-Development		-	Γīdt	Checked By	CR	
Rainfall Zone:	7	Frequency:		·		-
SHEET ELOW	(Applicable To Trdc Only)					
			Segment ID			
1) SURFACE DESCH	RIPTION (table 5-4)					
2) MANNNING'S RC	OUGHNESS COEFF., [n] (ta	ble 5-4)		0.08		
FLOW LENGTH,	[L] (TOTAL L <= 300 ft)		ft	300		
4) HIGH ELEVATION	۱, [A]		ft	70.0		
5) LOW ELEVATION	, [B]		ft	68.0		
6) TWO YEAR 24-hr	RAINFALL, [P]		in	4.92		
7) LAND SLOPE, [s]			ft/ft	0.007		
8) COMPUTE T dt ::	$T dt = (.007*(n*L)^{0.8})/(P^{0.8})$	0.5 * s^0.4)	hr	0.291 +		0.291
SHALLOW C					min =	17.4
			Segment ID			
9) SURFACE DESCE	RIPTION Enter 1 (Paved) or	2 (Unpayed)	oogmontib	1		
10) FLOW I ENGTH		e (onputou)	ft	4687		
11) HIGH ELEVATIO	N. [C]			68.0		
12) LOW ELEVATIO	N. [D]			52.0		
13) WATERCOURSE	E SLOPE, [s]		ft/ft	0.0034		
14) AVERAGE VELC	CITY, [V] **		ft/sec	1.19		
15) COMPUTE Todto] Tīdt□ = L / 3600*V		hr	1.10 +	=	1.10
					min =	65.8
CHANNEL FLOW						
			Segment ID			
16) CROSS SECTIO	JNAL FLOW AREA, [a]		π^2			
17) WEITED PERIM			π			
18) HYDRAULIC RA			П			
19) FLOW LENGTH,			П			
20) HIGH ELEVATIO	או נכו		1L ft			
21) LOW ELEVATIO			1L ft/ft			
22) CHAINNEL SLOP			IVIL			
24 COMPLITE V/·	$V = (1.49 \text{ r}^2/3 \text{ s}^{-1}/2) / \text{ n}$		ft/sec			
25 COMPLITE Traff	$T_{\text{rdt}} = 1 / 3600 \text{ V}$		hr			
			•••		min =	0.0
				TOTA	L TIME (hr)	1.39
** Reference: FDOT	Drainage Manual Chapter 5.5.	, TR-55 Chapter	3 & APP-F.	TOTA	L TIME (min)	83.2

CD-5 Rational Method							
Runoff Coefficient Calculations							
Land Use	Slope	Land Cover (%)	Runoff	Area (acre) - A	Product		
			Coefficient				
Residential	0-2%	40	0.45	43.61	19.63		
Commercial	0-2%	25	0.95	27.26	25.89		
Lawn flat 2%	0-2%	25	0.20	27.26	5.45		
Woods/Wetlands	0-2%	10	0.15	10.90	1.64		
			Total	109.03	52.61		
			Compos	ite Coefficient	0.48		
	Contributing	g Flow Rate for Va	rious Storm Fr	equency			
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q		
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)		
10-Year	1	0.1	2.55	0.48	134.15		
25-Year	1.1	0.04	2.95	0.53	170.71		
50-Year	1.2	0.02	3.25	0.64	225.68		
100-Year	1.25	0.01	3.60	0.80	312.49		
500-Year	-	0.002	-	-	540.99		
	Rational Formula						
		Q = CIA					

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-5 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 134 cfs

Design Flow: 226 cfs

Maximum Flow: 312 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-5 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
50.50	134.00	134.00	0.00	1
50.68	151.80	151.80	0.00	1
50.88	169.60	169.60	0.00	1
51.08	187.40	187.40	0.00	1
51.27	205.20	205.20	0.00	1
51.48	223.00	223.00	0.00	1
51.51	226.00	226.00	0.00	1
51.87	258.60	258.60	0.00	1
52.07	276.40	276.40	0.00	1
52.26	294.20	294.20	0.00	1
52.46	312.00	312.00	0.00	1
84.25	1603.28	1603.28	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-5

Rating Curve Plot for Crossing: CD-5



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
134.00	134.00	50.50	3.027	3.495	3-M1t	2.566	2.181	3.230	2.730	4.318	0.000
151.80	151.80	50.68	3.278	3.682	3-M1t	2.755	2.325	3.230	2.730	4.892	0.000
169.60	169.60	50.88	3.516	3.876	3-M1t	2.938	2.466	3.230	2.730	5.465	0.000
187.40	187.40	51.08	3.741	4.075	3-M1t	3.119	2.598	3.230	2.730	6.039	0.000
205.20	205.20	51.27	3.957	4.266	3-M2t	3.299	2.727	3.230	2.730	6.613	0.000
223.00	223.00	51.48	4.164	4.475	3-M2t	3.479	2.849	3.230	2.730	7.186	0.000
226.00	226.00	51.51	4.198	4.509	3-M2t	3.509	2.869	3.230	2.730	7.283	0.000
258.60	258.60	51.87	4.558	4.871	3-M2t	3.845	3.076	3.230	2.730	8.333	0.000
276.40	276.40	52.07	4.747	5.067	3-M2t	4.037	3.182	3.230	2.730	8.907	0.000
294.20	294.20	52.26	4.934	5.262	2-M2c	4.238	3.289	3.289	2.730	9.269	0.000
312.00	312.00	52.46	5.117	5.455	2-M2c	4.453	3.390	3.390	2.730	9.472	0.000

Table 2 - Culvert Summary Table: CD-5

Straight Culvert

Inlet Elevation (invert): 47.00 ft, Outlet Elevation (invert): 46.50 ft

Culvert Length: 374.00 ft, Culvert Slope: 0.0013

Culvert Performance Curve Plot: CD-5



Water Surface Profile Plot for Culvert: CD-5



Site Data - CD-5

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 47.00 ft Outlet Station: 374.00 ft Outlet Elevation: 46.50 ft Number of Barrels: 2

Culvert Data Summary - CD-5

Barrel Shape: Circular Barrel Diameter: 6.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
134.00	49.73	2.73
151.80	49.73	2.73
169.60	49.73	2.73
187.40	49.73	2.73
205.20	49.73	2.73
223.00	49.73	2.73
226.00	49.73	2.73
258.60	49.73	2.73
276.40	49.73	2.73
294.20	49.73	2.73
312.00	49.73	2.73

Table 3 - Downstream Channel Rating Curve (Crossing: CD-5)

Tailwater Channel Data - CD-5

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 49.73 ft

Roadway Data for Crossing: CD-5

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 84.25 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 6

CD-6 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-6.

Flow Rate 10 =	112 ft ³ /s
Flow Rate 25 =	141 ft ³ /s
Flow Rate 50 =	190 ft ³ /s
Flow Rate 100 =	259 ft ³ /s
Flow Rate 500 =	449 ft ³ /s
Pipe Length =	427 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	7.24 ft
D =	86.92 in
A =	41.21 ft ²
Proposed Size =	2-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: LOCATION : BASIN NAME:	STATE ROAD NO. 408 EAST ORANGE COUNTY CD-6	ERN EXTENSI	N		NUMBER: FILE:	
G	ONDITIONS	COMPUTE		Water Reso	ources Group	Date
Pre-Development		T⊡dc	X	Computed By	KS	09/05/17
Post-Development		Т	īdt	Checked By	CR	
Rainfall Zone:	7	Frequency:		·	•	
SHEET FLOW	(Applicable To T⊡dc⊡Only)				,	
	PIRTION (table 5.4)		Segment ID			
2) MANNINING'S R	NICHNESS COEFE [n] (tab	le 5_1)		0.14		
2) FLOW LENGTH	$[1]$ (TOTAL L \leq 300 ft)	ie J-4)	ft	300		
4) HIGH ELEVATION	$[L] (101 \times L = 300 \text{ ft})$		ft	66.0		
5) I OW ELEVATION	, [7] J [B]		ft	65.0		
6) TWO YEAR 24-hr			in	4.92		
7) I AND SI OPE [s]	·····		ft/ft	0.003		
8) COMPUTE Tott	T⊡dt□ = (.007*(n*L)^0.8)/(P^0.	5 * s^0.4)	hr	0.626 +		0.626
-,		/			min =	37.6
SHALLOW C	ONCENTRATED FLOW					
		44	Segment ID			
9) SURFACE DESC	RIPTION Enter 1 (Paved) or 2	(Unpaved)	0	1		
10) FLOW LENGTH	, [L]	,	ft	3667		
11) HIGH ELEVATIO	DN, [C]			65.0		
12) LOW ELEVATIC	N, [D]			51.0		
13) WATERCOURS	E SLOPE, [s]		ft/ft	0.0038		
14) AVERAGE VELO	DCITY, [V] **		ft/sec	1.26		
15) COMPUTE T dt	I T Idt III = L / 3600*V		hr	0.81 +	=	0.81
CHANNEL FLOW					min =	48.7
			Segment ID			
16) CROSS SECTION	ONAL FLOW AREA, [a]		ft^2			
17) WETTED PERIN	/ETER, [Pːdwː]		ft			
18) HYDRAULIC RA	.DIUS, [r] = a / Pīdw⊡		ft			
19) FLOW LENGTH	, [L]		ft			
20) HIGH ELEVATIO	DN, [D]		ft			
21) LOW ELEVATIC	N, [E]		ft			
22) CHANNEL SLOP	PE, [s]		ft/ft			
23) MANNNING'S F	ROUGHNESS COEFF., [n]		6			
	$V = (1.49^{\circ} f^{2}/3^{\circ} s^{1}/2) / n$		π/sec			
	. I LUILI - L/3000 V		TH		=	0.0
						0.0
				то	TAL TIME (br)	1 44
** Reference: FDOT	Drainage Manual Chapter 5.5.	TR-55 Chapter 3	8 & APP-F.	TO	TAL TIME (min)	86.2
	J					

CD-6 Rational Method							
Runoff Coefficient Calculations							
Land Use	Slope	Land Cover (%)	Runoff	Area (acre) - A	Product		
			Coefficient				
Residential	0-2%	75	0.45	89.26	40.17		
Commercial	0-2%	0	0.95	0.00	0.00		
Lawn flat 2%	0-2%	5	0.20	5.95	1.19		
Woods/Wetlands	0-2%	20	0.15	23.80	3.57		
			Total	119.01	44.93		
	Composite Coefficient 0.38						
	Contributin	g Flow Rate for Va	arious Storm F	requency			
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q		
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)		
10-Year	1	0.1	2.5	0.38	112.32		
25-Year	1.1	0.04	2.85	0.42	140.84		
50-Year	1.2	0.02	3.2	0.50	189.77		
100-Year	1.25	0.01	3.5	0.62	259.45		
500-Year	-	0.002	-	-	448.87		
Rational Formula							
Q = CIA							

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-6 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 112 cfs

Design Flow: 190 cfs

Maximum Flow: 259 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-6

Headwater Elevation (ft)	Total Discharge (cfs)	CD-6 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
51.06	112.00	112.00	0.00	1
51.27	126.70	126.70	0.00	1
51.48	141.40	141.40	0.00	1
51.67	156.10	156.10	0.00	1
51.86	170.80	170.80	0.00	1
52.04	185.50	185.50	0.00	1
52.10	190.00	190.00	0.00	1
52.40	214.90	214.90	0.00	1
52.57	229.60	229.60	0.00	1
52.74	244.30	244.30	0.00	1
52.91	259.00	259.00	0.00	1
84.64	1588.91	1588.91	0.00	Overtopping

Rating Curve Plot for Crossing: CD-6



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
112.00	112.00	51.06	2.745	3.058	3-M2t	2.409	1.988	2.230	1.730	5.853	0.000
126.70	126.70	51.27	2.933	3.274	3-M2t	2.581	2.117	2.230	1.730	6.621	0.000
141.40	141.40	51.48	3.134	3.477	2-M2c	2.747	2.243	2.243	1.730	7.331	0.000
156.10	156.10	51.67	3.337	3.671	2-M2c	2.910	2.359	2.359	1.730	7.561	0.000
170.80	170.80	51.86	3.532	3.860	2-M2c	3.070	2.475	2.475	1.730	7.761	0.000
185.50	185.50	52.04	3.718	4.043	2-M2c	3.228	2.584	2.584	1.730	7.964	0.000
190.00	190.00	52.10	3.774	4.099	2-M2c	3.277	2.617	2.617	1.730	8.020	0.000
214.90	214.90	52.40	4.071	4.398	2-M2c	3.546	2.794	2.794	1.730	8.327	0.000
229.60	229.60	52.57	4.239	4.569	2-M2c	3.707	2.893	2.893	1.730	8.507	0.000
244.30	244.30	52.74	4.403	4.739	2-M2c	3.871	2.988	2.988	1.730	8.686	0.000
259.00	259.00	52.91	4.563	4.906	2-M2c	4.041	3.078	3.078	1.730	8.865	0.000

Table 2 - Culvert Summary Table: CD-6

Straight Culvert

Inlet Elevation (invert): 48.00 ft, Outlet Elevation (invert): 47.50 ft

Culvert Length: 427.00 ft, Culvert Slope: 0.0012

Culvert Performance Curve Plot: CD-6



Water Surface Profile Plot for Culvert: CD-6



Site Data - CD-6

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 48.00 ft Outlet Station: 427.00 ft Outlet Elevation: 47.50 ft Number of Barrels: 2

Culvert Data Summary - CD-6

Barrel Shape: Circular Barrel Diameter: 6.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-6)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
112.00	49.73	1.73
126.70	49.73	1.73
141.40	49.73	1.73
156.10	49.73	1.73
170.80	49.73	1.73
185.50	49.73	1.73
190.00	49.73	1.73
214.90	49.73	1.73
229.60	49.73	1.73
244.30	49.73	1.73
259.00	49.73	1.73

Tailwater Channel Data - CD-6

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 49.73 ft

Roadway Data for Crossing: CD-6

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 84.64 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 7

CD-7 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-7.

2-48" RCP

Flow Rate 10 =	98 ft ³ /s
Flow Rate 25 =	125 ft ³ /s
Flow Rate 50 =	165 ft ³ /s
Flow Rate 100 =	231 ft ³ /s
Flow Rate 500 =	401 ft ³ /s
Pipe Length = Change in FL Elevation from	129 ft
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	5.54 ft
D =	66.437 in
A =	24.074 ft ²

Proposed Size =

TIME OF CONCENTRATION

PROJECT TITLE: LOCATION : BASIN NAME:	STATE ROAD NO. 408 EAST ORANGE COUNTY CD-7	ERN EXTENSIO	N		NUMBER: FILE:	
G	ONDITIONS	COMPUTE		Water Res	ources Group	Date
Pre-Development		T⊡dc	X	Computed By	KS	09/05/17
Post-Development		Т	dt	Checked By	CR	
Rainfall Zone:	7	Frequency:				
SHEET FLOW	(Applicable To T⊡dc⊡Only)					
	PIPTION (table 5.4)		Segment ID			
2) MANNNING'S R	CLIGHNESS COFFE [n] (table	le 5-4)		0.36		
3) FLOW LENGTH	[1] (TOTAL 1 <= 300 ft)	0 0 4)	ft	300		
4) HIGH ELEVATIO	N. [A]		ft	68.0		
5) LOW ELEVATION	N, [B]		ft	67.0		
6) TWO YEAR 24-hr	RAINFALL, [P]		in	4.92		
7) LAND SLOPE, [s]			ft/ft	0.003		
8) COMPUTE T dt:	Tīdt□ = (.007*(n*L)^0.8)/(P^0.	5 * s^0.4)	hr	1.315 +		1.315
					min =	78.9
SHALLOW C	ONCENTRATED FLOW					
			Segment ID			
9) SURFACE DESC	RIPTION Enter 1 (Paved) or 2	(Unpaved)		1		
10) FLOW LENGTH	, [L]		ft	1400		
11) HIGH ELEVATIO	DN, [C]			67.0		
12) LOW ELEVATIC			ft /ft	<u>57.0</u>		
14) AVEDAGE VEL	E SLOFE, [5] ACITY [1/] **		ft/soc	1.72		
15) COMPLITE Traft	⊐ Trdt⊡ = 1 / 3600*\/		hr	0.23 +	=	0.23
			111	0.20	min =	13.6
CHANNEL FLOW						
			Segment ID			
16) CROSS SECTION	ONAL FLOW AREA, [a]		ft^2			
17) WETTED PERIN	/ETER, [Pːdw]		ft			
18) HYDRAULIC RA	∖DIUS, [r] = a / Pīdw⊡		ft			
19) FLOW LENGTH	, [L]		ft			
20) HIGH ELEVATIO	DN, [D]		ft			
21) LOW ELEVATIC	N, [E]		ft			
22) CHANNEL SLOP	PE, [s]		ft/ft			
23) MANNNING'S F	ROUGHNESS COEFF., [n]					
24) COMPUTE V:	$V = (1.49*r^2/3 * s^1/2) / n$		tt/sec			
25) COMPUTE I dt	$\Box I \Box \alpha \Box = L / 3600^{\circ} V$		nr		=	0.0
					min =	0.0
				тс	TAL TIME (br)	1 54
** Reference: FDOT	Drainage Manual Chapter 5.5	TR-55 Chanter 3	& APP-F	тс)TAL TIME (min)	92.5
	Branago manaa onaptor 0.0,	oo onapier e	· · · · · · · · · · · · · · · · · · ·	10	· · · · · · · · · · · · · · · · · · ·	52.5

CD-7 Rational Method							
Runoff Coefficient Calculations							
Runoff							
Land Use	Slope	Land Cover (%)	Coefficient	Area (acre) - A	Product		
Residential	0-2%	5	0.45	3.8975	1.75		
Commercial	0-2%	45	0.95	35.0775	33.32		
Lawn flat 2%	0-2%	20	0.20	15.59	3.12		
Woods/Wetlands	0-2%	30	0.15	23.385	3.51		
			Total	77.95	41.70		
			Composi	te Coefficient	0.54		
	Contributin	g Flow Rate for Va	rious Storm Fr	equency			
Storm Frequency	Storm Frequency	Rainfall	Intensity	Adjusted Runoff	Runoff Rate - Q		
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)		
10-Year	1	0.1	2.35	0.54	98.00		
25-Year	1.1	0.04	2.72	0.59	124.78		
50-Year	1.2	0.02	3	0.71	165.14		
100-Year	1.25	0.01	3.35	0.88	230.51		
500-Year	-	0.002	-	-	400.93		
Rational Formula							
Q = CIA							

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-7 HY-8 Culvert Analysis Report

Crossing Discharge Data

 $\label{eq:constraint} \text{Discharge Selection Method: Specify Minimum, Design, and Maximum Flow}$

Minimum Flow: 98 cfs

Design Flow: 165 cfs

Maximum Flow: 231 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-7

Headwater Elevation (ft)	Total Discharge (cfs)	CD-7 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
60.98	98.00	98.00	0.00	1
61.12	111.30	111.30	0.00	1
61.28	124.60	124.60	0.00	1
61.45	137.90	137.90	0.00	1
61.65	151.20	151.20	0.00	1
61.86	164.50	164.50	0.00	1
61.86	165.00	165.00	0.00	1
62.33	191.10	191.10	0.00	1
62.59	204.40	204.40	0.00	1
62.88	217.70	217.70	0.00	1
63.17	231.00	231.00	0.00	1
68.47	384.40	384.40	0.00	Overtopping

Rating Curve Plot for Crossing: CD-7


Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
98.00	98.00	60.98	3.115	4.481	4-FFf	1.960	2.096	4.000	4.000	3.899	0.000
111.30	111.30	61.12	3.370	4.621	4-FFf	2.115	2.240	4.000	4.000	4.428	0.000
124.60	124.60	61.28	3.621	4.778	4-FFf	2.270	2.377	4.000	4.000	4.958	0.000
137.90	137.90	61.45	3.873	4.953	4-FFf	2.426	2.505	4.000	4.000	5.487	0.000
151.20	151.20	61.65	4.132	5.146	4-FFf	2.586	2.629	4.000	4.000	6.016	0.000
164.50	164.50	61.86	4.401	5.356	4-FFf	2.754	2.745	4.000	4.000	6.545	0.000
165.00	165.00	61.86	4.411	5.364	4-FFf	2.760	2.749	4.000	4.000	6.565	0.000
191.10	191.10	62.33	4.985	5.830	4-FFf	3.142	2.959	4.000	4.000	7.604	0.000
204.40	204.40	62.59	5.305	6.094	4-FFf	4.000	3.058	4.000	4.000	8.133	0.000
217.70	217.70	62.88	5.647	6.375	4-FFf	4.000	3.151	4.000	4.000	8.662	0.000
231.00	231.00	63.17	6.012	6.674	4-FFf	4.000	3.239	4.000	4.000	9.191	0.000

Table 2 - Culvert Summary Table: CD-7

Straight Culvert

Inlet Elevation (invert): 56.50 ft, Outlet Elevation (invert): 56.00 ft

Culvert Length: 129.00 ft, Culvert Slope: 0.0039

Culvert Performance Curve Plot: CD-7



Water Surface Profile Plot for Culvert: CD-7



Site Data - CD-7

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 56.50 ft Outlet Station: 129.00 ft Outlet Elevation: 56.00 ft Number of Barrels: 2

Culvert Data Summary - CD-7

Barrel Shape: Circular Barrel Diameter: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-7)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
98.00	60.50	4.00
111.30	60.50	4.00
124.60	60.50	4.00
137.90	60.50	4.00
151.20	60.50	4.00
164.50	60.50	4.00
165.00	60.50	4.00
191.10	60.50	4.00
204.40	60.50	4.00
217.70	60.50	4.00
231.00	60.50	4.00

Tailwater Channel Data - CD-7

Tailwater Channel Option:Enter Constant Tailwater ElevationConstant Tailwater Elevation:60.50 ft

Roadway Data for Crossing: CD-7

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 68.47 ft Roadway Surface: Paved Roadway Top Width: 84.00 ft

Cross Drain 8

CD-8 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-8.

