LOCATION HYDRAULIC REPORT

SR 417 (Seminole Expressway) Sanford Airport Connector from SR 417 to Red Cleveland Boulevard

Project Development and Environment Study

Seminole County, FL

Project 417-246A

Prepared for:

CENTRAL FLORIDA EXPRESSWAY AUTHORITY

Central Florida Expressway Authority

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Prepared By:

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June 2025

PROFESSIONAL ENGINEER CERTIFICATION

I hereby certify that I am a registered professional engineer in the State of Florida practicing engineering with The Balmoral Group and that I have supervised the preparation of and approve the analysis, findings, opinions, conclusions and technical advice hereby reported for:

PROJECT: SR 417 (Seminole Expressway) Sanford Airport Connector PD&E Study

from SR 417 to Red Cleveland Boulevard

Location Hydraulic Report Project ID: 417-246A Seminole County, Florida

The engineering work represented by this document was performed through the following duly authorized engineering business:

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This report provides the results of a summary of data collection efforts, and limited calculation for the existing and the proposed cross drain and floodplain evaluations prepared for the conceptual analyses for the Location Hydraulic Report for the Project Development and Environment Study for the SR 417 (Seminole Expressway) Sanford Airport Connector improvements from SR 417 (Seminole Expressway) to the entrance of the Orlando Sanford International Airport at Red Cleveland Boulevard. I acknowledge that the procedures and references used to develop the results contained in this report are standard to the professional practice of hydrologic analysis and hydraulic engineering as applied through professional judgment and experience. This document is for planning purposes only and is not to replace any effort required for final design.

Any engineering analysis, documents, conclusions or recommendations relied upon from other professional sources or provided with responsibility by the client are referenced accordingly in the following report.

FLORIDA REGISTERED ENGINEER:

Jennifer A. Nunn, State of Florida, Professional Engineer, License No. 70709

This item has been electronically signed and sealed by:

Signature must be verified on any electronic copies.

EXECUTIVE SUMMARY

The Central Florida Expressway Authority (CFX) is conducting a Project Development and Environment (PD&E) Study to evaluate the proposed State Road (SR) 417 (Seminole Expressway) Sanford Airport Connector improvements from SR 417 (Seminole Expressway) to the entrance of the Orlando Sanford International Airport (SFB) at Red Cleveland Boulevard in Seminole County, FL.

The purpose of the Location Hydraulic Report (LHR) is to evaluate and identify floodplain impacts associated with the proposed improvements, discuss any potential encroachments, and describe measures for avoidance or minimization of these impacts. A preliminary cross drain analysis is included in order to demonstrate the minimization of impacts to flood elevations and limits as part of the proposed improvements.

The proposed roadway typical section consists of two 15-foot wide travel lanes, one in each direction, separated by a 32-foot grassed median. Initially, six potential alignments were considered as part of this PD&E study; however, Alignment 2A was determined to be the preferred alternative and is the only build alternative considered for this hydraulics analysis. Alignment 2A originates at a proposed interchange north of the existing toll plaza and continues in a northerly direction intersecting East Lake Mary Boulevard and terminating at Red Cleveland Boulevard. See **Figure 1**, **Project Location Map** in **Appendix A**, **Figures**.

The Federal Emergency Management Agency (FEMA) has determined the 100-year floodplain extents within the study area with an effective date of September 28, 2007. Alignment 2A does not encroach on any FEMA 100-year floodplain, and therefore, no floodplain impacts are anticipated. See **Figure 4, FEMA Floodplain Map** in **Appendix A, Figures**.

Alignment 2A is within the Navy Canal basin which discharges to Lake Jesup. The entire study area is within the Lake Jesup HUC12 030801011105 basin and is included in the Lake Jesup Basin Management Action Plan (BMAP). See **Figure 5**, **Waterbody ID (WBID) Map** in **Appendix A**, **Figures**.

In order to mimic existing drainage conditions, proposed cross drains are preliminarily located and sized based on the best available information to convey offsite flows through the Alternative 2A corridor and demonstrate no adverse impacts to offsite properties. Detailed investigations of the upstream and downstream condition were performed to assess existing cross drains, flows, and patterns in order to determine the best available information for estimation of proposed cross drain sizes. During the design phase, the analysis will be re-evaluated with site-specific design information to ensure hydraulic adequacy. Four (4) cross drains for Alternative 2A were located and sized and utilized the Rational Method for flow estimation and Federal Highway Administration (FHWA) HY-8 software for headwater stages.

The project is classified as having minimal encroachment. The proposed structures will perform hydraulically in a manner equal to or greater than the existing structures, and backwater surface elevations are not expected to increase. Thus, there will be no significant adverse impacts on natural and beneficial floodplain values. There will be no significant change in flood risk, and there will not be a

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significant change in the potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.

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1. Introduction

The CFX is conducting a PD&E Study to evaluate the proposed SR 417 (Seminole Expressway) Sanford Airport Connector improvements from SR 417 (Seminole Expressway) to the entrance of the Orlando Sanford International Airport (SFB) at Red Cleveland Boulevard.

Initially, six potential alignments were considered as part of this PD&E study within the study area shown in **Plate 1.** Alignment 2A was determined to be the preferred alternative and is the only build alternative considered for this hydraulics analysis. Alignment 2A originates at a proposed interchange north of the existing toll plaza and continues in a northerly direction intersecting East Lake Mary Boulevard and terminating at Red Cleveland Boulevard. See **Figure 1**, **Project Location Map** in **Appendix A**, **Figures**.

The proposed roadway typical section consists of two 15-foot wide travel lanes, one in each direction, separated by a 32-foot grassed median. Each travel direction includes a 4-foot outside paved shoulder with curb and gutter, 10-foot landscaped areas, and 27-foot sodded areas for a total width of 144 feet as shown in **Plate 2**. The proposed connector has a design speed of 45 miles per hour (mph) with the ramps to and from SR 417 having design speeds of 50 mph.

The project horizontal datum is Florida State Plane East Zone (NAD 1983), and the vertical datum is North American Vertical Datum of 1988 (NAVD). Conversion to NAVD elevation is accomplished by subtracting 1.04 feet from the National Geodetic Vertical Datum of 1929 (NGVD) elevation (i.e., 10.00 feet NGVD = 8.96 feet NAVD).

The project is located in Seminole County and within the St. Johns River Water Management District (SJRWMD) jurisdiction. The study area encompasses Township 20 South, Range 30 East, Sections 12 and 13, and within Township 20 South, Range 31 East, Sections 7-9, and 16-20. See **Figure 2, USGS Topographic Map** in **Appendix A, Figures**.

The Federal Emergency Management Agency (FEMA) has determined the 100-year floodplain extents within the study area with an effective date of September 28, 2007. Within the study area, flood zones classified as Zone X, Zone A, and Zone AE are present. Zone X is an area of minimal flood hazard and is determined to be outside the 100-year floodplain. Zones A and AE are areas which have a 1% chance of flooding annually (100-year event). There is one Zone A floodplain located east of SR 417 and north of Pine Way. The Zone AE flood zones have a determined base flood elevation (BFE) and are located in the vicinity of Lake Jesup with an established BFE of 9.00 feet NAVD. Alignment 2A does not encroach on any FEMA 100-year floodplain. See **Figure 4, FEMA Floodplain Map** in **Appendix A, Figures**.

The study area is located within the Middle St. Johns watershed and more specifically within the Lake Jesup Drain, Navy Canal, and Six Mile Creek basins. The study area drains primarily to two named waterways (Six Mile Creek and Phelps Creek/Navy Canal) and various channelized ditches which then

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discharge to Lake Jesup. The entire project limits are located within the Lake Jesup BMAP. There are no Outstanding Florida Waters (OFW) within the study area.

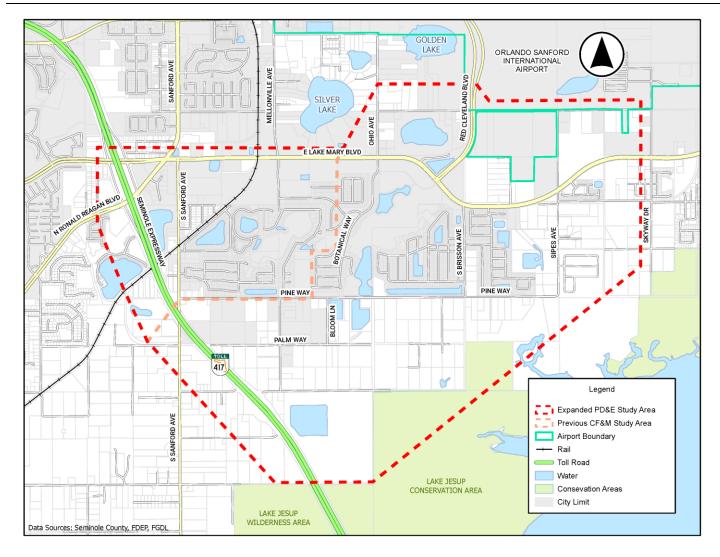


Plate 1 – SR 417 (Seminole Expressway) Sanford Airport Connector Study Area

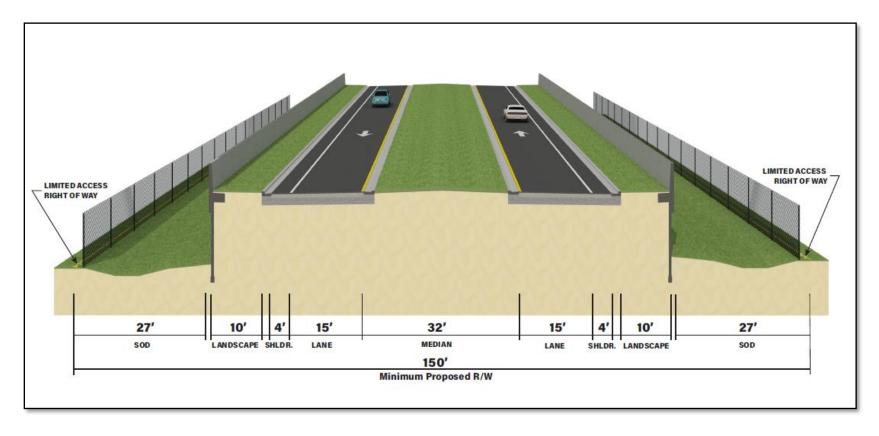


Plate 2 – SR 417 (Seminole Expressway) Sanford Airport Connector Proposed Typical Section

2. Purpose

The purpose of the proposed SR 417 (Seminole Expressway) Sanford Airport Connector is to provide a direct, limited access connection between SR 417 and SFB to provide better connectivity and accommodate future traffic growth in the area. The primary access to the airport is along East Lake Mary Boulevard via Red Cleveland Boulevard, which extends north from the airport entrance to the airport terminal. A proposed connector would provide a limited access connection directly to SFB from SR 417, thereby reducing the demand along East Lake Mary Boulevard and improving travel time for all users. The proposed improvements are to 1) enhance regional connectivity, 2) accommodate transportation demand, 3) provide needed capacity, 4) improve safety, 5) support modal connectivity, and 6) serve social and economic growth.

The purpose of this LHR is to evaluate and identify floodplain impacts associated with the proposed improvements, discuss any potential encroachments, and describe measures for avoidance or minimization of these impacts. The evaluation of cross drains is included in the hydraulic impacts associated with the proposed improvements in order to mimic existing drainage patterns. A preliminary cross drain analysis is included in order to demonstrate the minimization of impacts to flood elevations and limits as part of the proposed improvements.

3. Cross Drain Analysis Methodology

The existing land use within the study area consists mainly of roadways, residential (low density and rural), commercial and services, agriculture, and institutional. As this area is highly developed, runoff generally flows from north to south, and drains into existing ponds, roadside ditches, and swales before discharging into Lake Jesup. Existing stormwater management facilities (SMFs) include wet detention ponds, dry retention ponds, and linear swales.

The study area includes multiple Water Body Identification (WBID) basins that are part of the Middle St. Johns watershed that ultimately discharges to the St. Johns River. The study area is within the Lake Jesup HUC12 030801011105 basin and is included in the Lake Jesup BMAP with established Total Nitrogen and Total Phosphorous requirements. Alignment 2A is within the Navy Canal (WBID 2982), which is impaired for fecal coliform. See **Figure 5**, **Waterbody ID (WBID) Map** in **Appendix A**, **Figures**.

Offsite contributing areas draining to proposed Alternative 2A were delineated utilizing CatchmentSIM (CSIM) software, and refined utilizing existing permits, plans, and field reconnaissance of the project area. Relevant permit information is contained within **Appendix B, Existing Permitted Documents**. Proposed cross drain locations were determined from field review, LiDAR, and other available information including FEMA floodplains, USGS (United States Geological Survey) topographic information, and permits containing corridor-adjacent culverts. Generally, proposed cross drains were located where open channels or depressional areas exist. **Table 1** provides the storm events utilized for the preliminary cross drain analysis, (Florida Department of Transportation (FDOT) 2025 Drainage Manual (2025 DM) Section 4 and 2025 Drainage Design Guide (2024 DDG) Chapter 4). Proposed cross drains are sized for the 50-year design storm event. In addition, FDOT requires that the 100-year storm and either the 500-year storm (if greatest flood) or overtopping flood be analyzed for all cross drains.

Storm Event Frequency	Reason
10-year	Roadside Ditch Culverts; Pedestrian and Trail Bridges
25-year	Design Flood Event; (20-yr project of AADT < 1,500)
50-year*	Design Flood Event; (20-yr projection of AADT > 1,500)
100-year*	Base Flood Event
500-year	Greatest Flood Event

Table 1 – Storm Frequency Criteria

The proposed cross drains along the proposed alignment will be designed to allow the offsite flow to mimic the existing conditions. The peak flood flows for the Design (50-year), Base (100-year), and Greatest Flood (500-year) were assessed for all proposed cross drains. The Rational Method was

^{*} Design storms for this project

employed and utilized rainfall intensities from the National Oceanographic Atmospheric Agency (NOAA) Atlas 14, Point Precipitation Frequency estimates for the study.

Federal Highway Administration (FHWA) HY-8 (Version 8.0) software was used to estimate headwater stages associated with the offsite flows and assist with the determination of proposed cross drain sizes. Proposed cross drain culvert sizes were determined by assuming a maximum velocity of three feet per second (fps) during the design storm to minimize risk given the surrounding relatively flat terrain and to demonstrate no adverse conditions at upstream properties resulting from the proposed roadway corridor. Utilizing the continuity equation ($Q = V \times A$), the maximum velocity and offsite flow resulted in a required cross sectional area for the proposed cross drain. Standard culvert dimensions were utilized to provide a cross sectional area greater than required. The tailwater elevation was assumed to be constant and utilized the more reasonable value from the following: the BFE within a FEMA Flood Zone AE, the crown of pipe at the downstream end, or a permitted tailwater elevation. The culvert location, length, and invert elevations for each cross drain were determined using LiDAR to approximate the existing ground elevation at the proposed right-of-way line.

In all cases, overtopping for the basin was assumed to be the proposed roadway and utilized a preliminary roadway profile developed for Alternative 2A. If the 500-year discharge did not result in roadway overtopping, then the 500-year discharge and stage was utilized as the Greatest Flood. The proposed cross drains were sized to result in no roadway overtopping; therefore, the 500-year discharge was recorded as the Greatest Flood for all cross drains. The Flood Data Box is included in **Table 7** of this report. During the design phase, the cross drain design will be re-evaluated with site-specific design information. This includes survey, geotechnical data, and any existing infrastructure (e.g. underground utilities), as well as the final proposed roadway profile. It is also assumed that the basin overtopping analysis and floodplain analysis will be further evaluated in the design phase.

4. Existing Conditions

4.1 Previously Permitted Information

Existing drainage basin locations and previously permitted cross drains located upstream of the project were used to support proposed cross drain sizing and peak flow estimation. A site visit was performed on October 4, 2024 to verify the location and sizes of previously permitted cross drains. **Table 2** provides a list of SJRWMD Environmental Resource Permits (ERPs) reviewed for cross drain information within the study area. Permit information that includes pertinent cross drain data within the project vicinity can be found in **Appendix B, Existing Permit Documents**.

Table 2 – Existing Permits within Study Area

ERP App.	Project	Date Issued	Shows Pertinent Cross Drain?
21757	Baker Farms	1/08/1985	No
21945-12	Lake Mary Boulevard	4/08/1996	No
22290-2	Silver Lakes Industrial Park	12/07/1992	No
22290-3	Silver Lakes Industrial Park	1/11/1993	No
22290-10	Sylvestri Estates	9/29/2016	No
22290-12	Sylvestri Lakes SD Sanford	6/21/2021	No
22290-14	Sylvestri Lakes Amenity Center Sanford	10/14/2021	No
22290-15	Safari Commercial Parcels	2/05/2023	No
22290-17	Sylvestri Lakes S/D (Transfer) Sanford	7/24/2023	No
22290-18	SFB Crossing	Pending	No
22339-1	FDOT Borrow Pit	9/08/1992	No
22339-3	White Construction Borrow Pits SR 427	9/08/1992	No
22339-5	FDOT Borrow Pit	7/13/1993	No
22367-1	Marquette Shores Borrow Pit	2/09/1993	No
22381-1	CR 427	2/08/1994	No
22496-3	East Lake Mary Boulevard Segment IIA	6/10/2002	Yes
22496-4	East Lake Mary Boulevard Segment IIB	4/08/2003	Yes
22496-5	East Lake Mary Boulevard Segment I	11/12/2002	Yes
70929 - 1	Pine Way @ Navy Canal Culvert Replacement	5/02/2001	No
71069-1	Magnolia Park, PD	8/14/2001	No
90051-1	Navy Canal Stormwater Facility	9/07/2004	No
96997-1	The Preserve at Eagle Lake	7/29/2005	No

ERP App.	Project	Date Issued	Shows Pertinent Cross Drain?
110906-3	Brisson East	8/31/2012	No
110906-7	Brisson West Residential Development	11/3/2017	No
110906-5	Brisson East Residential Development	4/30/2014	No
181400-1	Skylar Crest Townhomes Stormwater Manag. System	5/09/2022	No
182187-2	Palmetto Pointe	10/11/2023	No

4.2 Existing Cross Drains

Existing cross drains along East Lake Mary Boulevard and Red Cleveland Boulevard were field reviewed. Field review notes are located in **Appendix C, Field Review Documentation**. The direction of flow was determined from LiDAR, existing permit data, and field visit observations. See **Figure 6, Existing Cross Drain Location Map** in **Appendix A, Figures** for existing cross drain locations. **Table 3** provides pertinent information for existing cross drains along East Lake Mary Boulevard and Red Cleveland Boulevard.

Table 3 - Pertinent Existing Cross Drains within Study Area

Existing Cross Drain	Location	Size	Flow Direction	SJRWMD ERP Number	Applicable Proposed Cross Drain	
CD-01_EX	Sta. 32+00	2 – 24" RCP	South	4-117-22496-5	N/A	
CD-02_EX	Sta. 33+40	3 – 48" RCP	South	4-117-22496-5	N/A	
CD-03A_EX	Sta. 56+18	30" RCP	South	4-117-22496-5	N/A	
CD-03B_EX	Sta. 64+20	30" RCP	South	4-117-22496-5	N/A	
CD-04_EX	Sta. 68+00	3 – 24" x 38" ERCP	South	4-117-22496-5	N/A	
CD-05_EX*	Sta. 22+00	3 – 30" RCP	Southeast	4-117-22496-3	CD-04_PR	
CD-06_EX	Sta. 93+00	3 – 30" RCP	South	4-117-22496-3	N/A	
CD-07_EX	Sta. 96+20	2 – 36" RCP	South	4-117-22496-3	N/A	
CD-08_EX	Sta. 111+90	3 – 10′ x 6′ CBC	South	4-117-22496-4	N/A	

^{*}Cross drain located on Red Cleveland Blvd. All other CDs located on E. Lake Mary Blvd.

The following discussion contains a brief description of each existing cross drain. The capacity of each existing cross drain to convey the 50-year storm event was assessed. For cross drains CD-01_EX, CD-02_EX, CD-3A_EX, and CD-3B_EX, peak flows were previously calculated for the 25-year/24-hour storm event; therefore, a statistical method was employed to estimate the 50-year peak flows. For cross drain CD-04_EX, peak flow data was not available in the permit documents; therefore, the 50-year peak flow was estimated using the Velocity Method and applying the Continuity equation $(Q = V \times A)$ with an

assumed velocity of three fps. For cross drains CD-05 EX, CD-06 EX, CD-07 EX, and CD-08 EX, the 50year peak flows were obtained directly from the permit documents. See Appendix B, Existing Permit **Documents** for existing permit documentation.

4.2.1 CD-01 EX

CD-01 EX is located at Station 32+00 on East Lake Mary Boulevard which is just west of the East Lake Mary Boulevard and the Seaboard Coastline Railroad Crossing (aka CSX Railroad) intersection. This cross drain is a double 24-inch reinforced concrete pipe (RCP) (per SJRWMD ERP 4-117-22496-5) as shown in Table 3. Within the permit documentation, CD-01 EX is referred to as "CULV 1" in the sub-basin B analysis.

CD-01 EX is located within FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-01 EX conveys the runoff from offsite areas north of East Lake Mary Boulevard to outfall into an existing ditch southwest of the railroad crossing intersection. The SJRWMD ERP 4-117-22496-5 indicates the CD-01 EX drainage basin to be 17.96 acres with a 25-year/24-hour event discharge of 23.57 cubic feet per second (cfs). The 50-yr flow rate was not provided in the permit documentation and was estimated to be 27.11 cfs using a statistical method.

During the field visit, the north (upstream) mitered endwall (ST-1) was observed to be in good condition and had no apparent scour or erosion. The water level at ST-1 was measured to be approximately 19inches above the pipe invert. Heavy vegetation was noted along the inflow ditch to the cross drain. The south (downstream) endwall (ST-2) was not visually observed due to heavy vegetation; however, a low water level was observed near the structure location. See field photos and notes in Appendix C, Field **Review Documentation.**

4.2.2 CD-02_EX

CD-02_EX is located at Station 33+40 on East Lake Mary Boulevard, which is just east of the East Lake Mary Boulevard and CSX Railroad intersection. This cross drain is a triple 48-inch RCP (per SJRWMD ERP 4-117-22496-5) as shown in **Table 3**. Within the permit documentation, CD-02 EX is referred to as "RRPOND" in the sub-basin B analysis.

CD-02_EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-02_EX conveys offsite runoff from north of East Lake Mary Boulevard. Runoff from the roadway is collected in a closed conveyance system and directed to wet detention Pond B, located northwest of the railroad crossing intersection. The Pond B outfall crosses the railroad north of East Lake Mary Boulevard and discharges into a canal that drains south into the upstream side of the existing cross drain. The existing cross drain discharges into a canal that flows into the triple 48-inch culvert to the south, which eventually discharges into a wetland area. The SJRWMD ERP 4-117-22496-5 indicates the CD-02 EX drainage basin to be 14.39 acres with a 25-year/24-hour event discharge of 35.56 cfs. The 50year flow rate was not provided in the permit documentation and was estimated to be 40.89 cfs using a statistical method.

During the field visit, the north (upstream) endwall (ST-3) was not visually observed due to heavy vegetation; however, a low water level was observed near the structure location. The south (downstream) end (ST-4) is connected to a triple 48-inch side drain that conveys the runoff east to the roadside ditch. See field photos and notes in **Appendix C**, **Field Review Documentation**.

4.2.3 CD-03A EX

CD-03A_EX is located at Station 56+18 on East Lake Mary Boulevard which is approximately 0.21 miles west of the East Lake Mary Boulevard and Ohio Avenue intersection. This cross drain is a 30-inch RCP (per SJRWMD ERP 4-117-22496-5) as shown in **Table 3**. Within the permit documentation, CD-03A_EX is referred to as "CULV 1" in the sub-basin C analysis.

CD-03A_EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-03A_EX conveys the runoff from a portion of the extension of East Lake Mary Boulevard (per SJRWMD ERP 42-11 7-0943NG) from the CSX Railroad to Ohio Avenue including the west side of Ohio Avenue. The offsite areas consist of industrial, residential, and agricultural land uses located primarily to the north of East Lake Mary Boulevard. The roadway runoff discharges into wet detention Pond C, which discharges into an existing ditch that drains south to the upstream side of CD-03A_EX.

CD-03A_EX discharges southward where it joins with CD-03B_EX at an existing 38-inch x 60-inch elliptical reinforced concrete pipe (ERCP). The ERCP outfall conveys runoff within Sylvestri Lakes Community (under construction – Permit App. No. 22290-18) and outfall into a wetland area located east of the community. The wetland area discharges into a ditch/canal system that ultimately drains to Lake Jesup. The SJRWMD ERP 4-117-22496-5 indicates the CD-03A_EX drainage basin to be 32.50 acres with a 25-year/24-hour event discharge of 36.48 cfs. The 50-year flow rate was not provided in the permit documentation and was estimated to be 41.95 cfs using a statistical method.

During the field visit, the north (upstream) mitered endwall (ST-5) was observed to be in good condition and had no apparent scour or erosion. The water level and stain marks were measured at approximately 5-inches and 8-inches above the pipe invert, respectively. The south (downstream) end (ST-6) is a storm sewer manhole where CD-03A_EX joins with CD-03B_EX. The manhole was observed to be in good condition and had no apparent scour or erosion. See field photos and notes in **Appendix C**, **Field Review Documentation**.

4.2.4 CD-03B EX

CD-03B_EX is located at Station 64+20 at East Lake Mary Boulevard, which is approximately 0.05 miles west of the East Lake Mary Boulevard and Ohio Avenue intersection. This cross drain is a 30-inch RCP (per SJRWMD ERP 4-117-22496-5) as shown in **Table 3**. Within the permit documentation, CD-03B_EX is referred to as "CULV_3" in the sub-basin C analysis.

CD-03B_EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-03B_EX conveys the runoff from offsite areas of primarily agricultural land uses located north of East Lake Mary Boulevard. CD-03B_EX discharges southward where it joins with CD-03A_EX at

an existing 38-inch x 60-inch ERCP. This system ultimately discharges to Lake Jesup as described for CD-03A_EX. The SJRWMD ERP 4-117-22496-5 indicates the CD-03B_EX drainage basin to be 19.08 acres with a 25-year/24-hour event discharge of 24.68 cfs. The 50-year flow rate was not provided in the permit documentation and was estimated to be 28.38 cfs using a statistical method.

During the field visit, the north (upstream) ditch bottom inlet (ST-7) was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review. The south (downstream) end (ST-6) is a storm sewer manhole where CD-03B EX joins with CD-03A EX. The manhole was observed to be in good condition and had no apparent scour or erosion. See field photos and notes in **Appendix C**, **Field Review Documentation**.

4.2.5 CD-04 EX

CD-04_EX is located at Station 68+00 on East Lake Mary Boulevard which is just east of the East Lake Mary Boulevard and Ohio Avenue intersection. This cross drain is a triple 24-inch by 38-inch ERCP (per SJRWMD ERP 4-117-22496-5) as shown in **Table 3**.

CD-04 EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-04 EX conveys the runoff from offsite areas of primarily residential and agricultural land uses located north of East Lake Mary Boulevard. CD-04 EX discharges southward and runoff flows into an undeveloped area of the Sylvestri Lakes Community (under construction – Permit App. No. 22290-18) to outfall into a wetland area. The wetland area discharges into a ditch/canal system that ultimately outfalls to Lake Jesup.

Although the cross drain is included in the construction plans, it could not be found within the drainage report. It appears that it was not included since neither the drainage area nor the structure of the cross drain was altered for the permitted improvements. Therefore, no design flow was provided in the permit documentation. The 50-year flow rate was estimated to be 45.90 cfs using the Velocity Method.

During the field visit, the north (upstream) endwall (ST-8) was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review. Some sedimentation (silt) and stain lines were observed inside the elliptical pipe. The south (downstream) endwall (ST-9) was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review. The structure had no sedimentation (silt), nor any observed stain lines. See field photos and notes in Appendix C, Field Review Documentation.

4.2.6 CD-05 EX

CD-05 EX is located at Station 22+00 on Red Cleveland Boulevard which is approximately 0.21 miles northeast of the Red Cleveland Boulevard and East Lake Mary Boulevard intersection. This cross drain was originally designed as a quintuple 24" x 38" configuration according to the permit documentation (SJRWMD ERP 4-117-22496-3); however, it was subsequently constructed as a triple 30-inch configuration, as shown in the construction plans and confirmed during the field visit (See Table 3). Within the permit documentation, CD-05_EX is referred to as "X-1L".

CD-05 EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-05_EX conveys the runoff from offsite areas of primarily industrial, residential, and agricultural land uses located west of Red Cleveland Boulevard to a wetland area upstream of CD-06 EX and CD-07_EX. Cross drains CD-06_EX and CD-07_EX drain into a ditch/canal system that ultimately drains to Lake Jesup. The SJRWMD ERP 4-117-22496-3 indicates the CD-05 EX drainage basin to be 21.95 acres with a 50-year design discharge of 60.31 cfs.

During the field visit, the northwest (upstream) mitered endwall (ST-10) was observed to be in good condition and had no apparent scour or erosion. The ST-10 had the water level approximately 8-inches above the pipe invert. The structure had no sedimentation (silt), nor any observed stain lines. The southeast (downstream) mitered endwall (ST-11) was observed to be in good condition and had no apparent scour or erosion. The structure had no sedimentation (silt), nor any observed stain lines. See field photos and notes in Appendix C, Field Review Documentation.

CD-06_EX 4.2.7

CD-06 EX is located at Station 93+00 on East Lake Mary Boulevard which is approximately 0.14 miles southeast of the East Lake Mary Boulevard and Red Cleveland Boulevard intersection. This cross drain is a triple 30-inch RCP (per SJRWMD ERP 4-117-22496-3) as shown in Table 3. Within the permit documentation, CD-06 EX is referred to as "X-2L".

CD-06 EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-06_EX and CD-07_EX both convey the runoff discharged upstream from CD-05_EX and the runoff from an offsite area located east of Red Cleveland Boulevard to a ditch/canal system that ultimately drains to Lake Jesup. The SJRWMD ERP 4-117-22496-3 indicates the CD-06 EX has a drainage basin of 34.5 acres and the 50-year design discharge of 47 cfs.

During the field visit, the north (upstream) mitered endwall (ST-12) was observed to be in good condition and had no apparent scour or erosion. The ST-12 had the water level approximately 6-inches above the pipe invert. The structure had no sedimentation (silt), nor any observed stain lines. The south (downstream) mitered endwall (ST-13) was observed to be in good condition and had no apparent scour or erosion. The ST-13 had the water level approximately 6-inches above the pipe invert. The structure had no sedimentation (silt), nor any observed stain lines. See field photos and notes in Appendix C, Field **Review Documentation.**

4.2.8 CD-07 EX

CD-07 EX is located at Station 96+20 on East Lake Mary Boulevard which is approximately 0.19 miles southeast of the East Lake Mary Boulevard and Red Cleveland Boulevard intersection. This cross drain is a double 36-inch RCP (per SJRWMD ERP 4-117-22496-3) as shown in Table 3. Within the permit documentation, CD-07 EX is referred to as "S-213".

CD-07 EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-07_EX and CD-06_EX both convey the runoff discharged from CD-05_EX and the runoff from an offsite area located east of Red Cleveland Boulevard to a ditch/canal system that ultimately drains to Lake Jesup. The SJRWMD ERP 4-117-22496-3 indicates the 50-year design discharge of 60 cfs; no drainage basin information was available for this cross drain.

During the field visit, the north (upstream) endwall (ST-14) was observed, although it could not be accessed due to the high vegetation. Standing water was observed. The south (downstream) endwall (ST-15) was not visible due to heavy vegetation. Standing water was observed. See field photos and notes in Appendix C, Field Review Documentation.

4.2.9 CD-08_EX

CD-08 EX is located at Station 111+90 on East Lake Mary Boulevard, which is approximately 0.50 miles southeast of the East Lake Mary Boulevard and Red Cleveland Boulevard intersection. CD-08 EX conveys Navy Canal through a triple 10-ft by 6-ft Concrete Box Culvert (CBC) (per SJRWMD ERP 4-117-22496-4) as shown in Table 3. Within the permit documentation, CD-08 EX is referred to as "X-4".

CD-08 EX is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. CD-08 EX conveys runoff from the Navy Canal drainage basin, which includes areas of residential and agricultural land uses located north of East Lake Mary Boulevard. Navy Canal ultimately drains to Lake Jesup. The SJRWMD ERP 4-117-22496-4 indicates a 50-year design discharge of 307 cfs, although there are previous calculations dating back to 1994 that indicate that the 50-year design flow was 920 cfs.

During the field visit, Navy Canal was observed with no vegetation and obstructions within the canal. The canal was highly vegetated in the overbanks. See field photos and notes in Appendix C, Field **Review Documentation.**

4.3 Summary of Flow Estimation for Existing Cross Drains

Table 4 provides an overview of each existing cross drain including location, size, and estimated 50-year peak flow along East Lake Mary Boulevard.

Table 4 – Summary of Peak Flow Estimation for Existing Cross Drains

Existing Cross Drain ID	Location	Number of Barrels	Size	50-year Peak Flow (cfs)	Method
CD-01_EX	Sta. 32+00	2	24" RCP	27.11	Statistical Method
CD-02_EX	Sta. 33+40	3	48" RCP	40.89	Statistical Method
CD-03A_EX	Sta. 56+18	1	30" RCP	41.95	Statistical Method
CD-03B_EX	Sta. 64+20	1	30" RCP	28.38	Statistical Method
CD-04_EX	Sta. 68+00	3	24" x 38" ERCP	45.90	Velocity Method
CD-05_EX*	Sta. 22+00	3	30" RCP	60.31	ERP 4-117-22496-3
CD-06_EX	Sta. 93+00	3	30" RCP	47.00	ERP 4-117-22496-3
CD-07_EX	Sta. 96+20	2	36" RCP	60.00	ERP 4-117-22496-4
CD-08_EX	Sta. 111+90	3	10' x 6' CBC	307.00	ERP 4-117-22496-4

^{*}Cross drain located on Red Cleveland Blvd. All other CDs located on E. Lake Mary Blvd.

5. Proposed Conditions

Potential floodplain impacts resulting from the SR 417 (Seminole Expressway) Sanford Airport Connector Alternative 2A were evaluated. As the proposed corridor does not encroach on any FEMA 100-year floodplains, no floodplain impacts are anticipated with the proposed improvements.

In order to mimic existing drainage conditions, proposed cross drains are preliminarily located and sized based on the best available information to convey offsite flows through the Alternative 2A corridor and demonstrate no adverse impacts to offsite properties. Detailed investigations of the upstream and downstream condition were performed to assess existing cross drains, flows, and patterns in order to determine the best available information for estimation of proposed cross drain sizes. It is recommended to reevaluate each proposed cross drain during the design phase to ensure hydraulic adequacy.

There are four (4) proposed cross drains for Alternative 2A. See Figure 7A and 7B, Proposed Cross Drain and Basin Maps in Appendix A, Figures for proposed cross drain locations and basin map exhibits. All proposed cross drains are located within Zone X, therefore there will be no encroachment into the FEMA 100-year floodplain. Refer to Figure 4, FEMA Floodplain Map in Appendix A, Figures for the FEMA Floodplain Map. The hydrologic soil groups for the proposed cross drain basins include Type A and Type A/D. Refer to Figure 3, NRCS Soil Map in Appendix A, Figures for the Natural Resources Conservation Service (NRCS) Soil Map.

5.1 Proposed Cross Drains

The cross drain analysis was conducted as described in **Section 3.** The following discussion contains a brief description of each proposed cross drain and their respective drainage basins.

The CD-01_PR drainage system receives runoff from a 13.43-acres drainage basin. The drainage basin draining to CD-01_PR encompasses a low-density residential area located south of Palm Way Street, east of Mellonville Avenue, and northwest of the SR 417 (Seminole Expressway) Sanford Airport Connector Alignment 2A. The hydrologic soil group within the basin is Type A/D.

CD-01_PR is proposed at Station 107+66 of the SR 417 (Seminole Expressway) Sanford Airport Connector. The proposed cross drain size is a 36-inch RCP draining to the southeast with discharge into an open area that drains into an existing ditch and ultimately drains to Lake Jesup. CD-01_PR will be located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. The 50-year flow rate was estimated to be 19.63 cfs.

The CD-02_PR drainage system receives runoff from a total 69.15-acres drainage basin. This drainage basin includes 15.12 acres of offsite wetland area and 54.03 acres from the permitted Sylvestri Lake

Community basin. The drainage area encompasses a wetland area located southeast of Sylvestri Lakes Community and northwest of the SR 417 (Seminole Expressway) Sanford Airport Connector Alignment 2A. In addition, CD-02_PR will convey the entire northern drainage system of the Sylvestri Lakes Community. Currently, the drainage system is routed to an existing wet detention pond which outfalls via a control structure to the wetland area. The hydrologic soil group within the basin is Type A/D.

CD-02_PR is proposed at Station 158+76 of the SR 417 (Seminole Expressway) Sanford Airport Connector. The proposed cross drain size is a 9-foot x 5-foot CBC draining to the southeast with discharge into a wetland area that ultimately drains to Lake Jesup. CD-02_PR will be located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. The 50-year flow rate was estimated to be 122.97 cfs. The peak flow rate from the 15.12 acre offsite basin was estimated using the Rational Method, and the peak flow rate from the Sylvestri Lakes Community basin was estimated using a statistical method, referencing the permit data.

5.1.3 CD-03_PR

The CD-03_PR drainage system receives runoff from a total 103.74-acre drainage basin. This drainage basin includes 23.85 acres of offsite wetland area, located south of East Lake Mary Boulevard, north and east of Sylvestri Lakes Community, and northwest of the SR 417 (Seminole Expressway) Sanford Airport Connector Alignment 2A. Additionally, it includes 28.27 acres from the CD-04_EX drainage basin and 51.62 acres from CD-03A_EX and CD-03B_EX drainage basins. The drainage basin for CD-03A_EX and CD-03B_EX was obtained from permit documentation, while the remaining drainage basin was delineated utilizing CSIM software. Runoff from CD-03A_EX and CD-03B_EX converges into an existing 38-inch x 60-inch ERCP located within the Sylvestri Lakes Community. This conduit conveys flows through the community and discharge into the adjacent wetland system. The hydrologic soil group within the basin is Type A/D.

CD-03_PR is located at Station 170+30 of the SR 417 (Seminole Expressway) Sanford Airport Connector. The proposed cross drain size is an 8-foot x 6-foot CBC draining to the south with discharge into the wetland area that ultimately drains to Lake Jesup. CD-03_PR is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. The 50-year flow rate is estimated to be 140.68 cfs. The peak flow rate for the offsite basin was estimated using the Rational Method. The flow rate from CD-03A_EX and CD-03B_EX was estimated using a statistical method, and the flow rate from CD-04_EX was estimated using the Velocity Method.

5.1.4 CD-04_PR

CD-04_PR is located at Station 188+59 of the SR 417 (Seminole Expressway) Sanford Airport Connector which is the same location of CD-05_EX (Station 22+00 on Red Cleveland Boulevard). The drainage system receives runoff from a total 21.95-acre drainage basin according to SJRWMD ERP 4-117-22496-3 permit documentation. The hydrologic soil groups within the basin are Type A and Type A/D.

The proposed cross drain configuration considers replacement of the existing triple 30-inch pipes with triple 36-inch pipes. During the design phase, it is recommended to determine whether the existing triple 30-inch pipes are in adequate condition and can be extended for the new alignment. To ensure no adverse conditions, an additional proposed pipe will be required in parallel for this option. Additionally, it should be noted that the proposed cross drain dimensions may require upsizing during the design phase, if it is determined that the existing Pond 4A needs to be modified to handle additional flow.

The proposed structure will drain to the southeast with discharge into a wetland area upstream of CD-06_EX and CD-07_EX. Cross drains CD-06_EX and CD-07_EX drain into a ditch/canal system that ultimately drains to Lake Jesup. CD-04_PR is located in FEMA Flood Zone X, which is an area having a moderate or minimal risk of flooding. The 50-year flow rate is estimated to be 60.31 cfs according to permit documentation.

The existing cross drain CD_05-EX was originally designed as a quintuple 24" x 38" configuration according to the permit documentation (SJRWMD ERP 4-117-22496-3); however, it was subsequently constructed as a triple 30-inch RCP configuration, as shown in the construction plans and confirmed during the field visit. Since the permit calculations were based on a configuration different from the one constructed, calculations were performed for the as-built structure, allowing the water surface elevation to be compared with the proposed conditions (See **Table 5**).

Design Storm	Existing Condition Stages (ft NAVD)	Proposed Condition Stages (ft NAVD)	Difference (ft)		
50-	31.95	31.94	-0.01		
100-	32.20	32.08	-0.12		
500-	32.85	32.24	-0.61		

Table 5 – Comparison of Stages for CD-04_PR

Table 6 provides a summary of the proposed cross drains for Alternative 2A. See **Table 7** for the Flood Data Box. See **Appendix D, Proposed Hydrologic and Hydraulic Calculations** for proposed calculations, assumptions, and HY-8 results.

$Table\ 6-Alternative\ 2A\ Proposed\ Cross\ Drains$

Cross Drain	Culvert Size	Flow Direction	Total Basin Area (acres)	Peak Flow Methodology	Within Flood Zone?	Peak Design Storm Flow (cfs)
CD-01_PR	36" RCP	Southeast	13.43	Rational	No	19.63
CD-02_PR	9-ft x 5-ft	Southeast	69.15	Rational	No	122.97

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CD-03_PR	8-ft x 6-ft	South	103.74	Rational	No	140.68
CD-04_PR	Triple 36" RCP	Southeast	21.95	SJRWMD ERP 4-117-22496-3	No	60.31

Table 7 - Alternative 2A Flood Data Box

		DESIGN	FLOOD	BASE	FLOOD	OV.	DTODDING	ri oon			DEATECT E	1000	
STRUCTURE NO.	Cross Drain Size	2% PROB	50 YR FREQ	1% PROB	100 YR FREQ	OVE	RTOPPING	FLOOD		G	REATEST F	LOOD	
	Cross Drain Size	DISCHARGE	STAGE	DISCHARGE	STAGE	DISCHARGE	STAGE	PROB %	FREQ YR	DISCHARGE	STAGE	PROB %	FREQ YR
CD-01_PR	36-inch RCP	19.63	14.25	22.09	14.35	1		1		25.62	14.38	0.2%	500
CD-02_PR	9-ft x 5-ft CBC	122.97	34.02	206.67	34.42					217.75	34.48	0.2%	500
CD-03_PR	8-ft x 6-ft CBC	140.68	34.89	167.03	35.01					206.37	35.22	0.2%	500
CD-04_PR	Triple 36-inch RCP	60.31	31.94	69.32	32.08					88.20	32.24	0.2%	500

Note: The hydraulic data is shown for informational purposes only, to indicate the flood discharges and water surface elevations which may be anticipated in any given year. This data was generated using highly variable factors determined by a study of the watershed. Many judgements and assumptions are required to establish these factors. The resultant hydraulic data is sensitive to changes, particularly of antecedent conditions, urbanization, channelization, and land use. Users of this data are cautioned against the assumption of precision which cannot be attained. Discharges are in cubic feet per second (cfs) and stages are in feet, NAVD 88.

5.2 Floodplain Minimal Encroachment Evaluation

Per Section 13.2.2.5 of the FDOT PD&E Manual, the LHR has requirements for each level of significance of encroachment. This project qualifies as a Minimal Encroachments level due to minimal impacts to floodplain encroachments. The location of pertinent information and/or discussion of the following items to be contained within the LHR for a project with Minimal Encroachments are summarized below:

- General description of the project: See Section 1 Introduction, Plate 1 SR 417 (Seminole Expressway) Sanford Airport Connector Study Area, Plate 2 – SR 417 (Seminole Expressway) Sanford Airport Connector Proposed Typical Section, and Figures 1-5 in Appendix A.
- Determination of whether the proposed action is in the base floodplain: See Section 1 Introduction and See Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain.
- History of flooding of the existing facilities and/or measures to minimize any impacts due to the proposed improvements: Permit documentation (ERP 22290-12) indicates that the area south of Pine Way has had historic flooding issues, but the associated permitted improvements (Sylvestri Lakes Community) would assist in alleviating flooding in that area. Other documented comments from public input were received regarding reoccurring flooding issues. The proposed improvements will follow standard water quality and water quantity criteria and will not exacerbate any existing conditions.
- Determination of whether the encroachment is longitudinal or transverse, and if it is a longitudinal encroachment, an evaluation and discussion of practicable avoidance alternatives: See Section 1 Introduction and See Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain.
- The practicability of avoidance alternatives and/or measures to minimize impacts: See Section 1 Introduction and see Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain.
- Impact of the project on emergency services and evacuation: The project seeks to increase regional mobility and accommodate the future traffic needs. As travel lanes will be increased, the project is not anticipated to have any negative impacts on emergency services and evacuation.
- Impacts of the project on the base flood, likelihood of flood risk, overtopping, location of overtopping, backwater: Preliminary calculations have been prepared to provide preliminary cross drain sizes in order to convey offsite runoff and have no adverse impact to offsite properties. See Section 5.1 Proposed Cross Drains. During design, final hydrologic and hydraulic calculations will need to be performed.

- Determination of the impact of the project on regulatory floodways, if any, and documentation of coordination with FEMA and local agencies to determine the requirements for the project to be developed consistent with the regulatory floodway: There is no FEMA Regulatory floodway within the study area (see Figure 4, FEMA Floodplain Map in Appendix A, Figures).
- The impacts on natural and beneficial floodplain values and measures to restore and preserve these values: See Section 1 Introduction and See Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain.
- Consistency of the project with the local floodplain development plan or the land use elements in the Local Government Comprehensive Plan (LGCP), and the potential of encouraging development in the base floodplain: See Section 1 Introduction and see Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain. As part of the PD&E study, regular coordination meetings with Seminole County and the City of Sanford have been occurring.
- Measures to minimize floodplain impacts associated with the project and measures to restore and preserve the natural and beneficial floodplain values impacts by the project: See Section 1 Introduction and see Figure 4, FEMA Floodplain Map in Appendix A, Figures. Alignment 2A, the preferred Build Alternative, does not encroach within the FEMA 100-year floodplain.
- A map showing project location, and impacted floodplains: See Figure 1, Project Location Map and Figure 4, FEMA Floodplain Map in Appendix A, Figures.
- Results of any risk assessments performed: See Table 6 Alternative 2A Proposed Cross Drains and Table 7 – Alternative 2A Flood Data Box for the results of the proposed cross drain analysis.

6. Conclusion

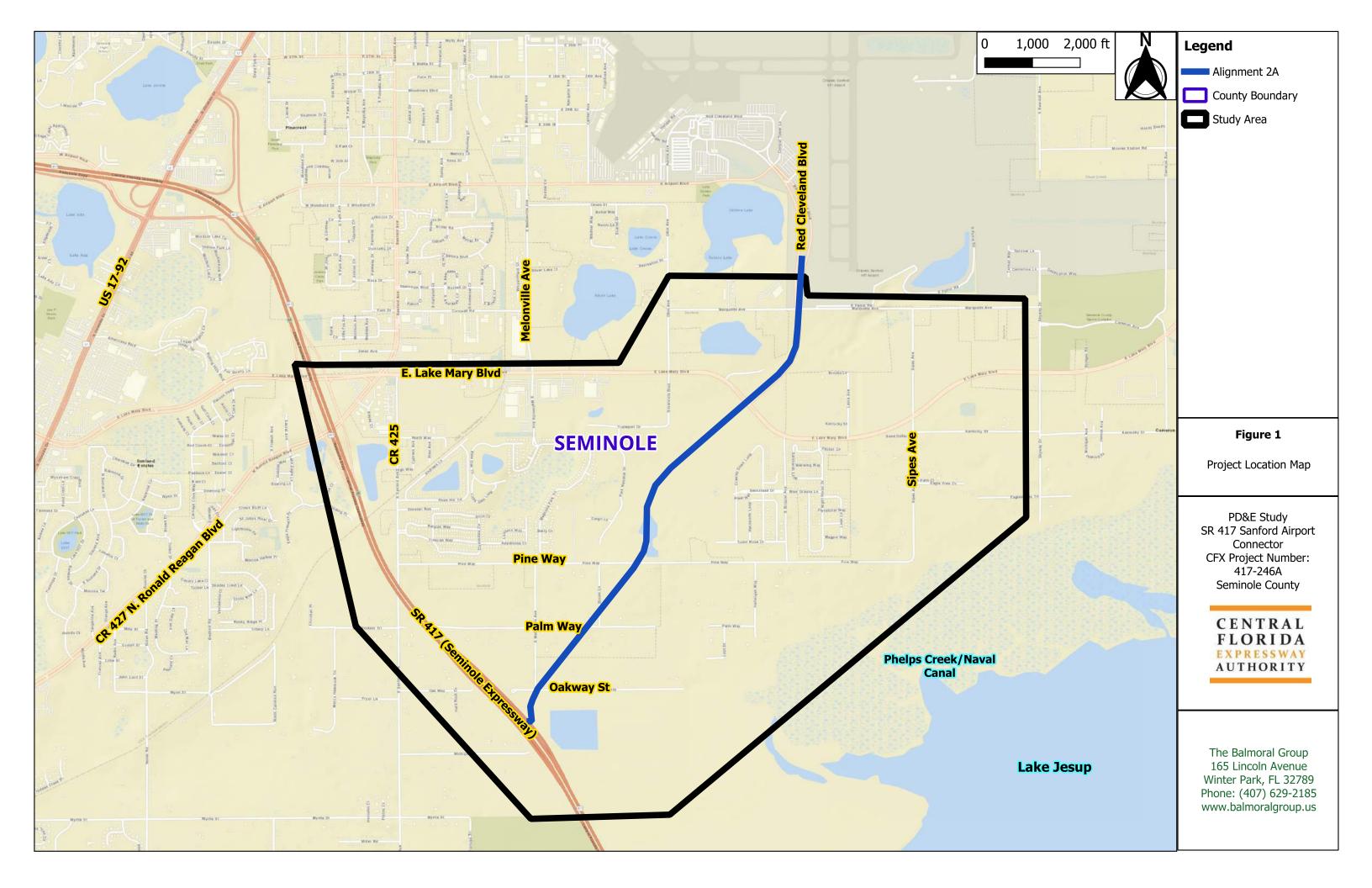
In summary, this report determined that there is anticipated to be no FEMA 100-year floodplain encroachment from the proposed Alignment 2A of the SR 417 (Seminole Expressway) Sanford Airport Connector. Additionally, in order to mimic existing drainage patterns, preliminary cross drain sizes and locations have been provided to demonstrate that there will not be any adverse impact to offsite flood stages and flood limits. The proposed roadway improvements are expected to have no adverse impact on the existing cross drains located at East Lake Mary Boulevard or Red Cleveland Boulevard. During final design, it is recommended to update the proposed cross drain analysis with project-specific survey, detailed tailwater information and the final roadway profile to demonstrate no adverse impacts.

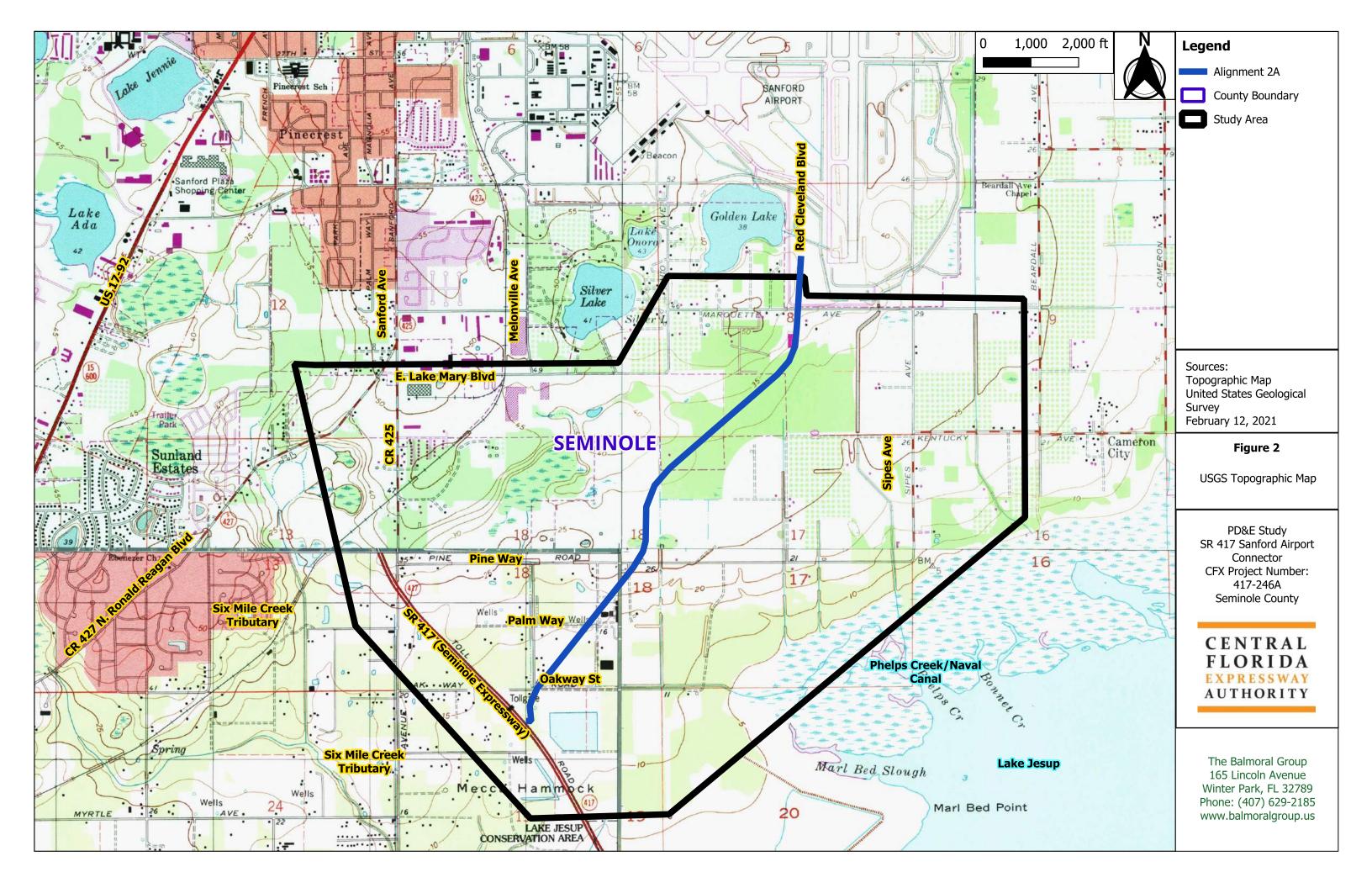
The project is classified as having minimal encroachment. The proposed structures will perform hydraulically in a manner equal to or greater than the existing structures, and backwater surface elevations are not expected to increase. Thus, there will be no significant adverse impacts on natural and beneficial floodplain values. There will be no significant change in flood risk, and there will not be a significant change in the potential for interruption or termination of emergency service or emergency evacuation routes. Therefore, it has been determined that this encroachment is not significant.

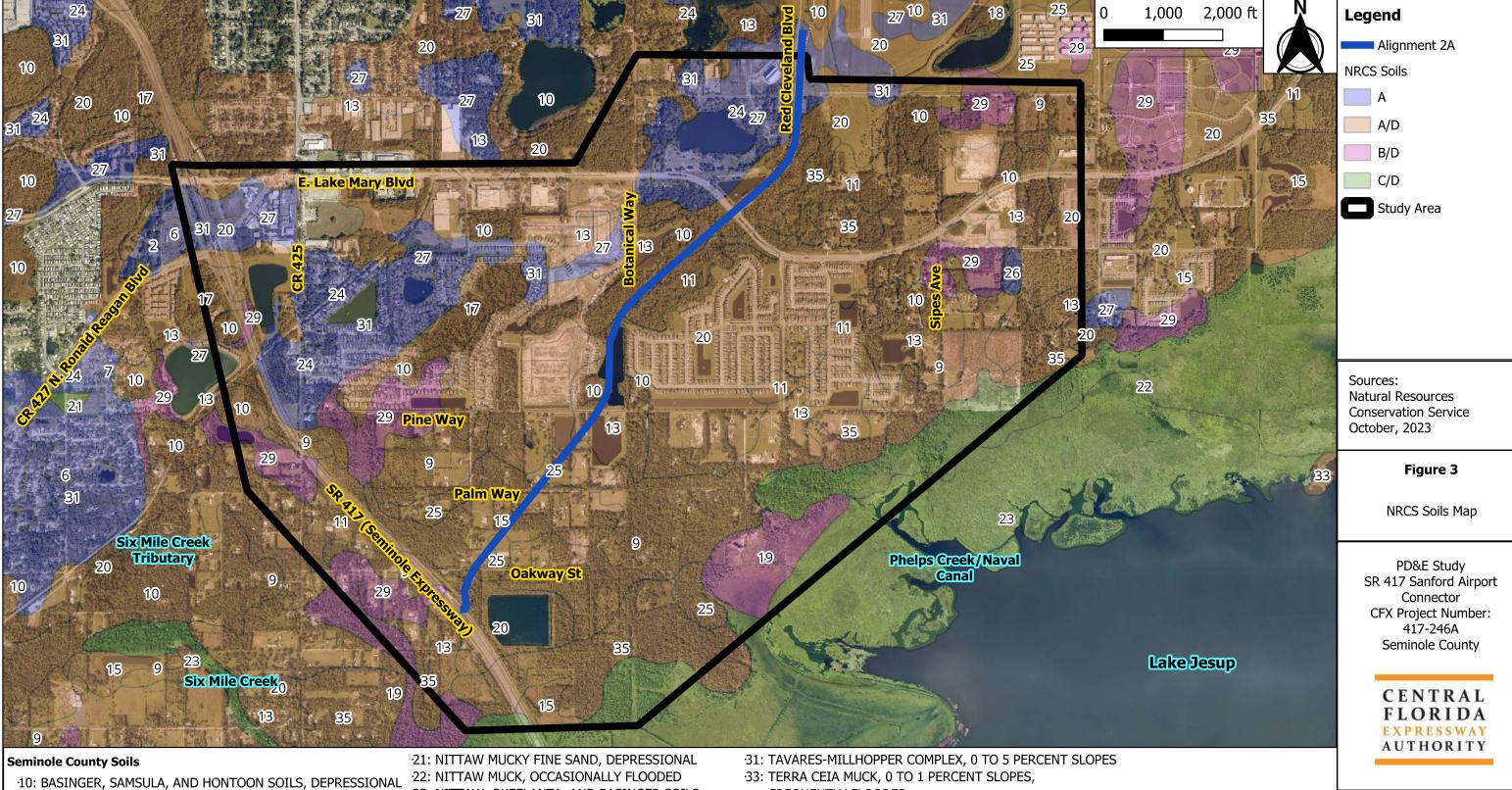
7. References

- 1. Central Florida Expressway Authority (March 2025). 2025 Design Guidelines.
- 2. Federal Emergency Management Agency (Effective September 28, 2007). Flood Insurance Rate Maps, Jackson County, Florida and incorporated Areas. Community-Panel Numbers 12117C0070F, 12117C0090F, 12117C0160F and 12117C0180F.
- 3. Federal Emergency Management Agency (Effective September 28, 2007). Flood Insurance Study, Seminole County, Florida and incorporated Areas. Community-Panel Numbers 12117CV000A.
- 4. Federal Highway Administration (May 2024). HY-8 Culvert Hydraulic Analysis Program User Manual.
- 5. Florida Department of Transportation (January, 2025). *Design Manual*.
- 6. Florida Department of Transportation (January, 2025). *Drainage Manual*.
- 7. Florida Department of Transportation (January, 2025). FDOT Standard Plans for Road Construction.