Flow Rate 10 =	133 ft ³ /s
Flow Rate 25 =	169 ft ³ /s
Flow Rate 50 =	223 ft ³ /s
Flow Rate 100 =	309 ft ³ /s
Flow Rate 500 =	535 ft ³ /s
Pipe Length =	447 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	7.80 ft
D =	93.615 in
A =	47.80 ft ²
Proposed Size =	1-10'x5' CBC

TIME OF CONCENTRATION

PROJECT TITLE: LOCATION : BASIN NAME:	STATE ROAD NO. 408 EAST ORANGE COUNTY CD-8	ERN EXTENSIC	DN		NU	JMBER: FILE:		
C	ONDITIONS	COMPUTER	VARIABLE	Water	Resource	s Group	Date	
Pre-Development	X	Tīdc	X	Computed	By	KS	09/0	5/17
Post-Development		T	dt	Checked E	3y	CR		
Rainfall Zone:	7	Frequency:						
SHEET FLOW	(Applicable To T⊡dc⊡Only)							
	DIDTION (table 5.4)		Segment ID					
2) MANNNING'S P	RIPTION (lable 5-4)	051)		0.36				
	$[1]$ (TOTAL L \leq - 300 ft)	e J-4)	ft	300				
4) HIGH ELEVATION	[L] (101AL L = 300 R)		ft	68.0				
5) I OW FLEVATION	י, [ה] ו [B]		ft	67.0				
6) TWO YEAR 24-hr			in	4.92				
7) LAND SLOPE. [s]			ft/ft	0.003				
8) COMPUTE T dt	T⊡dt□ = (.007*(n*L)^0.8)/(P^0.	5 * s^0.4)	hr	1.315	+		1.3	315
,		,				min =	7	'8.9
SHALLOW C	ONCENTRATED FLOW							
			Segment ID					
9) SURFACE DESC	RIPTION Enter 1 (Paved) or 2	(Unpaved)	Ū	1				
10) FLOW LENGTH,	[L]		ft	2300				
11) HIGH ELEVATIO	DN, [C]			67.0				
12) LOW ELEVATIO	N, [D]			50.0				
13) WATERCOURS	E SLOPE, [s]		ft/ft	0.0074				
14) AVERAGE VELC	DCITY, [V] **		ft/sec	1.75	_			
15) COMPUTE T dt	∃ Tīdt□ = L / 3600*V		hr	0.37	+	=	C).37
						min =	2	21.9
			Segment ID					
16) CROSS SECTION	NAL FLOW AREA [2]		ft^2					
17) WETTED PERIM			ft					
18) HYDRAULIC RA	DIUS $[r] = a / P dw \square$		ft					
19) FLOW LENGTH			ft					
20) HIGH ELEVATIO	N. [D]		ft					
21) LOW ELEVATIO	N, [E]		ft					
22) CHANNEL SLOP	PE, [s]		ft/ft					
23) MANNNING'S F	ROUGHNESS COEFF., [n]							
24) COMPUTE V:	V = (1.49*r^2/3 * s^1/2) / n		ft/sec					
25) COMPUTE T dt	∃ Tīdt□ = L / 3600*V		hr			=		
						min =		0.0
					TOTAL	IIME (hr)	1	.68
** Reference: FDOT	Drainage Manual Chapter 5.5,	FR-55 Chapter 3	& APP-F.		TOTAL	TIME (min)	10	0.8

CD-8 Rational Method									
Runoff Coefficient Calculations									
Land Use	Land Use Slope Land Cover (%) Runoff Area (acre) - A Product								
			Coefficient						
Residential	0-2%	5	0.45	6.072	2.73				
Commercial	0-2%	40	0.95	48.576	46.15				
Lawn flat 2%	0-2%	25	0.20	30.36	6.07				
Woods/Wetlands	0-2%	30	0.15	36.432	5.46				
			Total	121.44	60.42				
			Compos	ite Coefficient	0.50				
	Contributin	g Flow Rate for Va	arious Storm F	requency					
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q				
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)				
10-Year	1	0.1	2.2	0.50	132.92				
25-Year	1.1	0.04	2.55	0.55	169.47				
50-Year	1.2	0.02	2.8	0.66	223.30				
100-Year	1.25	0.01	3.1	0.82	309.03				
500-Year	-	0.002	-	-	534.59				
Rational Formula									
		Q = CIA							

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-8 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 133 cfs

Design Flow: 223 cfs

Maximum Flow: 309 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-8

Headwater Elevation (ft)	Total Discharge (cfs)	CD-8 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
53.78	133.00	133.00	0.00	1
53.85	150.60	150.60	0.00	1
53.94	168.20	168.20	0.00	1
54.03	185.80	185.80	0.00	1
54.14	203.40	203.40	0.00	1
54.25	221.00	221.00	0.00	1
54.27	223.00	223.00	0.00	1
54.51	256.20	256.20	0.00	1
54.65	273.80	273.80	0.00	1
54.80	291.40	291.40	0.00	1
54.96	309.00	309.00	0.00	1
84.68	1356.63	1356.63	0.00	Overtopping

Rating Curve Plot for Crossing: CD-8



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
133.00	133.00	53.78	3.008	5.269	4-FFf	2.270	1.764	5.000	5.000	2.660	0.000
150.60	150.60	53.85	3.259	5.344	4-FFf	2.473	1.917	5.000	5.000	3.012	0.000
168.20	168.20	53.94	3.501	5.430	4-FFf	2.671	2.063	5.000	5.000	3.364	0.000
185.80	185.80	54.03	3.735	5.524	4-FFf	2.865	2.205	5.000	5.000	3.716	0.000
203.40	203.40	54.14	3.963	5.628	4-FFf	3.054	2.342	5.000	5.000	4.068	0.000
221.00	221.00	54.25	4.186	5.742	4-FFf	3.240	2.475	5.000	5.000	4.420	0.000
223.00	223.00	54.27	4.211	5.755	4-FFf	3.261	2.490	5.000	5.000	4.460	0.000
256.20	256.20	54.51	4.621	5.997	4-FFf	3.603	2.732	5.000	5.000	5.124	0.000
273.80	273.80	54.65	4.837	6.138	4-FFf	3.780	2.855	5.000	5.000	5.476	0.000
291.40	291.40	54.80	5.052	6.289	4-FFf	3.956	2.977	5.000	5.000	5.828	0.000
309.00	309.00	54.96	5.269	6.450	4-FFf	5.000	3.095	5.000	5.000	6.180	0.000

Table 2 - Culvert Summary Table: CD-8

Straight Culvert

Inlet Elevation (invert): 48.51 ft, Outlet Elevation (invert): 48.00 ft

Culvert Length: 447.00 ft, Culvert Slope: 0.0011

Culvert Performance Curve Plot: CD-8



Water Surface Profile Plot for Culvert: CD-8



Site Data - CD-8

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 48.51 ft Outlet Station: 447.00 ft Outlet Elevation: 48.00 ft Number of Barrels: 1

Culvert Data Summary - CD-8

Barrel Shape: Concrete Box Barrel Span: 10.00 ft Barrel Rise: 5.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-8)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
133.00	53.51	5.00
150.60	53.51	5.00
168.20	53.51	5.00
185.80	53.51	5.00
203.40	53.51	5.00
221.00	53.51	5.00
223.00	53.51	5.00
256.20	53.51	5.00
273.80	53.51	5.00
291.40	53.51	5.00
309.00	53.51	5.00

Tailwater Channel Data - CD-8

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 53.51 ft

Roadway Data for Crossing: CD-8

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 84.68 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 9

CD-9 Preliminary Culvert Sizing

The calculated flow rate for a 100-year storm event, determined by the Rational Method, was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-9.

Flow Rate 10 =	92 1	ft ³ /s
Flow Rate 25 =	117 1	ft ³ /s
Flow Rate 50 =	153 1	ft ³ /s
Flow Rate 100 =	212 1	ft ³ /s
Flow Rate 500 =	364 1	ft ³ /s
Pipe Length =	300 1	ft
Change in FL Elevation from		
Upstream to Downstream =	0.50 1	ft
Manning's "n" value =	0.012	
D= (2.159 Qn/S ^{0.5}) ^{3/8}		

D =	6.28 ft
D =	75.397 in
A =	31.006 ft ²
Proposed Size =	1-72" RCP

TIME OF CONCENTRATION

PROJECT TITLE: LOCATION : BASIN NAME:	STATE ROAD NO. 408 EAST ORANGE COUNTY CD-9	ERN EXTENSIO	N		NUMBER: FILE:	
C	ONDITIONS	COMPUTE		Water Res	ources Group	Date
Pre-Development		T⊡dc	X	Computed By	KS	09/05/17
Post-Development		Т	dt	Checked By	CR	
Rainfall Zone:	7	Frequency:				1
SHEET FLOW	【 (Applicable To T⊡c⊡Only)					
			Segment ID			
2) MANNNING'S P	RIPTION (lable 5-4)	051)		0.41		
	$[1]$ (TOTAL L \leq 300 ft)	e J-4)	ft	300		
4) HIGH ELEVATION	[L] (101AL L = 300 R)		ft	67.0		
5) I OW FLEVATION	י, [ה] ו (B)		ft	66.0		
6) TWO YEAR 24-hr			in	4.92		
7) I AND SI OPE [s]	·····		ft/ft	0.003		
8) COMPUTE Tott	T⊡dt□ = (.007*(n*L)^0.8)/(P^0.	5 * s^0.4)	hr	1.441 +		1.441
-,					min =	86.5
SHALLOW C	ONCENTRATED FLOW					L
			Segment ID			
9) SURFACE DESC	RIPTION Enter 1 (Paved) or 2	(Unpaved)	0	2		
10) FLOW LENGTH,	[L]		ft	1665		
11) HIGH ELEVATIO	DN, [C]			66.0		
12) LOW ELEVATIO	N, [D]			38.0		
13) WATERCOURS	E SLOPE, [s]		ft/ft	0.0168		
14) AVERAGE VELC	DCITY, [V] **		ft/sec	2.09		
15) COMPUTE T dt	I Tīdt□ = L / 3600*V		hr	0.22 +	=	0.22
CHANNEL FLOW					min =	13.3
	-		Segment ID			
16) CROSS SECTION	ONAL FLOW AREA, [a]		ft^2			
17) WETTED PERIN	1ETER, [Pīdwí]		ft			
18) HYDRAULIC RA	.DIUS, [r] = a / P⊡dw⊡		ft			
19) FLOW LENGTH	, [L]		ft			
20) HIGH ELEVATIO	DN, [D]		ft			
21) LOW ELEVATIO	N, [E]		ft			
22) CHANNEL SLOP	PE, [s]		ft/ft			
23) MANNNING'S F	OUGHNESS COEFF., [n]					
24) COMPUTE V:	$V = (1.49^{\circ}r^{2}/3^{\circ}s^{*}1/2) / n$		ft/sec			
25) COMPUTE LOU	$1 \text{ L}(1) = L / 3000^{\circ} \text{ V}$		nr		=	0.0
						0.0
				тс	TAL TIME (br)	1 66
** Reference: FDOT	Drainage Manual Chapter 5.5	TR-55 Chapter 3	& APP-F	тс	TAL TIME (min)	99.7
	Eranago manaa Onaptor 0.0,	oo onapior c	· · · · · · · · · · · · · · · · · · ·	10		55.1

CD-9 Rational Method									
Runoff Coefficient Calculations									
Land Use Slope Land Cover (%) Runoff Area (acre) - A Product									
			Coefficient						
Residential	0-2%	5	0.45	3.79	1.71				
Commercial	0-2%	45	0.95	34.12	32.41				
Lawn flat 2%	0-2%	25	0.20	18.96	3.79				
Woods/Wetlands	0-2%	25	0.15	18.96	2.84				
			Total	75.82	40.75				
			Compos	site Coefficient	0.54				
	Contributin	g Flow Rate for Va	arious Storm F	requency					
Storm Frequency	Storm Frequency	Rainfall	Intensity - I	Adjusted Runoff	Runoff Rate - Q				
	Factor	Frequency	(in/hr)	Coefficient - C	(cfs)				
10-Year	1	0.1	2.25	0.54	91.69				
25-Year	1.1	0.04	2.6	0.59	116.55				
50-Year	1.2	0.02	2.85	0.71	153.31				
100-Year	1.25	0.01	3.15	0.89	211.82				
500-Year	-	0.002	-	-	364.25				
Rational Formula									
		Q = CIA							

** The "Adjusted Runoff Coefficient" will need to be corrected during the final design. The storm frequency factor should be multiplied by the raw 10-year composite coefficient for each storm event.



CD-9 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow Minimum Flow: 92 cfs Design Flow: 153 cfs Maximum Flow: 212 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-9 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
42.87	92.00	92.00	0.00	1
42.97	104.00	104.00	0.00	1
43.08	116.00	116.00	0.00	1
43.21	128.00	128.00	0.00	1
43.35	140.00	140.00	0.00	1
43.50	152.00	152.00	0.00	1
43.51	153.00	153.00	0.00	1
43.84	176.00	176.00	0.00	1
44.03	188.00	188.00	0.00	1
44.23	200.00	200.00	0.00	1
44.45	212.00	212.00	0.00	1
54.79	532.70	532.70	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-9

Rating Curve Plot for Crossing: CD-9



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
92.00	92.00	42.87	3.698	6.367	4-FFf	2.889	2.572	6.000	6.000	3.254	0.000
104.00	104.00	42.97	3.989	6.468	4-FFf	3.108	2.747	6.000	6.000	3.678	0.000
116.00	116.00	43.08	4.265	6.583	4-FFf	3.325	2.909	6.000	6.000	4.103	0.000
128.00	128.00	43.21	4.529	6.710	4-FFf	3.542	3.060	6.000	6.000	4.527	0.000
140.00	140.00	43.35	4.784	6.849	4-FFf	3.764	3.206	6.000	6.000	4.951	0.000
152.00	152.00	43.50	5.034	7.001	4-FFf	3.991	3.345	6.000	6.000	5.376	0.000
153.00	153.00	43.51	5.055	7.014	4-FFf	4.011	3.356	6.000	6.000	5.411	0.000
176.00	176.00	43.84	5.527	7.341	4-FFf	4.496	3.612	6.000	6.000	6.225	0.000
188.00	188.00	44.03	5.775	7.531	4-FFf	6.000	3.741	6.000	6.000	6.649	0.000
200.00	200.00	44.23	6.026	7.732	4-FFf	6.000	3.862	6.000	6.000	7.074	0.000
212.00	212.00	44.45	6.284	7.946	4-FFf	6.000	3.980	6.000	6.000	7.498	0.000

Table 2 - Culvert Summary Table: CD-9

Straight Culvert

Inlet Elevation (invert): 36.50 ft, Outlet Elevation (invert): 36.00 ft

Culvert Length: 300.00 ft, Culvert Slope: 0.0017

Culvert Performance Curve Plot: CD-9



Water Surface Profile Plot for Culvert: CD-9



Site Data - CD-9

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 36.50 ft Outlet Station: 300.00 ft Outlet Elevation: 36.00 ft Number of Barrels: 1

Culvert Data Summary - CD-9

Barrel Shape: Circular Barrel Diameter: 6.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-9)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
92.00	42.50	6.00
104.00	42.50	6.00
116.00	42.50	6.00
128.00	42.50	6.00
140.00	42.50	6.00
152.00	42.50	6.00
153.00	42.50	6.00
176.00	42.50	6.00
188.00	42.50	6.00
200.00	42.50	6.00
212.00	42.50	6.00

Tailwater Channel Data - CD-9

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 42.50 ft

Roadway Data for Crossing: CD-9

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 54.79 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 10

CD-10 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-10.

Flow Rate 10 =	265 ft ³ /s
Flow Rate 25 =	312 ft ³ /s
Flow Rate 50 =	353 ft ³ /s
Flow Rate 100 =	398 ft ³ /s
Flow Rate 500 =	530 ft ³ /s
Pipe Length =	310 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	

8.01 ft
96.11 in
50.38 ft ²
2-6'x4' CBC



CD-10 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 265 cfs

Design Flow: 353 cfs

Maximum Flow: 398 cfs

Headwater Elevation (ft)	Total Discharge (cfs)	CD-10 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
43.19	265.00	265.00	0.00	1
43.31	278.30	278.30	0.00	1
43.44	291.60	291.60	0.00	1
43.58	304.90	304.90	0.00	1
43.72	318.20	318.20	0.00	1
43.86	331.50	331.50	0.00	1
44.02	344.80	344.80	0.00	1
44.11	353.00	353.00	0.00	1
44.34	371.40	371.40	0.00	1
44.51	384.70	384.70	0.00	1
44.69	398.00	398.00	0.00	1
55.97	896.98	896.98	0.00	Overtopping

Table 1 - Summary of Culvert Flows at Crossing: CD-10

Rating Curve Plot for Crossing: CD-10



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
265.00	265.00	43.19	4.210	5.190	4-FFf	3.199	2.474	4.000	4.000	5.521	0.000
278.30	278.30	43.31	4.364	5.313	4-FFf	3.321	2.556	4.000	4.000	5.798	0.000
291.60	291.60	43.44	4.519	5.441	4-FFf	3.441	2.637	4.000	4.000	6.075	0.000
304.90	304.90	43.58	4.677	5.576	4-FFf	3.561	2.717	4.000	4.000	6.352	0.000
318.20	318.20	43.72	4.838	5.716	4-FFf	3.680	2.795	4.000	4.000	6.629	0.000
331.50	331.50	43.86	5.001	5.863	4-FFf	3.799	2.872	4.000	4.000	6.906	0.000
344.80	344.80	44.02	5.169	6.015	4-FFf	4.000	2.949	4.000	4.000	7.183	0.000
353.00	353.00	44.11	5.274	6.112	4-FFf	4.000	2.995	4.000	4.000	7.354	0.000
371.40	371.40	44.34	5.515	6.338	4-FFf	4.000	3.099	4.000	4.000	7.737	0.000
384.70	384.70	44.51	5.695	6.509	4-FFf	4.000	3.172	4.000	4.000	8.015	0.000
398.00	398.00	44.69	5.880	6.685	4-FFf	4.000	3.245	4.000	4.000	8.292	0.000

Table 2 - Culvert Summary Table: CD-10

Straight Culvert

Inlet Elevation (invert): 38.00 ft, Outlet Elevation (invert): 37.50 ft

Culvert Length: 310.00 ft, Culvert Slope: 0.0016

Culvert Performance Curve Plot: CD-10







Site Data - CD-10

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 38.00 ft Outlet Station: 310.00 ft Outlet Elevation: 37.50 ft Number of Barrels: 2

Culvert Data Summary - CD-10

Barrel Shape: Concrete Box Barrel Span: 6.00 ft Barrel Rise: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-10)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
265.00	42.00	4.00
278.30	42.00	4.00
291.60	42.00	4.00
304.90	42.00	4.00
318.20	42.00	4.00
331.50	42.00	4.00
344.80	42.00	4.00
353.00	42.00	4.00
371.40	42.00	4.00
384.70	42.00	4.00
398.00	42.00	4.00

Tailwater Channel Data - CD-10

Tailwater Channel Option:Enter Constant Tailwater ElevationConstant Tailwater Elevation:42.00 ft

Roadway Data for Crossing: CD-10

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 55.97 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 11

CD-11 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-11.

6.71 ft² 2-24" RCP

Flow Rate 10 =	14 ft ³ /s
Flow Rate 25 =	18 ft ³ /s
Flow Rate 50 =	21 ft ³ /s
Flow Rate 100 =	24 ft ³ /s
Flow Rate 500 =	35 ft ³ /s
Pipe Length =	395 ft
Change in FL Elevation from Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	2.92 ft
D =	35.08 in

A =

Proposed Size =



CD-11 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 14 cfs

Design Flow: 21 cfs

Maximum Flow: 24 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-11

Headwater Elevation (ft)	Total Discharge (cfs)	CD-11 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
58.44	14.00	14.00	0.00	1
58.50	15.00	15.00	0.00	1
58.57	16.00	16.00	0.00	1
58.64	17.00	17.00	0.00	1
58.72	18.00	18.00	0.00	1
58.80	19.00	19.00	0.00	1
58.89	20.00	20.00	0.00	1
58.98	21.00	21.00	0.00	1
59.08	22.00	22.00	0.00	1
59.18	23.00	23.00	0.00	1
59.28	24.00	24.00	0.00	1
83.94	107.98	107.98	0.00	Overtopping

Rating Curve Plot for Crossing: CD-11


Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
14.00	14.00	58.44	1.370	2.436	4-FFf	1.320	0.939	2.000	2.000	2.228	0.000
15.00	15.00	58.50	1.429	2.501	4-FFf	1.391	0.974	2.000	2.000	2.387	0.000
16.00	16.00	58.57	1.486	2.570	4-FFf	1.467	1.006	2.000	2.000	2.546	0.000
17.00	17.00	58.64	1.542	2.643	4-FFf	1.552	1.038	2.000	2.000	2.706	0.000
18.00	18.00	58.72	1.597	2.721	4-FFf	2.000	1.069	2.000	2.000	2.865	0.000
19.00	19.00	58.80	1.651	2.803	4-FFf	2.000	1.098	2.000	2.000	3.024	0.000
20.00	20.00	58.89	1.705	2.890	4-FFf	2.000	1.126	2.000	2.000	3.183	0.000
21.00	21.00	58.98	1.758	2.981	4-FFf	2.000	1.158	2.000	2.000	3.342	0.000
22.00	22.00	59.08	1.812	3.077	4-FFf	2.000	1.186	2.000	2.000	3.501	0.000
23.00	23.00	59.18	1.865	3.177	4-FFf	2.000	1.213	2.000	2.000	3.661	0.000
24.00	24.00	59.28	1.919	3.282	4-FFf	2.000	1.239	2.000	2.000	3.820	0.000

Table 2 - Culvert Summary Table: CD-11

Straight Culvert

Inlet Elevation (invert): 56.00 ft, Outlet Elevation (invert): 55.50 ft

Culvert Length: 395.00 ft, Culvert Slope: 0.0013

Culvert Performance Curve Plot: CD-11





Water Surface Profile Plot for Culvert: CD-11

Site Data - CD-11

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 56.00 ft Outlet Station: 395.00 ft Outlet Elevation: 55.50 ft Number of Barrels: 2

Culvert Data Summary - CD-11

Barrel Shape: Circular Barrel Diameter: 2.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-11)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
14.00	58.00	2.00
15.00	58.00	2.00
16.00	58.00	2.00
17.00	58.00	2.00
18.00	58.00	2.00
19.00	58.00	2.00
20.00	58.00	2.00
21.00	58.00	2.00
22.00	58.00	2.00
23.00	58.00	2.00
24.00	58.00	2.00

Tailwater Channel Data - CD-11

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 58.00 ft

Roadway Data for Crossing: CD-11

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 83.94 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 12

CD-12 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-12.