Appendix A – Figures





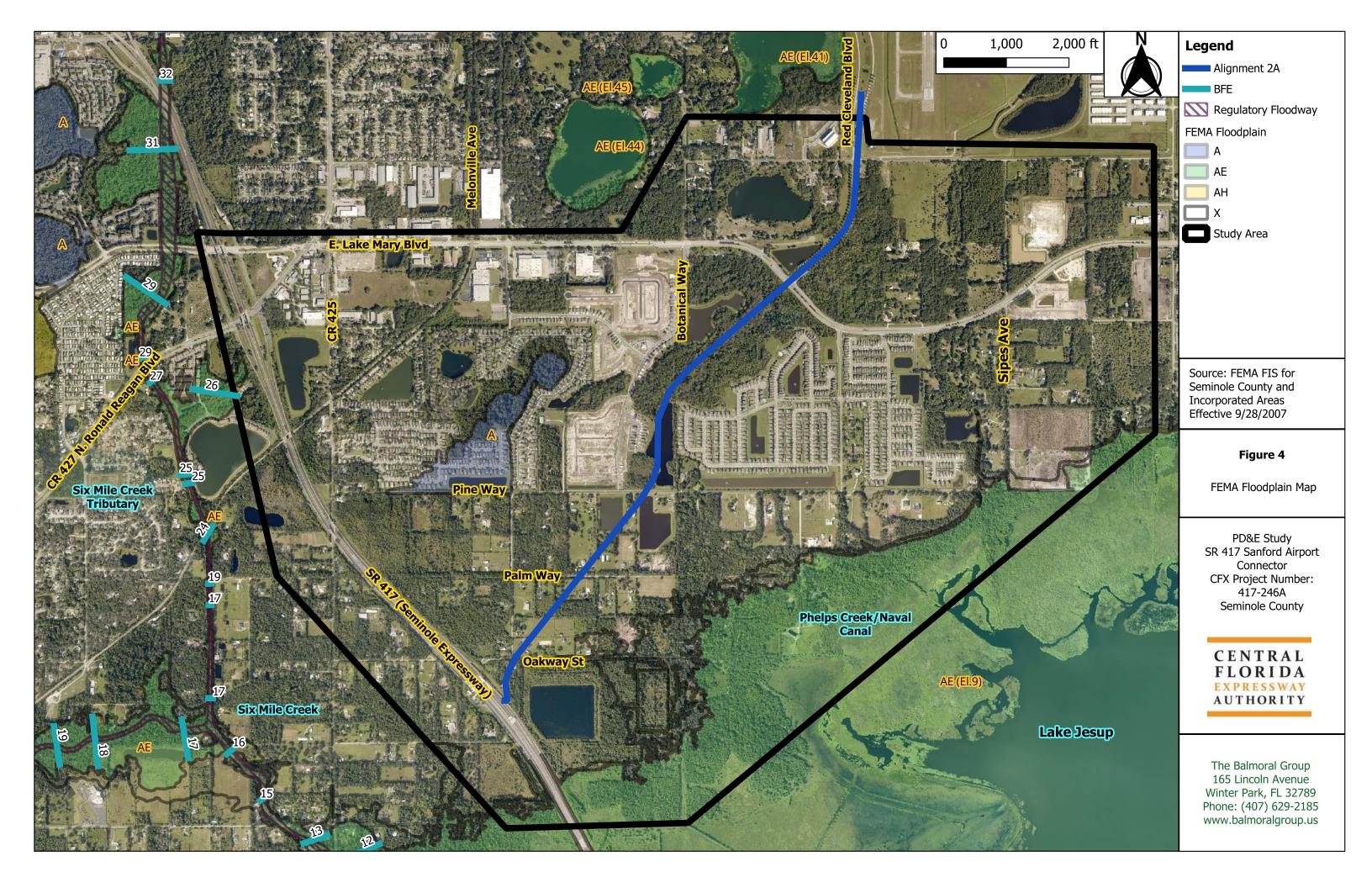


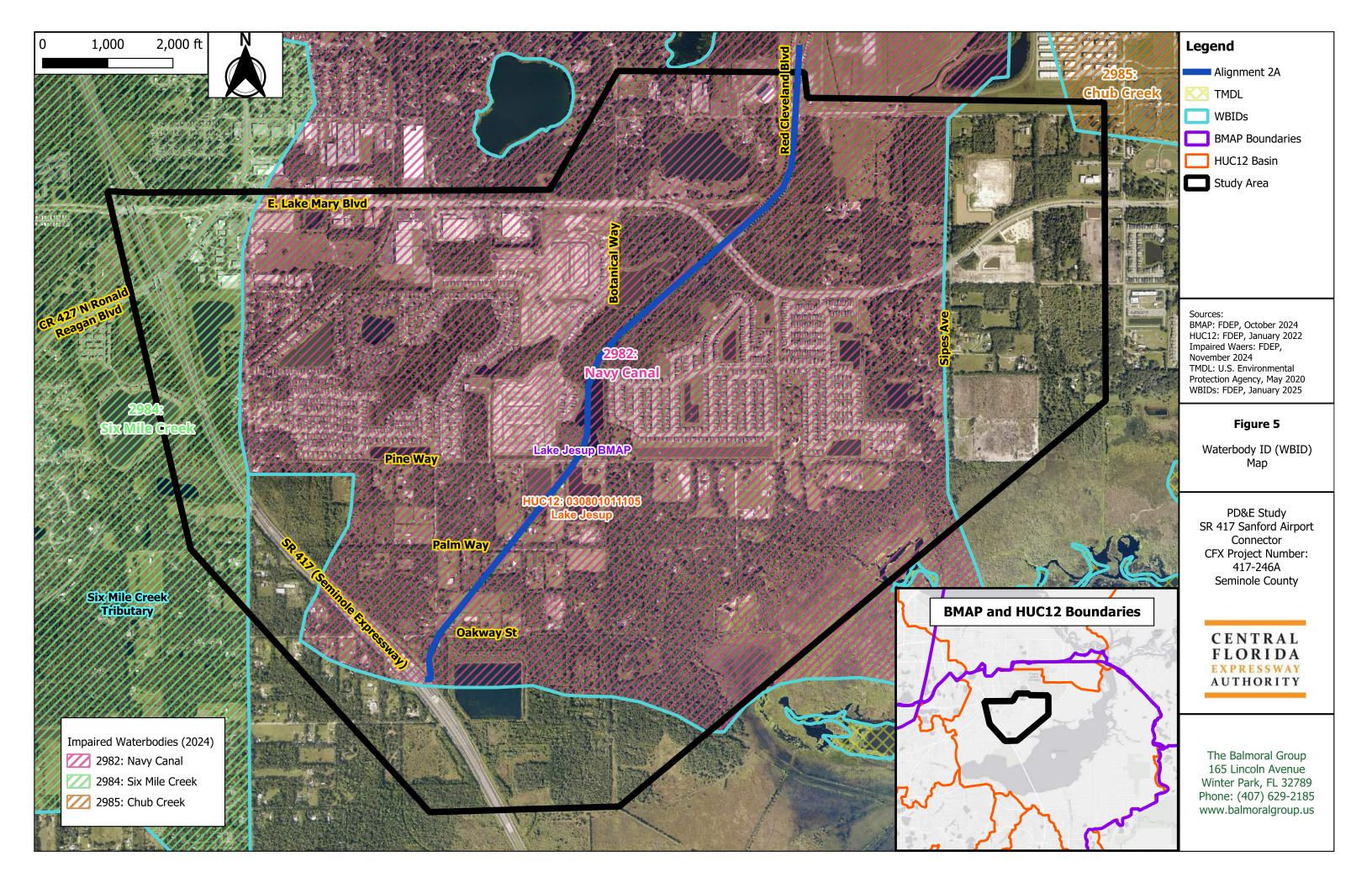
- 11: BASINGER AND SMYRNA FINE SANDS, DEPRESSIONAL
- ·13: EAUGALLIE AND IMMOKALEE FINE SANDS
- ·15: FELDA AND MANATEE MUCKY FINE SANDS, DEPRESSIONAL
- ·17: BRIGHTON, SAMSULA, AND SANIBEL MUCKS
- ·18: MALABAR FINE SAND, 0 TO 2 PERCENT SLOPES
- ·19: MANATEE, FLORIDANA, AND HOLOPAW SOILS, FREQUENTLY FLOODED
- 2: ADAMSVILLE-SPARR FINE SANDS
- 20: MYAKKA AND EAUGALLIE FINE SANDS

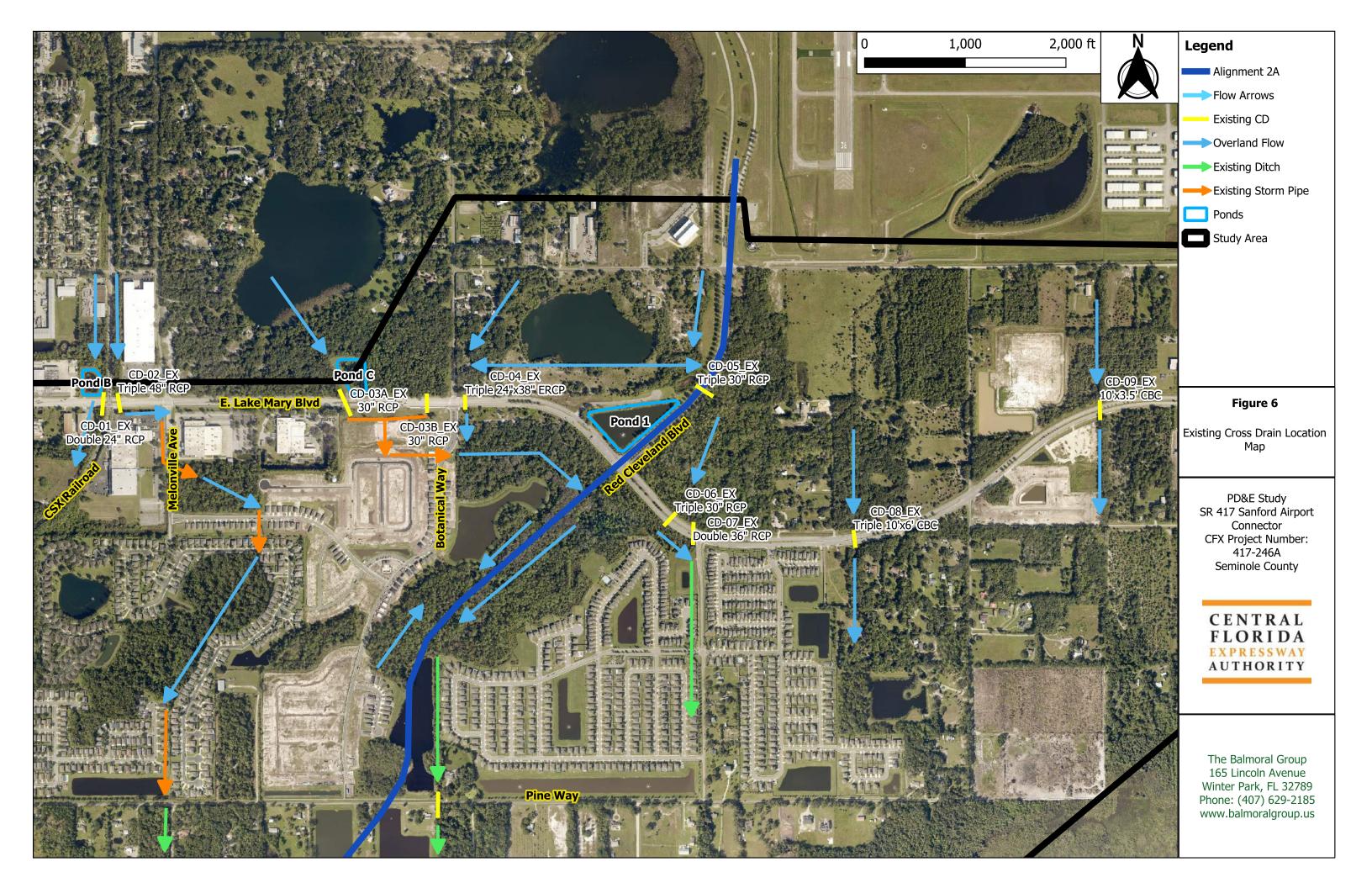
- 23: NITTAW, OKEELANTA, AND BASINGER SOILS, FREQUENTLY FLOODED
- 24: PAOLA-ST. LUCIE SANDS, 0 TO 5 PERCENT SLOPES 35: WABASSO FINE SAND, 0 TO 2 PERCENT SLOPES
- 25: PINEDA-PINEDA, WET, FINE SAND, 0 TO 2 PERCENT SLOPES
- 26: UDORTHENTS, EXCAVATED
- 27: POMELLO FINE SAND, 0 TO 5 PERCENT SLOPES
- 29: ST. JOHNS AND EAUGALLIE FINE SANDS
- 3: ARENTS, 0 TO 5 PERCENT SLOPES

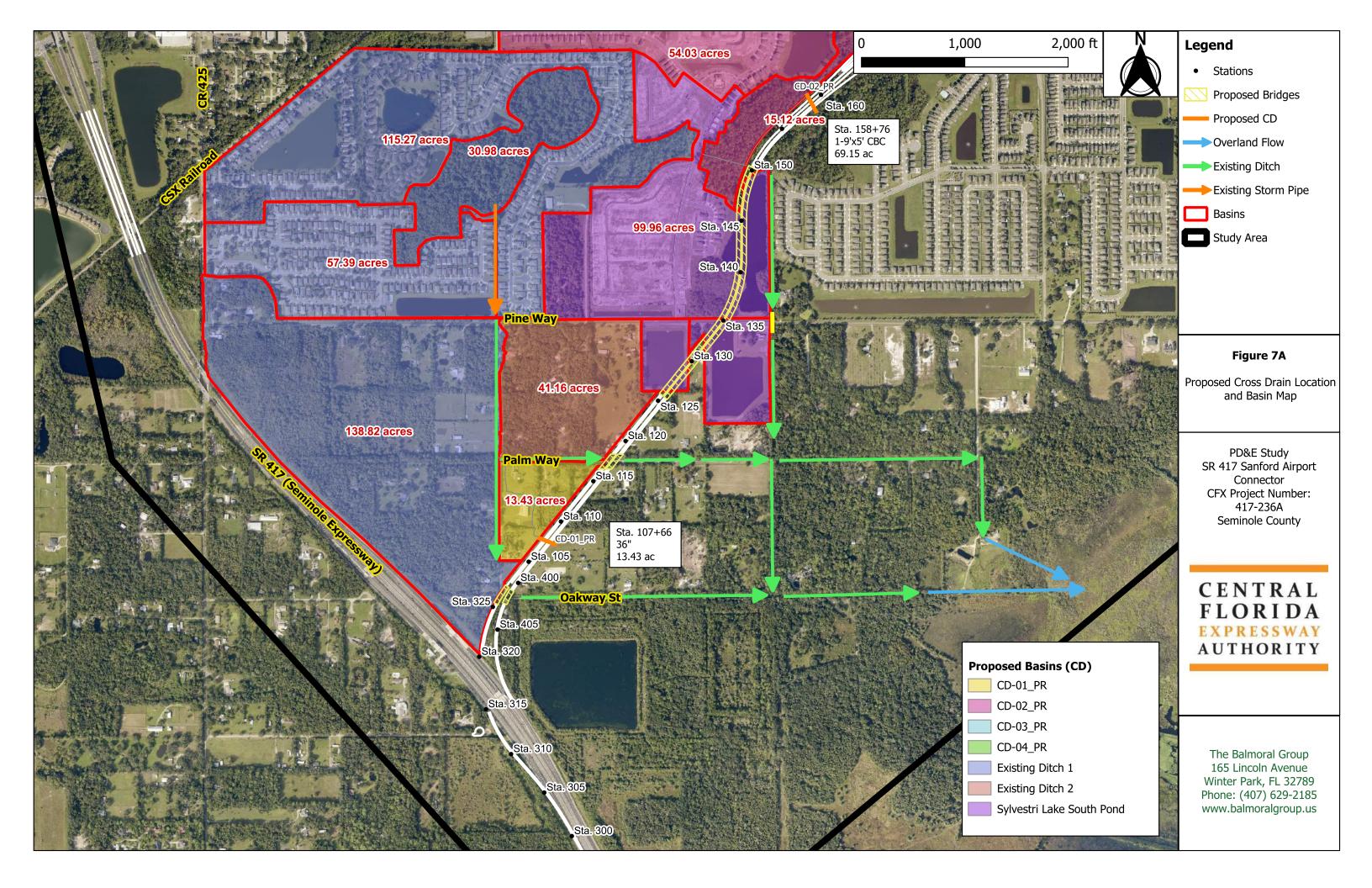
- FREQUENTLY FLOODED
- 34: URBAN LAND, 0 TO 2 PERCENT SLOPES
- 6: ASTATULA-APOPKA FINE SANDS, 0 TO 5 PERCENT SLOPES
- 7: ASTATULA-APOPKA FINE SANDS, 5 TO 8 PERCENT
- 8: ASTATULA-APOPKA FINE SANDS, 8 TO 12 PERCENT SLOPES
- 9: BASINGER AND DELRAY FINE SANDS
- 99: WATER

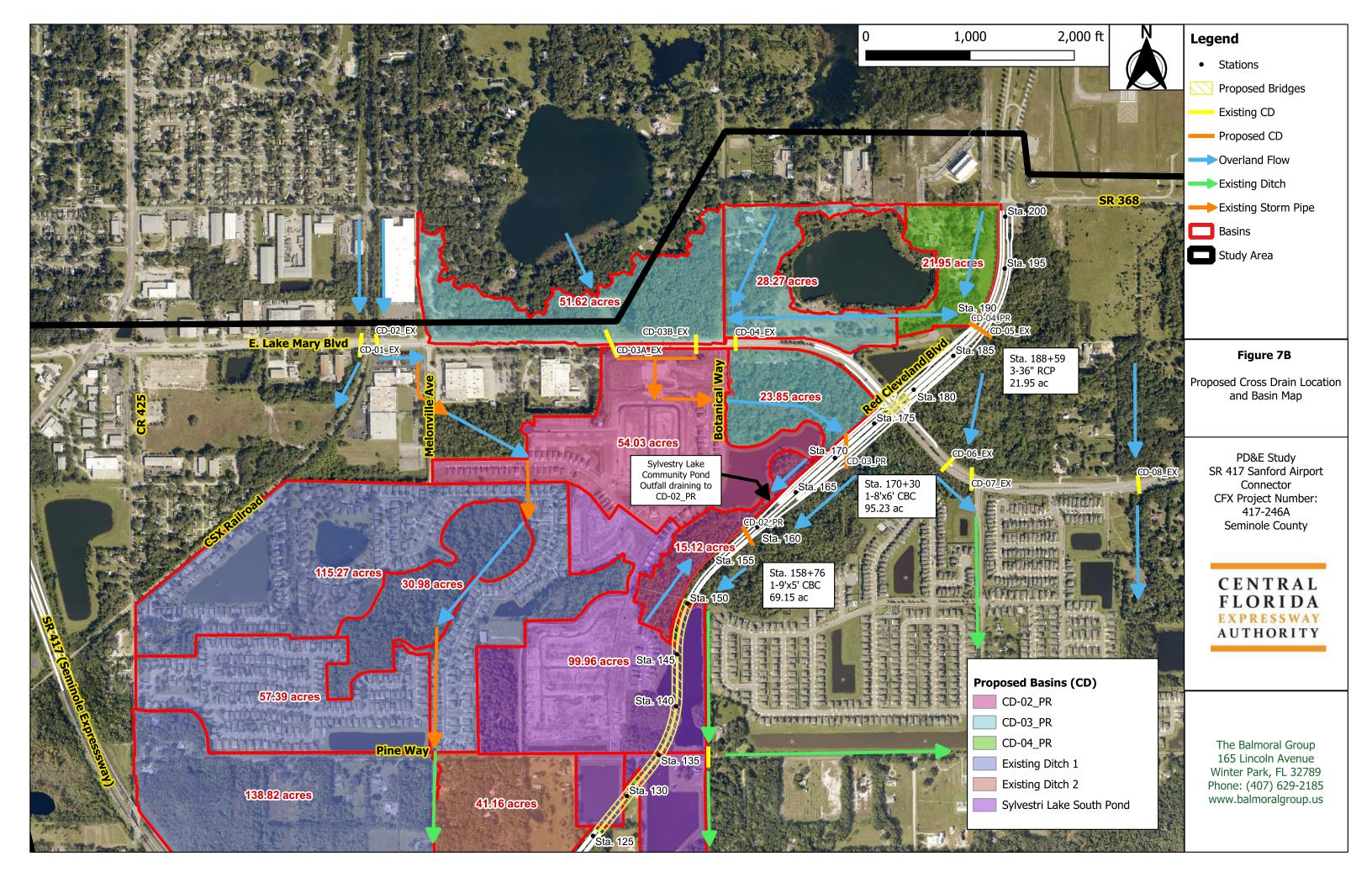
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Appendix B – Existing Permitted Documents

CROSS DRAIN CD-01_EX
AND
CROSS DRAIN CD-02_EX

STORMWATER MANAGEMENT CALCULATIONS

Volume I

East Lake Mary Boulevard

Segments I

From Sanford Avenue to Ohio Avenue

SEMINOLE COUNTY, FLORIDA

PREPARED BY:

22495-5 -

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Division of CH2M HILL
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Orlando, FL 32801-4322

ando, FL 32801-4322 407-423-0030 RECEIVED

SEP 2 7 2002

PDS ALTAMONTE SVC. CTR.

SUBMITTED FOR:

SEMINOLE COUNTY ENGINEERING DEPARTMENT

September 2002

1/2/102

Seaboard Coastline Railroad Crossing. At this point the runoff turns south and crosses ELMB where it must stage up to above elevation 48 NGVD where it then crosses the railroad bridge and is collected in the triple 48" culvert mentioned above. The flow continues east in a series of triple 48" culverts and ditches and then south into the Mellonville Road outfall.

The **third sub-basin** includes a portion of the extension of ELMB designed by Seminole County (42-117-0943NG sub-basin C and D) from approximately 550 feet east of Seaboard Coastline Railroad to approximately 850 feet west of Ohio Avenue including the west side of Ohio Avenue. The area drains in roadside ditches to a 30" RCP culvert located 1000 feet west of Ohio Avenue where it discharges to the south and into the SilverVista Storrnwater Management System (4-117-0317M2). This sub-basin includes a large offsite area to the north consisting of undeveloped or agricultural land use. The water quality volume from this portion of the roadway is collected and treated in roadside swales with ditch blocks and made to percolate into the surficial groundwater table.

2.2 PROPOSED SURFACE WATER MANAGEMENT SYSTEMS

The proposed stormwater management systems are not intended to significantly alter historical paths of conveyance for existing flows. The intent is to collect only the roadway runoff into the wet detention ponds while directing the offsite flows to their existing outfall points.

2.2.1 SEGMENT

Proposed drainage along the Segment I project corridor will consist of three (3) drainage sub-basins.

The first sub-basin, or sub-basin A, extends from Sanford Avenue to approximately 600 feet east along ELMB and consists of 1.46 acres roadway and 5.69 acres of Industrial type land use. The runoff from this basin drains toward a retention pond in the area bounded by ELMB on the south, Sanford Avenue on the east and CR 427 on the northwest. The Brindley Pieters design for the Sanford Avenue/ELMB/CR 427 intersection includes a new pond south of ELMB between Sanford Avenue and CR 427 that accepts runoff from ELMB west of Sanford Avenue. The pond to the north of ELMB will be designed to accept the runoff from the system east of Sanford Avenue. The outfall for the pond north of ELMB will tie into the outfall for the pond south of ELMB and then into the existing CR 427 Outfall.

The second sub-basin, or sub-basin B, includes ELMB from approximately 600 feet east of Sanford Avenue to the Seaboard Coastline Railroad and consists of 3.89 acres of roadway, 32.88 acres of undeveloped and 34.79 acres of Industrial type land use. This

sub-basin includes offsite area to the north and south including a portion of the Cardinal Homes Site that drains into an adjacent lake. The drop structure outfall for this lake will remain while the 24" RCP outfall will be eliminated. The proposed roadway runoff will be collected in an enclosed conveyance system and directed to Wet Detention Pond B located northwest of the Railroad and ELMB intersection. The proposed discharge structure for the existing RL Best Machine Shop Pond will tie into the roadway system while all other offsite runoff will be routed in a separate conveyance system and directed to its existing outfall at the Railroad crossing. The Pond B outfall will cross the Railroad north of ELMB and discharge into a canal that drains to the existing triple 48" culverts to the south. This system will ultimately discharge to the **Mellonville Road Outfall** to the east.

The third sub-basin, or sub-basin C, includes a portion of the extension of ELMB designed by Seminole County (42-117-0943NG sub-basin C and D) from the Seaboard Coastline Railroad Crossing to Ohio Avenue including the west side of Ohio Avenue and consists of 51.58 acres of primarily Industrial, Residential and Agricultural land uses located mostly to the north of ELMB. The proposed roadway runoff will discharge into Wet Detention Pond C and outfall into the silverVista stom1water Management System Outfall and eventually Lake Jesup.

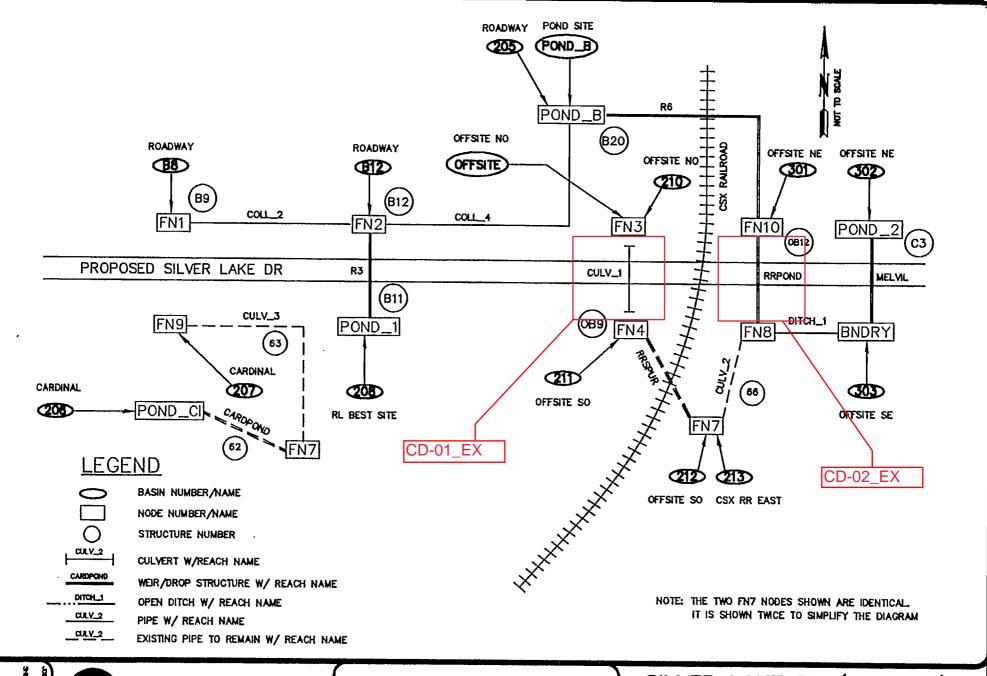
2.3 ENVIRONMENTAL IMPACT ASSESSMENT

2.3.1 JURISDICTIONAL WETLAND AREAS

A field delineation of all wetland areas within the original 1995 alignment for both Segments I and II was performed by Environmental Management Systems, Inc. (EMS) and a copy of this assessment is included as an attachment to this report. These jurisdictional areas consisted of primarily natural streams (Chub Creek) and manmade irrigation ditches. The most significant wetland along both the **original** Segment I and II alignments was the area near the Airport Entrance Road. Several cross culverts were to be placed in this area to maintain the hydrologic connection and therefore reduce the impacts to this wetland. Additionally, one of these culverts were sized (48") to act as a "critter crossing". With the **re-alignment of Segment IIA**, the encroachment into that wetland has been reduced. **Again**, application is for Segment I, only.

Only one **wetland** area, other than manmade ditches was considered jurisdictional in the Segment I corridor. This is a small wetland (0.13 acre total area with 0.02 acres of impact) known as Wetland #1 and located in the northwest quadrant of the Mellonville Road intersection. No additional mitigation, **other than that as provided AND PREVIOUSLY CONSTRUCTED** is proposed for this re-permitting project. There were eight (8) other soggy bottom roadside or railroad or road crossing manmade ditches that

POST-CONSTRUCTION



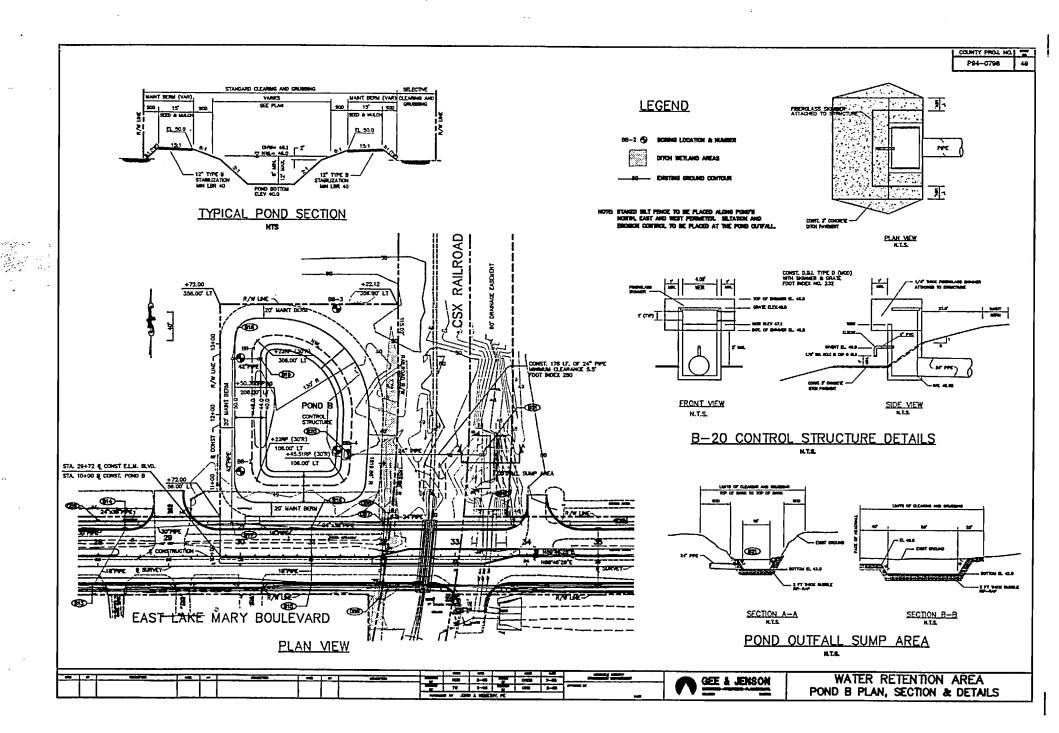




GEE & JENSON

POST-CONSTRUCTION

SILVER LAKE DR (BASIN B) NODE/REACH DIAGRAM



SILVER LAKE DRIVE BASIN 8 POST-CONST 25YR/24HR EVENT 10/20/95

10/20/95					
BASIN NAME	OFFSITE		812	205	206
NODE NAME	FN3	ENI	FN2	POND_8	POND_CI
UNIT HYDROGRAPH	UH256	UH484	UH484	UH484	UH484
PEAKING FACTOR	256.	484.	484.	484.	484.
TERRING TRIOTOR	230,	101.	1011	707.	101.
RAINFALL FILE	FLMOD	FLMOD	FLMOD	FLMOD	FLMOD
RAIN AMOUNT (in)	8.50	8.50	8.50	8.50	8.50
STORM DURATION (hrs)	24.00	24.00	24.00	24.00	24.00
AREA (ac)	10.94		1.38	1.75	5.47
CURVE NUMBER	90.00		73.00	73.00	93.50
DCIA (%)	.00		85.00	85.00	.00
TC (mins)	101.00	10.00	10.00	10.00	10.60
LAG TIME (hrs)	.00	.00	.00	.00	.00
8ASIN STATUS	OFFSITE	ONSITE	ONSITE	ONSITE	OFFSITE
BASIN QMX (cfs) TMX	(hre) VOI	(in) NOTES			
OFFSITE 15.00	13.02	7.28 8ASIN	203 & 204	MINIIS ROAD	WΔY
88 4.55	12.02	7.92 PROPOS			MIN I
812 8.26	12.02	7.92 PROPOS			
205 10.48	12.02	7.92 PROPOS			
206 33.16	12.01	7.71 CARDIN			
8ASIN NAME NODE NAME	207 FN9	208 POND_1	210 FN3	211 FN4	212 FN7
UNIT HYDROGRAPH	HUDE	HUDE	HUDE	HUOE (luior.
PEAKING FACTOR	UH256 256.	UH256 256.	UH256 256.	UH256 256.	UH256 256.
renaind includ	230,	230.	230.	230.	230.
RAINFALL FILE	FLMOD	FLMOD	FLMOD	FLMOD	FLMOD
RAIN AMOUNT (in)	8.50	8.50	8.50	8.50	8.50
STORM DURATION (hrs)	24.00	24.00	24.00	24.00	24.00
()					
AREA (ac)	1.01		7.02	6.29	16.58
CURVE NUMBER	75.20		73.00	75.20	73.00
DCIA (%)	.00	.00	.00	.00	.00
TC (mins)	21.20	23.20	71.20	75.00	45.00
LAG TIME (hrs) BASIN STATUS	.00 OFFSITE	.00 OFFSITE	.00.	.00.	.00
9H2T4 21H102	OLLOTIC	0112115	OFFSITE	ONSITE	ONSITE
208 1.38 210 8.99 21! 8.19	(hrs) VOL 12.15 12.17 12.82 12.83 12.50	(in) NOTES 5.52 CARDIN 7.65 RL 8ES 5.25 OFFSIT 5.52 OFFSIT 5.25 OFFSIT	T MACHINE E NORTH OF E AREA SOL	SHOP WAREHOUSES ITH	3

DRAINAGE BASINS FOR:

CD-01_EX: OFFSITE AND 210 TOTAL DRAINAGE AREA: 17.96 AC

CD-02_EX: B8, B12, 205, 208, 301, AND POND B TOTAL DRAINAGE AREA: 14.39 AC

SILVER LAKE DRIVE BASIN B POST-CONST 25YR/24HR EVENT 1C/20/95

				_	
BASIN NAME NODE NAME	213 FN7	PONDB	301	302 POND_2	303 BNDRY
NUDE NAME	rn/	POND_B	FN10	PUNU_2	ואטמם
UNIT HYDROGRAPH	UH256	UH256	UH4B4	UH4B4	UH4B4
PEAKING FACTOR	256.	256.	484.	484.	484.
RAINFALL FILE	FLMOD	FLMOD	FLMOD	FLMOD	FLMOD
_					
RAIN AMOUNT (in)	8.50		8.50		8.50
STORM DURATION (hrs)	24.00	24.00	24.00	24.00	24.00
AREA (ac)	1.05	1.76	B.34	6.41	2.40
CURVE NUMBER	81.50	85.70	B8.40	90.60	91.70
DCIA (%)	.00	.00	.00	.00	.00
TC (mins)	26.90	10.00	22.30	17.30	10.00
LAG TIME (hrs)	.00	.00	.00	.00	.00
BASIN STATUS	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
BASIN QMX (cfs) TMX	(hrs) VOL	(in) NOTES			
213 2.B9	12.25	6.27 EASTS	IDE OF RR	SOUTH OF SL	D
PONDB 8.13	12.04	6.78 PROPO	SED POND S	ITE AREA	
301 40.89	12.09	7.09 NO OF	SLD BETWE	EN RR & MEL	LONVILLE
302 34.74	12.07	7.36 NO OF	SLD BETWE	EN RR & MEL	LONVILLE
303 14.47	12.02	7.49 SO OF	SLD BETWE	EN RR & MEL	LONVILLE

CD-01 EX

SILVER LAKE DRIVE BASIN B POST-CONST 10/31/95

>>REACH NAME : CULV_1

FROM NODE : FN3

TO NODE : FN4

: CULVERT, CIRCULAR w/ ROADWAY REACH TYPE

FLOW DIRECTION : POSITIVE AND NEGATIVE FLOWS ALLOWED

TURBO SWITCH : OFF

CULVERT DATA

SPAN (in): 24.000 RISE (in): 24.000 LENGTH (ft): 125.000 MANNING N:

U/S INVERT (ft): 46.350 D/S INVERT (ft): 46.050

.500 # OF CULVERTS: 2.000 ENTRNC LOSS:

: RECTANGULAR ROADWAY/BERM WEIR POSITION A

CREST EL. (ft): 49.800 CREST LN. (ft): 293.000 WEIR COEF.: 2.800 RESERVED: ******

RESERVED: ****** RESERVED:******

POSITION B : RECTANGULAR ROADWAY/BERM WEIR

CREST EL. (ft):****** CREST LN. (ft):****** WEIR COEF .: ****** RESERVED: ******

RESERVED: ****** RESERVED: ******

NOTE: CROSS CULVERT WEST OF RAILROAD

: CULV_2 . NREACH NAME

: FN7 ROM NODE TO NODE : FN8

: CULVERT, CIRCULAR w/ ROADWAY REACH TYPE

FLOW DIRECTION : POSITIVE AND NEGATIVE FLOWS ALLOWED

TURBO SWITCH : OFF

CULVERT DATA

LENGTH (ft): 243.000 SPAN (in): 36.000 RISE (in): 36.000 .012

U/S INVERT (ft): 45.800 D/S INVERT (ft): 43.100 MANNING N:

ENTRNC LOSS: .500 # OF CULVERTS: 1.000

POSITION A : NOT USED

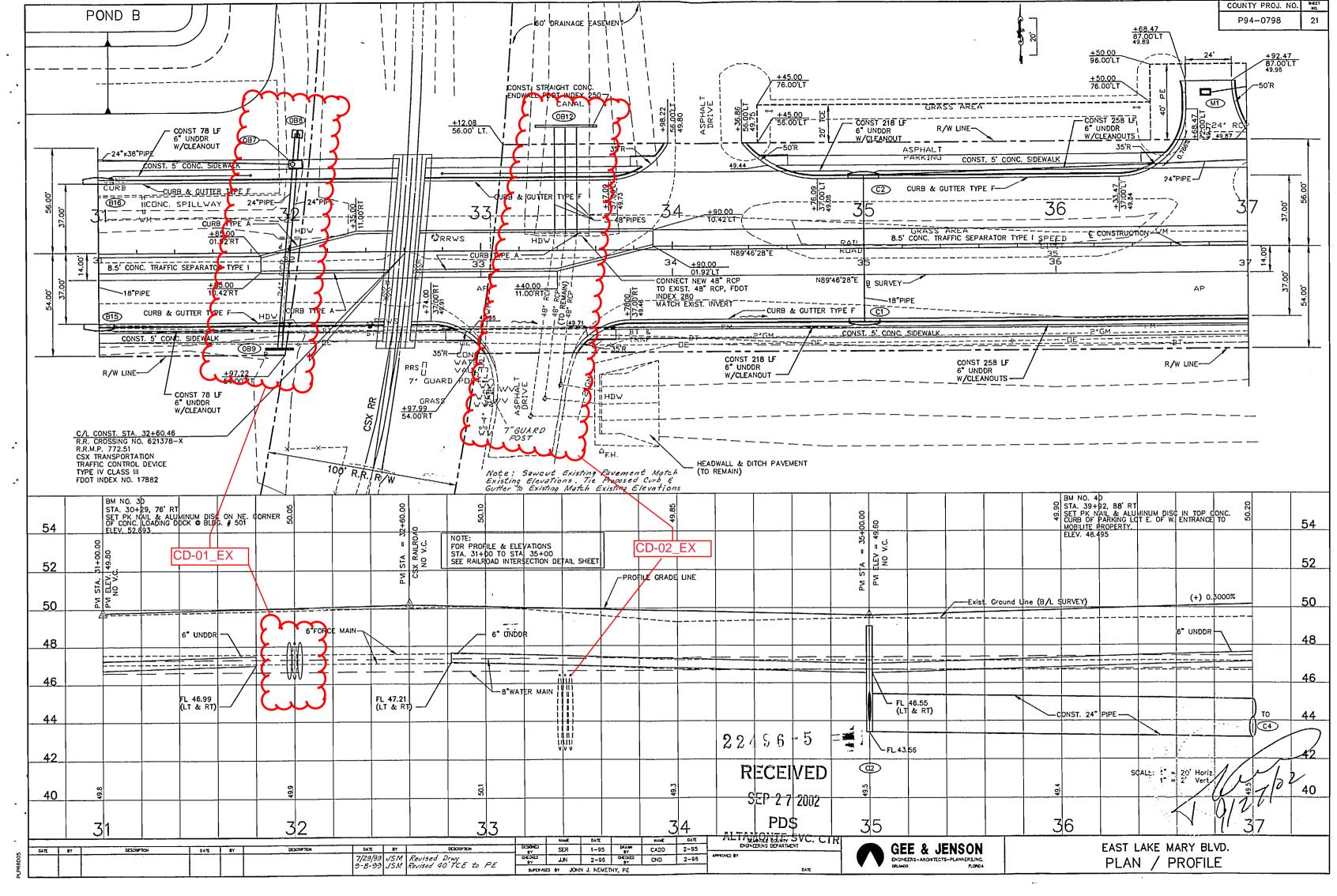
POSITION 8 : NOT USED

NOTE: CULVERT FROM RR BRIDGE TO (3) 48"

SILVER LAKE DRIVE 8ASIN 8 POST-CONST 25YR/24HR EVENT 10/31/95

REACH MAXIMUM FLOW REPORT

	REACH ID	TIME (hrs)	FLOW (cfs)	FR NODE NAME	STAGE (ft)	TO NODE NAME	STAGE (ft)	CD-01_EX
	RRSPUR	13.00	31.45	FN4	48.29	FN7	46.90	OB-01_EX
	CO_L_2	12.00	4.33	FN1	48.41	FN2	48.34	
Γ	CO <u>LL_4</u> CULV_1	12.00 13.00	10.95 23.57	FN3	48.34 48.91	<u> </u>	47.77 48.29	\neg /
_	CU_V_2	16.50	16.57			FN8	43.43	
	CULV_3	4.75	.64	FN9 POND_1	45.80 48.29	FN7 FN2	45.80 48.07	CD-02_EX
	R3 Melvil	12.75 12.25	1.08 25.09	POND_1 POND_2	49.68	8NDRY	42.93	
	R6	12.50	12.14	POND_8			46.80	
г	CARDPOND	12.25	16.83	POND_CI	48.45	FN7	46.22	 /
	RRPOND	12.50	35.56	FN10	46.80	FN8	43.69	Y
Ī	DITCH_1	12.50	38.53	FN8	43.69	8NDRY	42.95	



CROSS DRAIN CD-03A_EX
AND
CROSS DRAIN CD-03B_EX

STORMWATER MANAGEMENT CALCULATIONS

Volume I

East Lake Mary Boulevard

Segments I

From Sanford Avenue to Ohio Avenue

SEMINOLE COUNTY, FLORIDA

PREPARED BY:

22498-5 -

Gee & Jenson,
Division of CH2M HILL
225 E. Robinson Street, Suite 505

225 E. Robinson Street, Suite 509 Orlando, FL 32801-4322 407-423-0030

SUBMITTED FOR:

RECEIVED

SEP 2 7 2002

PDS ALTAMONTE SVC. CTR.

SEMINOLE COUNTY ENGINEERING DEPARTMENT

September 2002

1/2/102

Seaboard Coastline Railroad Crossing. At this point the runoff turns south and crosses ELMB where it must stage up to above elevation 48 NGVD where it then crosses the railroad bridge and is collected in the triple 48" culvert mentioned above. The flow continues east in a series of triple 48" culverts and ditches and then south into the Mellonville Road outfall.

The **third sub-basin** includes a portion of the extension of ELMB designed by Seminole County (42-117-0943NG sub-basin C and D) from approximately 550 feet east of Seaboard Coastline Railroad to approximately 850 feet west of Ohio Avenue including the west side of Ohio Avenue. The area drains in roadside ditches to a 30" RCP culvert located 1000 feet west of Ohio Avenue where it discharges to the south and into the SilverVista Storrnwater Management System (4-117-0317M2). This sub-basin includes a large offsite area to the north consisting of undeveloped or agricultural land use. The water quality volume from this portion of the roadway is collected and treated in roadside swales with ditch blocks and made to percolate into the surficial groundwater table.

2.2 PROPOSED SURFACE WATER MANAGEMENT SYSTEMS

The proposed stormwater management systems are not intended to significantly alter historical paths of conveyance for existing flows. The intent is to collect only the roadway runoff into the wet detention ponds while directing the offsite flows to their existing outfall points.

2.2.1 SEGMENT

Proposed drainage along the Segment I project corridor will consist of three (3) drainage sub-basins.

The first sub-basin, or sub-basin A, extends from Sanford Avenue to approximately 600 feet east along ELMB and consists of 1.46 acres roadway and 5.69 acres of Industrial type land use. The runoff from this basin drains toward a retention pond in the area bounded by ELMB on the south, Sanford Avenue on the east and CR 427 on the northwest. The Brindley Pieters design for the Sanford Avenue/ELMB/CR 427 intersection includes a new pond south of ELMB between Sanford Avenue and CR 427 that accepts runoff from ELMB west of Sanford Avenue. The pond to the north of ELMB will be designed to accept the runoff from the system east of Sanford Avenue. The outfall for the pond north of ELMB will tie into the outfall for the pond south of ELMB and then into the existing CR 427 Outfall.

The second sub-basin, or sub-basin B, includes ELMB from approximately 600 feet east of Sanford Avenue to the Seaboard Coastline Railroad and consists of 3.89 acres of roadway, 32.88 acres of undeveloped and 34.79 acres of Industrial type land use. This

sub-basin includes offsite area to the north and south including a portion of the Cardinal Homes Site that drains into an adjacent lake. The drop structure outfall for this lake will remain while the 24" RCP outfall will be eliminated. The proposed roadway runoff will be collected in an enclosed conveyance system and directed to Wet Detention Pond B located northwest of the Railroad and ELMB intersection. The proposed discharge structure for the existing RL Best Machine Shop Pond will tie into the roadway system while all other offsite runoff will be routed in a separate conveyance system and directed to its existing outfall at the Railroad crossing. The Pond B outfall will cross the Railroad north of ELMB and discharge into a canal that drains to the existing triple 48" culverts to the south. This system will ultimately discharge to the Mellonville Road Outfall to the east.

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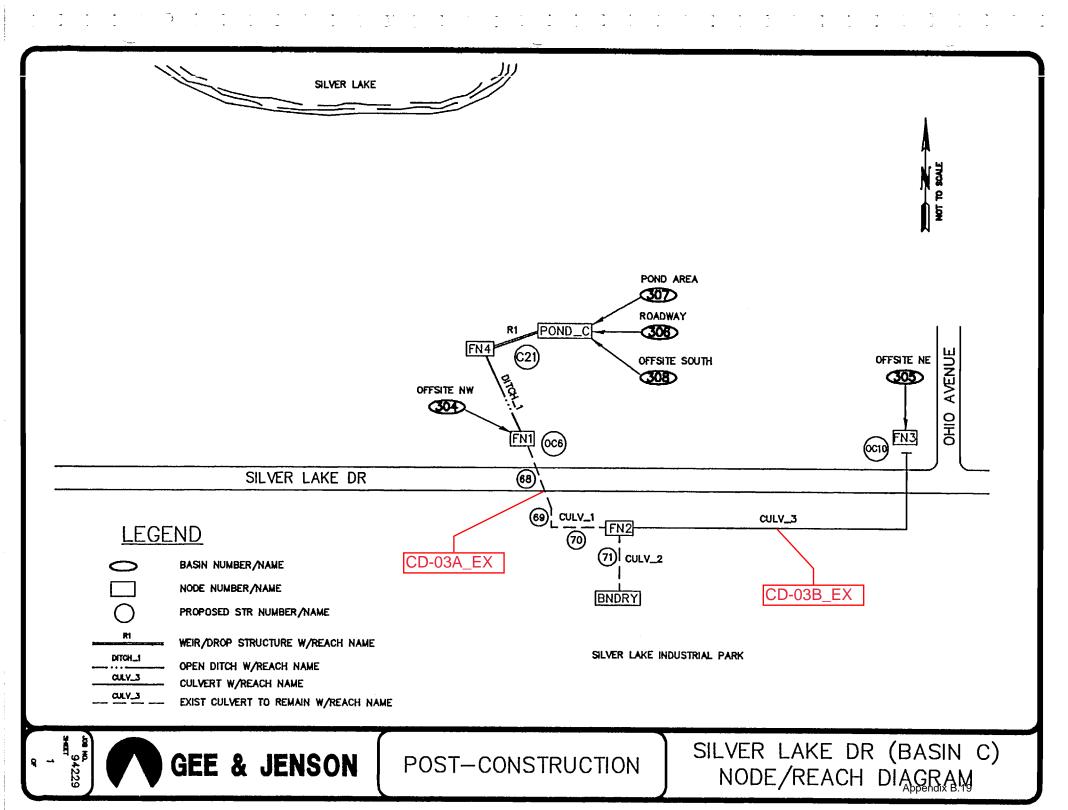
2.3 ENVIRONMENTAL IMPACT ASSESSMENT

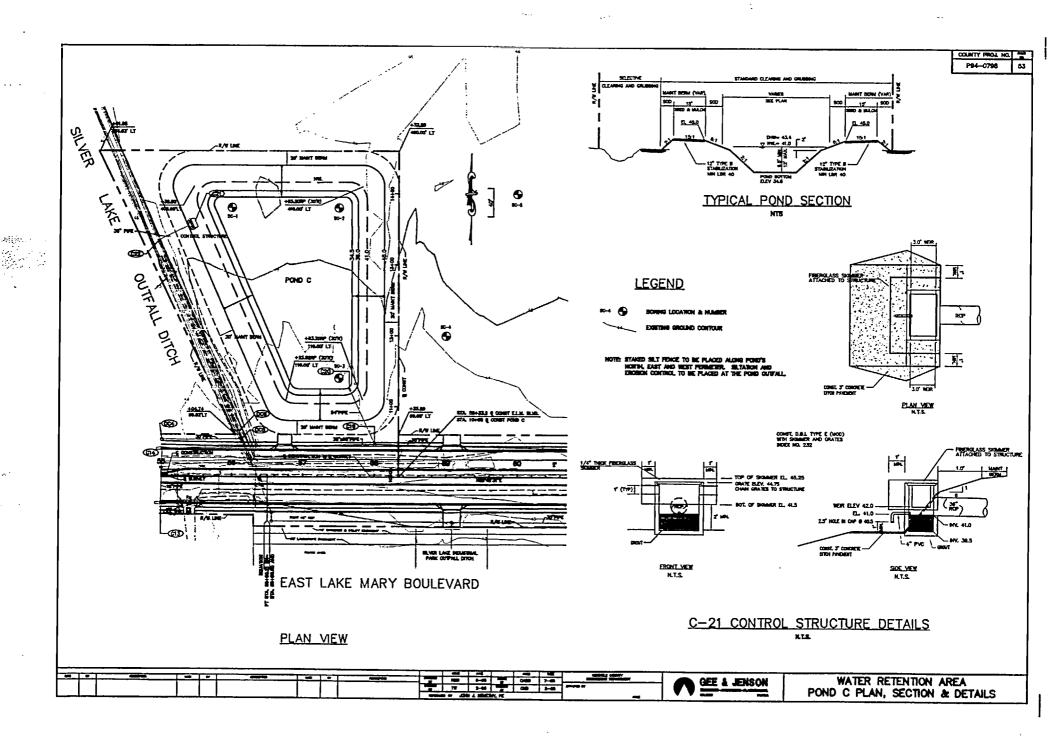
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Only one **wetland** area, other than manmade ditches was considered jurisdictional in the Segment I corridor. This is a small wetland (0.13 acre total area with 0.02 acres of impact) known as Wetland #1 and located in the northwest quadrant of the Mellonville Road intersection. No additional mitigation, **other than that as provided AND PREVIOUSLY CONSTRUCTED** is proposed for this re-permitting project. There were eight (8) other soggy bottom roadside or railroad or road crossing manmade ditches that

POST-CONSTRUCTION





SILVER LAKE DRIVE BASIN C POST-CONST 25YR/24HR EVENT 11/2/95

BASIN NAME NODE NAME	304 FN1		306 POND_C	307 POND_C	
UNIT HYDROGRAPH	UH256		UH484		
PEAKING FACTOR	256.	256.	484.	256.	256.
RAINFALL FILE	FLMOD		FLMOD	FLMOD	FLMOD
RAIN AMOUNT (in)	8.50	8.50	8.50	8.50	8.50
STORM DURATION (hrs)	24.00	24.00	24.00	24.00	24.00
AREA (ac)	20.10	19.08	8.02	2.40	1.98
CURVE NUMBER	74.90	78.00	77.00	89.40	77.00
DCIA (%)	.00		65.00		
TC (mins)	84.30	80.40	27.00	10.00	
LAG TIME (hrs)	.00	.00	.00	.00	.00
BASIN STATUS	ONSITE	ONSITE	ONSITE	ONSITE	ONSITE
BASIN QMX (cfs) TMX	(hrs) VOL	(in) NOTES			
· · · · · · · · · · · · · · · · · · ·	12.93	5.48 OFFSI1	F NORTHWES	ST.	
		5.85 OFFSIT			
					40540
306 36.32	12.18	7.46 PROPOS	OFN RHOTH (, KUAUWAY	AKEAS

7.22 PROPOSED POND SITE

5.72 OFFSITE SOUTHSIDE

307

303

11.57

2.22

12.04

12.97

DRAINAGE BASINS FOR:

CD-03A_EX: 304, 306, 307, AND 308 TOTAL DRAINAGE AREA: 32.50 AC

CD-03B_EX: 305 TOTAL DRAINAGE AREA: 19.08 AC

SILVER LAKE DRIVE BASIN & POST-CONST 25YR/24HR EVENT 4/29/96

REACH MAXIMUM FLOW REPORT

REACH ID	TIME (hrs)	FLOW (cfs)	FR NODE NAME	STAGE (ft)	TO NODE Name	STAGE (ft)	CD-03A_EX
CULY_1	13.00	36.48	FN1	43.08	FN2	42_33	Combined Flow
CULV_2	13.00	61.16	FN2	42.33	BNDRY	38.69	
CULV_3	13.00	24.68	FN3	45.06	FN2	42.33	
R1	12.50	15.37	POND_C	43.24	FN4	42.89	CD-03B_EX
DITCH_1	12.50	14.73	FN4	42.89	FN1	42.84	

SILVER LAKE DRIVE BASIN C POST-CONST 4/29/96

>>REACH NAME

: CULV 1 CD-03A_EX

FROM NODE

: FN1

TO NODE

: FN2

REACH TYPE

: CULVERT, CIRCULAR w/ ROADWAY

FLOW DIRECTION : POSITIVE AND NEGATIVE FLOWS ALLOWED

TURBO SWITCH

: OFF

CULVERT DATA

SPAN (in): 42.000

RISE (in): 42.000

U/S INVERT (ft): 39.340 D/S INVERT (ft): 39.100

.800 # OF CULVERTS: 1.000 ENTRNC LOSS:

POSITION A

: TRIANGULAR ROADWAY/BERM WEIR

CREST EL. (ft): 44.400 VERTEX ANG (dg): 179.620

RESERVED: ******

RESERVED:*****

WEIR COEF.: 2.800 RESERVED: *******

LENGTH (ft): 335.000

.012

MANNING N:

CONSTRUCTION PLANS

INDICATED 30" RCP

POSITION B

: RECTANGULAR ROADWAY/BERM WEIR

CREST EL. (ft):9999.000 CREST LN. (ft): .000

RESERVED: ******

WEIR COEF.: 2.800 RESERVED: ******

RESERVED: ******

NOTE: EXISTING CROSS CULVERT

* * NREACH NAME

: CULV_2

/ROM NODE

: FN2

TO NODE . REACH TYPE : BNDRY : CULVERT, ELLIPTICAL w/ ROADWAY

FLOW DIRECTION : POSITIVE AND NEGATIVE FLOWS ALLOWED

TURBO SWITCH

: OFF

CULVERT DATA

SPAN (in): 60.000

U/S INVERT (ft): 39.100 D/S INVERT (ft): 37.900

RISE (in): 38.000

LENGTH (ft): 104.000 MANNING N: .012

ENTRNC LOSS: .500 # OF CULVERTS: 1.000

POSITION A : RECTANGULAR ROADWAY/BERM WEIR CREST EL. (ft):9999.000 CREST LN. (ft):

RESERVED: ******

RESERVED: ******

WEIR COEF .: 2.800 RESERVED: ******

POSITION B

: RECTANGULAR ROADWAY/BERM WEIR

CREST EL. (ft): ****** CREST LN. (ft): ******

WEIR COEF .: ******

RESERVED: ******

RESERVED: ******

RESERVED: ******

NOTE: OUTFALL INTO SL INDUSTRIAL PARK

SILVER LAKE DRIVE BASIN C POST-CONST 4/29/96

. .>>REACH NAME : CULY_3 CD-03B_EX

FROM NODE : FN3
TO NODE : FN2

REACH TYPE : CULVERT, CIRCULAR w/ ROADWAY

FLOW DIRECTION : POSITIVE AND NEGATIVE FLOWS ALLOWED

TURBO SWITCH : OFF

CULVERT DATA

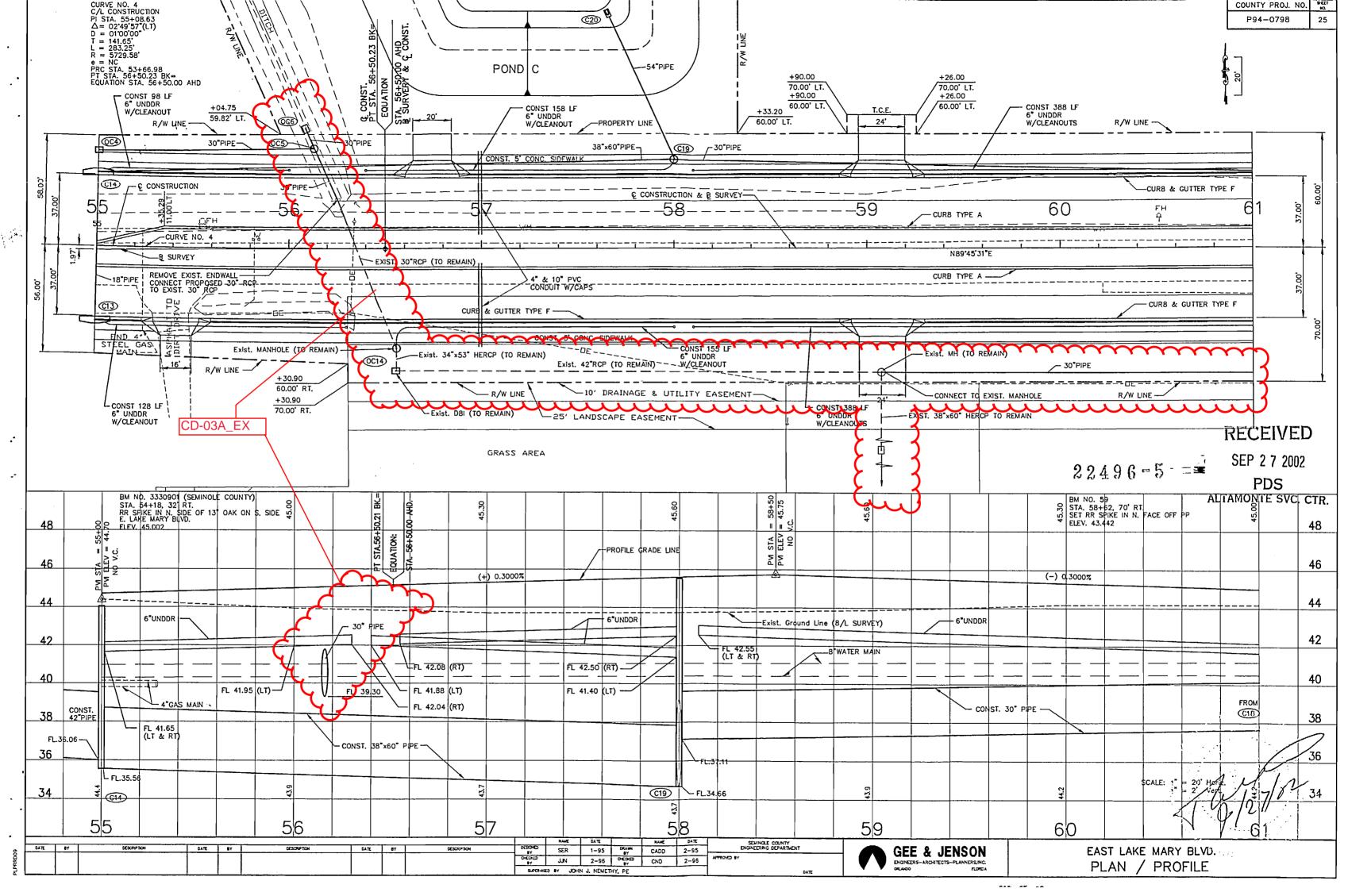
SPAN (in): 30.000 RISE (in): 30.000 LENGTH (ft): 566.000 U/S INVERT (ft): 40.250 D/S INVERT (ft): 39.250 MANNING N: .012