Flow Rate 10 =	299 ft ³ /s
Flow Rate 25 =	340 ft ³ /s
Flow Rate 50 =	373 ft ³ /s
Flow Rate 100 =	409 ft ³ /s
Flow Rate 500 =	510 ft ³ /s
Pipe Length =	522 ft
Change in FL Elevation from	
Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012

D= (2.159 Qn/S^{0.5})^{3/8}

D =	8.92 ft
D =	107.059 in
A =	62.51 ft ²
Proposed Size =	2-8'x4' CBC



CD-12 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 299 cfs

Design Flow: 373 cfs

Maximum Flow: 409 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-12

Headwater Elevation (ft)	Total Discharge (cfs)	CD-12 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
54.01	299.00	299.00	0.00	1
54.09	310.00	310.00	0.00	1
54.17	321.00	321.00	0.00	1
54.25	332.00	332.00	0.00	1
54.33	343.00	343.00	0.00	1
54.42	354.00	354.00	0.00	1
54.51	365.00	365.00	0.00	1
54.57	373.00	373.00	0.00	1
54.70	387.00	387.00	0.00	1
54.79	398.00	398.00	0.00	1
54.89	409.00	409.00	0.00	1
75.36	1405.58	1405.58	0.00	Overtopping

Rating Curve Plot for Crossing: CD-12



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
299.00	299.00	54.01	3.746	5.012	4-FFf	3.200	2.214	4.000	4.000	4.672	0.000
310.00	310.00	54.09	3.840	5.088	4-FFf	3.286	2.267	4.000	4.000	4.844	0.000
321.00	321.00	54.17	3.934	5.166	4-FFf	3.371	2.321	4.000	4.000	5.016	0.000
332.00	332.00	54.25	4.028	5.247	4-FFf	3.456	2.374	4.000	4.000	5.188	0.000
343.00	343.00	54.33	4.123	5.332	4-FFf	3.541	2.426	4.000	4.000	5.359	0.000
354.00	354.00	54.42	4.217	5.418	4-FFf	3.624	2.477	4.000	4.000	5.531	0.000
365.00	365.00	54.51	4.312	5.508	4-FFf	3.708	2.528	4.000	4.000	5.703	0.000
373.00	373.00	54.57	4.382	5.575	4-FFf	3.768	2.565	4.000	4.000	5.828	0.000
387.00	387.00	54.70	4.505	5.695	4-FFf	3.874	2.629	4.000	4.000	6.047	0.000
398.00	398.00	54.79	4.602	5.793	4-FFf	4.000	2.678	4.000	4.000	6.219	0.000
409.00	409.00	54.89	4.701	5.893	4-FFf	4.000	2.728	4.000	4.000	6.391	0.000

Table 2 - Culvert Summary Table: CD-12

Straight Culvert

Inlet Elevation (invert): 49.00 ft, Outlet Elevation (invert): 48.50 ft

Culvert Length: 522.00 ft, Culvert Slope: 0.0010

Culvert Performance Curve Plot: CD-12





Water Surface Profile Plot for Culvert: CD-12

Site Data - CD-12

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 49.00 ft Outlet Station: 522.00 ft Outlet Elevation: 48.50 ft Number of Barrels: 2

Culvert Data Summary - CD-12

Barrel Shape: Concrete Box Barrel Span: 8.00 ft Barrel Rise: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge (90°) Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-12)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
299.00	53.00	4.00
310.00	53.00	4.00
321.00	53.00	4.00
332.00	53.00	4.00
343.00	53.00	4.00
354.00	53.00	4.00
365.00	53.00	4.00
373.00	53.00	4.00
387.00	53.00	4.00
398.00	53.00	4.00
409.00	53.00	4.00

Tailwater Channel Data - CD-12

Tailwater Channel Option: Enter Constant Tailwater Elevation Constant Tailwater Elevation: 53.00 ft

Roadway Data for Crossing: CD-12

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 75.36 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Cross Drain 13

CD-13 Preliminary Culvert Sizing

The flow rate for a 100-year storm event from the Bithlo Area Stormwater Management Master Plan was used to size this culvert. The Manning's Equation was used to produce a trial size for the cross drain. The trial size was used to perform HY-8 analysis. While performing the overtopping analysis, the cross drain was appropriately sized in order to not violate floodplain criteria. The following presents a detailed calculation for sizing CD-13.

1-48" RCP

Flow Rate 10 =	26 ft ³ /s
Flow Rate 25 =	35 ft ³ /s
Flow Rate 50 =	42 ft ³ /s
Flow Rate 100 =	51 ft ³ /s
Flow Rate 500 =	82 ft ³ /s
Pipe Length =	325 ft
Change in FL Elevation from Upstream to Downstream =	0.50 ft
Manning's "n" value =	0.012
D= (2.159 Qn/S ^{0.5}) ^{3/8}	
D =	3.74 ft
D =	44.872 in
A =	10.98 ft ²

Proposed Size =



CD-13 HY-8 Culvert Analysis Report

Crossing Discharge Data

Discharge Selection Method: Specify Minimum, Design, and Maximum Flow

Minimum Flow: 26 cfs

Design Flow: 42 cfs

Maximum Flow: 51 cfs

Table 1 - Summary of Culvert Flows at Crossing: CD-13

Headwater Elevation (ft)	Total Discharge (cfs)	CD-13 Discharge (cfs)	Roadway Discharge (cfs)	Iterations
56.19	26.00	26.00	0.00	1
56.23	28.50	28.50	0.00	1
56.27	31.00	31.00	0.00	1
56.32	33.50	33.50	0.00	1
56.36	36.00	36.00	0.00	1
56.42	38.50	38.50	0.00	1
56.47	41.00	41.00	0.00	1
56.50	42.00	42.00	0.00	1
56.59	46.00	46.00	0.00	1
56.66	48.50	48.50	0.00	1
56.73	51.00	51.00	0.00	1
64.50	173.94	173.94	0.00	Overtopping

Rating Curve Plot for Crossing: CD-13



Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
26.00	26.00	56.19	2.106	4.190	4-FFf	1.774	1.503	4.000	4.000	2.069	0.000
28.50	28.50	56.23	2.233	4.228	4-FFf	1.870	1.578	4.000	4.000	2.268	0.000
31.00	31.00	56.27	2.354	4.270	4-FFf	1.964	1.647	4.000	4.000	2.467	0.000
33.50	33.50	56.32	2.471	4.315	4-FFf	2.058	1.718	4.000	4.000	2.666	0.000
36.00	36.00	56.36	2.583	4.364	4-FFf	2.150	1.786	4.000	4.000	2.865	0.000
38.50	38.50	56.42	2.692	4.416	4-FFf	2.243	1.850	4.000	4.000	3.064	0.000
41.00	41.00	56.47	2.798	4.472	4-FFf	2.335	1.913	4.000	4.000	3.263	0.000
42.00	42.00	56.50	2.840	4.496	4-FFf	2.372	1.937	4.000	4.000	3.342	0.000
46.00	46.00	56.59	3.002	4.594	4-FFf	2.524	2.030	4.000	4.000	3.661	0.000
48.50	48.50	56.66	3.100	4.661	4-FFf	2.621	2.086	4.000	4.000	3.860	0.000
51.00	51.00	56.73	3.197	4.731	4-FFf	2.720	2.139	4.000	4.000	4.058	0.000

Table 2 - Culvert Summary Table: CD-13

Straight Culvert

Inlet Elevation (invert): 52.00 ft, Outlet Elevation (invert): 51.50 ft

Culvert Length: 325.00 ft, Culvert Slope: 0.0015

Culvert Performance Curve Plot: CD-13







Site Data - CD-13

Site Data Option: Culvert Invert Data Inlet Station: 0.00 ft Inlet Elevation: 52.00 ft Outlet Station: 325.00 ft Outlet Elevation: 51.50 ft Number of Barrels: 1

Culvert Data Summary - CD-13

Barrel Shape: Circular Barrel Diameter: 4.00 ft Barrel Material: Concrete Embedment: 0.00 in Barrel Manning's n: 0.0120 Culvert Type: Straight Inlet Configuration: Square Edge with Headwall Inlet Depression: None

Table 3 - Downstream Channel Rating Curve (Crossing: CD-13)

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
26.00	56.00	4.00
28.50	56.00	4.00
31.00	56.00	4.00
33.50	56.00	4.00
36.00	56.00	4.00
38.50	56.00	4.00
41.00	56.00	4.00
42.00	56.00	4.00
46.00	56.00	4.00
48.50	56.00	4.00
51.00	56.00	4.00

Tailwater Channel Data - CD-13

Tailwater Channel Option:Enter Constant Tailwater ElevationConstant Tailwater Elevation:56.00 ft

Roadway Data for Crossing: CD-13

Roadway Profile Shape: Constant Roadway Elevation Crest Length: 100.00 ft Crest Elevation: 64.50 ft Roadway Surface: Paved Roadway Top Width: 136.00 ft

Appendix: H

Design Aids

FDOT Drainage Manual

4.3 DESIGN FREQUENCY

4.3.1 Permanent Facilities

Standard design frequencies for permanent culverts, bridge-culverts, and bridges are as follows:

FACILITY	FREQUENCY
Mainline Interstate	50 years
High Use or Essential: Projected 20-year AADT [*] > 1,500	50 years
Other: Projected 20-year AADT [*] < 1,500	25 years
Roadside ditch culvertsPedestrian and trail bridges	10 years

Table 4.1: Design Storm Frequencies of Permanent Facilities

* AADT preferred but if not available ADT may be used.

Note: The flood frequencies used for scour analysis differ. See Section 4.9.2.

4.3.2 Temporary Facilities

Design temporary traversing works accounting for the permitted duration of the work. Temporary traversing work will cause no more than a one-foot increase in the Design Storm Frequency (DSF) flood elevation immediately upstream and no more than one tenth of a foot increase in the DSF flood elevation 500 feet upstream.

Minimum standard design frequencies for temporary culverts, bridge-culverts, and bridges are as follows:

Drainage Manual IDF Curves



FDOT Drainage Design Guide

4.7.2 Small Cross Drains

This information applies to cross drains having an area of opening up through a 48-inchdiameter round culvert or the equivalent.

• Conduct hydrologic analysis

Estimate discharges for design year frequency, base flood, and greatest flood. Use one of the following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Rational Equation (up to 600 acres)
- Regional or Local Regression Equation
- Select trial culvert size based on the following:

$$A = Q/V$$

Where:

- A = Culvert area (square feet)
- Q = Design discharge (e.g., 50 year)
- V = Average velocity (feet per second); use an average velocity of four feet per second
 - Estimate tailwater. If the outlet is in a free-flowing condition, the crown of the pipe at the outlet may be assumed.
 - **Conduct hydraulic analysis** using techniques provided in FHWA HDS 5. Compute headwater conditions for the selected size for the design flood, base flood, and greatest flood or overtopping flood as appropriate.
 - **Check hydraulic results** against design standards for backwater, minimum size, and scour. If these standards are satisfied, the trial culvert size is acceptable.
 - **Determine the most economical culvert size** that satisfies all standards. If the trial selected size does not satisfy all design standards, obtain a variance.
 - Document as required in the Drainage Manual.

Example 4.7-3 illustrates this procedure.

Example 4.7-3—Design of Small Cross Drain

Referring back to Example 4.7-2, you determined that the two-foot x two-foot concrete box culvert should be replaced. A design frequency of 50 years was determined as the minimum for this roadway. The existing length of the two-foot x two-foot concrete box culvert was 50 feet. However, since the structure will have to be extended four feet on each side, the design length of the proposed structure will be 58 feet.

Proposed Elevations are as follows: Allowable headwater (edge of travel lane) = 104.6 ft Flow line (upstream) = 100.1 ft Flow line (downstream) = 99.7 ft

• Conduct hydrologic analysis

Estimate discharges for design-year frequency, base flood, and greatest flood. Use one of following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Rational Equation (up to 600 acres)
- Regional or Local Regression Equation

Use the same discharges from Example 4.7-2:

 $Q(50) = 35 \text{ ft}^3/\text{sec}$ $Q(100) = 52 \text{ ft}^3/\text{sec}$ $Q(500) = 88 \text{ ft}^3/\text{sec}$

• Select trial culvert size

$$A = \frac{Q}{V} = \frac{35 \ ft^3/s}{4 \ ft/s} = 8.8 \ ft^2$$

D = 3.3 ft., so try D = 36-inch pipe and 42-inch pipe

• Conduct hydraulic analysis using FHWA HDS 5 procedures.

The hydraulic analysis would be similar to what was done in Example 4.7-1 and Example 4.7-2. A worksheet of the calculations for the 50-year frequency is shown in Figure 4.7-3. The other frequencies also would need to be analyzed for an actual project. The analysis shown in Figure 4.7-3 is for the proposed conditions.

• Check hydraulic results against design standards.

Review of the worksheet in Figure 4.7-3 indicates that the roadway will not overtop for the 50-year frequency for either culvert size. There is very little difference between the 36-inch and 42 inch pipe as far as controlling headwater. Therefore, either pipe size would be adequate. However, it is recommended that the 36-inch pipe be installed since it would be slightly less in cost than the 42-inch pipe. In addition, it would be recommended that a rubble ditch lining design be installed at the outlet end due to velocities exceeding six feet per second.

• If design does not meet standards or if you can use more economical culvert size that satisfies the standards, then perform new computations for that design.

Document as required in the *Drainage Manual*.

4.7.3 Large Cross Drains

This information applies to cross drains having an area of opening greater than a 48-inch diameter pipe and less than a 20-foot bridge. The procedure for large cross drains is similar to that for small cross drains except that a greater level of effort and detail is expected in developing the hydrologic estimates and the determination of tailwater conditions.

• Conduct hydrologic analysis

Estimate discharges for design-year frequency, base flood, and greatest flood. Use one of following procedures as appropriate (see Section 4.7 of the *Drainage Manual*):

- Frequency analysis of observed conditions
- Regional or Local Regression Equation
- Rational Equation (up to 600 acres)

The remaining steps are the same as those identified in Section 4.7.2 for small cross drains.

	<u>Value</u>	Recommended <u>Range of Values</u>
Concrete	0.011	0.010 - 0.013
Asphalt	0.012	0.010 - 0.015
Bare sand ^a	0.010	0.010 - 0.016
Graveled surface ^a	0.012	0.012 - 0.030
Bare clav-loam (eroded) ^a	0.012	0.012 - 0.033
Fallow (no residue) ^b	0.05	0.006 - 0.16
Chisel plow (<1/4 tons/acre residue)	0.07	0.006 - 0.17
Chisel plow (1/4 - 1 tons/acre residue)	0.18	0.070 - 0.34
Chisel plow (1 - 3 tons/acre residue)	0.30	0.190 - 0.47
Chisel plow (>3 tons/acre residue)	0.40	0.340 - 0.46
Disk/Harrow (<1/4 tons/acre residue)	0.08	0.008 - 0.41
Disk/Harrow (1/4 - 1 tons/acre residue)	0.16	0.100 - 0.25
Disk/Harrow (1 - 3 tons/acre residue)	0.25	0.140 - 0.53
Disk/Harrow (>3 tons/acre residue)	0.30	
No till (4 tons/acre residue)</td <td>0.04</td> <td>0.030 - 0.07</td>	0.04	0.030 - 0.07
No till (1/4 - 1 tons/acre residue)	0.07	0.010 - 0.13
No till (1 - 3 tons/acre residue)	0.30	0.160 - 0.47
Plow (Fall)	0.06	0.020 - 0.10
Coulter	0.10	0.050 - 0.13
Range (natural)	0.13	0.010 - 0.32
Range (clipped)	0.08	0.020 - 0.24
Grass (bluegrass sod)	0.45	0.390 - 0.63
Short grass prairie ^a	0.15	0.100 - 0.20
Dense grass ^c	0.24	0.170 - 0.30
Bermuda grass ^c	0.41	0.300 - 0.48
Woods	0.45	

Table B-1: Overland Flow Manning's n Values

All values are from Engman (1983), unless noted otherwise.

^aWoolhiser (1975).

^bFallow has been idle for one year and is fairly smooth.

^CPalmer (1946). Weeping love grass, bluegrass, buffalo grass, blue gamma grass, native grass mix (OK), alfalfa, lespedeza.

Note: These values were determined specifically for overland flow conditions and are not appropriate for conventional open channel flow calculations. See Chapter 3, for open channel flow procedures.

Table B-5: Design Storm Frequency Factors for Pervious Area Runoff Coefficients*

Return Period (years)	Design Storm <u>Frequency Factor, X_T</u>
2 to 10	1.0
25	1.1
50	1.2
100	1.25

Reference: Wright-McLaughlin Engineers (1969).

* DUE TO THE INCREASE IN THE DURATION TIME THAT THE PEAK OR NEAR PEAK DISCHARGE RATE IS RELEASED FROM STORMWATER MANAGEMENT SYSTEMS, THE USE OF THESE SHORT DURATION PEAK RATE DISCHARGE ADJUSTMENT FACTORS IS NOT APPROPRIATE FOR FLOOD ROUTING COMPUTATIONS.

Appendix: I

Big Econ River Basin Stormwater Management Master Plan



CDM

Table 5-1 Big Econ Stormwater Management Master Plan Orange County, Florida Existing Conditions Results