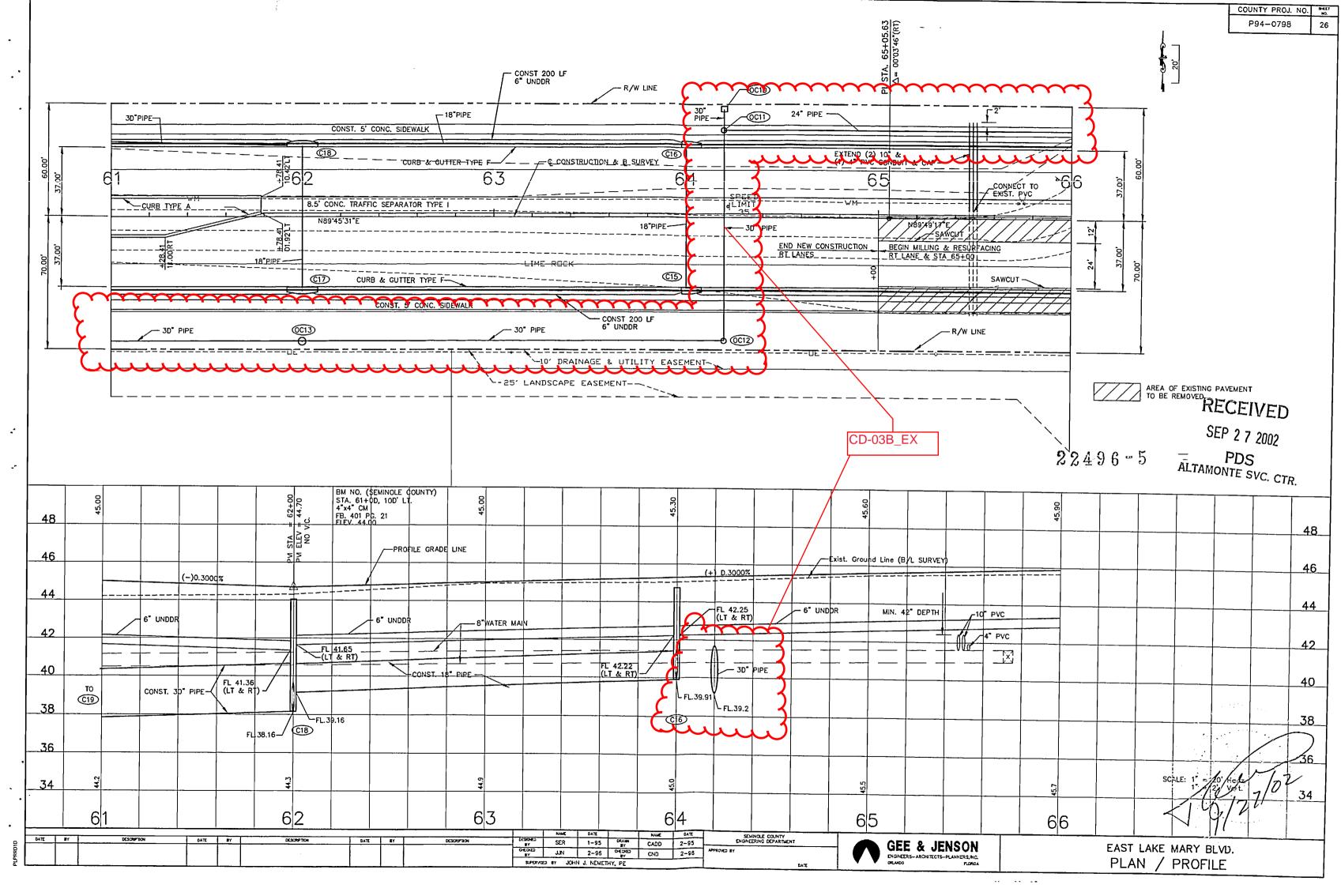
ENTRNC LOSS: 1.500 # OF CULVERTS: 1.000

POSITION A : NOT USED

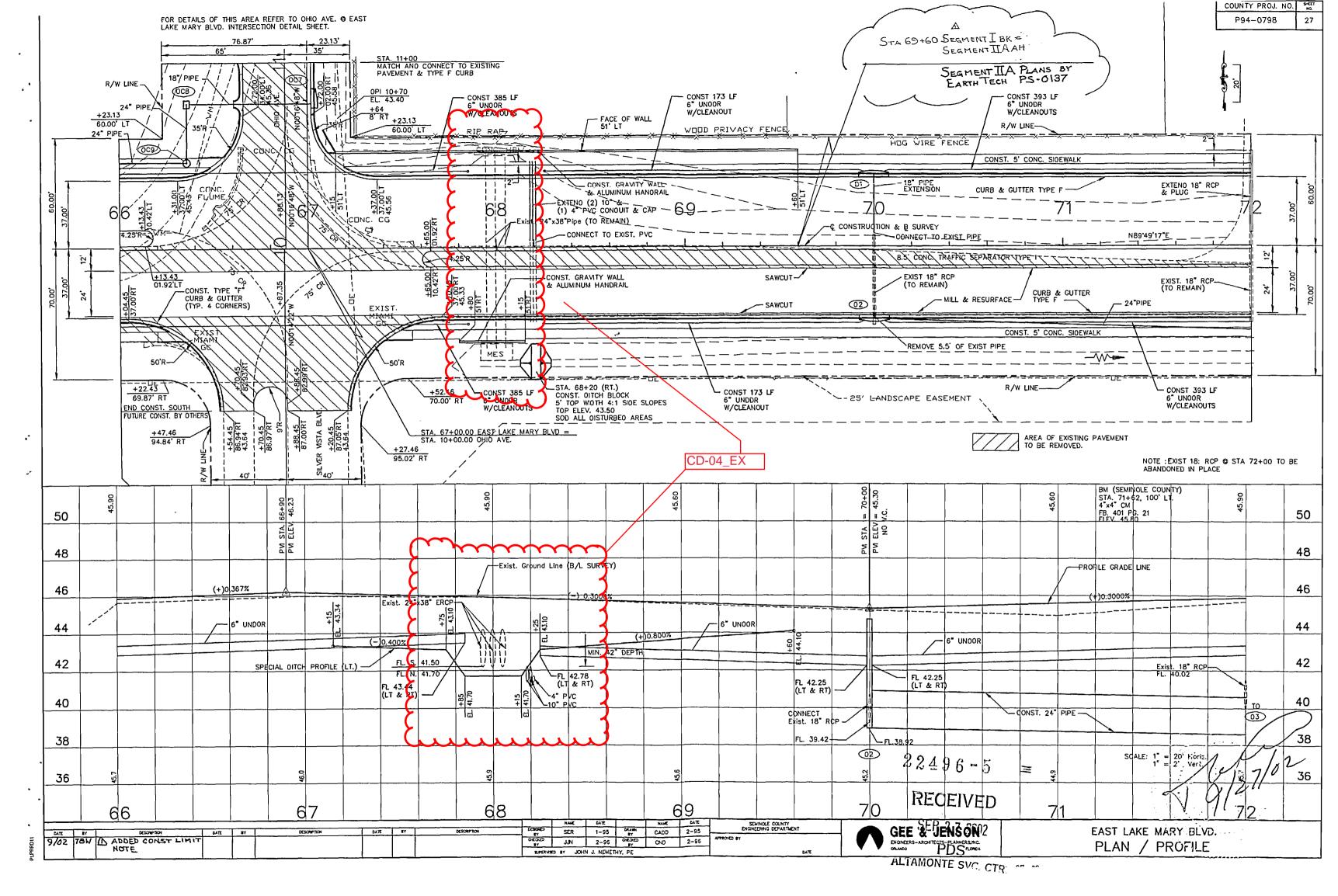
POSITION B : NOT USED

NOTE: OFFSITE COLLECTOR FROM OHIO ST





CROSS DRAIN CD-04_EX



CROSS DRAIN CD-05_EX,
CROSS DRAIN CD-06_EX
AND
CROSS DRAIN CD-07_EX

DRAINAGE CALCULATIONS AND PERMITTING NARRATIVE FOR

EAST LAKE MARY BLVD.

SEGMENT IIA

Sta. 69+60.00 to Sta. 96+59.70

Prepared For:

Seminole County
Public Works Department
Engineering Division

Prepared By:

Earth Tech Consulting, Inc. 30 South Keller Road, Suite 500 Orlando, Florida 32810

January 2002
Revised: April 4, 2002

A State Or A 47612

3. PROPOSED CONDITIONS

The proposed East Lake Mary Boulevard Segment 2A includes the reconstruction of East Lake Mary Boulevard from 280 feet east of Ohio Avenue to 1,000 feet east of the proposed intersection of East Lake Mary Boulevard and Airport Entrance Road. It also includes the reconstruction of Airport Entrance Road from the proposed East Lake Mary Boulevard to Marquette Avenue. A new Frontage Road will be provided to access the Marquette borrow pit. None of the proposed roadways lie in the 100-year flood zone according to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map, included in Appendix D-1.

The proposed East Lake Mary Boulevard and Airport Entrance Road will consist of a four-lane divided urban section with curb and gutter, a raised median, a 5-foot sidewalk on the left and an 8-foot sidewalk on the right side of the proposed roadways.

The proposed Frontage Road will consist of a two-lane rural section with onsite and offsite ditches along the proposed roadway with curb and gutter at the intersection of East Lake Mary Boulevard and the Frontage Road.

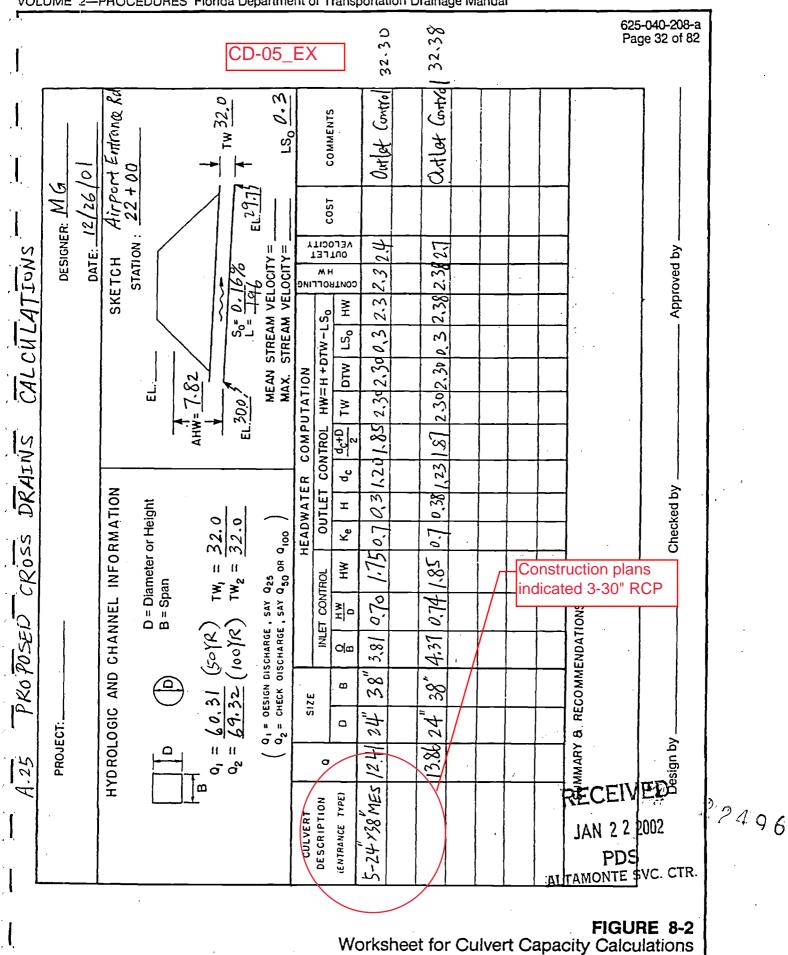
The drainage facilities for this project will include two stormwater management ponds, storm sewer systems, cross drains, and open ditches.

Runoff from East Lake Mary Boulevard and Airport Entrance Road will be collected by curb inlets and be conveyed by storm sewer to the proposed stormwater management pond 1. A portion of runoff from Frontage Road will drain into curb inlets or onsite open ditches then be conveyed by storm sewer to the proposed wet Pond 1. Runoff from a portion of Frontage Road covering an area of 0.133 acres will drain into Pond 1 directly. Runoff from the proposed East Lake Mary Boulevard between the airport entrance road and the eastern edge of segment IIA will drain into curb inlets then be conveyed by storm sewer to the proposed wet Pond 2.

Offsite runoff will be separated from the runoff of the proposed roadways. Offsite ditches will collect and convey runoff from an area of 22.0 acres to station 22+00 of Airport Entrance Road where three (3) proposed 30 inch in cross drains will convey runoff further southeasterly to a wetland area. Additionally, a triple 30-inch cross drain is proposed at Sta. 93+00 to continue the existing drainage patterns towards Lake Jessup. There is an existing ditch on the west side of Brisson Avenue that is maintained in the proposed condition. A double 36-inch cross drain is proposed at Sta. 96+20 to maintain the existing drainage patterns.

The proposed stormwater management Pond 1 will be located in an area, consisting of an existing wet pond and a grassed area immediately east of the pond, encompassed by the proposed East Lake Mary Boulevard, Airport Entrance Road, and Frontage Road. The proposed Pond 1 will discharge southeasterly into a low area, and eventually discharge into Lake Jessup. The proposed stormwater management Pond 2 will be located approximately 300 feet south of the eastern end of the proposed East Lake Mary Boulevard. The proposed Pond 2 will discharge southeasterly into Lake Jessup.

-CD-07 EX



A TUEO INTERNATIONAL LTD. COMPANY	CALCULATION SHEET	PAGE OF
	proposed	PROJECT NO. 46547
CLIENT Seminole County	SUBJECT Cross Drain	Prepared By MG DATE 01 02/02
PROJECT East Lake Mary	Calculation	Reviewed By DATE
Bonlevard, Segment 2A		Approved By DATE

Drainage Area (A) = 21.953 AC

$$T_c = 20 \text{ min}$$

Intensity (F== 7.0 in/c(C=0.337×1.2=0.404)

Intensity (
$$I_{50} = 7.0 \text{ in/hr} (C_{50} = 0.337 \times 1.2 = 0.404)$$

 $I_{100} = 7.5 \text{ in/hr} (C_{50} = 0.337 \times 1.25 = 0.421)$

$$Q_{50} = C_{50}I_{50}A$$

= 0.404 × 7.0 × 21.953 = 62.08 cfs

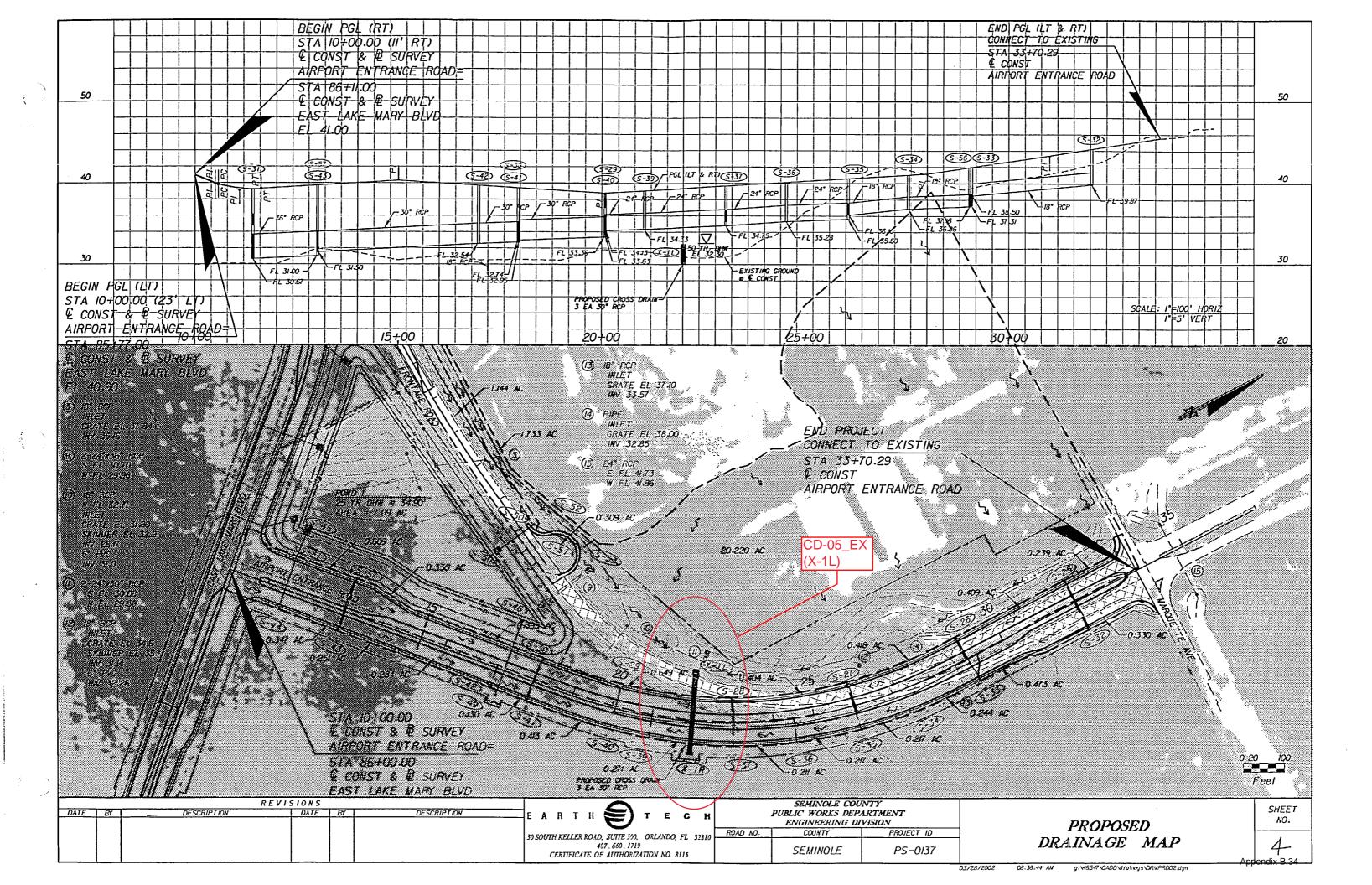
$$Q_{100} = C_{100} I_{100} A$$

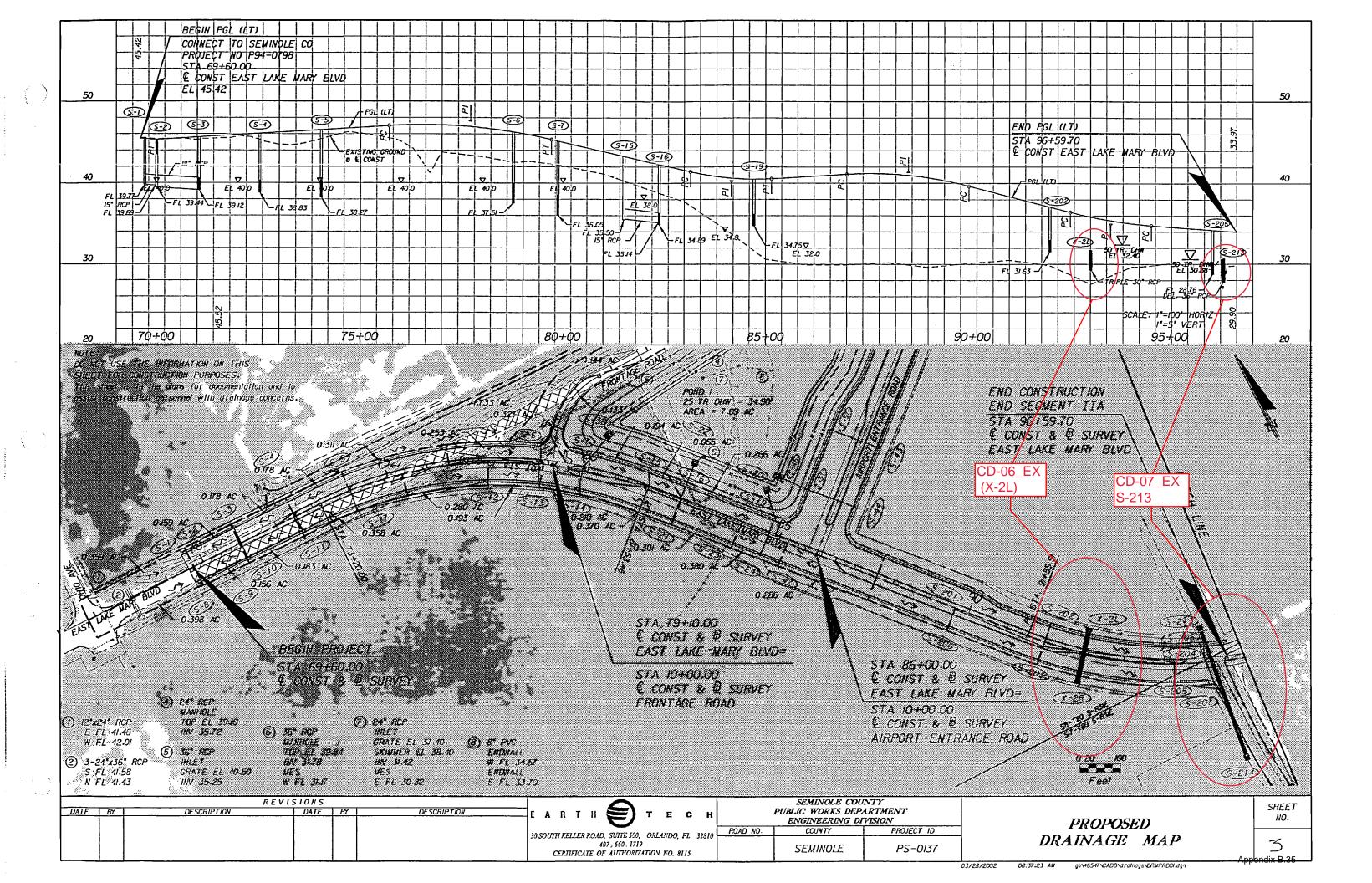
= 0. $421 \times 7.5 \times 21.953 = 69.32$ cfs

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CLIENT Seminole County 3 = Calculations for PROJECTEST Die Mary Cross Drain at 617d. Coopert ZA Station 93 +00

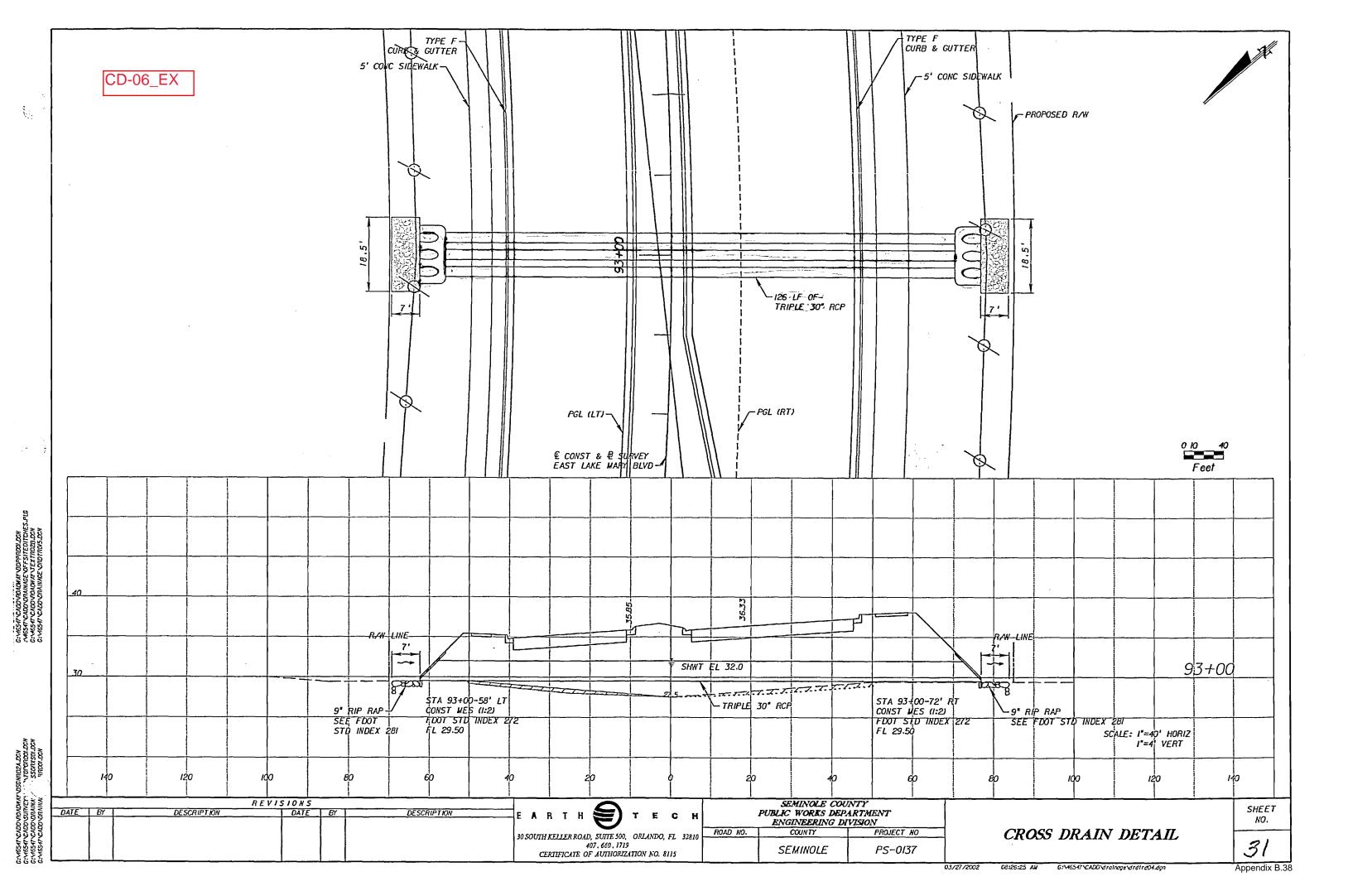
MG

Drainage Area to the proposed cross drain (A) = 34.5 Ac

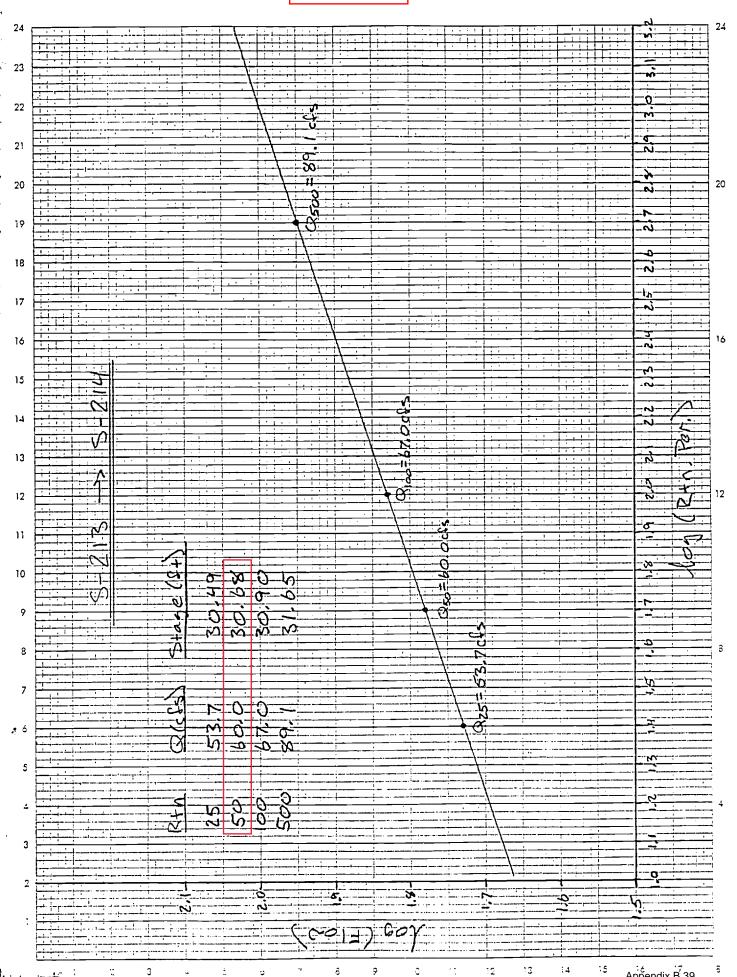
Travel Time = 37 min

Trequency C I (in/hr) Discharge (Q. cfs)