						Mean Ann	ual		10 Year - 24 Hour					25 Year - 24	Hour	100 Year - 24 Hour					
Model ID	U/S Node	D/S Node	Critical Elevation ¹	Location	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	Comments
BEBE010C	BEBE010N	BEBE015N	65.8	Wewahootee Road	62.4	61.8	-	89	63.9	62.3		170	64.5	62.4		197	65.2	62.5		224	
BEBE011C	BEBE010N	BEBE015N	65.8	Wewahootee Road	62.4	61.8		172	63.9	62.3	-	347	64.5	62.4	-	416	65.2	62.5		498	
BEBE010W	BEBE010N	BEBE015N	65.8	Wewahootee Road - Overflow	62.4	61.8		0	63.9	62.3		0	64.5	62.4		0	65.2	62.5		0	
BEBE015X	BEBE015N	BEBE020N	57.6		61.8	55.2		393	62.3	56.8		732	62.4	57.3		863	62.5	58.1	0.5	1011	
BEBE020X	BEBE020N	BEBE025N	62.1	Beeline Bridge Equivalent	55.2	55.2	-	998	56.8	56.8		1967	57.3	57.3		2338	58.1	58.1		3067	
BEBE020W	BEBE020N	BEBE025N	62.15	Beeline - Overflow	55.2	55.2		0	56.8	56.8	-	0	57.3	57.3	-	0	58.1	58.1		0	
BEBE025X	BEBE025N	BEBE030N	56.6		55.2	53.8		992	56.8	55.8	-	1931	57.3	56.4		2291	58.1	57.2	0.5	3023	
BEBE030X	BEBE030N	BEBE035N	57.4		53.8	53.6	-	971	55.8	55.7	•	1861	56.4	56.3	•	2186	57.2	57.0		2961	
BEBE035X	BEBE035N	BEBE040N	50.2		53.6	52.5	2.3	2300	55.7	54.8	4.6	4418	56.3	55.4	5.2	5169	57.0	56.1	5.9	6007	Hal Scott - flooding not a problem
BEBE040X	BEBE040N	BEBE045N	49.8		52.5	52.1	2.3	2371	54.8	54.2	4.4	4758	55.4	54.8	5.0	5638	56.1	55.5	5.7	6735	Hal Scott - flooding not a problem
BEBE045X	BEBE045N	BEBE050N	48.3		52.1	45.5		2519	54.2	48.1	-	5187	54.8	48.8	0.5	6181	55.5	49.8	1.5	7516	Hal Scott - flooding not a problem
BEBE050X	BEBE050N	BEBE055N	47		45.5	44.7	-	2529	48.1	47.4	0.4	5310	48.8	48.1	1.1	6360	49.8	49.2	2.2	7843	Hal Scott - flooding not a problem
BEBE055X	BEBE055N	BEBE060N	43.1		44.7	44.6	1.5	2813	47.4	47.2	4.1	5700	48.1	47.9	4.8	6883	49.2	49.0	5.9	8642	Hal Scott - flooding not a problem
BEBE05X	BEBE05LK	BEBE255N	49.2		47.6	46.3		18	48.4	47.5	•	48	48.7	47.8	-	60	49.2	48.5		83	Hal Scott - flooding not a problem
BEBE060X	BEBE060N	BEBE065N	37.4		44.6	44.6	7.2	2967	47.2	47.2	9.8	6150	47.9	47.9	10.5	7360	49.0	49.0	11.6	9211	Hal Scott - flooding not a problem
BEBE065C	BEBE065N	BEBE070N	44.7	Powerline Bridge Equivalent	44.6	44.5	•	178	47.2	47.2	2.5	186	47.9	47.9	3.2	188	49.0	49.0	4.3	159	Hal Scott - flooding not a problem
BEBE065W	BEBE065N	BEBE070N	44.7	Powerline Overflow	44.6	44.5	· ·	0	47.2	47.2	2.5	419	47.9	47.9	3.2	492	49.0	49.0	4.3	542	Hal Scott - flooding not a problem
BEBE065X	BEBE065N	BEBE070N	44.7		44.6	44.5	· · · ·	2779	47.2	47.2	2.5	5606	47.9	47.9	3.2	6766	49.0	49.0	4.3	8661	Hal Scott - flooding not a problem
BEBE070X	BEBE070N	BEBE075N	44.8		44.5	44.4		2900	47.2	47.0	2.2	6086	47.9	47.8	3.0	7302	49.0	48.8	4.0	9145	Hal Scott - flooding not a problem
BEBE075X	BEBE075N	BEBE080N	43.4		44.4	44.1	0.7	3025	47.0	46.6	3.2	6435	47.8	47.3	3.9	7783	48.8	48.4	5.0	9697	Floodplain of Big Econ
BEBE080X	BEBE080N	BEBE085N	42.9		44.1	43.9	1.0	2957	46.6	46.4	3.5	6390	47.3	47.1	4.2	7730	48.4	48.2	5.3	9579	Floodplain of Big Econ
BEBE085X	BEBE085N	BEBE090N	42.8		43.9	43.6	0.8	2904	40.4	40.1	3.3	6358	47.1	46.8	4.0	7719	48.2	47.9	5.1	9566	Floodplain of Big Econ
BEBE090X	BEBE090N	BEBE095N	40.6		43.0	43.3	2.1	2002	40.1	40.0	5.0	6437	40.8	40.3	5./	7704	47.9	47.4	0.8	9855	Floodplain of Big Econ
BEBE095X	BEBE095N	BEBEIOON	40.7		43.3	41.1	0.4	2024	40.0	43.7	3.0	6407	40.3	44.0	5.9	7042	47.4	40.1	5.3	10216	Floodplain of Big Econ
BEBE100X	BEBE100N	BEBE105N	38.4		41.1	40.5	2.1	2002	43.7	43.1	4./	0497	44.0	43.9	3.0	8020	40.1	45.5	5.6	10462	Floodplain of Big Econ
BEBE105X	BEBEIUSN	BEBEITUN	39.3		40.5	39.0	0.3	35	46.3	40.5	2.9	0307	45.9	40.8	3.9	118	45.5	41.5	5.0	173	Pioodplain of Big Econ
BEBEIIOX	BEBEIULK	DEDE250N	41.7		39.6	39.1	1.3	2866	42.2	41.7	39	6510	43.2	42.8	5.0	7969	44.9	44.6	6.8	10388	Eloodalain of Big Econ
BEBEITUA	DEDETION DEDETION	BEBE120N	37.0		39.1	37.9	1.0	2855	41.7	41.1	31	6453	42.8	42.2	4.2	7909	44.6	44.2	62	10322	Eloodplain of Big Econ
DEDETION	BEBE110N	BEBE125N	37.0		37.9	37.7		2832	41.1	40.9	3.0	6379	42.2	42.0	4.1	7840	44.2	44.0	6.1	10295	Eloodplain of Big Econ
BEBE125X	BEBE125N	BEBE155N	35.1		37.7	36.6	1.5	2812	40.9	40.3	5.2	6312	42.0	41.5	6.4	7792	44.0	43.6	8.5	10364	Floodplain of Big Econ
BEBE130X	BEBE130N	BEBE135N	61.8		72.4	51.9		117	72.7	53.8	-	233	72.8	54.2	-	277	72.9	55.2		360	- Hoodplain of Big Loon
BEBE135C	BEBE135N	BEBE145N	53.4	Sunflower Trail Extension	51.9	51.5	-	109	53.8	53.0	0.4	207	54.2	53.8	0.8	209	55.2	55.2	1.8	208	Problem Area 12 - Sunflower Trail
BEBE135W	BEBE135N	BEBE145N	53.4	Sunflower Trail - Overflow	51.9	51.5	-	0	53.8	53.0	0.4	59	54.2	53.8	0.8	154	55.2	55.2	1.8	301	Problem Area 12 - Sunflower Trail
BEBE145C	BEBE145N	BEBE150N	55.8	Sunflower Trail	51.5	50.5		140	53.0	51.2	-	284	53.8	51.3	-	343	55.2	51.5	-	420	
BEBE145W	BEBE145N	BEBE150N	55.8	Sunflower Trail - Overflow	51.5	50.5	-	0	53.0	51.2	-	0	53.8	51.3	-	0	55.2	51.5	-	0	
BEBE150X	BEBE150N	BEBE125N	37.9		50.5	37.7		139	51.2	40.9	3.0	283	51.3	42.0	4.1	342	51.5	44.0	6.1	420	Floodplain of Big Econ
BEBE152C	BEBE152N	BEBE153N	62	State Road 50	59.6	57.4	•	84	60.6	58.3	•	200	61.1	58.4		200	61.9	58.6		201	
BEBE152W	BEBE152N	BEBE153N	62	State Road 50 - Overflow	59.6	57.4	-	0	60.6	58.3		0	61.1	58.4	•	0	61.9	58.6	-	0	
BEBE153X	BEBE153N	BEBE154N	52		57.4	50.8		128	58.3	53.6	1.6	171	58.4	53.7	1.7	180	58.6	53.7	1.7	200	Floodplain of Big Econ Tributary
BEBE154C	BEBE154N	BEBE155N	54	Old Cheney Highway	50.8	36.6	· · ·	84	53.6	40.3	•	152	53.7	41.5	· · · ·	153	53.7	43.6	· ·	154	
BEBE154W	BEBE154N	BEBE155N	54	Old Cheney - Overflow	50.8	36.6	<u> </u>	0	53.6	40.3		19	53.7	41.5	-	27	53.7	43.6		45	
BEBE155X	BEBE155N	BEBE160N	32.7		36.6	36.5	3.8	2780	40.3	40.1	1 7.4	6250	41.5	41.3	8.6	7742	43.6	43.3	10.6	10366	Floodplain of Big Econ
BEBE160X	BEBE160N	BEBE165N	44./	SR 50 Bridge Equivalent	36.5	30.4		2/63	40.1	40.1	-	6220	41.3	41.3		//16	43.3	43.3	-	10360	
BEBE160W	BEBEIGON	BEBE165N	44.6	SR 50 Bridge - Overnow	30.5	30.4		0750	40.1	40.1	21	6104	41.0	41.3	12	7602	40.0	43.3	E.A.	10256	Electricia of Dia Coop
BEBE165X	BEBEIGON	BEBEITUN	30.5	South Tannor Road	35.7	35.7		167	40.1	39.6	3.1	201	41.5	40.8	4.3	266	43.5	42.9	1.6	171	Overtepping due largely to tailwater in BC
BEBE169C	BEBEIDIN	BEBEITON	41.3	South Tanner - Overflow	35.7	35.7		0	40.3	39.6		0	41.6	40.8	0.3	49	42.9	42.9	1.0	200	Overtopping due largely to tailwater in BE
BEBE 109W	BEBE170N	BEBE220N	31.7	Goutt Taniter - Overnow	35.7	35.4	3.7	2711	39.6	39.3	7.6	6121	40.8	40.5	8.8	7620	42.9	42.7	11.0	10338	Floodolain of Big Econ
AA-4B	AA	AR	65.4	Waterford Chase Parkway - d/s of pond 4A	64.9	64.9		4	65.5	65.3	0.1	9	65.7	65.4	0.3	12	66.1	65.5	0.7	17	Problem Area 10 - Maple Creek Drive
48-4-2	48	4-2	66.5	Control structure out of pond 4-B	64.9	63.6		0	65.3	64.3	-	11	65.4	64.7	-	16	65.5	65.4		24	
4-1-4-2	4-1	4-2	66.5	Waterford Chase Parkway - d/s wetland 4-2	63.6	63.6		0	64.3	64.3		0	64.6	64.7	•	0	65.2	65.4		0	
4-1-3	4-1	3	66	Drop structure - Maple Creek Drive	63.6	63.6		2	64.3	64.1	-	8	64.6	64.3	-	10	65.2	64.6	•	12	
3-2	3	2	66.5	Oak Chase Drive	63.6	63.6	-	20	64.1	64.0	-	42	64.3	64.2	-	61	64.6	64.4	-	96	
2-99	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4	-	10	64.0	59.9	-	16	64.2	60.1	-	17	64.4	60.4	-	19	
2-99A	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4		2	64.0	59.9		27	64.2	60.1	-	38	64.4	60.4		48	
2-99B	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4	•	0	64.0	59.9	-	0	64.2	60.1	•	7	64.4	60.4		30	
BEBE190X	BEBE190N	BEBE195N	52.5		59.4	54.6	2.1	108	59.9	54.7	2.2	252	60.1	54.8	2.3	311	60.4	54.8	2.3	419	Floodplain of Big Econ Tributary
BEBE195X	BEBE195N	BEBE200N	47.8		54.6	46.5	•	169	54.7	47.8	0.0	301	54.8	48.3	0.5	370	54.8	49.3	1.5	496	Floodplain of Big Econ Tributary
BEBE200C	BEBE200N	BEBE205N	49.5	Old Cheney Highway Bridge Equivalent	46.5	44.7	-	258	47.8	45.2	-	513	48.3	45.7	•	621	49.3	47.5		817	
BEBE200W	BEBE200N	BEBE205N	49.5	Old Cheney - Overflow	46.5	44.7	-	0	47.8	45.2		0	48.3	45.7	· · ·	0	49.3	47.5	· ·	0	
BEBE210C	BEBE205N	BEBE215N	49.9	SR 50	44.7	44.6	-	353	45.2	45.0	-	512	45.7	45.4	· ·	621	47.5	47.1		807	
BEBE210W	BEBE205N	BEBE215N	49.9	SR 50 - Overflow	44.7	44.6	-	0	45.2	45.0	-	0	45.7	45.4	· · ·	0	47.5	47.1		0	
BEBE215X	BEBE215N	BEBE170N	36.5		44.6	35.7		403	45.0	39.6	3.1	512	45.4	40.8	4.3	621	47.1	42.9	6.4	805	Floodplain of Big Econ Tributary
BEBE220X	BEBE220N	BEBE222N	34.6		35.4	34.8	0.2	2676	39.3	38.9	4.3	6051	40.5	40.1	5.5	7568	42.7	42.3	7.7	10318	Floodplain of Big Econ
BEBE222X	BEBE222N	BEBE225N	44.7	Lake Pickett Bridge Equivalent	34.8	34.8	· · ·	2724	38.9	38.9		6137	40.1	40.1	•	7792	42.3	42.3		10408	
BEBE222W	BEBE222N	BEBE225N	41.4	Lake Pickett - Overflow	34.8	34.8		0	38.9	38.9	· · ·	0	40.1	40.1	· · · · · · · · · · · · · · · · · · ·	0	42.3	42.3	0.9	194	Floodplain of Big Econ
BEBE225X	BEBE225N	BEBE230N	38.3		34.8	32.5	·	2/23	38.9	35.9	· · · · · · · · · · · · · · · · · · ·	6135	40.1	37.6		7/00	42.3	40.5	2.2	10601	Floodplain of Big Econ
BEBE230X	BEBE230N	BEBE235N	41.7		32.5	32.2		2/19	35.9	35.6	•	6129	37.6	37.3	· · ·	7696	40.5	40.3	·	10600	

Notes: 1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels. 2) Flow taken from Link Maximum Conditions Report (cfs) 3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Table 5-1 Big Econ Stormwater Management Master Plan Orange County, Florida Existing Conditions Results

					Mean Annual				10 Year - 24 Hour					25 Year - 24	Hour		100 Year - 24	Hour			
Model ID	U/S Node	D/S Node	Critical Elevation ¹	Location	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	Comments
BEBEO10C	BEBEO10N	BEBE015N	65.8	Wewahootee Boad	62.4	61.8	-	89	63.9	62.3		170	64.5	62.4		197	65.2	62.5		224	
BEBEOILIC	BEBEOION	BEBEO15N	65.8	Wewahootee Boad	62.4	61.8	-	172	63.9	62.3	-	347	64.5	62.4		416	65.2	62.5		498	
BEBEOTOW	BEBEOLON	BEBEO15N	65.8	Wewahootee Boad - Overflow	62.4	61.8		0	63.9	62.3		0	64.5	62.4		0	65.2	62.5		0	
BEBEOISY	BEBEO15N	BEBEO20N	57.6	Trendhoolde Houd Orenien	61.8	55.2		393	62.3	56.8		732	62.4	57.3		863	62.5	58.1	0.5	1011	·····
DEBEODOX	BEBEOTON	BEBEO25N	62.1	Beeline Bridge Equivalent	55.2	55.2		998	56.8	56.8		1967	57.3	57.3		2338	58.1	58.1		3067	
DEDEO20A	DEDE020N	DEBEO25N	62.15	Beeline - Overflow	55.2	55.2		0	56.8	56.8		0	57.3	57.3		0	58.1	58.1		0	
DEDEO20W	BEBEO20N	DEBEO20N	56.6	Beamine	55.2	53.8		992	56.8	55.8		1931	57.3	56.4		2291	58.1	57.2	0.5	3023	
BEBEU20A	DEDE020N	DEDE030IN	50.0		53.8	53.6		971	55.8	55.7		1861	56.4	56.3		2186	57.2	57.0	0.0	2061	
BEBEUJUA	DEDE030N	DEBEOJON	50.2		53.6	52.5	23	2300	55.7	54.8	4.6	4418	56.3	55.4	52	5160	57.0	56.1	50	6007	Hal Scott - flooding oot a problem
BEBEUJOA	DEDE030N	DEDE040IN	50.2		52.5	52.0	2.0	2371	54.8	54.0	4.0	4758	55.4	54.8	5.0	5638	56.1	55.5	57	6735	Hal Scott - flooding not a problem
BEBE040X	BEBEU4UN	BEBEU45N	49.8		52.5	JZ.1	2.0	2510	54.0	19.2	4.4	5197	54.8	19.0	0.5	6191	55.5	40.8	1.5	7516	Hal Scott - flooding not a problem
BEBE045X	BEBE045N	BEBE050N	48.3		02.1	43.5	<u> </u>	2519	J4.2	40.1		5107	34.0	40.0	0.5	6260	35.5	49.0	1.5	7040	Hai Scott - flooding not a problem
BEBE050X	BEBE050N	BEBE055N	4/		45.5	44.7		2029	40.1	47.4	0.4	5310	40.0	40.1	1.1	6000	49.0	49.2	2.2	7043	Hai Scott - flooding not a problem
BEBE055X	BEBE055N	BEBE060N	43.1		44.7	44.0	1.5	2013	47.4	47.2	4.1	5700	48.1	47.9	4.8	6083	49.2	49.0	5.9	8642	Hal Scott - flooding not a problem
BEBE05X	BEBE05LK	BEBE255N	49.2		47.6	46.3		18	48.4	47.5		48	48.7	47.8	-	00	49.2	48.5		83	Hal Scott - flooding not a problem
BEBE060X	BEBE060N	BEBE065N	37.4		44.6	44.6	1.2	2967	47.2	47.2	9.8	6150	47.9	47.9	10.5	7360	49.0	49.0	11.6	9211	Hal Scott - flooding not a problem
BEBE065C	BEBE065N	BEBE070N	44.7	Powerline Bridge Equivalent	44.6	44.5	· ·	1/8	47.2	47.2	2.5	186	47.9	47.9	3.2	188	49.0	49.0	4.3	159	Hal Scott - flooding not a problem
BEBE065W	BEBE065N	BEBE070N	44.7	Powerline Overflow	44.6	44.5		0	47.2	47.2	2.5	419	47.9	47.9	3.2	492	49.0	49.0	4.3	542	Hal Scott - flooding not a problem
BEBE065X	BEBE065N	BEBE070N	44.7		44.6	44.5		2779	47.2	47.2	2.5	5606	47.9	47.9	3.2	6766	49.0	49.0	4.3	8661	Hal Scott - flooding not a problem
BEBE070X	BEBE070N	BEBE075N	44.8		44.5	44.4	-	2900	47.2	47.0	2.2	6086	47.9	47.8	3.0	7302	49.0	48.8	4.0	9145	Hal Scott - flooding not a problem
BEBE075X	BEBE075N	BEBE080N	43.4		44.4	44.1	0.7	3025	47.0	46.6	3.2	6435	47.8	47.3	3.9	7783	48.8	48.4	5.0	9697	Floodplain of Big Econ
BEBE080X	BEBE080N	BEBE085N	42.9		44.1	43.9	1.0	2957	46.6	46.4	3.5	6390	47.3	47.1	4.2	7736	48.4	48.2	5.3	9579	Floodplain of Big Econ
BEBE085X	BEBE085N	BEBE090N	42.8		43.9	43.6	0.8	2904	46.4	46.1	3.3	6358	47.1	46.8	4.0	7719	48.2	47.9	5.1	9566	Floodplain of Big Econ
BEBE090X	BEBE090N	BEBE095N	40.6		43.6	43.3	2.7	2862	46.1	45.6	5.0	6437	46.8	46.3	5.7	7852	47.9	47.4	6.8	9855	Floodplain of Big Econ
BEBE095X	BEBE095N	BEBE100N	40.7		43.3	41.1	0.4	2824	45.6	43.7	3.0	6355	46.3	44.6	3.9	7724	47.4	46.1	5.3	9761	Floodplain of Big Econ
BEBE100X	BEBE100N	BEBE105N	38.4		41.1	40.5	2.1	2852	43.7	43.1	4.7	6497	44.6	43.9	5.5	7943	46.1	45.5	7.1	10316	Floodplain of Big Econ
BEBE105X	BEBE105N	BEBE110N	39.3		40.5	39.6	0.3	2879	43.1	42.2	2.9	6567	43.9	43.2	3.9	8029	45.5	44.9	5.6	10462	Floodplain of Big Econ
BEBE10X	BEBE10LK	BEBE250N	41.7		45.3	39.7		35	46.3	40.5	•	93	46.6	40.8	-	118	47.1	41.6		173	
BEBE110X	BEBE110N	BEBE115N	37.8		39.6	39.1	1.3	2866	42.2	41.7	3.9	6510	43.2	42.8	5.0	7969	44.9	44.6	6.8	10388	Floodplain of Big Econ
BEBE115X	BEBE115N	BEBE120N	38		39.1	37.9	•	2855	41.7	41.1	3.1	6453	42.8	42.2	4.2	7909	44.6	44.2	6.2	10322	Floodplain of Big Econ
BEBE120X	BEBE120N	BEBE125N	37.9		37.9	37.7	-	2832	41.1	40.9	3.0	6379	42.2	42.0	4.1	7840	44.2	44.0	6.1	10295	Floodplain of Big Econ
BEBE125X	BEBE125N	BEBE155N	35.1		37.7	36.6	1.5	2812	40.9	40.3	5.2	6312	42.0	41.5	6.4	7792	44.0	43.6	8.5	10364	Floodplain of Big Econ
BEBE130X	BEBE130N	BEBE135N	61.8		72.4	51.9		117	72.7	53.8	-	233	72.8	54.2	-	277	72.9	55.2		360	
BEBE135C	BEBE135N	BEBE145N	53.4	Suoflower Trail Extension	51.9	51.5		109	53.8	53.0	0.4	207	54.2	53.8	0.8	209	55.2	55.2	1.8	208	Problem Area 12 - Supflower Trail
DEBE135W	BERE135N	BEBE145N	53.4	Sunflower Trail - Overflow	51.9	51.5	-	0	53.8	53.0	0.4	59	54.2	53.8	0.8	154	55.2	55.2	1.8	301	Problem Area 12 - Sunflower Trail
DEDE105W	BEBE145N	BEBE150N	55.8	Sunflower Trail	51.5	50.5		140	53.0	51.2	-	284	53.8	51.3	-	343	55.2	51.5		420	Troboni filou ie Guinionei filan
DEDE1450	DEDE145N	BEBE150N	55.8	Sunflower Trail - Overflow	51.5	50.5		0	53.0	51.2		0	53.8	51.3		0	55.2	51.5		0	
DEDE 145W	DEDE150N	BEBE125N	37.0	Guiniower Hun Oreniow	50.5	37.7		139	51.2	40.9	30	283	51.3	42.0	41	342	51.5	44.0	61	420	Eloodolain of Big Econ
DEDEISOA	DEDETSON	DEDETEON	62	State Boad 50	59.6	57.4		84	60.6	58.3	0.0	200	61.1	58.4		200	61.9	58.6		201	risouplair of big 2001
BEBE152C	BEBEISZN	DEDEIDUN	62	State Read 50 - Overflow	59.6	57.4		04	60.6	58.3		200	61.1	58.4		0	61.9	58.6		0	
BEBEISZW	BEBE 152N	DEDE153IN	52	State Hoad SU - Overlidw	57.4	50.8		128	58.3	53.6	16	171	58.4	53.7	17	180	58.6	53.7	17	200	Floodplain of Big Econ Tributant
BEBEI53A	BEBE 153N	BEBE154N	52	Old Changy Highway	50.9	36.6		94	53.6	40.3	1.0	152	53.7	41.5		153	53.7	43.6		154	Plotoplain of big Econ moutary
BEBE154C	BEBE154N	BEBEISSN	54	Old Chappey Quadley	50.0	30.0		04	53.0	40.3		10	52.7	41.5		27	53.7	43.0		154	
BEBE154W	BEBE154N	BEBEISSN	54	Old Cherley - Overnow	30.0	30.0	20	2700	33.0	40.3	74	6250	33.7 41.5	41.3	0.6	7740	42.6	43.0	10.6	10200	Electric of Dis Essa
BEBE155X	BEBE155N	BEBE160N	32.7		30.0	30.5	3.0	2700	40.3	40.1	1.4	6250	41.0	41.3	0.0	7742	43.0	43.3	10.6	10300	Floodplain of Big Econ
BEBE160X	BEBE160N	BEBE165N	44./	SR 50 Bridge Equivalent	30.5	30.4	· · · ·	2/03	40.1	40.1		0220	41.3	41.3		1/10	43.3	43.3		10360	
BEBE160W	BEBE160N	BEBE165N	44.6	SH 50 Bridge - Overnow	30.5	30.4	· · ·	0750	40.1	40.1		0	41.3	41.3		7000	43.3	43.3		10050	
BEBE165X	BEBE165N	BEBE170N	36.5		36.4	35.7	· ·	2/52	40.1	39.6	3.1	6194	41.3	40.8	4.3	7693	43.3	42.9	0.4	10356	Floodplain of Big Econ
BEBE169C	BEBE169N	BEBE170N	41.3	South Tanner Hoad	35.7	35.7		167	40.3	39.6		291	41.6	40.8	0.3	200	42.9	42.9	1.6	1/1	Overtopping due largely to tailwater in BE
BEBE169W	BEBE169N	BEBE170N	41.3	South Lanner - Overflow	35.7	35.7		0	40.3	39.6		0	41.6	40.8	0.3	49	42.9	42.9	1.6	299	Overtopping due largely to tailwater in BE
BEBE170X	BEBE170N	BEBE220N	31.7		35.7	35.4	3.7	2/11	39.6	39.3	7.6	6121	40.8	40.5	8.8	7620	42.9	42.7	11.0	10338	Floodplain of Big Econ
4A-4B	4A	4B	65.4	Waterford Chase Parkway - d/s of pond 4A	64.9	64.9		4	65.5	65.3	0.1	9	65.7	65.4	0.3	12	60.1	65.5	0.7	1/	Problem Area 10 - Maple Creek Drive
4B-4-2	48	4-2	66.5	Control structure out of pond 4-B	64.9	63.6		0	65.3	64.3	-	11	65.4	64.7		16	65.5	65.4	· · ·	24	
4-1-4-2	4-1	4-2	66.5	Waterford Chase Parkway - d/s wetland 4-2	63.6	63.6		0	64.3	64.3	•	0	64.6	64.7		0	65.2	65.4	····	0	
4-1-3	4-1	3	66	Drop structure - Maple Creek Drive	63.6	63.6		2	64.3	64.1	•	8	64.6	64.3	· · · ·	10	65.2	64.6	·	12	
3-2	3	2	66.5	Oak Chase Drive	63.6	63.6		20	64.1	64.0	-	42	64.3	64.2		61	64.6	64.4	•	96	
2-99	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4		10	64.0	59.9		16	64.2	60.1	-	17	64.4	60.4		19	
2-99A	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4	· ·	2	64.0	59.9	•	27	64.2	60.1	-	38	64.4	60.4		48	
2-99B	2	BEBE190N	66	Waterford Chase outfall	63.6	59.4	•	0	64.0	59.9	-	0	64.2	60.1	•	7	64.4	60.4		30	
BEBE190X	BEBE190N	BEBE195N	52.5		59.4	54.6	2.1	108	59.9	54.7	2.2	252	60.1	54.8	2.3	311	60.4	54.8	2.3	419	Floodplain of Big Econ Tributary
BEBE195X	BEBE195N	BEBE200N	47.8		54.6	46.5	•	169	54.7	47.8	0.0	301	54.8	48.3	0.5	370	54.8	49.3	1.5	496	Floodplain of Big Econ Tributary
BEBE2000	BEBE200N	BEBE205N	49.5	Old Cheney Highway Bridge Equivalent	46.5	44.7	•	258	47.8	45.2	-	513	48.3	45.7		621	49.3	47.5	-	817	
BEBE200W	BEBE200N	BEBE205N	49.5	Old Cheney - Overflow	46.5	44.7	-	0	47.8	45.2	-	0	48.3	45.7	-	0	49.3	47.5	-	0	
BEBE2100	BEBE205N	BEBE215N	49.9	SR 50	44.7	44.6	-	353	45.2	45.0	-	512	45.7	45.4	-	621	47.5	47.1	-	807	
BEBE210W	BEBE205N	BEBE215N	49.9	SR 50 - Overflow	44.7	44.6		0	45.2	45.0		0	45.7	45.4	-	0	47.5	47.1	-	0	
BEBE215	BEBE215N	BEBE170N	36.5		44.6	35.7		403	45.0	39.6	3.1	512	45.4	40.8	4.3	621	47.1	42.9	6.4	805	Floodplain of Big Econ Tributery
BEBEOON	BEBE220N	BERESSON	34.6		35.4	34.8	0.2	2676	39.3	38.9	4.3	6051	40.5	40.1	5.5	7568	42.7	42.3	7.7	10318	Eloodplain of Big Econ
BCBC220/	BEREDOON	BEREDOCK	44.7	Lake Pickett Bridge Foulyalant	34.8	34.8	0.2	2724	38.0	38.0		6137	40.1	40.1	0.0	7792	42.3	42.3		10408	riouplan of big Econ
DEBE222	DEDE222N	BEBERRA	41.7	Lake Dickett - Overflow	24.9	34.0		0	38.0	38.0		0	40.1	40.1		0	42.2	42.2	0.0	194	Elondolain of Rin Free
BEBE222V	DEBE222N	DEDE225N	91.4	Land Fickell - Overnow	24.0	22.5		2700	20.9	35.9		6105	40.1	27.6		7700	42.0	40.5	2.0	10601	Floodplain of Dig Econ
BEBE225	BEBE225N	BEBE230N	38.3		34.0	32.5		0740	30.9	05.9		0135	40.1	37.0		7600	42.0	40.0	6.6	10001	Floooplain of Big Econ
BEBE230	BEBE230N	BEBE235N	41./		32.5	32.2		2/19	35.9	35.6	· · ·	0129	37.6	37.3		1090	40.5	40.3	· · ·	10000	

Notes: 1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels. 2) Flow taken from Link Maximum Conditions Report (cfs) 3) Stages taken from Node Maximum Conditions Report (ft NGVD)

					Mean Annual			10 Year - 24 Hour						25 Year - 24	Hour		100 Year - 24	Hour			
Model ID	U/S Node	D/S Node	Critical Elevation ¹	Location	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	U/S Stage ³	D/S Stage ³	Flooding	Flow ²	Comments
CH-4B	CH-4A	CH-4B	51		47.7	47.0	1 -	816	49.0	48.2		1769	49.9	49.3		2117	50.0	49.1		2778	From Avalon Park FEMA floodplain study
CH-4C	CH-4B	CH-5	49		47.0	46.0		815	48.2	47.1		1768	49.3	48.8		2116	49.1	48.8		2779	From Avalon Park FEMA floodplain study
CH-5	CH-5	CH-6	50		46.0	44.4		820	47.1	47.0		1775	48.8	47.8		2114	48.8	48.8		2701	From Avalon Park FEMA floodplain study
CH-6	CH-6	CH-7	50		44.4	44.4		816	47.0	47.0		1736	47.8	47.8		2047	48.8	48.8		2671	From Avalon Park FEMA floodplain study
CH-7	CH-7	BEBE075N	44.8		44.4	44.4		784	47.0	47.0	22	1617	47.8	47.8	30	1886	48.8	48.8	40	2420	From Avalon Park FEMA floodplain study
CONSS-W	BESBOSON	C1	78	Weir flow to Alafava Trail Culverts	76.2	74.7		82	76.4	75.4		196	76.5	75.7	0.0	243	76.6	76.1	4.0	2723	FION AVAION FAIX FEMA hoodplain study
PETCODEY	BETCOOSN	BETCO20N	55.4	How to Handya Han outforto	55.6	53.9		498	56.2	55.9	0.5	080	56.7	56.5	11	1161	57.1	57.1	17	1000	Electelais of Turkey Creek
BETCOLOX	BETCOION	BETCOISN	62.6	the second s	73.0	64.8	22	1828	73.6	65.6	3.0	2762	73.8	65.9	2.2	3132	74.1	66.4	2.0	2004	Floodplain of Turkey Creek
BETCOTOX	BETCOTON	BETCOZONI	49.8		64.8	53.9	51	802	65.6	55.0	7.1	1546	65.0	56.5	7.7	1916	66.4	57.1	0.0	0004	Floodplain of Turkey Creek
BETCOTSA	BETCOTON	BEREOZENI	40.0 57.4		52.0	53.6		1047	55.0	55.7		2018	56.5	56.3	1.1	2225	57.1	57.0	0.0	2339	Proodplain of Turkey Greek
BETCOZOX	BEIG020N	BEBEUSSIN	07.4		65.5	65.4	0.2	1047	66.7	66.6	1.5	771	67.0	66.0	17	2000	67.4	57.0		2505	
BEWF005X	BEWFOUSN	BEWFUTUN	05.1	Culuat Biggs in Wadgefield Canal	05.5	61.0	0.3	440	66.6	60.0	1.5	421	67.0	00.0	1.7	912	07.4	07.2	2.1	1160	Floodplain of Wedgetield Canal
8EWF010P	BEWF010N	BEWF015N	65.3	Cuivert Riser in wedgeneid Canal	05.4	61.0	0.1	400	00.0	63.5	1.3	431	66.8	63.7	1.5	433	67.2	64.1	1.9	435	Floodplain of Wedgefield Canal
BEWF010W	BEWF010N	BEWF015N	65.3	and a second	65.4	61.0	0.1	13	00.0	63.5	1.3	461	66.8	63.7	1.5	603	67.2	64.1	1.9	851	Floodplain of Wedgefield Canal
BEWF015X	BEWF015N	BEWF020N	61.1	O Local Disease in the design of the Ocean	61.0	61.0	·	66/	63.5	63.5	2.4	//1	63.7	63.7	2.6	912	64.1	64.1	3.0	1160	Floodplain of Wedgefield Canal
BEWF020P	BEWF020N	BEWF025N	62.3	Culvert Hiser in Wedgetield Canal	61.0	57.4		401	63.5	59.0	1.2	482	63.7	59.2	1.4	488	64.1	59.6	1.8	494	Floodplain of Wedgefield Canal
BEWF020W	BEWF020N	BEWF025N	62.3		61.0	57.4		0	63.5	59.0	1.2	397	63.7	59.2	1.4	539	64.1	59.6	1.8	784	Floodplain of Wedgefield Canal
BEWF025X	BEWF025N	BEWF030N	57.8		57.4	57.4		379	59.0	59.0	1.2	764	59.2	59.2	1.4	909	59.6	59.6	1.8	1155	Floodplain of Wedgefield Canal
BEWF030P	BEWF030N	BEWF035N	57.5	Culvert Riser in Wedgefield Canal	57.4	54.6	•	348	59.0	57.9	1.5	413	59.2	58.1	1.7	421	59.6	58.6	2.1	430	Floodplain of Wedgefield Canal
BEWF030W	BEWF030N	BEWF035N	57.5		57.4	54.6		0	59.0	57.9	1.5	571	59.2	58.1	1.7	720	59.6	58.6	2.1	974	Floodplain of Wedgefield Canal
BEWF035X	BEWF035N	BEWF040N	54.8		54.6	54.6		348	57.9	57.9	3.1	761	58.1	58.1	3.3	906	58.6	58.6	3.8	1153	Floodplain of Wedgefield Canal
BEWF040P	BEWF040N	BEWF045N	56.8	Culvert Riser in Wedgefield Canal	54.6	52.1	•	330	57.9	54.2	1.1	465	58.1	54.8	1.3	482	58.6	55.5	1.8	501	Floodplain of Wedgefield Canal
BEWF040W	BEWF040N	BEWF045N	56.8		54.6	52.1		0	57.9	54.2	1.1	324	58.1	54.8	1.3	477	58.6	55.5	1.8	747	Floodplain of Wedgefield Canal
BEWF045X	BEWF045N	BEBE045N	54.6		52.1	52.1	-	322	54.2	54.2	-	717	54.8	54.8	0.2	858	55.5	55.5	0.9	1098	Floodplain of Wedgefield Canal
BEWF050X	BEWF050N	BEWF055N	55		65.3	51.9	•	414	66.7	52.7	•	809	67.1	52.8	•	1010	67.5	52.7		1501	
BEWF055X	BEWF055N	BEBE050N	48.3		51.9	45.5	-	668	52.7	48.1		1387	52.8	48.8	0.5	1624	52.7	49.8	1.5	2022	Floodplain of Wedgefield Canal
BEWF060X	BEWF060N	BEWF065N	63.7		60.9	60.3	-	379	63.4	63.1	-	510	64.2	64.0	0.3	546	65.5	65.3	1.6	651	Floodplain of Wedgefield Canal
BEWF065P	BEWF065N	BEWF070N	64.9	Culvert Riser in Wedgefield Canal	60.3	58.0	•	379	63.1	59.7		505	64.0	60.3		536	65.3	61.1	0.4	569	Floodplain of Wedgefield Canal
BEWF065W	BEWF065N	BEWF070N	64.9		60.3	58.0		0	63.1	59.7		0	64.0	60.3		0	65.3	61.1	0.4	78	Floodplain of Wedgefield Canal
BEWE070X	BEWF070N	BEWF075N	60.3		58.0	58.0	-	727	59.7	59.7		711	60.3	60.3		729	61.1	61.1	0.8	713	Floodnlain of Wedgefield Canal
BEWE075P	BEWE075N	BEWF080N	60.7	Culvert Riser in Wedgefield Canal	58.0	56.2	-	378	59.7	56.5		502	60.3	56.6		533	61.1	56.9	0.4	570	Floodolain of Wedgefield Canal
BEWE075W	BEWE075N	BEWF080N	60.7		58.0	56.2		0	59.7	56.5	-	0	60.3	56.6		0	61.1	56.9	0.4	74	Floodplain of Wedgefield Canal
BEWEOBOX	BEWE080N	BEWE085N	56		56.2	56.1	0.1	378	56.5	56.4	0.4	502	56.6	56.5	0.5	532	56.9	56.7	0.7	643	Floodplain of Wedgefield Canal
BEWE085P	BEWE085N	BEWENOON	55.4	Culvert Riser in Wedgefield Canal	56.1	49.2	0.7	210	56.4	50.7	1.0	215	56.5	51.8	11	216	56.7	53.5	13	216	Elocaplain of Wedgefield Canal
BEWEORSW	BEWEO85N	BEWEOGON	55.4	Curor in recigoroid curu	56.1	49.2	0.7	168	56.4	50.7	10	286	56.5	51.8	11	332	56.7	53.5	13	480	Floodplain of Wedgefield Canal
DEWFOOOY	BEWEOOON	BEWEOOSN	52.6		49.2	48.6		378	50.7	50.3	1.0	500	51.8	51.5		530	53.5	53.4	0.8	642	Floodplain of Wedgeheld Canal
DEWF090A	DEWFOOD	DEWE100N	52.0	Culvert Biser in Wedgefield Canal	48.6	44.6		378	50.3	47.2		497	51.5	47.9		528	53.4	49.0	0.0	601	Floodplain of Wedgefield Canal
BEWFU95P	BEWFU95N	BEWFIOON	53	Cuivert hisor in Wedgeneid Canal	48.6	44.6		0	50.3	47.2		457	51.5	47.9	· · · ·	0	52.4	49.0	0.4	591	Floodplain of Wedgefield Canal
BEWF095W	BEWFU95N	BEWFILLIN	33		40.0	44.0	1.5	270	47.2	47.2	41	407	47.0	47.9	4.0		33.4	49.0	0.4	00	Floodplain of Wedgefield Canal
BEWFILLOS	BEWFIOUN	BEBEUGUN	43.1		62.2	617	1.5	570	64.1	60.0	4.1	497		60.0	4.0	167	49.0	49.0	5.9	042	Floodplain of Wedgefield Canal
BEWF105X	BEWF105N	BEWFITON	09.3	Culuat Picer in Wedgefield Conel	617	61./		50	62.0	50.1		155	60.0	62.3		107	65.0	62.4	· ·	194	
BEWFITOP	BEWFITON	BEWFIIDN	04.0	Culvert Hiser in Wedgeneid Canal	61.7	50.4		- 55	62.2	59.1	· · ·	155	62.3	59.2		107	02.4	59.3	· · ·	194	
BEWFITOW	BEWFITON	BEWFIISN	04.0		50.4	50.4	<u> </u>	62	50.1	59.1		155	62.3	59.2	· · ·	107	02.4	59.3	· · ·	0	
BEWF115X	BEWFIIS	BEWF120N	61.5	Outwart Plans in Wadaofield Conal	50.4	50.4		50	59.1	50.9	· · ·	155	59.2	50.9	· ·	107	59.3	59.0	· ·	194	
BEWF120P	BEWF120N	BEWF125N	60.5	Culvert Hiser in Wedgeneid Canal	50.4	53.8	·	55	50.9	54.4		155	58.9	54.4		167	59.0	54.6		194	
BEWF120W	BEWF120M	N BEWF125N	60.5		50.4	53.0	· · ·	0	50.9	54.4	· · · ·	040	50.9	54.4	· ·	0	59.0	54.6		0	
BEWF125X	BEWF125N	N BEWF130N	50.4	O front Disco in Mindro field Operal	53.0	53.8	· · ·	221	54.4	54.3	· · ·	240	54.4	54.4	· · · ·	249	54.6	54.5	<u> </u>	250	
BEWF130P	BEWF130N	N BEWF135N	54.9	Culvert Riser in Wedgeneid Canal	53.0	50.0		53	54.3	50.6		155	54.4	50.7		16/	54.5	52.4	•	194	
BEWF130W	BEWF130N	BEWF135N	54.9		53.8	50.0	<u>+</u>	0	54.3	50.6	-	105	54.4	50.7		100	54.5	52.4	· · · ·	0	
BEWF135X	BEWF135	BEWF140N	5/	Output Dissult West - Full On 1	50.0	50.0		53	50.6	50.6		405	50.7	50.7		426	52.4	52.4		421	
BEWF140P	BEWF140N	BEWF145N	53.7	Cuivert Hiser in Wedgetield Canal	50.0	46.5	·	52	50.6	48.3		155	50.7	48.8		166	52.4	50.2	-	194	
BEWF140W	BEWF140M	N BEWF145N	53.7		50.0	46.5	<u> · · · · · · · · · · · · · · · · · · ·</u>	0	50.6	48.3		0	50.7	48.8	-	0	52.4	50.2		0	
BEWF145X	BEWF145	BEWF150N	53.3	O hard Direction of The Direction	46.5	46.4	· · · ·	52	48.3	48.3		808	48.8	48.8	•	808	50.2	50.2		799	
BEWF150P	BEWF150	N BEWF155N	50.2	Culvert Hiser in Wedgefield Canal	46.4	43.8	·	52	48.3	46.9		153	48.8	47.1		165	50.2	48.0	-	191	
BEWF150W	BEWF150N	N BEWF155N	50.2		46.4	43.8		0	48.3	46.9	· · ·	0	48.8	47.1	-	0	50.2	48.0	•	0	
BEWF155X	BEWF155	N BEWF160N	49		43.8	43.8		52	46.9	46.9		153	47.1	47.1	-	164	48.0	47.9	-	191	
BEWF160F	BEWF160	N BEWF165N	46.6	Culvert Riser in Wedgefield Canal	43.8	43.6	· · ·	52	46.9	46.1	0.3	149	47.1	46.8	0.5	149	47.9	47.9	1.3	129	Floodplain of Wedgefield Canal
BEWF160W	BEWF160	N BEWF165N	46.6		43.8	43.6		0	46.9	46.1	0.3	37	47.1	46.8	0.5	92	47.9	47.9	1.3	172	Floodplain of Wedgefield Canal
BEWF165X	BEWF165	N BEBE090N	48.9		43.6	43.6	· ·	52	46.1	46.1	•	153	46.8	46.8	•	164	47.9	47.9		190	Floodplain of Wedgefield Canal
CULV-2	81X	82	74	Woodbury Road	69.9	69.3		170	71.2	69.9	-	350	71.6	70.1		416	72.6	70.6	-	526	
CHANL-5	82	24	65		69.3	62.8	-	171	69.9	63.6		352	70.1	63.8		416	70.6	63.9		526	
CHANL-6	24	26	65		62.8	59.7		200	63.6	61.2	-	414	63.8	61.6	•	467	63.9	62.3	-	545	
CULV-10	26	13A	60		59.7	55.4		268	61.2	55.7	1.2	560	61.6	55.9	1.6	656	62.3	56.2	2.3	795	Floodplain of Big Econ Tributary
13A-13B	13A	13B	55		55.4	53.7	0.4	63	55.7	55.0	0.7	72	55.9	55.3	0.9	74	56.2	55.8	1.2	76	Floodplain of Big Econ Tributary
B13A-13B	13A	13B	55		55.4	53.7	0.5	240	55.7	55.0	0.5	570	55.9	55.3	0.5	675	56.2	55.8	0.5	834	Floodplain of Big Econ Tributary
CHN-12-0	13B	STA-9700	57		53,7	52.0		342	55.0	53.2		873	55.3	53.3		1007	55.8	53.7	•	1312	
BEWI 015)	STA-9700	BEWL020N	49		52.0	50.1	1.1	339	53.2	50.4	1.4	873	53.3	51.1	2,1	1013	53.7	52.1	3.1	1322	Eloodolain of Big Econ Tributany
BEWI 0200	BEWI 020	N BEWL025	57.8	Bridgeway Blvd - Bridge Equivalent	50,1	50.1	-	531	50.4	50.3		1136	51.1	51.0	-	1325	52.1	52.0		1690	
BEWI 020V	BEWI 020	N BEWL025N	57.8	Bridgeway Blvd Overflow	50.1	50.1	-	0	50.4	50.3		0	51.1	51.0		0	52.1	52.0		0	
BEWI 0251	BEWI 025	N BEWI 030M	47.8		50.1	46.4		531	50.3	49.5	1.7	1136	51.0	50.2	24	1324	52.0	51.3	3.5	1605	Eloodolain of Big Econ Tributon
DEWL020/	DEWL020	NI BEW/LOOP	54.4	SB 50	46.4	44.4	-	612	49.5	45.0		1354	50.2	45.1	T int	1540	51.0	45.4	0.0	2000	roouplain of big Econ Thoulary
DEWEL0300	010111030	DETTEOJO	04.4	51100	1 10/1	1 71.7		014	10.0	1.0.0		1004	00.6	10.1		1040	01.0	40.4		2000	and a second second second reaction of the

Notes: 1) Critical Elevation refers to road overtopping elevation for culverts and top of bank for open channels. 2) Flow taken from Link Maximum Conditions Report (cfs) 3) Stages taken from Node Maximum Conditions Report (ft NGVD)

Appendix: J

Bithlo Area Stormwater Management Master Plan
Bithlo Area Stormwater Management Master Plan Update

Final Report





Board of County Commissioners Orange County, Florida





Singhofen & Associates, Inc. Stormwater Management and Civil Engineering

September 2002





Table 6.1 Identification and Location Information for Structures at Major Crossings and/or Outfalls Bithlo South Sub-System

Lipstream -			
ID Name Name	(in)		

Culverts

1	PK-120	NK-120	27-22\$-32E	24	24	C.R. 13 south of Seventeenth Avenue
2	PKE-030	NKE-030	34-225-32E	96	84	C.R. 13, Roberts Branch
3	PKE-080A	NKE-080	27-22S-32E	72	72	Lansing St.
4	PKE-120	NKE-120	27-22S-32E	36	36	Fairfield St.
5	PKE-143	NKE-143	27-22S-32E	30	30	9th St. and 14th Ave.
6	PKE-165	NKE-165	27-22S-32E	24	24	8th St. between 15th and 16th Ave.
7	PKE-225	NKE-225	27-225-32E	18	12	7th St. culvert
8	PKE-245	NKE-245	27-22S-32E	24	24	14th Ave.
9	PKE-255	NKE-255	27-22S-32E	24	24	13th Ave.
10	PKE-265	NKE-265	27-22S-32E	24	24	12th Ave,
11	PL-020	NL-020	27-22S-32E	30	30	Rawles St.
12	PM-030	NM-030	27-22S-32E	48	48	Wellon St.
13	PM-050	NM-050	26-22S-32E	42	42	South discharge from pond
14	PN-015	NN-015	27-22S-32E	120	48	S.R. 50
15	PN-020	NN-020	26-22S-32E	120	108	Old Cheney Hwy.
16	PN-033	NN-033	27-22S-32E	24	24	Vermont St. and Exeter St.
17	PN-060	NN-060	22-22S-32E	36	36	Containment berm
18	PN-115	NN-110	22-22S-32E	15	15	3rd Ave.
19	PN-150	NN-150	22-22S-32E	24	24	3rd Ave.
20	PNA-030	NNA-030	22-225-32E	45	29	10th St.