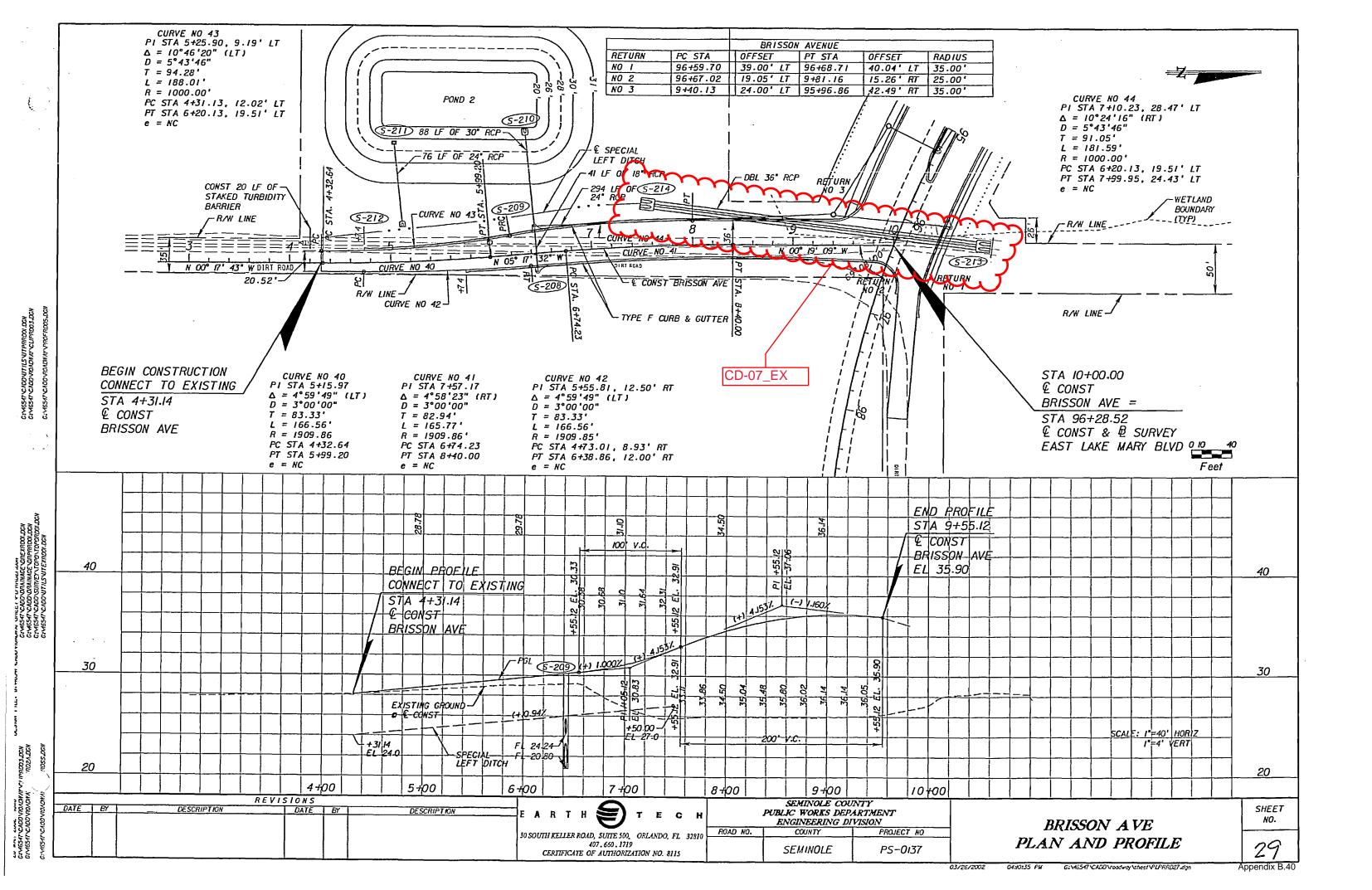
50-YEAR 0.24 5.4 46.6 100-YEAR 0.25 5.8 50.0



CD-07_EX



Appendix B.39



	STRUCTURE	TRUCTURE STATION	DESIGN FLOOD		BASE FLOOD		OVERTOPPING			GREATEST				
	NO.	STATION	2% PROB.	50 YR.FREQ.	IX PROB.	100 YR.FREQ.	FLOOD DISCHARGE STAGE PROB. FREQ. YR.		FLOOD FLOOD					
			DISCHARGE	STAGE	DISCHARGE	STAGE			DISCHARGE	STAGE	PROB.	FREQ. YR.		
CD-05_EX	X-1L	22+00.00	60.31	32.30	69.32	32.38					88.20	32.60	0.2	500
CD-06_EX	X-2L	93+00.00	46.60	32.40	50.00	32.50					53.40	32.70	0.2	500
CD-07_EX	S-213	96+20.00	60.00	30.68	67.00	30.90					89.10	31.65	0.2	500
							·····		<u> </u>					
								····			-	·-··		
ļ			· · · · · · · · · · · · · · · · · · ·											

NOTE: THE HYDRAULIC DATA IS SHOWN FOR INFORMATIONAL PURPOSES ONLY, TO INDICATE THE FLOOD DISCHARGES AND WATER SURFACE ELEVATIONS WHICH MAY BE ANTICIPATED IN ANY GIVEN YEAR. THIS DATA WAS GENERATED USING HIGHLY VARIABLE FACTORS DETERMINED BY A STUDY OF THE WATERSHED. MANY JUDGEMENTS AND ASSUMPTIONS ARE REQUIRED TO ESTABLISH THESE FACTORS. THE RESULTANT HYDRAULIC DATA IS SENSITIVE TO CHANGES, PARTICULARLY OF ANTECEDENT CONDITIONS, URBANIZATION, CHANNELIZATION, AND LAND USE. USERS OF THIS DATA ARE CAUTIONED AGAINST THE ASSUMPTION OF PRECISION WHICH CAN NOT BE ATTAINED. DISCHARGES ARE IN CUBIC FEET PER SECOND AND STAGES ARE IN FEET, NGVD, 1929.

DEFINITIONS:

DESIGN FLOOD: THE FLOOD SELECTED BY F.D.O.T. TO BE

UTILIZED TO ASSURE A STANDARD LEVEL

OF HYDRAULIC PERFORMANCE.

BASE FLOOD:

THE FLOOD HAVING A 1% CHANCE OF BEING

EXCEEDED IN ANY YEAR. (100 YR. FREQUENCY)

OVERTOPPING FLOOD: THE FLOOD WHERE FLOW OCCURS (A) OVER THE

HIGHWAY (B) OVER A WATERSHED DIVIDE OR (C) THRU EMERGENCY RELIEF STRUCTURES.

GREATEST FLOOD:

THE MOST SEVERE FLOOD WHICH CAN BE

PREDICTED WHERE OVERTOPPING IS NOT PRACTICABLE,

NORMALLY ONE WITH A 0.2% CHANCE OF BEING EXCEEDED IN ANY YEAR. (500 YR. FREQUENCY)

			REVISIONS					SEMINOLE COL			SHEET
F	DATE BY	DESCRIPTION	DATE	BY	DESCRIPTION	EARTH (E) TECH		PUBLIC WORKS DEP ENGINEERING DI			NO.
	1	ļ				30 SOUTH KELLER ROAD, SUITE 500, ORLANDO, FL 32810	ROAD NO.	COUNTY	PROJECT NO		
						407. 660. 1719 CERTIFICATE OF AUTHORIZATION NO. 8115		SEMINOLE	PS-0137	FLOOD DATA	5 Arnendix B 41

CROSS DRAIN CD-08_EX

DRAINAGE CALCULATIONS AND PERMITTING NARRATIVE

FOR

EAST LAKE MARY BLVD. SEGMENT IIB

Prepared For:
Seminole County
Public Works Department
Engineering Division



Prepared By:
Earth Tech Consulting, Inc.
30 South Keller Road, Suit 500
Orlando, Florida 32810



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August 23, 2002

22496-4

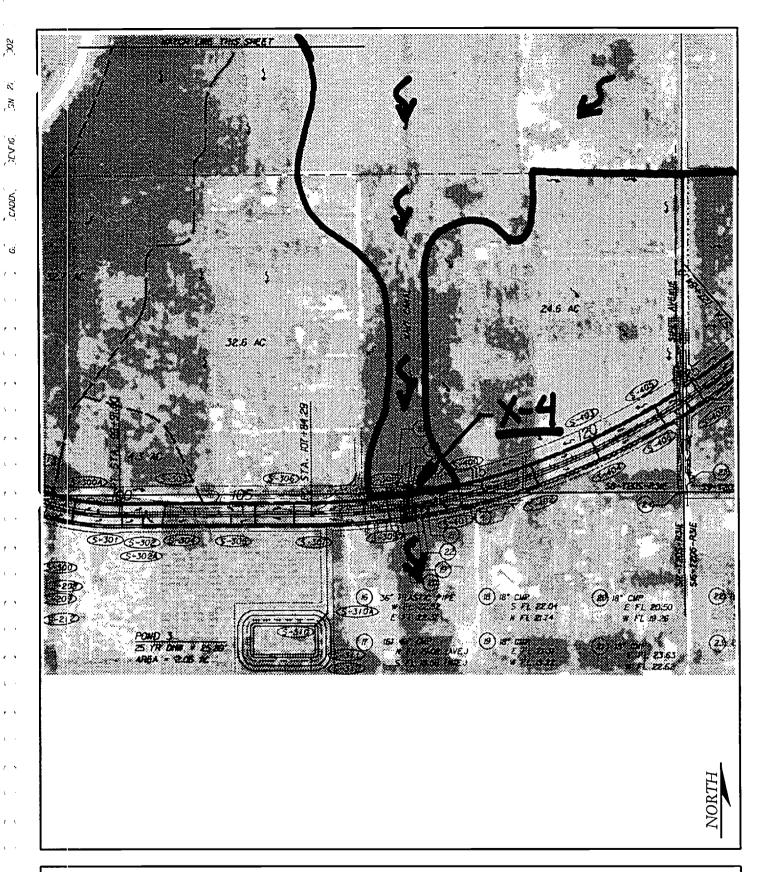
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X4

Seminole County East Lake Mary Blvd.

E A R T H



TECH

July 30, 2002

X-0	50 45		:=
		PROGRAM INPUT DATA	

DESCRIPTION	VALUE
Culvert Span (ft). Culvert Rise (ft). FHWA Chart Number. FHWA Scale Number (Type of Culvert Entrance). Manning's Roughness Coefficient (n-value). Entrance Loss Coefficient of Culvert Opening. Culvert Length (ft). Invert Elevation at Downstream end of Culvert (ft). Invert Elevation at Upstream end of Culvert (ft). Culvert Slope (ft/ft).	10.0
Starting Flow Rate (cfs)	307.0 0.0 307.0
Starting Tailwater Depth (ft)	2.3 0.0 2.3

COMPUTATION RESULTS

Flow Rate (cfs)	Depth	Headwater Inlet Control	(ft) Outlet Control	Normal Depth (ft)	Critical Depth (ft)	-	Outlet Velocity (fps)
307.0	2.3	5.26	5.34 24.34	6.0	3.08	3.08	9.96

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July 30, 2002

1/ // //		cary so,	2002			
X-4 100 y	<u>^</u>	========				
=======================================		ROGRAM INP		-==		
DESCRIPTION	F	NOGINALI INF	JI DAIA			VALUE
Culvert Span (ft)						10.0
Culvert Rise (ft)						6.0
FHWA Chart Number						8
FHWA Scale Number (Typ	e of Culve	rt Entranc	e)			3
Manning's Roughness Co	efficient	(n-value).				0.012
Entrance Loss Coeffici						0.5
Culvert Length (ft)						130.0
Invert Elevation at Do						19.0
Invert Elevation at Up						19.01
Culvert Slope (ft/ft).		• • • • • • • • • •	• • • • • • • •	• • • • • • • •		0.0001
Starting Flow Rate (cf	s)		.			340.0
Incremental Flow Rate	(cfs)					0.0
Ending Flow Rate (cfs)						340.0
	. 1 . (6)					2.5
Starting Tailwater Dep						2.5 0.0
Incremental Tailwater	Depth (It)	• • • • • • • • • • • •				2.5
Ending Tailwater Depth	(10)	• • • • • • • • • •				2.5
=======================================	========		========	=========	========	=======
	CC	MPUTATION	RESULTS			
Flow Tailwater	Headwater	(ft)	Normal	Critical	Depth at	Outlet
Rate Depth	Inlet	Outlet	Depth	Depth	Outlet	Velocity
(cfs) (ft)	Control	Control	(ft)	(ft)	(ft)	(fps)
340.0 2.5	5.64	5.71	6.0	3.3	3.3	10.3

July 30, 2002

500 yr PROGRAM INPUT DATA

DESCRIPTION	VALUE
Culvert Span (ft). Culvert Rise (ft). FHWA Chart Number. FHWA Scale Number (Type of Culvert Entrance) Manning's Roughness Coefficient (n-value). Entrance Loss Coefficient of Culvert Opening. Culvert Length (ft). Invert Elevation at Downstream end of Culvert (ft). Invert Elevation at Upstream end of Culvert (ft). Culvert Slope (ft/ft).	10.0
Starting Flow Rate (cfs). Incremental Flow Rate (cfs). Ending Flow Rate (cfs). Starting Tailwater Depth (ft). Incremental Tailwater Depth (ft). Ending Tailwater Depth (ft).	407.0 0.0 407.0 3.5 0.0 3.5
	=========

COMPUTATION RESULTS

Flow	Tailwater	Headwater	(ft)	Normal	Critical	-	Outlet
Rate	Depth	Inlet	Outlet	Depth	Depth		Velocity
(cfs)	(ft)	Control	Control	(ft)	(ft)		(fps)
407.0	3.5	6.37	6.43 25.43	6.0	3.72	3.72	10.94

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CLEVE Ceminolic Country Do sulations for Proposed Proposed Proposed Proposed

at Sta. (Navy Canal)

46547 MS

The properties cross draw well be located at Kentucky Ave. at Navy Canal.

The following Ania nos obtained i-tran wice Town Early Flood Plain Management Study, performed in 1994

Frequency feak Elevation (ft) Discharge (cfs)

25-YEAR

21.1

800

100-1EAR

21.5

1021

500-YEAR

22.5

1475

The Park Eleveton and discharge for En-JEAR-Palver Were interiored between It - EAR and 100 - FERR dota

50- FEAR =1.3 A 920 As

Calculations from

CROSS DRAIN CD-09_EX

DRAINAGE CALCULATIONS AND PERMITTING NARRATIVE

FOR

EAST LAKE MARY BLVD. SEGMENT IIB

Prepared For:
Seminole County
Public Works Department
Engineering Division



Prepared By:
Earth Tech Consulting, Inc.
30 South Keller Road, Suit 500
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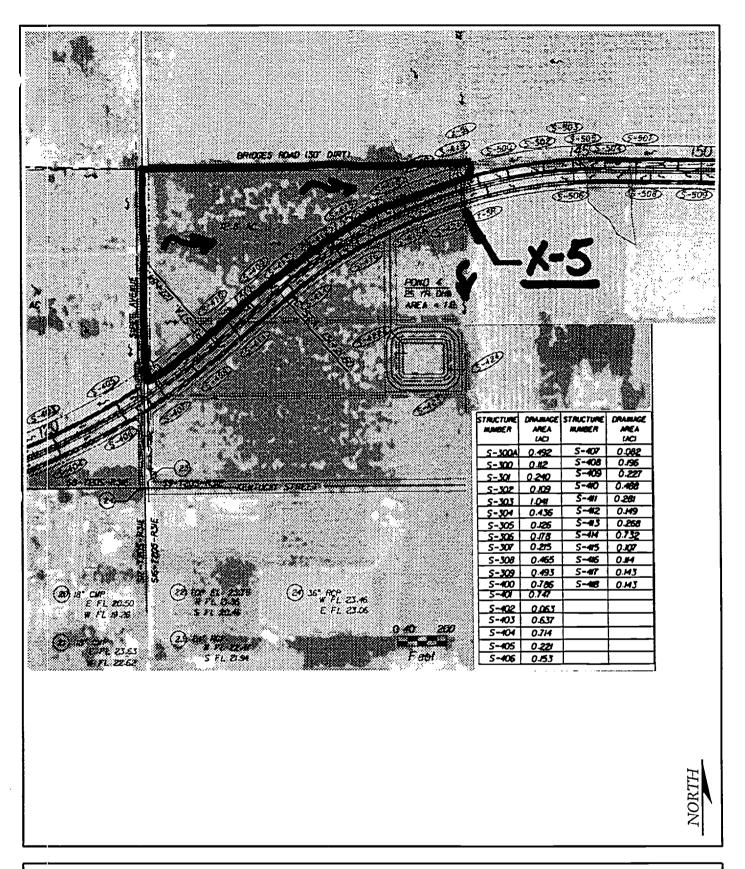


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Route Olderar 8-29-02



X-5

Seminole County East Lake Mary Blvd.

E A R T H



TECH

July 30, 2002

PROGRAM INPUT DATA

DESCRIPTION	VALUE
Culvert Span (ft)	
Culvert Rise (ft)	3.5
FHWA Chart Number	8
FHWA Scale Number (Type of Culvert Entrance)	3
Manning's Roughness Coefficient (n-value)	0.012
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	133.0
Invert Elevation at Downstream end of Culvert (ft)	21.5
Invert Elevation at Upstream end of Culvert (ft)	21.6
Culvert Slope (ft/ft)	0.0008
Starting Flow Rate (cfs)	148.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	148.0
Starting Tailwater Depth (ft)	2.9
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	2.9
	==========

COMPUTATION RESULTS

Flow Tai	lwater	Headwater	(ft)	Normal	Critical	-	Outlet
Rate	Depth	Inlet	Outlet	Depth	Depth		Velocity
(cfs)	(ft)	Control	Control	(ft)	(ft)		(fps)
148.0	2.9	3.24	3.51 2 5.0 1	2.91	1.9 ======	2.9	5.1

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July 30, 2002

X-5	10042				
=========	========	=========		-	
		PROGRAM	INPUT DATA	4	

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft) Culvert Rise (ft) FHWA Chart Number FHWA Scale Number (Type of Culvert Entrance) Manning's Roughness Coefficient (n-value) Entrance Loss Coefficient of Culvert Opening Culvert Length (ft) Invert Elevation at Downstream end of Culvert (ft) Invert Elevation at Upstream end of Culvert (ft) Culvert Slope (ft/ft)	10.0 3.5 8 3 0.012 0.5 133.0 21.5 21.6 0.0008
Starting Flow Rate (cfs)	164.0 0.0 164.0
Starting Tailwater Depth (ft)	3.0 0.0 3.0

COMPUTATION RESULTS

Flow Ta	ilwater	Headwater	(ft)	Normal	Critical	Depth at	Outlet
Rate	Depth	Inlet	Outlet	Depth	Depth	Outlet	Velocity
(cfs)	(ft)	Control	Control	(ft)	(ft)	(ft)	(fps)
164.0	3.0	3.47	3.71 2 5.2 1	3.12	2.03	3.0	5.47

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July 30, 2002

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								DDOOD			D 3 (D 2				
								PRUGRA	AM .	TNPOT.	DATE	4			

PROGRAM INPUT DATA	
DESCRIPTION	VALUE
Culvert Span (ft)	
Culvert Rise (ft)	
FHWA Chart Number	8
FHWA Scale Number (Type of Culvert Entrance)	3
Manning's Roughness Coefficient (n-value)	0.012
Entrance Loss Coefficient of Culvert Opening	0.5
Culvert Length (ft)	133.0
Invert Elevation at Downstream end of Culvert (ft)	21.5
Invert Elevation at Upstream end of Culvert (ft)	21.6
Culvert Slope (ft/ft)	0.0008
Starting Flow Rate (cfs)	196.0
Incremental Flow Rate (cfs)	0.0
Ending Flow Rate (cfs)	196.0
Starting Tailwater Depth (ft)	3.5
Incremental Tailwater Depth (ft)	0.0
Ending Tailwater Depth (ft)	3.5
	========

COMPUTATION RESULTS

Flow Ta Rate (cfs)	Depth		(ft) Outlet Control	Depth	Depth	Depth at Outlet (ft)	Velocity
196.0	3.5	3.91	4.32 25. 82	3.5	2.29	3.5	5.6

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Phone: (281)440-3787, Fax: (281)440-4742, Email:software@dodson-hydro.com
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CLETT Cem Nob Trick PROJECTERS LOS MOI FIND TOP INTO STORE TO !!

Calculations in Jan 19:1-19 (Kentucky Ditch)

405-57

Calculations from

The proposed cross Drain will be Lorand at 1400 ft downstream of Marquete Road at Kentucky Dian.

The following data was a otained from Lake Jesup Basin Drainage Study, performed in 1994.

rea yearsy	Pank Elevation of the	DISMORTE
25-YEAR	24. ŝ	82
(2) - (1) 20	24. 5	104
Lore PR	25.2	148

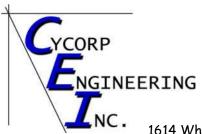
The Book Elevation and discharge for 50-1848 frequency retween = 5 / EAR and 12 - 15/16 down.

50- EAR

27.4 ft

94 cfs

Per Seminole Co. review and CDM model: Q₅₀ → 148 cfs (Per Ed Torres June 17,2002) **ANOTHER PERMIT INFORMATION**



1614 White Dove Dr. Winter Springs, FL 327708

Phone: 407-405-7819

Stormwater Calculations

SYLVESTRI LAKES

City of Sanford

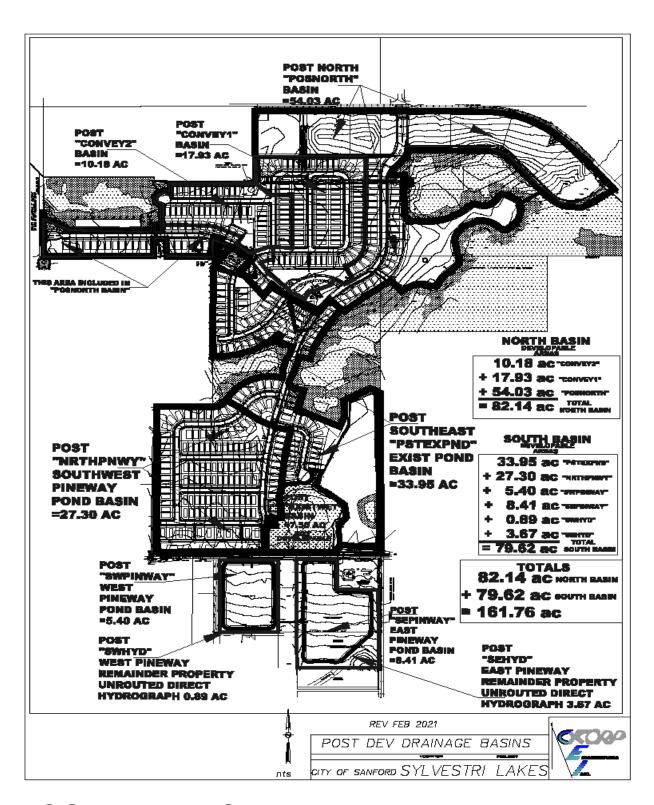


Prepared for:

Safari Investments, LLC

February 2021

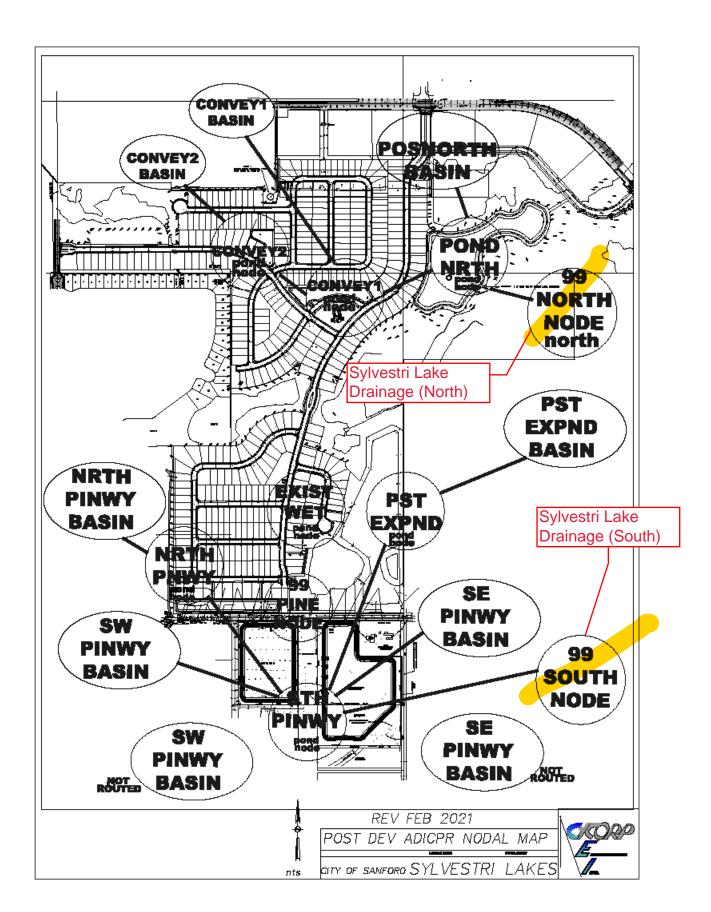


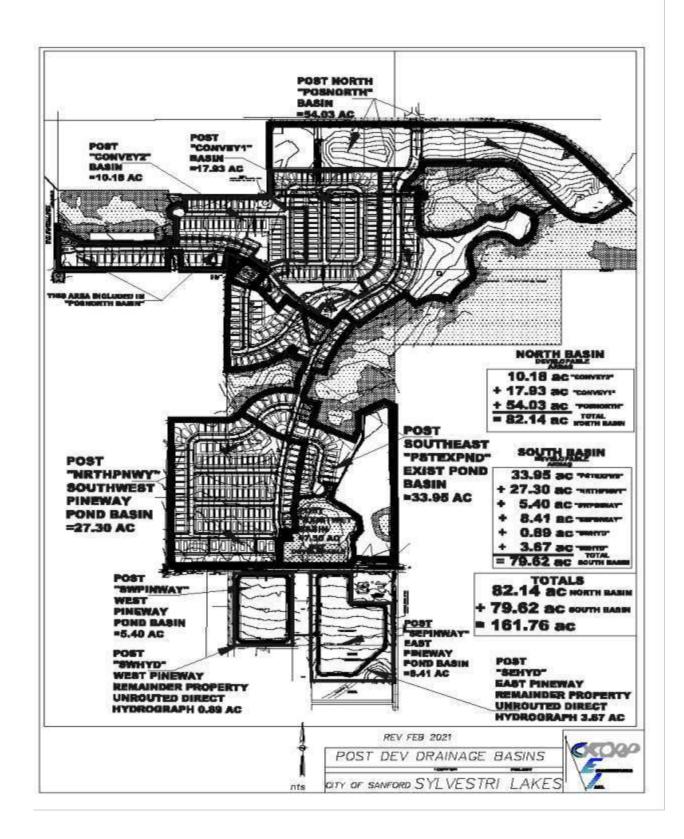


POST DEVELOPED MAP – also stand alone pdf

POST-DEVELOPMENT AdICPR

10 YEAR 25 YEAR 100 YEAR





NORTH

Sylvestri Lake South Drainage

Advanced Interconnected Channel & Pond Routing (ICPR Ver 2.20) [1]

Copyright 1995, Streamline Technologies, Inc.

SYLVESTRI NORTH BASIN POST

FEB 20

(Time units - hours)

Node Name	Group Name	Max Time Conditions	Max Stage (ft)	Warning Stage (ft)	Max Delta Stage (ft)	Max Surface Area (sf)	Max Time Inflow	Max Inflow (cfs)	Max Time Outflow	Max Outflow (cfs)
99PINE	BASE	12.00	23.50	30.00	0.0000	0.00	13.75	2.89	0.00	0.00
99S0UTH	BASE	12.00	17.00	30.00	0.0001	0.00	16.92	18.79	0.00	0.00
EXISTWET	BASE	13.75	23.95	28.00	0.0004	142745.50	12.00	35.90	13.75	2.89
NRTHPNWY	BASE	12.44	22.85	28.00	0.0009	55721.95	12.08	102.54	12.31	62.85
PSTEXPND	BASE	12.74	24.78	29.00	0.0003	382548.48	12.08	127.52	12.74	40.59
STHPINWY	BASE	16.92	22.73	28.00	0.0003	534502.65	12.08	144.21	16.92	18.79

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SYLVESTRI NORTH BASIN POST FEB 20

(Time units - hours)

Node Name	Group Name	Max Time Conditions	Max Stage (ft)	Warning Stage (ft)	Max Delta Stage (ft)	Max Surface Area (sf)	Max Time Inflow	Max Inflow (cfs)	Max Time Outflow	Max Outflow (cfs)
99PINE	BASE	12.00	23.50	30.00	0.0000	0.00	0.00	0.00	0.00	0.00
99S0UTH	BASE	12.00	17.00	30.00	0.0001	0.00	24.00	3.62	0.00	0.00
EXISTWET	BASE	24.00	23.59	28.00	0.0003	106869.83	12.00	14.97	0.00	0.00
NRTHPNWY	BASE	24.00	21.86	28.00	0.0003	48983.51	12.08	37.24	12.22	27.47
PSTEXPND	BASE	13.03	24.30	29.00	0.0001	375871.41	12.08	46.31	13.03	9.96
STHPINWY	BASE	24.00	21.86	28.00	0.0001	519357.51	12.08	61.29	24.00	3.62

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SYLVESTRI NORTH BASIN POST

FEB 20

(Time units - hours)

	Node	Group	Max Time	Max Stage	Warning	Max Delta	Max Surface	Max Time	Max Inflow	Max Time	Max Outflow
	Name	Name	Conditions	(ft)	Stage (ft)	Stage (ft)	Area (sf)	Inflow	(cfs)	Outflow	(cfs)
	99PINE	BASE	12.00	23.50	30.00	0.0000	0.00	15.59	1.56	0.00	0.00
	99SOUTH	BASE	12.00	17.00	30.00	0.0001	0.00	17.71	14.24	0.00	0.00
ľ	EXISTWET	BASE	15.59	23.90	28.00	0.0004	137646.75	12.00	30.77	15.59	1.56
	NRTHPNWY	BASE	17.63	22.52	28.00	0.0008	53432.32	12.08	86.15	12.29	55.11
	PSTEXPND	BASE	12.78	24.66	29.00	0.0002	380943.29	12.08	107.14	12.78	32.03
	STHPINWY	BASE	17.71	22.51	28.00	0.0002	530674.41	12.08	123.94	17.71	14.24

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SYLVESTRI NORTH BASIN POST

FEB 20

(Time units - hours)

(· - · · · · · · · · ·		/								
Node	Group	Max Time	Max Stage	Warning		Max Surface	Max Time	Max Inflow	Max Time	Max Outflow
Name	Name	Conditions	(ft)	Stage (ft)	Stage (ft)	Area (sf)	Inflow	(cfs)	Outflow	(cfs)
99PINE	BASE	12.00	23.50	30.00	0.0000	0.00	12.75	8.79	0.00	0.00
99SOUTH	BASE	12.00	17.00	30.00	0.0001	0.00	16.13	31.40	0.00	0.00
EXISTWET	BASE	12.75	24.12	28.00	0.0004	159399.04	12.00	48.17	12.75	8.79
NRTHPNWY	BASE	12.47	23.83	28.00	0.0013	62331.38	12.08	142.19	12.35	79.32
PSTEXPND	BASE	12.80	25.08	29.00	0.0004	386792.54	12.08	176.82	12.49	50.98
STHPINWY	BASE	16.13	23.27	28.00	0.0004	543734.40	12.08	192.49	16.13	31.40

South

Sylvestri Estates Master Stormwater Management System Calculations Report

January 13, 2016

SYLVESTRI LAKE NORTH DRAINAGE SYSTEM

Submitted To:
The City of Sanford
and
St. Johns River Water Management District

Prepared For

Safari Investments, LLC

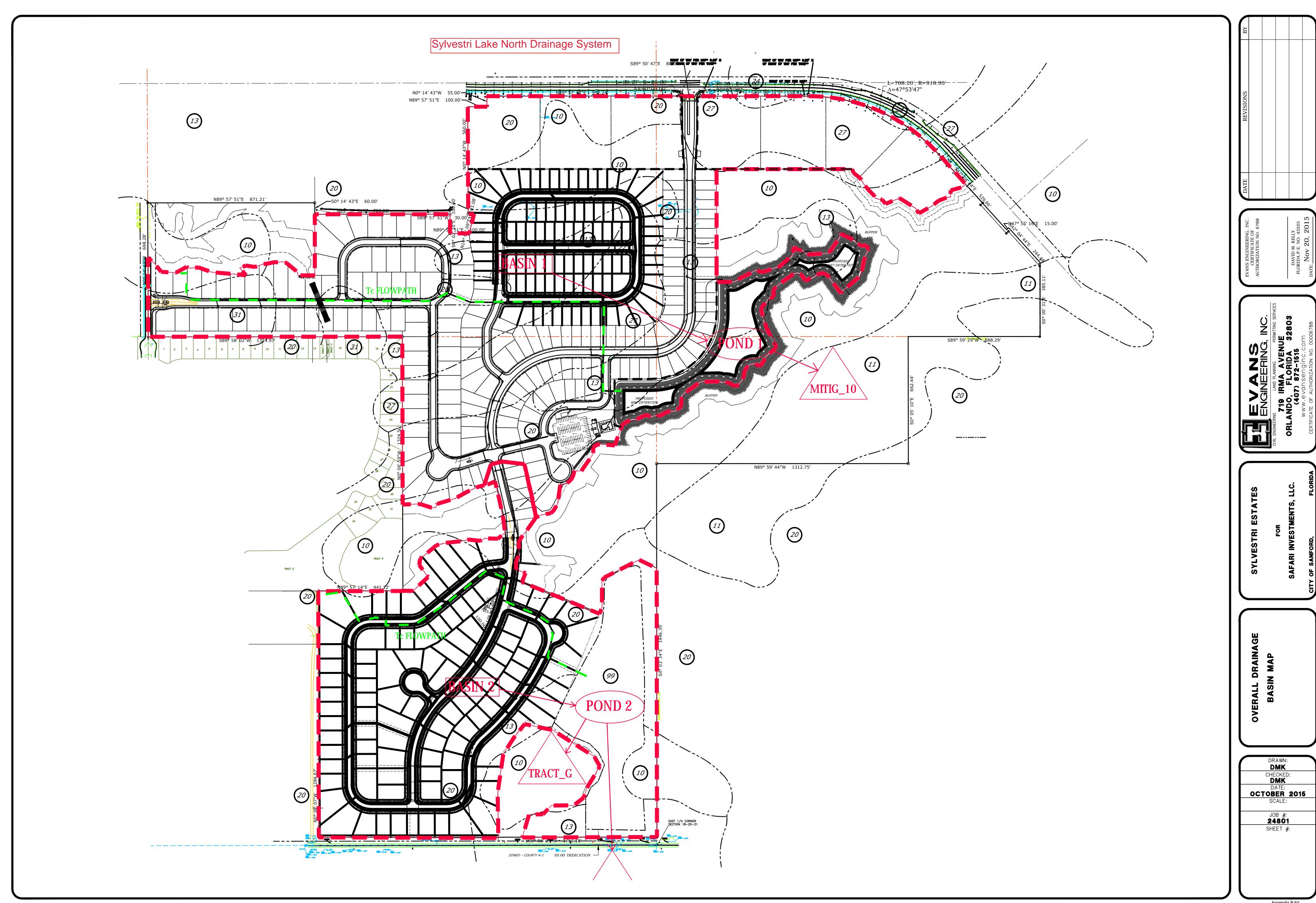
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- 4	CHILLICARC	W)	111071	1 1 1 ()	$\mathbf{U} / \alpha \alpha$

David L. Evans,	P.E.
Reg. # 4	6586
Date:	

1/13/2016



Routing Analysis

27	<u> </u>		Max Time	Max	Warning M					Max Time	Max
Name	Group	Simulation	Stage hrs	Stage ft	Stage ft	Stage ft	Area ft2	Inflow hrs	Inflow cfs	Outflow hrs	Outflow cfs
(Mitig_10)	Post	(Post 10 24)	0.00	31.00	31.00	0.0000	0	14.36	49.36	0.00	0.00
Pineway	Post	Post 10 24	0.00	22.00	22.00	0.0000	0	0.00	0.00	0.00	0.00
Pond 1	Post	Post 10 24	14.36	37.64	40.00	0.0047	253368	12.33	205.33	14.36	49.36
Pond 2	Post	Post 10 24	20.20	26.48	27.50	0.0017	406553	12.17	133.62	20.20	6.38
Tract G	Post	Post 10 24	0.00	24.00	24.00	0.0000	0	20.20	6.38	0.00	0.00
Mitig 10	Post	Post 100 24	0.00	31.00	31.00	0.0000	0	12.98	198.24	0.00	0.00
Pineway	Post	Post 100 24	0.00	22.00	22.00	0.0000	0	0.00	0.00	0.00	0.00
Pond 1	Post	Post 100 24	12.98	38.51	40.00	0.0050	267684	12.25	325.16	12.98	198.24
Pond 2	Post	Post 100 24	15.12	27.30	27.50	0.0021	417972	12.25	208.34	15.12	21.57
Tract G	Post	Post 100 24	0.00	24.00	24.00	0.0000	0	15.12	21.57	0.00	0.00
$Mitig_10$	Post	Post 25 24	0.00	31.00	31.00	0.0000	0	14.15	66.99	0.00	0.00
Pineway	Post	Post 25 24	0.00	22.00	22.00	0.0000	0	0.00	0.00	0.00	0.00
Pond 1	Post	Post 25 24	14.15	38.20	40.00	0.0050	262489	12.33	242.86	14.15	66.99
Pond 2	Post	Post 25 24	17.34	26.72	27.50	0.0019	409869	12.17	156.12	17.34	10.33
Tract G	Post	Post 25 24	0.00	24.00	24.00	0.0000	0	17.34	10.33	0.00	0.00
Mitig $\overline{10}$	Post	Post MA	0.00	31.00	31.00	0.0000	0	17.74	8.17	0.00	0.00
Pineway	Post	Post MA	0.00	22.00	22.00	0.0000	0	0.00	0.00	0.00	0.00
Pond 1	Post	Post MA	17.74	35.89	40.00	0.0026	225120	12.33	100.04	17.74	8.17
Pond 2	Post	Post MA	24.00	25.56	27.50	0.0009	393526	12.33	70.01	0.00	0.00
Tract G	Post	Post MA	0.00	24.00	24.00	0.0000	0	0.00	0.00	0.00	0.00

FLOW CONVEYED FROM CD-03A_EX AND CD-03B_EX TO WETLAND EAST OF SYLVESTRI LAKE

4-117-0317 AM

ENVIRONMENTAL ANALYSIS of THE SILVER LAKES INDUSTRIAL PARK, INC. SEMINOLE COUNTY, FLORIDA

MSSW PERMIT NO. 4-117-0137 MODIFICATION

ADDENDUM NO. 1

Submitted to:

ST. JOHNS RIVER WATER MANAGEMENT DISTRICT 618 East South Street Orlando, Florida 32801

Prepared by:

THE LAND PLANNING GROUP, INC. 1755 U.S. New Highway 441, West Mount Dora, Florida 32757

October, 1992

DONALD W. MONTOSH ASSOCIATES, INC ENGINEERS PLANNERS SURVEYORS 2200 PARK AVENUE NORTH, WINTER PARK, FLORIDA 32789 (407) 644-4068	BY <u>KW</u> DATE <u>B/9</u>
SILVER LAKES INDUSTRIAL PARK	NO
SUBJECT	SHEET G-2 OF
CASSELBERRY QUADRANGLE	MOD 10-92
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	DONALD	W. OCINTOSH PLANNER AVENUE NORTH, WINTER PARK, F	ASSOC	IATES,
	ENGINEERS 2200 PARK	PLANNER AVENUE NORTH, WINTER PARK, F	S Lorida 32789	SURVE (407) 644-4068
OJECT				

BY 6 DATE 8/91
CK DATE
NO
SHEET 6-3 OF 10/92

EXIST'S	D-03A_EX	CD-03B_EX		STREET
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HYDRAULIC NETWORK ANALYSIS AND DESIGN (C) Copyright 1983, Peter J. Singhofen, P.E.

G-12 MOD. 10/92

25- FLOWS

NODE	X	Υ	отот	GRND	TW
100	0.00	0.00	40.70	44.00	-999.00
1	0.00	0.00	42.70	43.00	-999.00
79	0.00	0.00	13.20	44.20	-999.00
2	0.00	0.00	42.70	42.50	-999.00
78	0.00	0.00	19.60	44.30	-999.00
77	0.00	0.00	19.60	43.00	-999.00
76	0.00	0.00	19.60	43.00	-999.00
3	0.00	0.00	3.50	43.70	-999.00
75	0.00	0.00	20.00	43.00	-999.00
4	0.00	0.00	61.40	43.00	-999.00
41	0.00	0.00	61.40	42.00	-999.00
5	0.00	0.00	82.50	40.00	-999.00
6	0.00	0.00	7.90	42.00	-999.00
. 7	0.00	0.00	13.20	42.00	-999.00
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77	0.00	0.00	16.80
76	0.00	0.00	16.80
3	0.00	0.00	3.20
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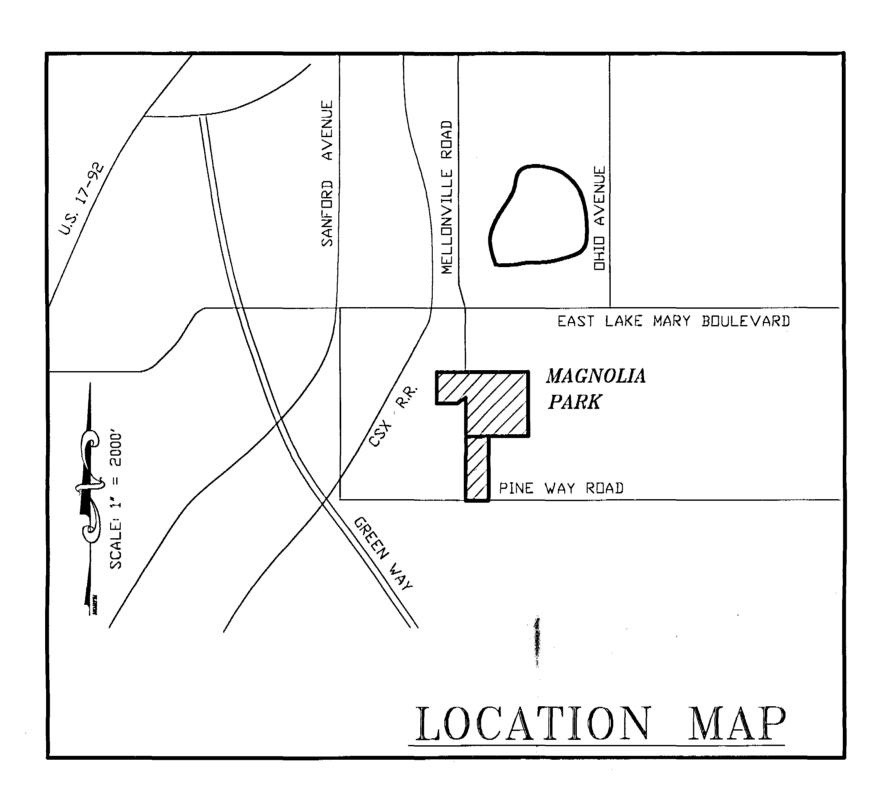
GENERAL CONSTRUCTION NOTES

- 1. ALL SITE WORK CONSTRUCTION SHALL COMPLY WITH APPLICABLE CITY OF SANFORD AND FDOT SPECIFICATIONS
- 2. THE CONTRACTOR SHALL NOTIFY THE OWNERS OF ALL UTILITIES TO LOCATE AND MARK THE LOCATION OF THEIR UTILITIES, SUCH NOTIFICATION INCLUDES CITY OF SANFORD FOR EXACT LOCATION AND INVERT ELEVATION OF SANITARY SEVER MAINS, GAS MAINS, WATER MAINS AND FORCE MAINS, VALVES, ETC. ADJACENT TO THE CONSTRUCTION SITE.
- 3. EXISTING TOPOGRAPHY WAS FURNISHED BY OTHERS AND IS BELIEVED TO BE ACCURATE HOWEVER THE CONTRACTOR SHALL VERIFY ALL PERTINENT FEATURES WHICH MAY AFFECT HIS BID PRIOR TO BIDDING THE PROJECT. DISCREPANCIES NOTED DURING CONSTRUCTION WILL NOT BE CONSIDERED CAUSE FOR EXTRA PAYMENT ON ANY OF THE PAY ITEMS IN THE
- 4. CONTRACTOR SHALL IMMEDIATELY NOTIFY DESIGN ENGINERER OF ANY DISCREPANCIES FOUND ON THE PLANS.
- 5. ANY PUBLIC LAND CORNER WITHIN THE LIMITS OF CONSTRUCTION IS TO BE PROTECTED. IF A CORNER MONUMENT IS IN DANGER OF BEING DESTROYED AND HAS NOT BEEN PROPERLY REFERENCED, THE CONTRACTOR SHOULD NOTIFY THE COUNTY 'S LOCATION SURVEYOR SUREYOR WITHOUT DELAY BY TELEPHONE.
- 6. MAINTENANCE OF TRAFFIC WILL BE IN ACCORDANCE WITH THE "MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES FOR STREETS AND HIGHWAYS" AND THE F.D.O.T. "ROADWAY AND YRAFFIC DESIGN STANDARDS' DATED JANUARY, 1992.
- 7. THERE SHALL BE ONE COMPACTION TEST PER 2500 S.F. (OR PORTION THEREOF) OF PAVEMENT, COMPACTION REQUIREMENTS FOR PIPE BEDS SHALL BE 95% OF MAXIMUM DRY DENSITY FOR UNPAVED AREAS AND 98% FOR PAVED AREAS.
- 8. UPON COMPLETION OF CONSTRUCTION, CITY OF SANFORD AND THE ENGINEER OF RECORD SHALL BE NOTIFIED IN WRITING FOR FINAL INSPECTION.
- 9. TEMPORARY DRAINAGE SHALL BE PROVIDED DURING CONSTRUCTION TO ELIMINATE ANY FLOODING OF PRIVATE PROPERTY.
- 10. UNSTABLE MATERIALS SHALL BE REMOVED FROM CONSTRUCTION AREAS AND BACK FILLED WITH SUITABLE MATERIALS. 11. CONSTRUCTION SHALL INCLUDE REPLACING WITH MATCHING MATERIALS, THE DRIVEWAYS, WALKS, CURBS AND LANDSCAPING THAT ARE DAMAGED OR REMOVED DUE TO CONSTRUCTION.
- THIS WORK SHALL BE COORDINATED WITH THE AFFECTED PROPERTY OWNERS. 12. ALL STORM SEWER LINES AND INLETS SHALL BE CLEANED OF DEBRIS AND ERODED MATERIALS AT LAST STAGES OF CONSTRUCTION.
- 13. ANY DRAINAGE PROBLEMS CREATED BY CONSTRUCTION, OR EXISTING BEFORE CONSTRUCTION AND NOT ALLEVIATED. SHOULD BE BROUGHT TO THE ATTENTION OF THE CITY, AND THE PROJECT ENGINEER.
- 14. THE CONTRACTOR SHALL TAKE PRECAUTIONS TO PROTECT EXISTING TREES SHOWN 'TO REMAIN' ON THE PLANS.
- 15. PRIOR TO FINAL CERTIFICATION, THE CONTRACTOR SHALL PROVIDE THE PROJECT ENGINEER FIVE (5) COPIES OF "AS-BUILT" PRINTS OF THE RECORD DRAWINGS, CLEARLY INDICATING ANY AND ALL CHANGES MADE, AND SIGNED AND SEALED BY A FLORIDA REGISTERED LAND SURVEYOR, AND ONE MYLAR REPRODUCTBLE COPY OF THE "AS-BUILT" DRAWINGS.

MASTER PLAN FOR

MAGNOLIA PARK, P.D.

A PLANNED RESIDENTIAL DEVELOPMENT IN THE OF SANFORD, FLORIDA



OWNER APPLICANT: MICHAEL D. MURRAY, AGENT MAGNOLIA PARK L.C. C/O GOLDEN FLORIDA MANAGEMENT 1399 WEST STATE ROAD 434 LONGWOOD, FLORIDA 32750 PHONE: (407) 331-4300

ENGINEER:

JOHN T. BRISKEY, P.E. BRISKEY AND ASSOCIATES, ENGINEERS, INC. P.O. BOX 7641 DAYTONA BEACH, FL 32116 PHONE: (904) 239-6999

SOILS:

MICHAEL D. SIMS, P.E. POINT FOUR ENGINEERING & TECHNOLOGICAL SERVICES 193 WEST NEW YORK AVENUE LAKE HELEN, FLORIDA 32744 PHONE: (407) 260-9449

ENVIRONMENTAL

ROBERT G. EPPERSON, JR., M.S. SHANNON SURVEYING, INC. 1035 SOUTH SEMORAN BOULEVARD SUITE 1013 WINTER PARK FL 32792 PHONE: (407) 678-1881

SURVEYOR:

JAMES R. SHANNON, JR. P.L.S. SHANNON SURVEYING, INC. 499 N. STATE ROAD 434-SUITE 2007, ALTIMONTE SPRINGS, FL 32714 PHONE: (407) 775-8372

INDEX OF DRAWINGS

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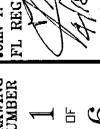


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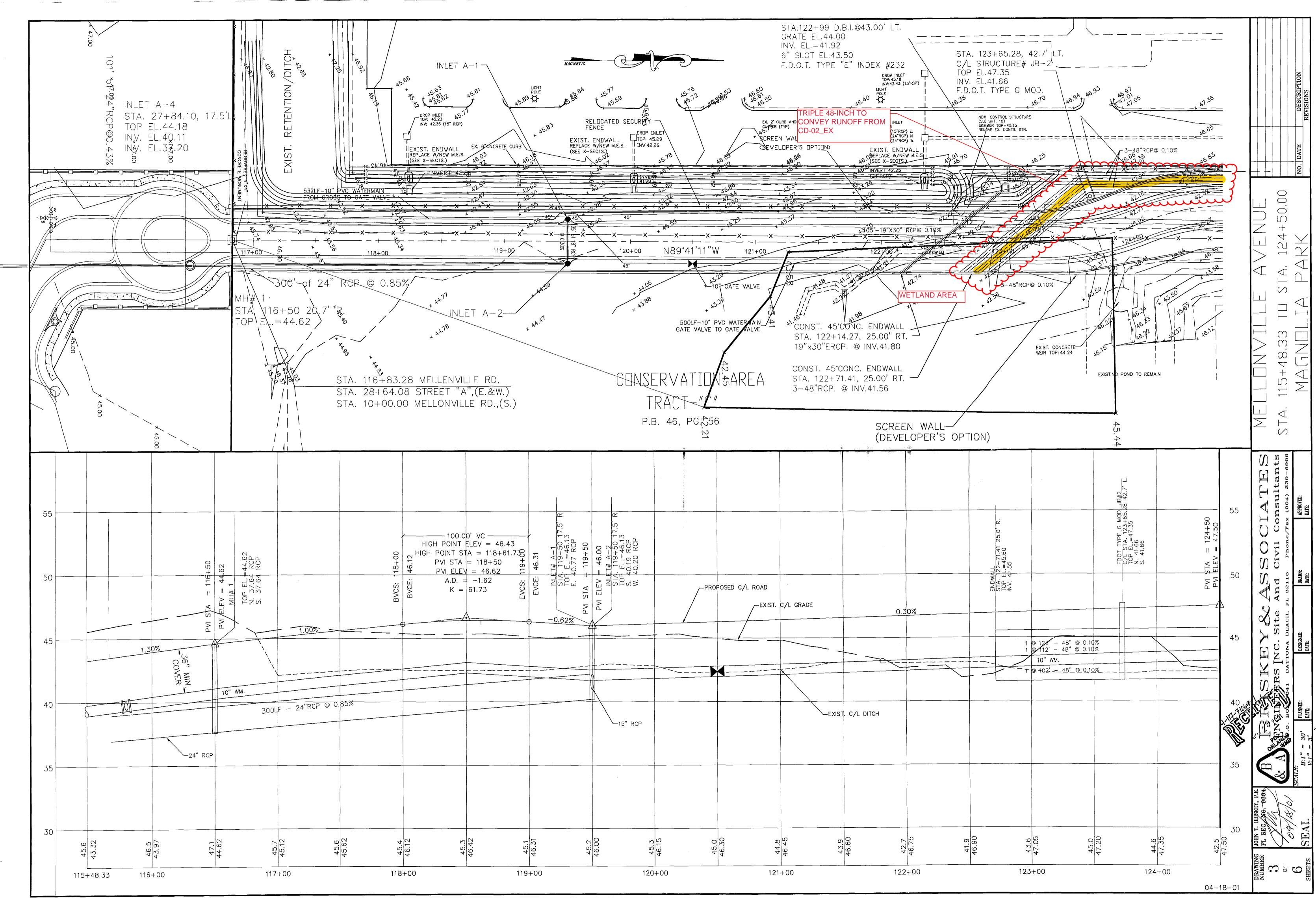
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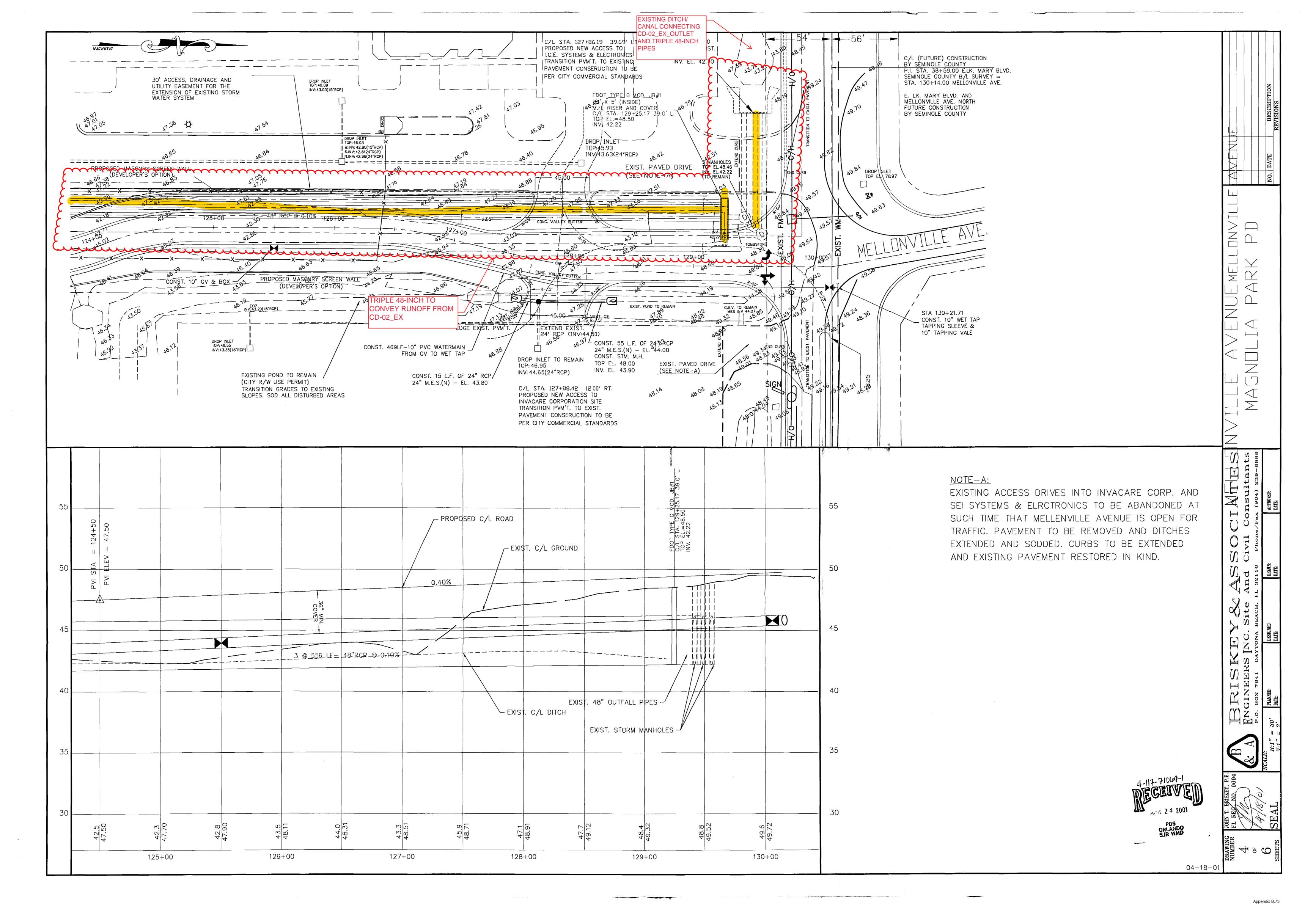
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04/18/01





Stormwater Computations and Environmental Resource Permit Application (Addendum 1)

MAGNOLIA CLUB AND ROSE HILL DRAINAGE SYSTEMS

SCANNED LIBITION

Magnolia Club

Sanford, Florida

Prepared for

D.R. Horton

Orlando, Florida

Prepared by

VHB/Vanasse Hangen Brustlin, Inc.

Orlando, Florida

EB# 3932

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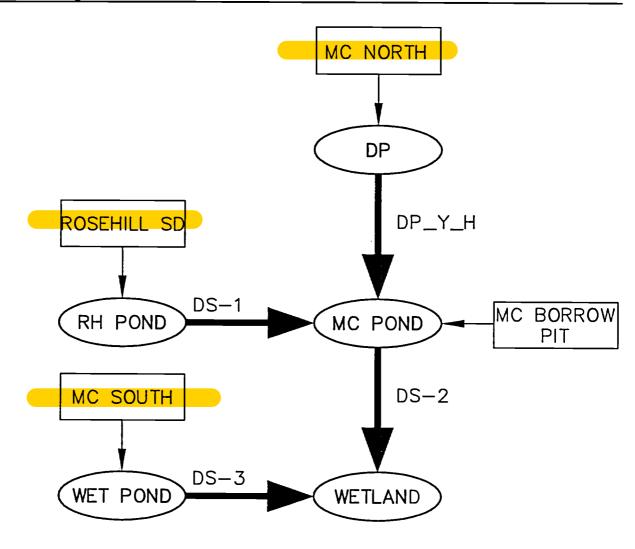
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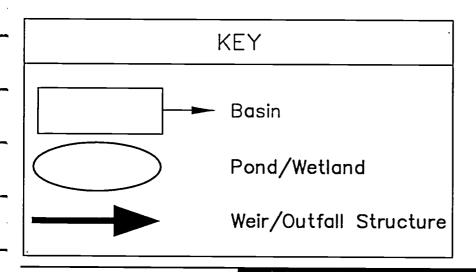
April 19, 2004

David | Bromberg, P.E.