Drop Structures

21	DM-070	NM-070	26-22S-32E	42	42	Control structure from North pond to South pond (new)	
					_		
Weirs							
22	M/M (180)	NN 010	26 225 225		_	Overflow chilway from Changel N to M	

22	WM-080	NN-010	26-22S-32E			Overflow spillway from Channel N to M
23	WN-060B	NN-060	22-225-32E	-	•	High stage discharge from Wetland (Pond KE-1)

Other

24	<u>-</u>	NK-110	27-22\$-32E	-	-	Wetland west of C.R. 13
25	-	NK-130	27-22S-32E	-	-	Wetland eastof C.R.13
26	-	NM-050	26-22S-32E	-	-	Pond M-2
27		NM-060	26-22S-32E		-	Pond M-3
28	-	NM-070	26-22S-32E	-	-	Pond M-1

Notes:

1. The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 6.1)

2. Detailed structure information for culverts, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.





Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).



		100-	Year								
	Storm Event										
:t	Curi	rent	Pro	ect							
low cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)							
621	47.34	784	47.35	787							
84	59.8	97	59.8	110							
18	60.6	43	60.6	24							
621	47.34	784	47.35	787							
523	50.6	668	50.5	659							
502	52.8	642	52.8	633							
449	54.2	575	54.1	565							
340	56.6	410	56.6	409							
330	57.3	399	57.3	397							
116	60.7	58	58.8	144							
24	61.5	24	60.0	31							
24	60.9	22	59.5	30							
20	62.2	20	61.4	25							
-	63.9	18	-	-							
19	-		62.6	24							
19	65.3	16	63.8	24							
16	65.9	14	64.4	21							
14	66.3	12	65.2	17							
10	66.6	11	65.5	17							
33	54.0	42	54.1	42							
27	56.0	37	56.0	38							

Bithlo Stormwater Management Master Plan Update

				Mean Storm	Annual i Event			5-Y Storm	'ear I Event			10- Storm	Year I Event			25- Storm	Year Event			100- Storm	-Year i Event	1
	1		Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	ject	Cur	rent	Pro	oject
LOC ID	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
Channel	M					1																
12	NM-030	Wellon St., E.	53.9	26	53.8	23	54.3	43	54.2	38	54.7	58	54.7	59	55.0	71	55.1	76	55.5	95	55.7	107
26	NM-050	Pond M-2	53.9	8	53.6	5	54.4	14	54.3	12	54.8	19	54.8	24	55.0	23	55.2	35	55.5	30	55.9	53
27	NM-060	Pond M-3	53.9	3	53.6	2	54.4	5	54.3	5	54.8	6	54.8	8	55.0	7	55.2	9	55.5	10	55.9	11
28	NM-070	Pond M-1	57.7	10	57.4	0	57.8	15	57.8	13	57.8	19	57.9	26	57.9	22	58.0	35	57.9	28	58.2	51
22	NM-080	Overflow spillway, S.	57.7	0	57.4	0	57.8	0	57.8	6	57.8	0	57.9	15	57.9	0	58.0	24	57.9	0	58.2	36
Channel	N					0.																
14	NN-010	S.R. 50, S.	57.3	126	57.4	131	57.9	192	57.8	186	58.2	232	58.1	217	58.4	266	58.2	243	58.7	319	58.5	284
15	NN-015	S.R. 50, N.	61.1	117	61.1	117	61.8	178	61.8	178	62.3	214	62.3	214	62.6	246	62.6	246	63.1	294	63.1	294
15	NN-020	Old Cheney Hwy., N.	61.1	93	61.1	93	61.9	143	61.9	143	62.3	171	62.3	171	62.6	195	62.6	195	63.2	236	63.2	236
17	NN-050	Struct from wetland, N.	61.5	20	61.5	20	62.3	38	62.3	38	62.7	52	62.7	52	63.1	63	63.1	63	63.6	84	63.6	84
18	NN-110	Third Ave., N.	62.0	1	62.0	1	62.9	1	62.9	1	63.4	1	63.4	1	63.9	1	63.9	1	64.5	1	64.5	1
19	NN-150	Third Ave., N.	62.0	10	62.0	10	63.3	15	63.3	15	64.0	21	64.0	21	64.4	25	64.4	25	65.0	33	65.0	33
Channel	NA							9 6							n antekolomietana							
20	NNA-030	Intersect 4th & 10th, W.	61.9	19	61.9	19	63.2	24	63.2	24	63.8	34	63.8	34	64.1	38	64.1	38	64.5	49	64.5	49
399	NNA-070	4th St., N.	61.6	21	61.6	21	62.5	25	62.5	25	63.0	27	63.0	27	63.3	27	63.3	27	63.8	28	63.8	28

Table 6.2 Maximum Stages and Flows at Selected Locations in the Bithlo South Sub-System (Current and Project Conditions).

Notes: 1. Flow

1. Flow represents the peak outflow at the referenced node.

2. Results are from the Bithlo Current Conditions model <EXIST> and the Bithlo Project Conditions model <B-PROJ1>.

3. The simulated storms are all 24-hr duration storms.

4. The LOC ID numbers associated with each location are included for the purpose of cross referencing to the system map (refer to Figure 6.1)











Table 5.1	Identification and Location Information for Structures at Major Crossings and/or Outfalis
	Bithlo West Sub-System

Location ID Culvert	Link Name	Upstream Node Name	SEC-TWN-RNG	Culvert Span (in)	Culvert Rise (in)	Location Description
1	PE-030A	NE-030	28-22S-32E	72	72	Story Partin Road
2	PE-070A	NE-070	21-22S-32E	48	48	Old Cheney Hwy, S. of S.R. 50
0	DE 080	NC 090	21,225,325	49	51	S.P. 50 (western most crossing)

Notes: 1. The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 5.1) 2. Detailed structure information for culverts, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.



Singhofen & Associates, Inc.

Bithio Stormwater Management Master Plan Update





Table 5.2 Maximum Stages and Flows at Selected Locations in the Bithlo West Sub-System (Current and Project Conditions).



	100-Year Storm Event										
	Cur	rent	Pro	ject							
ow fs}	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)							
8	65.0	106	65.0	106							
6	61.4	132	61.4	131							
35	54.2	295	54.2	295							
91	47.4	364	47.4	364							
12	46.5	398	46.5	398							



J-11

Table 3.1 Identification and Location Information for Structures at Major Crossings and/or Outfalls **Bithio Proper Sub-System**

|--|

Culverts

	-					
1	PA-015A	NA-015	28-22S-32E	48	48	Utility (power) Easement at south end of Channel A u/s of the Econ River
2	PA-070	NA-070	28-22S-32E	72	72	Seminole Trail
3	PA-110	NA-110	27-22S-32E	96	84	S.R. 60
4	PA-115	NA-115	22-22\$-32E	192	72	Old Cheney Highway
5	PA-220	NA-220	22-22S-32E	36	36	Belvedere Rd. at C.R. 13
6	PA-240	NA-240	21-22S-32E	60	38	Access road to Pond A-2
7	PAA-020	NAA-020	22-22S-32E	18	18	North side of S.R. 50 near Belvedere Rd.
8	PA8-030B	NAB-030	22-22S-32E	23	14	Belvedere Rd. at Old Cheney Hwy.
9	PB-010A	NB-010	22-22S-32E	54	54	C.R. 13
10	PB-040	NB-040	22-22S-32E	36	36	Channel B crossing 6th St.
11	PB-070	NB-070	22-22S-32E	30	30	Channel B crossing at Belvedere Rd.
12	PBA-020	NBA-020	22-22S-32E	36	36	8th St.
13	PBA-050	NBA-040	22-22S-32E	24	24	10th St.
14	PBA-060	NBA-060	22-22S-32E	38	24	East Orlando Rd.
15	PBB-030	NBB-030	15-22S-32E	23	14	Hollister Rd.
16	PF-130	NF-130	15-22S-32E	45	29	Hewlett Rd.
17	PC-025	NC-025	15-22S-32E	30	19	Hollister Rd.
18	PC-040	NC-030	15-22S-32E	30	19	6th St.
19	PC-080	NC-080	15-22S-32E	30	19	Hollister Rd.
20	PCB-020	NCB-020	15-22S-32E	24	24	Hewlett Rd.
21	PKW-110	NKW-110	27-22S-32E	30	30	5th St.
22	PN4-010	NN4-010	21-22S-32E	60	38	Under Belvedere Rd. (N-4 channel system)
23	P6-020	N6-020	22-22S-32E	30	19	6th St.
24	P6-050	N6-050	22-22S-32E	30	19	Belvedere Rd.
25	P6A-010	N6A-010	22-22S-32E	38	24	6thSt, cuivert (near BCC pond)

Drop Structures

26	DA-241A	NA-241	16-22S-32E	24	24	From perimeter ditch SW of Pond A-2
27	DA+241B	NA-241	16-22S-32E	15	15	From perimeter ditch NW of Pond A-2
28	DA-243A	NA-243	16-22S-32E	15	15	From perimeter ditch SE of Pond A-2
29	DA-243B	NA-243	16-22S-32E	15	15	From perimeter ditch east of Pond A-2
30	DA-243C	NA-243	16-22S-32E	15	15	From perimeter ditch NE of Pond A-2
31	DN4-035A	NN4-035	22-22S-32E	24	24	From depression west of C.R. 13 into Channel N4
32	DN4-035B	NN4-035	22-22\$-32E	24	24	From depression west of C.R. 13 into Channel N4

Other

33	-	NA-140	22-228-32E	-	•	Pond A-1
34	-	NA-240	16-22S-32E	-		Pond A-2
35	-	NA-250	16-22S-32E	- -	-	Pond A-3
36	-	NB-080	22-225-32E	-	-	Wetland at Channel B/BA confluence
37	-	NN-060	22-22S-32E	-	-	Wetland (Pond KE-1)
38		NBB-030	15-22S-32E	-	-	Wetland north of Hollister Rd.
39	-	NC-050	15-22S-32E	-	-	Wetland south of Hollister Rd.
Notes:						

The ID numbers associated with each structure are included for the purpose of correlating the structure locations with the system map. (See Fig. 3.1)
 Detailed structure information for culverts, weirs and drop structures is included in the drainage inventory tables presented in Appendix A.



			Mean Annual Storm Event			5-Year Storm Event			10-Year Storm Event			25-Year Storm Event				100-Year Storm Event						
		Current		Project		Current Proj		ject	Current		Project		Current Pr		Рго	ject	Current		Project			
LOC ID	Node ID	Location	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)	Stage (ft)	Flow (cfs)
Channel	Α																					
1	NA-015	Power Easement, N.	40.2	325	40.2	322	40.5	492	40.5	489	40.7	620	40.7	615	41.5	762	41.5	744	42.8	1027	42.8	1005
2	NA-060	Seminole Trl., W.	48.2	256	48.2	253	48.6	377	48.6	372	48.8	465	48.8	458	49.1	564	49.1	549	49.5	719	49.4	697
2	NA-070	Seminole Trl., E.	48.4	253	48.4	250	49.6	373	49.6	369	50.5	461	50.4	454	50.7	556	50.7	541	50.9	703	50.9	682
3	NA-110	SR 50, N.	57.0	204	57.0	204	58.3	310	58.3	310	59.04	379	59.05	380	59.5	425	59.5	425	60.3	499	60.3	499
4	NA-115	Old Cheney Hwy., N.	57.1	192	57.1	191	58.4	295	58.4	290	59.2	373	59.2	369	60.0	395	60.0	393	61.0	446	61.0	447
•	NA-130	CR 13, W.	60.1	182	60.1	182	60.4	280	60.4	280	60.6	345	60.6	345	60.9	386	60.9	387	61.5	446	61.5	447
33	NA-140	Pond A-1	60.3	10	60.3	10	60.8	15	60.8	15	61.1	22	61.1	22	61.4	27	61,4	27	62.0	34	62.0	34
5	NA-220	Belvedere Rd., N.	65.6	58	65.6	58	66.6	80	66.6	80	66.9	81	66.9	81	67.3	83	67.3	83	68.4	91	68.4	91
6	NA-230	Just S. of Pond A-2	67.1	56	67.1	56	67.9	87	67.9	87	68.2	93	68.2	93	68.4	90	68,4	90	68.8	106	68.8	106
34	NA-240	Pond A-2	67.6	56	67.6	56	68.7	86	68.7	86	69.2	91	69.2	91	69.6	86	69.6	86	69.9	74	69.9	74
35	NA-250	Pond A-3	68.6	11	68.6	11	69.3	29	69.3	29	69.8	34	69.8	34	70.4	38	70.4	38	71.3	42	71.3	42
Channel	AA													1000								
7	NAA-020	Belvedere Rd., W.	63.2	12	60.9	14	64.1	14	61.6	22	64.3	22	62.0	25	64.5	31	63.0	35	64.6	52	64.3	53
Channel .	AB						1															
8	NAB-030	Belvedere Rd., W.	63.5	9	63.3	20	64.5	14	63.3	20	64.6	20	63.8	20	64.6	24	64.4	22	64.7	31	64.6	31
Channel	B								0.00													
9	NB-010	Wetland, E. of CR 13	60.3	142	60.3	142	60.8	206	60.8	206	61.1	249	61.1	249	61.3	270	61.3	271	62.0	296	62.0	297
10	NB-040	Sixth St., E.	64.9	76	64.9	76	65.3	79	65.3	79	65.7	82	65.7	82	66.2	91	66.2	91	66.7	98	66.7	98
11	NB-070	Belvedere Rd., N.	66.6	59	66.6	59	67.3	64	67.3	64	68.2	71	68.2	71	68.8	79	68.8	79	69.3	85	69.3	85
-	NB-080	Channel B/BA confluence	67.5	50	67.5	50	68.0	62	68.0	62	68 .6	73	68.6	73	69.0	84	69.0	84	69.4	98	69.4	98
Channel BA				61																• • • • • • • • • • • • • • • • • • • •		
12	NBA-010	Eighth St., W.	68.3	12	68.3	12	68.8	13	68.8	13	69.0	11	69.0	11	69.1	10	69.1	10	69.4	10	69.4	10
12	NBA-020	Eighth St., E.	68.5	29	68.5	29	69.1	32	69.1	32	69.2	49	69.2	49	69.2	71	69.2	71	69.4	105	69.4	105
13	NBA-040	Tenth St., W.	68.5	16	68.5	16	69.1	23	69.1	23	69.2	24	69.2	24	69.3	25	69.3	25	69.5	26	69.5	26
14	NBA-060	East Orlando Rd., W.	66.2	2	66.2	2	66.3	3	66.3	3	66.4	4	66.4	4	66.4	4	66.4	4	66.5	5	66.5	5

Table 3.2 Maximum Stages and Flows at Selected Locations in the Bithlo Proper Sub-System (Current and Project Conditions).



Bithlo Stormwater Management Master Plan Update

Appendix: K

Excerpt from BJM Associates, Inc.



Appendix: L

Excerpt from Harling Locklin & Associates, Inc. Waterford Trails Plans & Avalon Park Blvd





















8' WIDE • 55.04 • 55.74 • 55.76 • 55.76 • 55.76 • 55.76 • 55.76 • 55.76	CONC. SIDE WALK 8" CONCRETE RETAINING WALL (SEE DETAILS) 4' CONC. CONCRETE APRON 54.68 54.68 54.68 54.16 55.17	WE TLAND (S-69) STA: 171+85. CONST. TYPE INDEX NO. 21 THROAT=51.5 FL. OUT=47.2 53.48 C/L BOX CUL STA: 170+22. FL. 46.50 54.20	POND A OUTFALL F (SEE POND PLANS & DETAILS) 22, 44.50' LT P-1 INLET 1 5 20 R/V VERTS (7) 0 I 53.13 6 CON	S-70 STA: CONS INDEX THRO. FL. FL. FL. FL. FL. FL. FL. FL. FL. FL	LANDSCAPE WAL (SEE LANDSCAPE 172+15.22, 4.5 LT T. TYPE P-2 INLET NO. 211 AT=51.45 IN=47.00 0UT=47.00 0UT=47.00 ST. 50 LF 8"RCP 40% 52.17	L PLANS) BEGN 517 S-71 F. 172+00 S-71 F. 172+00 S-71 F. 172+00 S-71 F. 172+00 F. 187RCP @ 0.68% F. 52.20 F. 52.25 F. 52.25	S-71 STA: 172±45.2 CONST. TYPE-F INDEX NO. 211 THROAT=51.48 FL. IN=46.80 FL. OUT=46.50 SO LF- 6" ADS 5 INDR @ 0.30% CO FL. 4 TYPE 'F' CURB & GUTTER CO FL. 50.00 173 52.63	2.44.50 LT -1_INLET POND WIDE CONC. MIDE CONC. 1DE WALK 52.10 CONST. 1. 9.64 0F 30"RC @ 0.39% 52.43 CONST. E OF 36"RC @ 0.34%
56.25 56.3 8' WIDE CONC. SIDEWALK 8" CONCRETE RETAINING WALL (SEE DETAILS) 4' CONC. CONCRETE APRON	55.96 55.96 55.44 55.22 CONST. TYPE P-INDEX NO. 211 THROAT=52.27 FL. 0UT=47.50	54.20 TYPE 'F' 54.76 54.76 44.50' RT 44.50' RT 1 INLET WETLAND	CURB & GUTTER S-68 STA: 172+15.22, 44.5 CONST. TYPE P-2 INI INDEX NO. 211 THROAT=52.15 FL. IN=47.30 FL. OUT=47.30	S-66 G 52.27 CONST. 30 LF OF 18"RCP @ 0.67% S-66 G 52.27 CONST. 30 LF OF 18"RCP @ 0.67% S-66 G S-7%	67 52.15 5-68 52.72 <i>S</i> -68 <i>S</i> -68	52.20 52.20 52.20 52.20 0F 18"RCP @ 0.67% 52.76 52.76 52.76 52.76 52.76 52.76 0 0.67% 52.76	52.45 52.45 52.43 52.43 52.43 52.43 52.43 52.43 52.43 52.43 52.43 52.43 52.43 52.43 53.40 53.40 53.40 53.40	53.00 53.00 CONST. 18 LF OF 30"RCP @ 0.33% CO FL. 50.20-5 53.40 73 180*
58 58 56 54 54 52 50	HGH POINT ELEV = 55.76 $HIGH POINT STA = 169+23.02$ $PVI STA = 169+65$ $PVI ELEV = 56.45$ $A.D. = -3.37$ $K = 59.29$ $RADE$	EVCS: 170+65 EVCS: 170+65 EVCS: 170+65 BVCS: 170+65 EVCS: 170+75 EVCS:	FULL S.E RT E.O.P. LOW LOW P Ped Crown EL n Existing verts as TW CD-4 T. (7) x 5' HIGH CULVERTS	POINT ELEV = 52.17 $POINT ELEV = 52.17$ $POINT STA = 172+22.87$ $VI STA = 171+55$ $VI ELEV = 51.90$ $A.D. = 2.73$ $K = 65.92$ $S = 100$ $S = 68$	69 S-70 S-71	EVCS: 172+45 EVCS: 172+45 EVCE: 52/20 EVCE: 52/20 EVCE	R :D.P	T. E.O.P
169 48 46 46 46 47 46 44 169 Plotted: Apr 27, 2001 - 11:54om DATE: BY DESCRIPTION	I TO BY DESCRIPTION DATE	FL. E FL. E SEASONAL LEVEL AS DEVO SEE (DA TED: (PROJECT BY DES	LEV. 46.50 HIGH GROUNDWATER PROVIDED BY REERAM, Ph.D., P.E. 03/20/01, No. 00-549.01). 171 SCRIPTION DATE:	FL. 47.20 CONST. 29 LF OF 18" RCP @ 0.68% BY DESCRIPTION	FL. 47.00 FL. 47.00 CONST. 29 LF OF 18" RCP - 46.80 @ 0.68% 172 NAME DESIGNED BY CHECKED BY SUPERVISED BY:	DATE 2/01 EXAMPLE NU 2/01 DATE 2/01 DESIGNED BY CHECKED BY HLH	CONST. 128 LF OF 30 RCP _/ Ø 0.39% 173 AME DATE H/A LO E AE	FL. FL. FL. FL. FL. FL. FL. CONSU PLANN 850 CO ORLAND PHONE:

END END 20 40 S=76 SCALE: 1"=40' 5 STA: 173+75.9, 45.1' LT CONST. TYPE J-7T MH 6'SQ.77 THROAT=53.20 ----FL. IN=46.00 FL: IN=44.00 FL: OUT=43.50 165 LF-6" ADS UNDR @ 0.67% 77' UNDR FL. 49.40 53.42 ____ CO FL. 49.90 CONST. 168 LF OF 42"RCF -. CONST. 53 LF OF 42"RCP (@ 0.38% S-74) @ 0.65% × 52.59• STA: 174+40, 5.0' RT CONST. TYPE P-1 INLET THROAT=52.60 FL. OUT=48.60 175 28 LF Γ FL. 49.80 52.72 CONST. 63 LF OF 18 RCP 174 0 0.48% 52.96 52.86 175 52.59 - 52.81 88 LF 52.62 -----52.87 TYPE 'E' CURB. & GUTTER 52.83 UNDR 100 LF-6" ADS_ FL. 49.60 UNDR @ 0.30% -9 60'-6" ADS 100'-6" ADS J- UNDR @ 0.30% > 75 LF-6" ADS UNDR @ 0.67% \UNDR @ 0.40% 52.83 \checkmark 53.19 CO S-75 FL. <u>49.80</u> STA: 173+76.83, 6.12' RT CONST. TYPE P-1 INLET THROAT=52.63 FL. IN=44.35 FL. IN=48.30 FL. OUT=44.20 STA: 017=44.20 STA: 173+76.83, 6.12' RT S-5' WIDE CONC. SIDEWALK -------(5-73-) STA: 173+36.16, 83.41' RT T3 STA: 173+36.16, 83.41' RT CONST. TYPE P-1 INLET T2 THROAT=53.40 FL. IN=44.65 FL. OUT=44.65 (S-72) STA: 173+54, 88.5' RT CONST. TYPE J-7T MH \odot TOP=54.00 FL. OUT=44.71 S-72 RT | S.E. TRANS. – LT. E.O.P. 140' S.E. TRANS. - RT. E.O.P. 58 ഗ IRAN. TRAN 72.00 9 CEND S.E.GTRANS. PBEGIN NO 420. 4.C. E.O.P. 53.424 ULL S.E. F.O.H 53.1 END N. (BEGIN - LTI E ELEV END F BEGIN STA: ELEV – EXISTING GRADE (S-76) 0 34% ____ 52 ____ -----------------50 Concession of the local division of the loca . ------CONST. 169 LF OF 42" RCP 48 @ 0.65% 46 ---- FL. 42.50 46.00 -1'' = 40' HORIZ.1'' = 4' VERT.SCALE: 44 \frown (RCP TO U 1-1 310 AT BRATE 174 44.00 E ULTING ENGINEERS NERS • SURVEYORS OURTLAND STREET IDO, FLORIDA 32804 E: (407) 629-1061 ORANGE COUNTY, FLORIDA AVALON PARK BOULEVARD M.4. 1.N 70394 PLAN & PROFILE SHEET 29 OF 121 60% SUBMITTAL 4-06 101

------S-56 [S-55] (S-57) STATION STA: 164+50.22, 55.5' LT CONST. MASONRY PLUG STA: 164+20.72, 44.50' LT CONST. TYPE P-1 INLET FL. TN=48.30 (E) INDEX NO. 211 CONST. 12 LF OF 18"RCP / @ 0.83% CONST. 184 LF (S-55) (FUTURE INLET) THROAT = 52.71OF 30"RCP FL.=48.10 @ 0.24% UNDR. UNDR. FL. 49.70 FL. OUT=46.40 FL. 49.70 UNDR. 52.64 \$52.65 CO S-57 183 LF-6"ADS FL. 50.55 ⁻FL. 49.60 ' (S-50) - 30 LF- _ 6"ADS_UNDR @ 0.33% UNDR. @ 1.00% S-56 CONST. 31 LF OF 24"RCP 210 LF-6"ADS CONST. 30 LF CONST. 45 LF @ 0.32% UNDR. @ 0.90% OF 24"RCP OF 18"RCP @ 0.22% 53.36 S-54 @ 0.33% 52.82 53.37 • 54.37 163 54.61 165 CO FL. 50.93 T.CO 53.36 53.37 CONST. 45 LF 53.36 (FL. 51.60 OF **18"**RCP CONST. 30 LF OF 18"RCP CONST. 30 LF OF 18"RCP 176 LF-6"ADS @ 0.22% UNDR. @ 1.00% @ 0.33% UNDR. @ 0.33%7 *S–51* ⁻FL. 49.60 FL. 50.55 \checkmark 52.71 52 UNDR. _ 30 LF-FL. 49.70 6"ADS UNDR @ 0.33% UNDR. FL. 49.70 (S-51) S-52 (S-53) STA: 164+19.69, 44.50' RT STA: 164+50.22, 44.50' RT CONST. TYPE P-2 INLET CONST. TYPE P-1 INLET INDEX NO. 211 THROAT=52.71 INDEX NO. 211 THROAT=52.60 E FL. OUT=48.50 (S-52 FL. IN=48.40 NO 0 (S-54) *FL. OUT=48.40* STA: 164+50.22, 0.0' RT CONST. TYPE P-1 INLET WETLAND CONST. TYPE P-7NT MH INDEX NO. 211 TOP=53.90 THROAT=52.76 FL. IN=48.30 FL. OUT=48.50 60 200.00° VC -BVC 5163+00 60 BVCE: 54.42 8 LOW POINT ELEV = 53.3604 40.40 LOW POINT STA = 164+61.11RT. & LT. E.O.P. -NO WINY C END N. BEGIN - RT. 1 ELEV: PVI STA = 164+00 PVI ELEV = 53.10 A.D. = 1.64 (S-57) K = 122.225-50 [*S*–*56*] 54 -1.329 52 - . 50 - FL. 48.60 48 CONST 30 LF - OF 24" RCP FL. 48.10-CONST. 184 L -FL. 48.50 @ 0.33% CONST. 31 LF OF 18" RCP -ØF 30" RCA 46 @ 0.25% @ 0.33% 18" RCP TO FL. 48.20-<u>(S-54</u> 165 163 164 FL. 48.20 Plotted: Apr 27, 2001 - 11:57am DESCRIPTION DATE: BY DESCRIPTION DATE: BY DESCRIPTION DATE: BY



Appendix: M

Excerpt from Orange County Public Schools Timber Creek High School Construction Plans



M-1



M-2

Appendix: N

SR-50 Straight Line Diagram



Appendix: O

Excerpt from Lochner Regional Drainage Map



USER: Jaoff or 2/6/203

Appendix: P

Excerpt from SR-50 Original Construction Plans


DRAINAGE MAP STATE OPANCE Sa 1891445 Eust dzd Core Bat HL IT 3943 HL FT 5330 Corst dxd Conc. Box Culvit. Exin.; FL 5940 Asst4 35 Che Const 3-36 Conc. Pipe Curve Extra (Skew) FLU:58.4 NOTE: 1945 H.W.ARE ESTIMATED AS A BOYE FREQUENCY STORM. a 50 211.2 AG. 117. I AC. No. And Address of the **SR-50** CD-7 212 SQ. MILES



DRAINAGE MAP 3. P. Nº 520 DEFETTLT) 60 PROVILES ON S. D. 520





TELLEDAD STATE FROM NE FIGAL SHEET TOTAL DINK NO SHEET SO SHEET State Job Nº 15060-3505 0 695~00 -Const 100 or Guardrail a substant is sub-to sub-to state his sub-to s Const 50' of Guardrail -Remove all Guardrail Lt of Bdwy. Store as directed by the Engineer. To be hauled by maintenance department. 01 BEGIN RESURFACING RT. ROADWAY STA, G93+15,05[±] 10 1.10 60 50 +0,25% 7 0.00%7 -Sta 693+11 Const Inlet Type C in Med. FL 39.0 P-4









PEDINOAD STATE PEDINE VIEW SS SECTOR State Job No 75080-3505 820:00 Mod. 190 8184 34000 010500 1390 3 MN 70 PLEXE97 R. B. SPIKE IN 8 FIME 14 'ET ± 574 810155 30 Jule 20 **P-8**









TED READ FRATE PROVING PRESENT TO THE PROVING THE PROVING PRESENT FRATE PROVING PRESENT TO THE PROVING PRESENT FRATE PROVING FQUATION 935400. Sta. 10400 (UNE-2 Sta. 236420.95 93 [12:00 Linc 132.30 0---------Sta 3364 4540-PC Sta. 10400 10. 335405 300.050 4 N Nº 82 ELEV (G.3. R. SPRE IN 12' PINE 10 T & STA 938104 £5.250 71:33(£) RD Si all 10.35 £ 1 _Rt 0.91.653 Sto 340100 Cons 18 Pice Curvi e Inie. FL Inier LE 67.2 FL Inier LE 67.3 FL RE 65.3



5747E F-022-1(5) 62 2/ STATE 2 0 State Job Nº 75060-3505 58. M. N¹²85 ELEV 63085 10 V88 Dridge Spike in 10 Pine 139 Rf. & Sta. 368+35 (ND R.C. REQD.) 71.22 0.20% UT.D.PI. 6655- SFEC. DT. DT. -0.15% Sla scaloo const B' Pice Calif F Inlet TL Inlet 675; FL.P. 673 67.5. 8 P-13

Appendix: Q

Excerpt from Lochner SR-50 Widening Construction Plans

COMPONENTS OF CONTRACT PLANS SET

A DETAILED INDEX APPEARS ON THE KEY SHEET OF EACH COMPONENT

ROADWAY PLANS SIGNING AND PAVEMENT MARKING PLANS SIGNALIZATION PLANS ITS PLANS

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION



CONTRACT PLANS

FINANCIAL PROJECT ID 239203-4-52-01



FDOT PROJECT MANAGER: CHRISTOPHER L. DABSON, P.E.

\$DATE\$

ROADWAY SHOP DRAWINGS TO BE SUBMITTED TO: JOHN N. BOX P.E. NO. 41832 H.W. LOCHNER INC. 13577 FEATHER SOUND DR., SUITE 600 CLEARWATER, FLORIDA 33762

PLANS PREPARED BY:

LOCHNER

H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 15577 FEATHER SOUND DR., SUITE 600 CLEARWATER, FLORIDA 33762 VENDOR NO. 36-2338811 CONTRACT NO. C-7461 C.A. 894

NOTE: THE SCALE OF THESE PLANS MAY HAVE CHANGED DUE TO REPRODUCTION.

PLANS UPDATE PERMIT SUBMITTAL SEPTEMBER 2012

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> V	ROADWAY PLANS ENGINEER OF RECORD (E.O.R.):
	P.E. NO

TISCAL YEAR	SHEET NO.
14	/

JOHN N. BOX, P.E.

41832

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DATE BY DESCRIP	REVISIONS TION DATE BY	DESCRIPTION	H. W. LOCHNER, INC. CONSULTING ENGINEERS AND PLANNERS 13577 FEATHER SOUND DRIVE, SUITE. 600 CLEARWATER, FLORIDA 33762 THERESA D. ELLISON, P.E. NO. 53918	STATE OF FLO. DEPARTMENT OF TRAN ROAD NO. COUNTY S.R. 50 ORANGE	S.88 AC. RIDA VSPORTATION FINANCIAL PROJECT ID 239203-4-52-01

9/6/2012



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BEGIN SIEEL HANDRAIL/ CONST. 63.4' x 12.5' RUBBLE RIP RAP) WING WALL DITCH LINING (INDEX 28) STA. 680+76.34, 80.83' LT	ND STEEL HANDRAIL/ HNG WALL TA. 681+39.68, 80.83' LT		JURISDICTIONA WETLAND LIMITS	R/W LINE
Asphalt SW Brown 24 TO BE REMOVED	S V S S	<u></u>	н н н н н н н н н н н н н н н н н н н	ND GUARDRAIL W/ CARALLEL END ANCHORAGE
	(s=70) — -5' - CONC5	W		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	T. 158' OF 4" PIPES == = = = = = = =		0NST. 307' OF 19" X 30 	PIPE
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	\$-702A	· · ·		<u>3.00 LT</u>
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CONST = 18" PIPE = BEGIN STEEL PICKET RAILING/	■ END GUARDRAIL I TYPE—II END—ANG STA. 681+71.22,	W/-038		CONST.
	6=702B			
EXIST. FLICE			(5-771) +00.9/ 84.00' RT	<u></u>
Image: State	ID STEEL PICKET RAILING NG WALL A. 681+43.49, 87.41' RT	+17.31 103.20' RT	L/A R/W LINECONST.	299' OF 18" PIPE
BM#34 STA. 68/+/9.50, /50.95' RT. (B S.R. 50)	702B			
BRASS DISK STAMPED FLORIDA D.O.T. SURVEY MARKER D5PNC 750371, EL. 60.448 (+) 50.000% LT		GRADE LINE	0.300% (-) 0.300% (D	(-) 0.3(
(+) 0.300% (-62/B)	Exist. Grd. @	€ Const. S.R. 50		
60	$F_{L} = $.640%		
DP LT. = 58.57				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	FL 56.58		Const. 19"x	lip. Ripe (+) 0.050%
55 (-) 0.2672 (-) 50.000% RT.			BEGIN SE	END SE
25 CONSV. 10 TIPE	DP1 RT. 681+40.19		683+00.0	0 EL. 57.00 685+00
<u>680+76.34</u>	EL. 57.73	682+50.00	D EL. 59.53	
	+) 50.000% RT.			
	<u>681+25.85</u> <u>EU 50 56</u>			
50 EL 50.96 DP/ RT. (+) 0.000%				
680+93.59 E1. 50.56				
	682		683	684
			STATE OF	FLORIDA
DATE DI DESCRIFTIUN DATE DI DESCRIPTIUN	13577 FEATHER SOUND DR. CLEARWATER, FLORIDA 333 FBPR CERTIFICATE OF AUT	SUITE 600 762 FH. [#] 894	DEPARTMENT OF 2	FINANCIAL PROJECT ID 230203
	JOHN N. BOX, P.E. [#] 41832	3.	n. ju UKANGE	holden 7/19/2012



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		00+202	+10.52 R/W LINE 24' 24' 24"RCP	RCP	CONST. 127		BEGIN S	TEEL PICK	KET RAILING					CONST RUBBLE DITCH L	100 ¹ 0' x 17 RIP RAP INING (INDI	ET RAI	LING/	E	W W			END G
		STA. 7		The second secon				<u>5' CONC.</u>	SW	BI				WING-W STA: 7	ALL	83.00' ^	<u>L</u> T		BT	18		S7A.
,00,00			\$-730			ST. 142' 18" PIPE	5-734	BEGIN GUA	RDRAIL W/ ND ANCHORAGE				YPE F C&	G	<u>· · · · · · · · · · · · · · · · · · · </u>	COI	VST. 10)7'		5-8	303	CONS
	2.00'		CONST. 36"	PIPE EXI	STING STRUC E TO BE RE	TURE &	B CONST.	<u>BEGIN E</u>	BRIDGE CULVER	LT T.75083	3	× × × ×	CON:	ST. 151' 12' x 8'	OF CBC	0F 	18" Pl.	PE 				OF 2
	56	,00		·		9°48'25" e	e = - 4.00'	59 STA. T	10+00.05			0'7 BC					— € co	NST. 8	& B SUR	VEY S.R.	50	
			i			/ ≥ ¥l	2		16.00' LT					LI	l				l			I
	16.00			CON	51, 118' 6"PIPE	<u> </u>						VENT	\+42.1 4.00'	8 <u>N</u> 8	9° 55′	14" E						·
	,00			AND B	NST. JACK ORE PIPE CONST	142' —	STA. 700	8+42.06	CONST. S.R.	<u>+92</u> 16.0	0'_ <u>R</u> T	BFC -		BRIDGE	CUI VERT.	50027	- В	F 0		BF		
,00	40.0			in management	BFD - OF d8"	PIPE		1+00.00 @ 35)— —	EXISTING END	REMOVED		}	STA.	710+26.	55 S-802		CON: OF	ST. 101 18" P11	PE	5-8	304	
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			8	MILLING & RE CURB RETURN	SURF AC ING		SR 50 CD	-3	CONST RUBBL DITCH	, 150.0' E RIP F LINING	x 20.0' RAP (INDEX 2		6) 	RE TUF		S PC 713+-	STA 45.70	0FFSE 56,00'	ET ELEN RT 5.	2.76	PT ST 28+96.6	A OF 57 //.e
				BM#38 BRASS [Sta, 710-).SK +42.91, 88.02	''LT.(B2 S	5.R. 50)						BM#3 	9 710+68 CONC.	R 50	RT. (B	S.R. 5	50)				+
				HEADWAL D5PNC 7	L STAMPED 50374	FLORIDA D	D.O.T. SURVEY N	IARKER				54.57	<u>WITH</u> D.D.T	BRASS &		IPED FL BM# 70	ORIDA DELEV	46.39				
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						SPEC.	EL. 45.10		9+50.00 EL. 45	.54					- - <u>END</u> \$PE 7/0+50.0	C. DT		E4.	47.50	*	+	SPEC
	45	5							*)PI LT.	DP1 LT. 710+26.04	/^D /\co /\co 7/	PI RT. 10+48.40		0 21. 41	(+) 3.0					SPEC.
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										FBPR C.	I BOX, P.E	E OF AUTH. # . # 41832	894	S.	.R. 50	OF	RANGE		239203	3-4-52	-01	
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																	CL	EARV	VATER, FLO	ORIDA 3	3762 1754 [#]	804		ROAL	NO.	-	COL	UNTY		FINA	ANC/AL	PROJEC	TID	l	
																	JO	HN N	. BOX, P.E.	# 41832) I FI. "	074		S.R	50		ORA	ANGE		239	3203	-4-52	2-01	l	
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	STA. 721+02.63 /00.00' LT +14.14 //////////////////////////////////	URF &		38	
	PIPE TO BE REN 18 CMP CR-10 +27.62 83.99' LT	OVED		BT	
	4 S	5' CONC. SW			
100.00	(\$-820) CONST. 24" PIPE ≤	CONST. 159' (S-822) DF 24" PIPE	CONST. 132' (S-824) OF 24" PIPE		(S-826) CONST. 117' OF 18" PIPE
			- € CONST. & ₽ SURVEY S.R. 50		7.00
0,16.0		TYPE E C&G			
16.0		+07.25 +57.25	<u>N 89° 55′ 14″ E</u>		
40.00'	EXISTIN PIPE TO IB" RCP		EXIS PIPE	TING STRUCTURES &	EXISTING STRUC PIPES TO BE R IB"RCP CONST. OF IB"
0.001	W OJE	CONST. 24" PIPE	OF 24" PIPE	OF 18" PIPE	
	HT HT COncrete SW 27'	5' CONC. SW TYPE F, C&G	s - 24' - 0' STEL намовал	24' D'STE D'STE HANDRA	24' 5-852) 10' STL HANDR/ HANDR/
<u>↓</u>	<i>LEGEND:</i> <i>HILLING & RESURFACING</i> <i>CURB RETURN</i>	R/W LINE	<u>+13.80</u> / <u>+13.80</u> / CONST- 89' OF 18"	PIPE CONST. 105	5' OF 18" PIPE
	95.90				
60					
		FILE GRADE LINE (5-823)			
55		(+) 1.000% FL 52.28 - FL 52	FL 52.41	- FL 52.91	FL_53.16
	Const. 24" Pipe ⁽⁺⁾ 0.526%		Const. 24" Pipe	Const.	
50	6.5" WATER		END SPEC. DT RT. 723+50-00 EL. 54-45		
	25.97				
	721 722 REVISIO	N S	└ <i>7≵4</i> ── I @©HNER	5725 STATE OF FL	726
DATE	BY DESCRIPTION D	AIL BY DESCRIPTION	13577 FEATHER SOUND DR. SUITE 600 CLEARWATER, FLORIDA 33762	DEPARTMENT OF TRA ROAD NO. COUNTY	ANSPORTATION FINANCIAL PROJECT ID
			FBPR CERTIFICATE OF AUTH. [#] 894 JOHN N. BOX, P.E. [#] 41832	S.R. 50 ORANGE	239203-4-52-01

SEE PEBBLE BEACH BLVD. PLAN-PROFILE SHEET			SR 50 CD-4	
5 5 100.00' LT				2
HE2:48 HE	S STRUCTURE JURISDICTIONAL REMOVED WETLAND	TYPE F Č&G		
€ Const. C. 10 PEBBLE BEACH BLVD. CONST. 10 90°00'90" 435.58	8"-PIPE	OF18"PIPE		OF 18" PIPE STA. 734+04.93 € CONST STA. 30+00.00 € CONST, +00.00
SEE SPECIAL DETAILS	730	/— € CONST. & ₱ SURVEY S.R. 50 731	232 024 027 02 02 02 02 02 02 02 02 02 02 02 02 02	133
STA. 728+	02.54 € CONST. S.R.50 = 0.00 € CONST. PEBBLE BEACH BLVD	TYPE E C&G - N 89° 55' 14	" E	·
00.99 0.	RUCTURE VED IB" RCP IB" RCP CR 21 4	CONST. 97. BE D 3 8 - 833	EXISTING STRUCTURE TO BE REMOVED CONST. 42' OF 30" PIPE S-902	EXISTING STRUCTU PIPE TO BE REMO
Q	VALLEY JALLEY SCONC			sF/- ^S -58-43-
HOLE CR-24 CR-24 CR-24 CR-24 BT CR-24	GUTTER 26' 5-856 9 CONST. 8' OF C	TYPE F C&G 30' 5-861 S-860 BT O C BT O C BT C	CONST. OF -18"	247' PIPE EL. 58.2
LEGEND: MILLING & RESURFACING CURB RETURN) • • • • • • • • • • • • • • • • • • •	Image: style	(\$-870) 	STA. /73 100.24' <u>MAT</u> STA
BM#4/ STA. 729+74.16, 117.45' RT. (& S.R. 50) BRASS DISK STAMPED FLORIDA D.O.T. SURVEY MARKER D5PNC 750376 FL 58.278			BM#42 STA. 733+96.64, 1258.59' MAG NAIL & DISK STAMPED D5PNC 7 EL. 54.481	RT (& S.R. 50)
	PROFILE GRA	ADE LINE 945	Exist. Grd. @ Const. S.R. 50	
60 (-) 0.3	00 % (\$-830)		(\$-90/)	(+) 0.30
BEGIN SPEC. DT RT. 728+50.00 EL: 55.25 AL 53.55	53.55 FL 53.70 - FL	53.70 DP/ RT. 730+50.00 DP/ RT.	-870 - FL 54.23	,
55	(-) 0.300%	/EL. 54.6573/+50.00 /EL. 53.10	Const. 30" Pipe	
Const. 18" Pipe	Const. 18" Pipe	st. 18" Pipe (-) 1650%		
		FL 53185 - FL 52.18 -		END SPEC. DT RT.
50				
28.14				
728 729				733
DATE BY DESCRIPTION DATE	BY DESCRIPTION	LUGHNEK 13577 FEATHER SOUND DR. SUITE 600 CLEARWATER, FLORIDA 33762 FBPR CERTIFICATE OF AUTH # 894	ST. OF FLORIDA DEPARTME. OF TRANSPOR ROAD NO. (Y FIN)	ANCIAL PROJECT ID
		JOHN N. BOX, P.E. [#] 41832	S.R. 50 URANGE 239	9203-4-52-01

2.00'	STA. 735+00	CONS	5" RC +18 8"CMP 24'	P .95 Asp	PPE			P44 RCC	-905				STR BE 79777 18"	UCT RE 20 СМР 8.23 60 0F	URE: MOVE + 	S & 53.6 	65 67 67 67 7 7 7 7 7 7 7 7 7 7 7 7 7 7		TY1 5' (F - C. 	- R / 86 -	W LI	NE = + = +			22	478 4' 18"CM	.72 P	1.56			6 S 0 E		TURI EMOV	ES 8 /ED	 							R/W E P	LIM XIST IPE U V CONS OF_I	E TO DE TI VARI SURI ST. 8"_1	STF BE ECTA NING ACE 247' PIPE	RUCT REM ABLE	URE IOVE	5 & D D GUT	30+84 10.30 TER -
:00, 5	,									736		-¢	CON	S <i>T</i> .	& 4	₿ si	URVI	EY S	5.R. 7	50 37									738	3								73	39					_	_			740)	R=3	R
16.00' 4	ч 1		_		I							7	YPE	E	C&G																A	- 89	<u>+</u>	5	<u> </u>	E														R	3' -(
40.00'	MATCH LINE		NST. EGEN			LINE NG & RE 1	s RE TURN	CO OF S SURF	NST - 18" - 906 	. 127 - PIP 5' CO TYPE	RE TU (2)	SW C&G	; ; RAI		s	B B B B B B B B B B B B B B B B B B B	s	BT	0FF 9.00	۵. ۲۱۹۵۶		- CC OF 308	0NST - 18" - 18" - 18" - 18" - 19 - 19 - 19 - 19 - 19 - 19 - 19 - 19	- 127 PIP 	PT S D+70 D+70	TA 0.00 3.9/	0F 20. 59.	18" FSE 33' 00'	<i>RCP 24¹ 24¹ 1 1 1 1 1 1 1 1 1 1</i>		EX PII VATI 5.30 5.30						CONS OF 1		37' IPE			TA. IA. S	740	+68 			ONST -911	FI S I S I C S I C	S.R.5 RANK BFL 2 0.44 7 1. 00.00	60 = 51 	43.80
60	59.07															- PR(E G	RAD																				BM ST BR ST CON EL	#44 ISS IMPE TROL 56.7	0+8 DISK D 01 2 L- 752	24.99 RAM €609	9, 10 GE 1-05	00.69 COUI	9' <u>(</u> 7 VTY	τ. μ ENG	₽ s. R. L	R. S	50) T.		
			-) 0.	300	<u>/</u>	 FL	53.	68 -		5-90	5		 71 5.	3.68				 FL	53.				907) K			— E 53.4	 B	. Gra	/. @ 	Ę .	Cons 53.4	t. S	5.R.	50	9	 F	 5.	3,10							52.6	5 -		<u>s</u> -9/	2		
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				5' CONC. SW				<u>*</u>		
	CONST. 92' (OF 18" PIPE	S-917 C	CONST. 332' DF 24" PIPE	TYPE F C&G —	· · · · · · · · · · · · · · · · · · ·	¢	CONST. & 🖻 SUR	(S	-920 DE TECTABLE WARNING SURFACE	
	743	·	744	TYPE E C&G —	745	N 89° 55′ 14′	746 	· · · · · · · · · · · · · · · · · · ·	747	
CONST. IB" PIPE S-916 R/W LINE LEGEND: MILLING & X CURB RETU	CONST. 92' OF IB'S PIPE	5-918 0 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	5' CONC. SW	PE F C&G	BF0		STA STA STA BF (5-919 WWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWWW	. 747+51.90 & COI . 30+00.00 & COI . 30+00.00 & COI 	NST. S.R.50 = IST. SMITH STREET OF T. (ATION PT STA 5.12 - 30+72.97 IB 1.99 747+84.41 55 RA	20057.238 24" PIF 24" PIF 579' LT 379' LT 300' ET W LINE —
		\$-917)			00.00+ 13 (+) 0.300%; (-) (D.700%	Exist. Grd. @	€ Const. S.R. 50	9.00- <i>E</i> L 56.04	55,90
FL 51.89	FL 48.66 (-) 0.220% FL 48.80 (-) 0.050%	22-1/2 22-1/2 22-1/2	9 2 2 2 3 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		Δ. Δ			25 ¹ 95 773 00°05+ 82 1 65°95 FL 1 12°95 FL	(S-920) +	
DPI RT. 742+50-00 EL. 50.33 DESCRIPTIO	/ / / / <td>S E BY</td> <td>2 48.16 744 DESCRIPTION</td> <td></td> <td>745 0 CHNE [FEATHER SOUND D</td> <td>4" Pipe</td> <td>746</td> <td>STATE OF FLORA</td> <td></td> <td>47+00.00 L-50.10</td>	S E BY	2 48.16 744 DESCRIPTION		745 0 CHNE [FEATHER SOUND D	4" Pipe	746	STATE OF FLORA		47+00.00 L-50.10
	CONST. IB" PIPE S-916	CONST18" PIPE CONST. 92' G-96 OF 18" PIPE NILLING & RESURFACING NILLING & RESURFACING <td>CONST 18" PIPE G-96 CONST. 92' OF 18" PIPE CONST. 92' OF 18' OF 18' O</td> <td>CONST. 18" PIPE CONST. 92' C-90° CONST. 92' C-90° CONST. 92' C-90° CONST. 92' C S CONC. SW S CONC. SW C S CONC. SW S CONST. 18" PIPE S S S S S S S S S S S S S S S S S S S</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>CONSIL 18", PIPE CONST, 52" G-90" OF 18" PIPE S' CONC, SN NULLING & RESURFACING ORB RETURN ISSUE ISSU</td> <td>Image: Elission Image: Elission Image: Elission Image: Elission Image: Elission Image: Elission Image:</td> <td>Image: State of the s</td> <td>Image: Line Image: Line</td> <td>1/11/2 C. W. N 89° 55° 14° E 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. W. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. W. W. W. W. W. W. 1/11/2 M. S. W. W.</td>	CONST 18" PIPE G-96 CONST. 92' OF 18" PIPE CONST. 92' OF 18' OF 18' O	CONST. 18" PIPE CONST. 92' C-90° CONST. 92' C-90° CONST. 92' C-90° CONST. 92' C S CONC. SW S CONC. SW C S CONC. SW S CONST. 18" PIPE S S S S S S S S S S S S S S S S S S S	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	CONSIL 18", PIPE CONST, 52" G-90" OF 18" PIPE S' CONC, SN NULLING & RESURFACING ORB RETURN ISSUE ISSU	Image: Elission Image: Elission Image: Elission Image: Elission Image: Elission Image: Elission Image:	Image: State of the s	Image: Line Image: Line	1/11/2 C. W. N 89° 55° 14° E 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. W. W. S. M. 167-56.00 C. W. 1. 1/11/2 C. W. W. W. W. W. W. W. 1/11/2 M. S. W. W.

,00.00'	.00' STA. 756+00	R/W LINE 15"RCP 	JURISDICTIONAL WETLAND-LIMITS CONST. 8' ÖF 19' x 30" PIPE	+56.67 99.37' LT 5-97) CONST 27' 8 42' PIDE	+06.00 100.00' LT +40.00 /76.68' LT +40.00 /60.00' LT +40.00 /60.00' LT END PROJECT STA, 759 +00,00 	JURISDICTIONAL WETLAND LIMITS R/ STA 100. 9"x30"RCPE +26.00 60.00" LT	W LINE 5 W LINE
,00.001	VE 41.50' 41.50' 56'	409.72 409.72 409.72 409.72 409.72 409.72 409.75 409.86 14.98' RT 409.86 14.98' RT 409.86 14.98' RT 5' CONC SW	102 TYPE 400' T 102 TYPE 102 TYPE	E C&G	N 89° 55' 14" N 89° 55' 14" E CONST. E 18"RCP +80.29 56.00' F	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	90°00'00" 90°00'00"
<u> </u>	52.50 MATCH LII	TYPE F C&G	$Curve = R22$ $Delta = 102+33.3$ $Delta = 3^{\circ} 53' 1$ $Delta = 3^{\circ} 53' 1$ $Delta = 3^{\circ} 63' 1$ $Delta = 6,878.00$ $PC STA. 100+00.00$ $PT STA. 104+66.59$	39 12.63" (LT) 58'91"	SHLDR. 4'	SHLDR. 	9 TB 1 2 30 2 2 2 2 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	55	PGL LEF	STA. 755700.00 & CONST. STA. 100+00.00 & E.B. TR PGL LT @ 16' LT OF & CONS -933 	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2 0.600X -7 0.700X ===================================	PGL LT ====================================	END PGL LT MATCH EXISTING PAVT. STA. 760+26.00 EL 50.99 PGL RT @ EB SR 50 \$-935A (-) 0.700% \$.R. 50 DPI RT.
	45 55.95 7	(-) 0.340% FL 43.50 - Const. 30" Pipe IOL 56 7	FL 44.60 FL 43.50 FL 43.50 Const. 42" Pipe Image: State of the state	STA. 759+00 9 EL. 5/,73	STA. 759+00 EL. 5/.74 SPEC. SPEC. Const. 42	DT RT.	761+00.00 EL. FL 105 761
DAT	<u>E B</u> ì	DESCRIPTION	V I S I O N S DATE BY DESCRIPTION	LOCHNE 13577 FEATHER SOUND CLEARWATER, FLORI FBPR CERTIFICATE O JOHN N. BOX, P.E. # 4	D DR. SUITE 600 DA 33762 F AUTH. [#] 894 1832	STATE OF DEPARTMENT OF ROAD NO. COUNTY S.R. 50 ORANGE	F FLORIDA TRANSPORTATION F INANCIAL PROJECT ID 239203-4-52-01

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Appendix: R

Excerpt from Comprehensive Engineering Services, Inc.

SR-50 Widening Construction Plans

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	EXIST. F.L. AND RIPE SIZES ARE FROM	I FIELD SURVEY.				
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45	(A-11)	PGL Lt.				
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				E	XIST. GROUND LINE	AT & CONST. SR 50
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35		FL 41.20	FL 39.40J			
	8					
						FL 30.60-
25	772 774 776	778 780 7	782 784 786	78	8 790	792
(24	$\begin{array}{c} 18" \ CMP \\ W \ INV. \ 44.46 \\ E \ INV. \ 44.46 \\ E \ INV. \ 44.62 \\ E \ INV. \ 43.32 \\ C \\ E \ INV. \ 44.62 \\ W \ INV. \ 43.00 \\ 18" \ RCP \\ 29 \\ 18" \ PIPE \\ W \ INV. \ 43.00 \\ F \ INV. \ 45.02 \\ F \ HN4. \ 42.75 \\ F \ HA4. \ 42.75 \ HA4. $) 18" CMP W INV 42.01 E INV. 42.01 W INV. 39.50 E INV. 41.72 W INV. 39.28 E INV. 41.72 W INV. 42.00 W INV. 40.75 E INV. 41.70 B-4 B-5 E INV. 40.50 B-4 B-5 E INV. 41.70 B-3 T 80 B-3 T 80 B-3 B-3 B-3 B-3 B-3 B-3 B-3 B-3 B-3 B-3	$E = (43) AS'' PIPE (46) 34'' \times 53'' \\ 40.00 W INV. 40.10 \\ 5 INV. 38. \\ N INV. N/ \\ 34 \\ -7 \\ 34 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -7 \\ -$	ERCP ^J (49) .30 A	18 PIPE 52 5 NV. 34.25 N INV. 33.75 790 T	10" CPP W INV. UNK. E INV. 38.96 SR-50 Econ-Bi
	22 · 23 · 24 (1) 22 · 23 · 24 (1) 2.39 Ac.	$\begin{array}{c} B-2 \\ 25 \\ 25 \\ 59 \\ Ac. \\ 0 \\ SB-2 \\ SB-2$	32 C. 35 35 8-8 5B-5 32 C. 35 35 8-8 5B-5 35 35 8-8 35 35 8-8 35 35 8-8 35 35 35 38 42 43 43 43 43 43 43 43 43 43 43		46	NECONIOCEHARTCHE
		SHERMAN ST.		~*		S "35 "EF ALLER
REVISIONS DATE DESCRIPTION DATE PRELIMINARY DATE NOT FOR CONSTRUCTION		SIONS DESCRIPTION	Comprehensive Engineering Services, Inc.	_	STATE OF FLC	DRIDA
			201 S Orange Ave, Suite 1300 Orlando, EL 32801-3442	DEP	ARTMENT OF TRANS	PORTATION
			Certificate of Authorization No: 7862 Eric Arp. P.E., License No: 53971	SR 50	ORANGE	239203-7-52-01
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	EXIST. F.L. AND PIPE SIZES ARE FROM FIELD S FPID 433607-1-52-01, 239203-4-52-01 AND 43067 DO NOT USE THE INFORMATIO SHEET FOR CONSTRUCTION PL	SURVEY, 3-1-52-01. N ON THIS IRPOSES.	EXIST. GROUND LINE	AT Q COWS	T. SR 50	
55	This sheet is in the plans for	documentation			PGL L	t. & Rt.
	and to assist construction per	sonnel with				
	drainage concerns.					(B-32)
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(54) 30" W 1	RCP (58) 30" CMP (61) 18" PIPE NV 36 28 W INV 37 32 W INV 39 44	64 18" PIPE 5 S INV. 41.15 W INV. 44.44		1 acres	<~	
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(56) 18"	PIPE (59) 18" PIPE / 62A) 30" RCP	(66) 18" PIPE	15		5 41	- 101
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DATE DESCRIPTION DATE PRELIMINARY NOT FOR CONSTRUCTION		DESCRIPTION	Comprehensive Engineering Services, Inc. 201 S Orange Ave, Suite 1300 Orlando, FL 32801-3442	STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION		
				ROAD NO.	COUNTY	FINANCIAL PROJECT ID
			Certificate of Authorization No: 7862 Eric Arp, P.E., License No. 53971	SR 50	ORANGE	239203-7-52-01
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R-6











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R-16

Appendix: S

SR-50 Field Visit Photos (May 2016)



SR 50- CD1 (2-8' x 6' CBC) (Looking North Side of the Culvert)



SR 50- CD2 (2-24" RCP)

(North side of the Culvert)



SR 50-CD3 (2-12.95' x 8.5' CBC)

(South Side of the Culvert)



SR 50-CD4 (1-30" RCP) (South Side of the Culvert)



SR 50-CD5(3-10'x6' CBC) (South Side of the Culvert)



SR 50-CD6 (3-36" RCP) (South side of the Culvert)



SR 50-CD7 (4' x 4' CBC & 1-54" RCP Jointed)

(South Side of the Culvert)



SR 50- CD8 (1-30" RCP)

(South side of the culvert)



SR 50- CD9 (1-8'x7' CBC) (South Side of the Culvert)



SR 50-CD10 (1-10'x4' CBC)

(South Side of the Culvert)



SR 50-CD11 (1-24" RCP) (South Side of the Culvert)

Appendix: T

Excerpt from CAD Engineering and Design, Inc

Waterford Creek





Appendix: U

Excerpt from The Civil Design Group University Meadows & Bridgewater Plans



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No. 1991

U-1





NOTE: ALL LOTS TO BE GRADED AS SHOWN ON THIS LOT GRADING PLAN. FINIHED LOT GRADE FOR BUILDING PADS SHALL BE 6° BELOW THE FINISHED FLOOR ELEVATIONS SHOWN ON THE PLANS BELOW.

Used for Finished Floor Elevations located within the Floodplain Map

LEGEND:

- 62.4 / FINISHED GRADE ELEVATION 64.3 FINISHED FLOOR ELEVATION EXIST. GROUND SURFACE CONTOURS
- × 62.4 GROUND SHOTS FROM ACTUAL FEILD SURVEY



MASTER GRADING PLAN 215700 21-095-20788-Y OCTOBER, 2001 BRIDGEWATER PHASE III RECEIVED 1" = 60'NOY 07 2001 SHEET NO. 4 OF 20 PDS ALTAMONTE SVC. CTR.

U-2

Appendix: V

Excerpt from Glace and Radcliffe, Inc.

Deerwood Plans



Appendix: W

Excerpt from George Garrett, P.E.

Avalon II Plans



v








W-4

Appendix: X

Excerpt from Kisinger Campo & Associates Corp. The Fairways – Self Storage



X-1

1



- ROAD AND DRAINAGE NOTES
 All workmanship and materials shall conform to Fla. D.O.I. STANDARD SPECIFICATIONS FOR ROAD AND
 BRUGGE CONSTRUCTION, 2004 edition and all Orange County Technical Manuals.
 This drawing shows droinage and grading design to within 5 feel of the building(s) only and specifically
 accludes designs for structures, relatining walls, waterprofile and the building(s) only and specifically
 accordinate with others to insure that support designs have been completed by other design professionals
 and that no conflicts estist with any other construction, with sformwater runoff directed to them.
 Over-excavation and burying any debris beneating the prohibide. If dewatering is required the
 contractor shall be excavated prior to any other construction, with sformwater runoff directed to them.
 Order-excavation and burying any debris beneating the prohibide. If dewatering is required the
 contractor shall be excavated prior to any other construction, with sformwater runoff directed to them.
 Contractor shall be excavated prior to any other construction and the prohibide. If dewatering is required the
 contractor shall be seen and solded per the plan.
 4. EROSION / SEDMENTATION CONTROL: The Contractor shall supply all erosion / sedimentation barriers (hay
 bales, sill screens and so forth) to prevent sillation and excess quantities of earth from being fransported
 either by natural drainage or vehicular traffic onto any adjacent properties, streets, storm savers,
 woresway, conservation areas and so forth). The Contractor shall che and restore any areas affected by
 erosion / sedimentation. Erosian control measures are to be in place at the stort of construction and to
 remain in place until construction is completed as a public set. Store any areas of feet. The
 Sourveyor of all drainage and grading construction within 30 days of construction completion.
 4. OPERATION & MAINENANCE OF THE STORWATER MANAGEMENT SYSTEM:
 (a) Regularly cl

Traffic Control Plan: 1. The Permittee shall conduct his operations such that there will be a minimum of interference with or interruption of traffic upon and along the roadway. This applies to both the initial installation and the continuing maintenance and operation of facilities except in emergencies. There shall be no interference with or interruption of traffic upon and along the roadway until a maintenance of traffic plan approved by the county.

to interruption of traffic upon and along the roadway until a maintenance of traffic plan approved by the county. 2. During the installation of the facilities authorized by the Use Permit, the Permittee shall at all times maintain flaggers, signs, lights, flares, barricades, and other sofely devices as required by the applicable slandards or as the County may reasonably deem necessary to properly protect traffic upon the roadway, and to war and asfeguard the public, work crews or County employees against injury or damage. 3. For work within County Right-of-way, submit a maintenance of traffic plan to Orange County Traffic Department.

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Kisinger Campo Associates Corp.	KISINGER 2203	KISINGER CAMPO & ASSOCIATES CORP. 2203 NORTH LOIS AVENUE, SUITE 1200 TAMPA, FL 33607 (813) 871-5331 BOARD OF PROFESSIONAL ENGINEERS CERTIFICATE OF AUTHORIZATION No.00002317	
NO. DATE	REVISIONS	THE FAIRWAYS - SELF STORAGE PAVING & DRAINAGE DETAILS	
		DESIGNED BY: STATE: 06/09/05 DRAWN BY: STATE: 06/09/05 CHECKED BY: NTS. CHECKED BY: NTS. FILE'NO. 2200418	
		ARON CHRISTIPHEN VERSES OF C6	
		Dudle Eliza	