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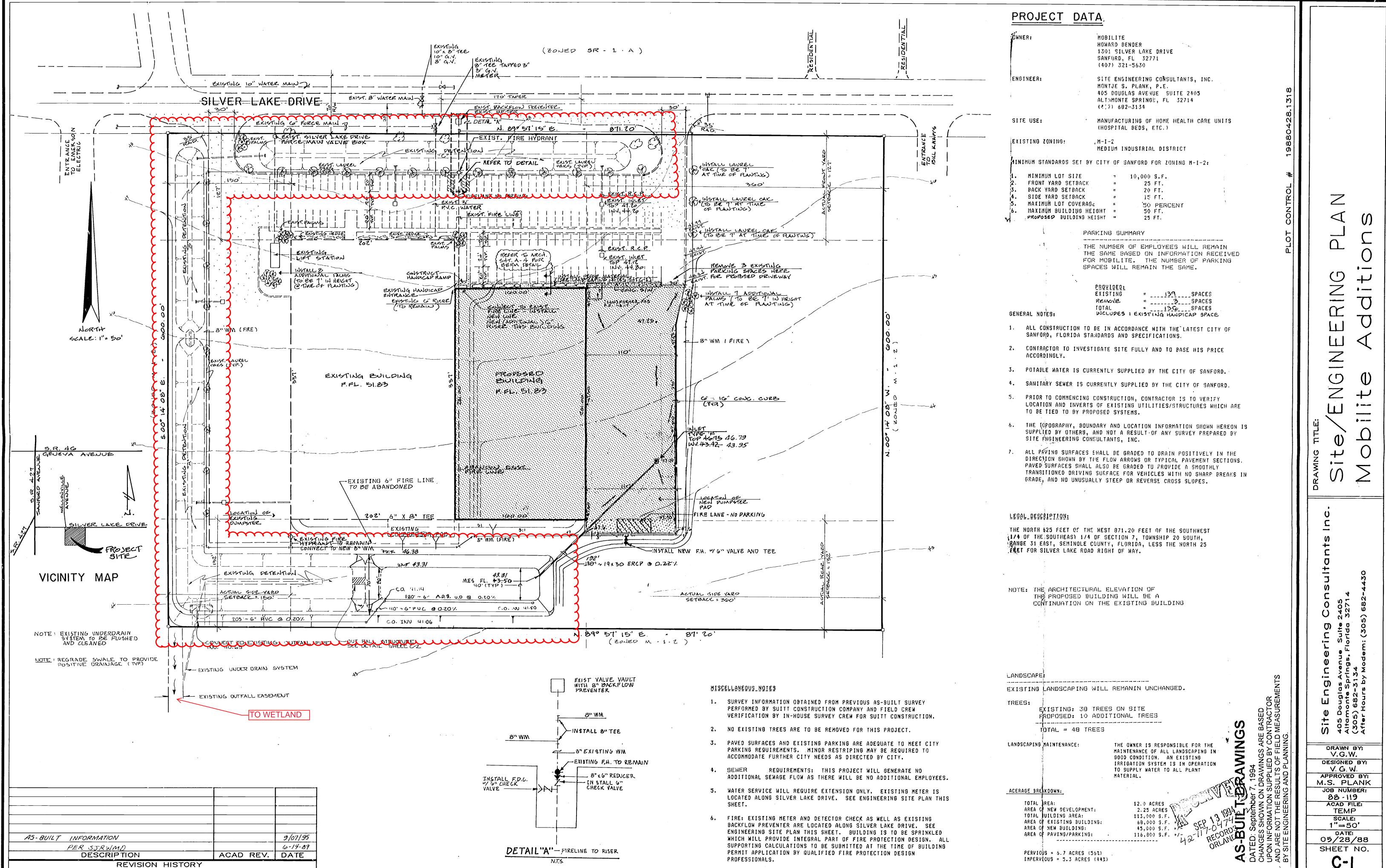
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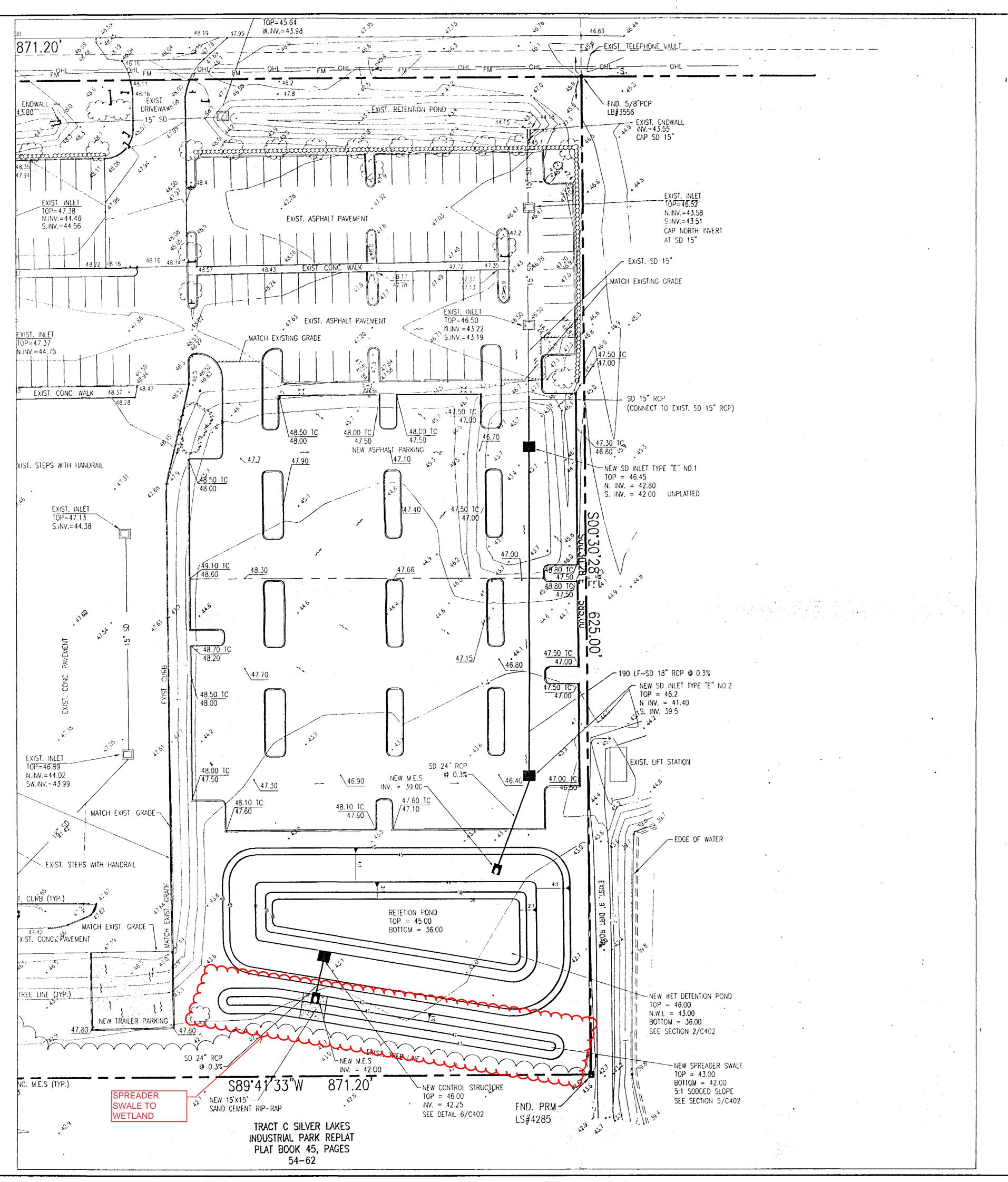
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Magnolia Club Post-Development Nodal Diagram Figure 8 (Revised) May 24, 2004



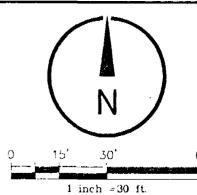
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Appendix B.77



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GENERAL NOTES:

- 1. ALL DISTURBED AREAS SHALL BE SODDED.
- COMPLY WITH FLORIDA DEPT. OF TRANSPORTATION ROADWAY & TRAFFIC DESIGN STANDARDS FOR THE FOLLOWING:
 - TYPE "E" & "C" INLET = INDEX No. 232

 MITERED END SECTION = INDEX No. 273

 TYPE J MANHOLE = INDEX No. 200

 SD HEADWALL = INDEX No. 250
- 3. ALL STORM DRAIN INLETS LOCATED IN VEHICULAR TRAFFIC AREAS SHALL RECEIVE A STEEL ANGLE CRATE SEAT. ALL GRATES SHALL BE TRAFFIC BATED.
- SEE SHEET C-002 FOR EROSION PROTECTION MEASURES DURING CONSTRUCTION.
- 5. PROJECT IS NOT LOCATED WITHIN A SPECIAL FLOOD AREA FEMA CLASSIFICATION ZONE "6"

LEGEND

	<u>EXIST.</u>	NEW
FINISH GRADE	36.33	63.0
FLOW PATTERN		~ -
CONTOUR		
STORM DRAIN INLET		
STORM DRAN LINE	SD	
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MITERED END SECTION		B

URBAN DESIGN PLANNING ENGINEER
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URBAN DES 1053 N. ORLANDO AVE. \$ S TELEPHONE 407-629-4288

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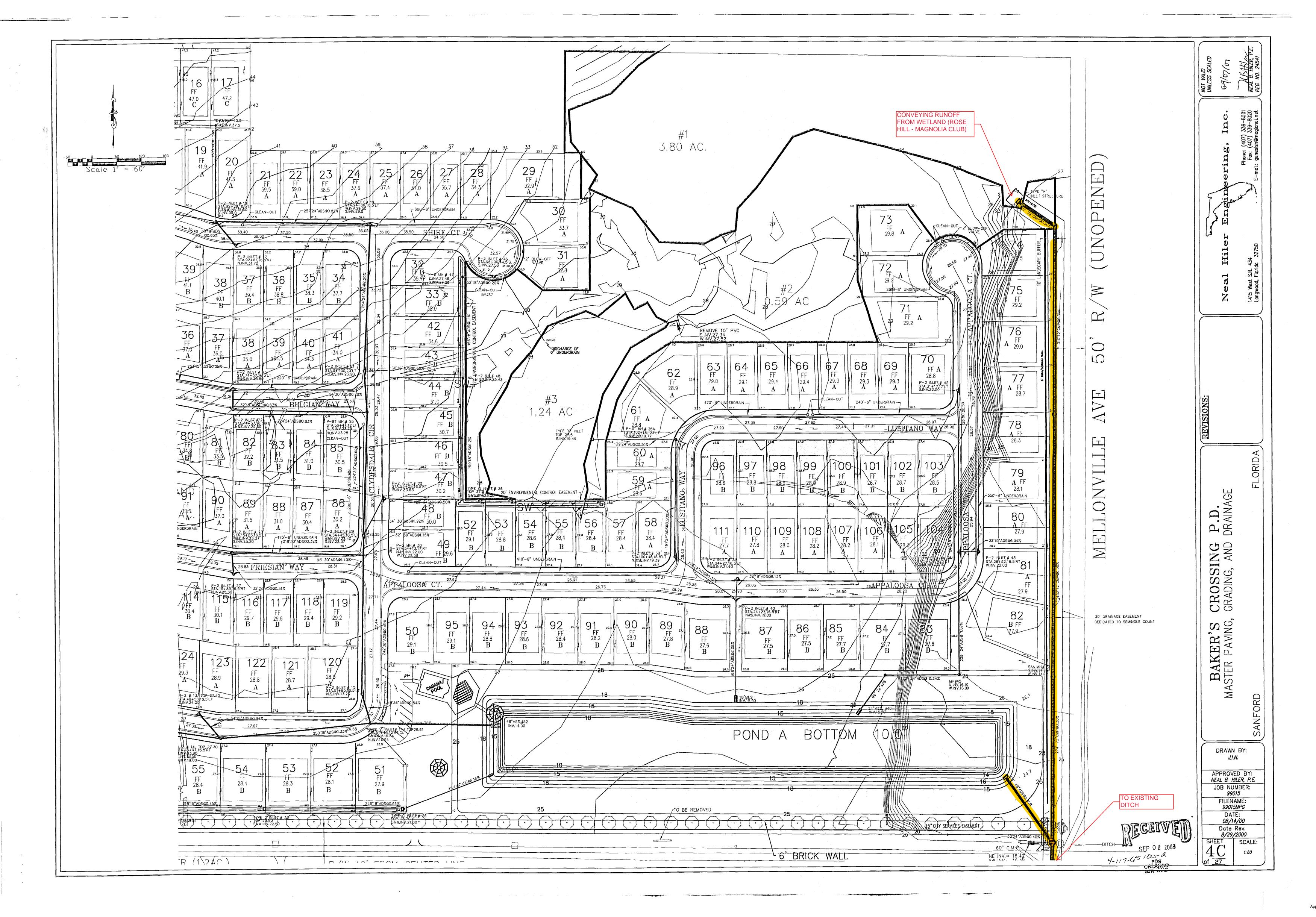
Drawn by:
T.OTTAWAY
Checked:
M. KALAGHCHI
File No:
0253/0253C2018.DWG

C-201

issue Date and Purpose

12/26/02 90% PRICE SET 1/16/03 PERMIT SET

Appendix B.78



Appendix B.79

Appendix C – Field Review Documentation





Photo 1: View of north (upstream) mitered endwall (ST-1) of CD-01_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. Heavy vegetation was noted along the inflow ditch to the cross drain. The water level in ST-1 measured approximately 19-inches above the pipe invert.



Photo 2: View south and immediately downstream of endwall (ST-2) of CD-01_EX. Endwall not visible due to heavy vegetation. Standing water was observed.



Photo 3: View north and immediately upstream of endwall (ST-3) of CD-02_EX. Endwall not visible due to heavy vegetation. Standing water was observed.



Photo 4: View south of the downstream CD-02_EX (ST-4) where it joins the 48-inch triple side drain.





Photo 5: View northwest of triple 48-inch side drain downstream of CD-02_EX which conveys the runoff to an roadside ditch.



Photo 6: View east of roadside ditch downstream of triple 48-inch side drain which conveys the runoff from CD-02_EX and other areas to triple 48-inch pipes.



Photo 7: View southeast of triple 48-inch pipes which receive the runoff from the roadside ditch and conveys the runoff to a downstream wetland. This structure is located at East Lake Mary Blvd approximately 100-ft west of Mellonville Avenue.



Photo 8: View of scour on the headwall structure of triple 48-inch pipes. This structure is located at East Lake Mary Blvd approximately 100-ft west of Mellonville Avenue.





Photo 9: View of manholes structures corresponding to a triple 48-inch pipes which conveys the runoff from the roadside ditch to a downstream wetland. These structures are located at Mellonville Avenue approximately 640-ft south of East Lake Mary Blvd, on the west side next to the sidewalk just before the beginning of a tall concrete wall.



Photo 10: View of quadruple pipes structure which receive the runoff from the triple 48-inch pipes and conveys the runoff to a downstream wetland. This structure is located at Hidden Palm Dr. approximately 860-ft east of Mellonville Avenue.



Photo 11: View of north (upstream) mitered endwall (ST-5) of CD-03A_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. The water level and stain marks were measured at approximately 5-inches and 8-inches above the pipe invert, respectively.



Photo 12: View of storm manhole (ST-6) which joins CD_03A and CD_03B at the downstream side. From manhole, a 38" x 60" ERCP conveys runoff within Sylvestri Lakes Community and outfalls into a wetland area located east of the community.





Photo 13: View of north (upstream) ditch bottom inlet (ST-7) of CD-03B_EX. Ditch bottom inlet was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review.



Photo 14: View of north (upstream) endwall (ST-8) of CD-04_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review. The structure had no sedimentation (silt), nor any observed stain lines.



Photo 15: View of ditch with stone revetment upstream CD-04_EX looking east.



Photo 16: View inside of elliptical pipe of CD-04_EX looking south. Some sedimentation and stain lines were observed.





Photo 17: View of south (downstream) endwall (ST-9) of CD-04_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. There was no standing water or flow on the day of the field review. The structure had no sedimentation (silt), nor any observed stain lines. A DBI structure was observed downstream the endwall, however, it could not be determined in the field how it is related to the drainage system.



Photo 18: View of northwest (upstream) mitered endwall (ST-10) of CD-05_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. The water level was measured at approximately 8-inches above the pipe invert. The structure had vegetation, there was no sedimentation (silt), and no stain lines were observed.



Photo 19: View of southeast (downstream) mitered endwall (ST-11) of CD-05_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. The structure had vegetation, there was no sedimentation (silt), and no stain lines were observed.



Photo 20: View of north (upstream) mitered endwall (ST-12) of CD-06_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. The water level for ST-12 was approximately 6-inches above the pipe invert. The structure had no sedimentation (silt), nor any observed stain lines.





Photo 21: View of south (downstream) mitered endwall (ST-13) of CD-06_EX. Endwall was observed to be in good condition and had no apparent scour or erosion. The water level for ST-13 was approximately 6-inches above the pipe invert. The structure had no sedimentation (silt), nor any observed stain lines.



Photo 22: View north and immediately upstream of endwall (ST-14) of CD-07_EX. Endwall was observed, although it could not be accessed due to the high vegetation. Standing water was observed.



Photo 23: View south and immediately downstream of endwall (ST-15) of CD-07_EX. Endwall not visible due to heavy vegetation. Standing water was observed.



Photo 24: View north and immediately upstream of CD-07_EX at Navy Canal. Navy canal was observed with no vegetation and obstructions within the canal. The canal was highly vegetated along the overbanks.

Appendix D – Proposed Hydrologic and Hydraulic Calculations

NOAA RAINFALL (ATLAS 14)



NOAA Atlas 14, Volume 9, Version 2 Location name: Sanford, Florida, USA* Latitude: 28.7511°, Longitude: -81.2546° Flevation: m/ft**

Elevation: m/ft**

* source: ESRI Maps

** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

D		Average recurrence interval (years)								
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	5.69 (4.62-6.98)	6.50 (5.27-7.99)	7.78 (6.29-9.60)	8.78 (7.07-10.9)	10.1 (7.80-12.9)	11.1 (8.36-14.4)	12.0 (8.75-16.0)	12.8 (8.99-17.8)	13.9 (9.37-19.9)	14.6 (9.65-21.5)
10-min	4.16 (3.38-5.12)	4.76 (3.86-5.86)	5.69 (4.60-7.03)	6.43 (5.17-7.99)	7.39 (5.71-9.43)	8.09 (6.12-10.5)	8.75 (6.40-11.7)	9.38 (6.58-13.0)	10.2 (6.86-14.6)	10.7 (7.07-15.8)
15-min	3.38 (2.75-4.16)	3.87 (3.14-4.76)	4.63 (3.74-5.72)	5.23 (4.20-6.49)	6.01 (4.64-7.67)	6.58 (4.98-8.56)	7.11 (5.20-9.54)	7.62 (5.35-10.6)	8.25 (5.58-11.9)	8.69 (5.74-12.8)
30-min	2.78 (2.26-3.42)	3.17 (2.58-3.91)	3.79 (3.06-4.68)	4.27 (3.43-5.30)	4.90 (3.79-6.25)	5.36 (4.06-6.97)	5.79 (4.24-7.77)	6.20 (4.35-8.61)	6.71 (4.53-9.64)	7.06 (4.67-10.4)
60-min	1.85 (1.50-2.27)	2.12 (1.72-2.61)	2.54 (2.06-3.14)	2.88 (2.32-3.58)	3.32 (2.57-4.25)	3.65 (2.76-4.75)	3.96 (2.89-5.31)	4.25 (2.98-5.90)	4.61 (3.12-6.63)	4.87 (3.22-7.19)
2-hr	1.15 (0.942-1.41)	1.32 (1.08-1.62)	1.60 (1.30-1.96)	1.82 (1.47-2.24)	2.10 (1.64-2.66)	2.31 (1.76-2.99)	2.51 (1.85-3.34)	2.70 (1.91-3.72)	2.94 (2.00-4.20)	3.11 (2.07-4.55)
3-hr	0.832 (0.684-1.01)	0.960 (0.788-1.17)	1.16 (0.953-1.42)	1.33 (1.08-1.64)	1.55 (1.22-1.97)	1.72 (1.32-2.22)	1.88 (1.40-2.51)	2.04 (1.45-2.82)	2.25 (1.54-3.21)	2.40 (1.60-3.51)
6-hr	0.477 (0.395-0.577)	0.548 (0.454-0.664)	0.669 (0.551-0.812)	0.773 (0.633-0.943)	0.921 (0.732-1.17)	1.04 (0.806-1.35)	1.16 (0.870-1.55)	1.29 (0.926-1.78)	1.46 (1.01-2.09)	1.60 (1.08-2.32)
12-hr	0.273 (0.228-0.328)	0.310 (0.258-0.372)	0.378 (0.314-0.456)	0.441 (0.364-0.535)	0.540 (0.436-0.693)	0.624 (0.491-0.812)	0.716 (0.543-0.959)	0.816 (0.594-1.13)	0.961 (0.671-1.37)	1.08 (0.730-1.56)
24-hr	0.157 (0.132-0.188)	0.178 (0.149-0.213)	0.219 (0.183-0.262)	0.259 (0.215-0.312)	0.324 (0.265-0.417)	0.381 (0.303-0.496)	0.445 (0.341-0.596)	0.516 (0.379-0.714)	0.621 (0.438-0.885)	0.708 (0.482-1.01)
2-day	0.090 (0.077-0.107)	0.104 (0.088-0.123)	0.129 (0.109-0.154)	0.155 (0.130-0.185)	0.195 (0.161-0.250)	0.231 (0.185-0.299)	0.271 (0.209-0.360)	0.315 (0.233-0.433)	0.380 (0.270-0.538)	0.434 (0.297-0.617
3-day	0.067 (0.057-0.079)	0.077 (0.065-0.091)	0.096 (0.081-0.114)	0.114 (0.096-0.136)	0.144 (0.119-0.183)	0.170 (0.136-0.218)	0.198 (0.153-0.262)	0.230 (0.170-0.314)	0.276 (0.197-0.389)	0.315 (0.216-0.446
4-day	0.054 (0.046-0.064)	0.062 (0.053-0.073)	0.077 (0.065-0.091)	0.092 (0.077-0.109)	0.114 (0.095-0.145)	0.134 (0.108-0.172)	0.156 (0.121-0.206)	0.181 (0.134-0.246)	0.217 (0.154-0.304)	0.246 (0.170-0.348
7-day	0.037 (0.032-0.044)	0.042 (0.036-0.049)	0.051 (0.043-0.060)	0.059 (0.050-0.070)	0.072 (0.060-0.091)	0.084 (0.068-0.107)	0.097 (0.075-0.126)	0.111 (0.082-0.149)	0.131 (0.094-0.182)	0.147 (0.102-0.207
10-day	0.030 (0.026-0.035)	0.033 (0.029-0.039)	0.040 (0.034-0.047)	0.046 (0.039-0.054)	0.055 (0.046-0.069)	0.063 (0.051-0.080)	0.072 (0.056-0.094)	0.081 (0.061-0.109)	0.095 (0.068-0.132)	0.106 (0.074-0.149
20-day	0.020 (0.018-0.024)	0.023 (0.020-0.026)	0.027 (0.023-0.031)	0.030 (0.026-0.035)	0.035 (0.029-0.043)	0.039 (0.032-0.049)	0.044 (0.034-0.056)	0.048 (0.036-0.064)	0.055 (0.039-0.075)	0.060 (0.042-0.083
30-day	0.017 (0.014-0.019)	0.019 (0.016-0.022)	0.022 (0.019-0.025)	0.024 (0.021-0.029)	0.028 (0.023-0.034)	0.031 (0.025-0.038)	0.034 (0.027-0.043)	0.037 (0.028-0.049)	0.041 (0.030-0.056)	0.044 (0.031-0.061
45-day	0.014 (0.012-0.016)	0.015 (0.013-0.018)	0.018 (0.016-0.021)	0.020 (0.017-0.023)	0.023 (0.019-0.028)	0.025 (0.020-0.031)	0.027 (0.021-0.034)	0.029 (0.022-0.038)	0.032 (0.023-0.043)	0.033 (0.023-0.046
60-day	0.012	0.014	0.016	0.018	0.020	0.022	0.023 (0.018-0.029)	0.025	0.027	0.028

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

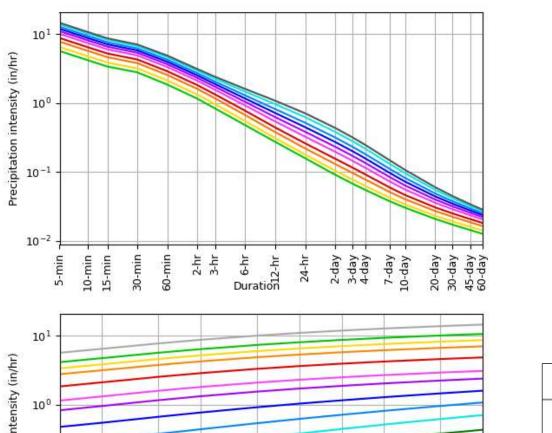
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

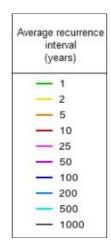
Please refer to NOAA Atlas 14 document for more information.

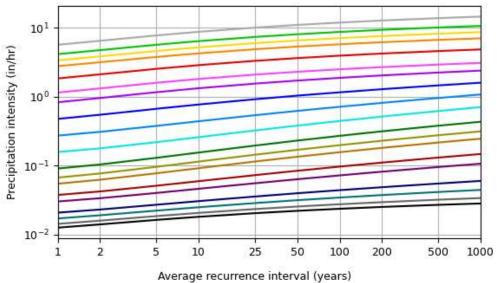
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PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 28.7511°, Longitude: -81.2546°









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Maps & aerials

Small scale terrain

CROSS DRAIN CD-01_PR

PROJECT:	Sanford Airport Connector	PREPARED:	LCM	DATE:	04/28/25
LOCATION:	Seminole County, Florida	CHECKED:	LCS	DATE:	04/28/25

Proposed Offsite Conveyance Calculations

Proposed Cross Drain at Sanford Airport Connector

Cross Drain Name	CD-01_PR
Affected Corridor(s)	2a
Pervious C-Value	0.20
Impervious C-value	0.95
Time of Concentration (min)	21.0

Basin Runoff Calculations for Offsite CD-01 PR Basin

Dasili Kulloli Calculations for Offsite CD-01_FK Dasili					
Total Contributing Area (acres)	13.43				
Pervious Contributing Area (acres)	13.43				
Impervious Contributing Area (acres)	0.00				
Weighted Runoff Coefficient (C ₅₀) ¹	0.24				
Weighted Runoff Coefficient (C ₁₀₀₋₅₀₀) ¹	0.25				
Design Event ²	50-year				
Rainfall Intensities ³					
Design Event I ₅₀ (in/hr)	6.09				
I ₁₀₀ (in/hr)	6.58				
l ₅₀₀ (in/hr)	7.63				
Peak Flows					
Design Q ₅₀ (cfs)	19.63				
Q ₁₀₀ (cfs)	22.09				
Q ₅₀₀ (cfs)	25.62				

Cross Drain Sizing Calculations

Cross Brain Gizing Galcalations					
Assumed Velocity (ft/s)	3				
Cross-sectional Area Required (ft²)	6.54				
Recommended Culvert Conveyance Size	36 inch				
Provided Cross Sectional Area (ft²)	7.07				
Upstream Est. SHWL Elev (ft-NAVD88)	11.14				
Upstream Est. Ground Elev (ft-NAVD88)	11.14				
Downstream Est. Ground Elev (ft-NAVD88)	10.90				
Additional Culvert Height Required	0 ft				
Recommended Culvert Size	36 inch				
Tailwater (ft-NAVD88) ⁴	13.9 ft				
Length ⁵	142 ft				

Notes:

Design Storm Frequency Factors for Pervious Area Runoff Coefficients

Table T-5 (FDOT Hydrology Handbook, Feb. 2012)

Return Period (years)	Design Storm Frequency		
2 to 10	1.00		
25	1.10		
50	1.20		
100	1.25		

¹ Frequency Factor for Pervious Area Runoff Coefficients will be applied per Design Storm Event (Table B-5, FDOT Drainage Design Guide, January 2017).

² Per FDOT Drainage Manual, 50-year considered design event for mainline interstates and 100-year used if culvert proposed within regulated floodway.

³ Design Intensity calculated from NOAA IDF Curve (NOAA Atlas 14 Website).

⁴ Crown of culvert

⁵ Approximate Length = R/W Length - 10-ft each side for riprap

PROJECT: LOCATION:		port Connector	PREPARED:	LCM LCS	DATE: 4/28/2	
		oncentration Calculations	CHECKED:	LCS	DATE: 4/28/2	:025
EXISTING	or	DEVELOPED / UNDEVELOPED		BASIN:	Offsite CD-01_PR	
Тс	or	Tt (through subarea)				
Sheet flow (Applicable Segment ID 1. Surface descr 2. Mannings rou 3. Flow length, L 4. 2-year, 24-hot 5. Land slope, s 6. Compute Tt in Subtotal Shallow Concentrate Segment ID	iption [†] ghness coeff., (total L ≤ 100 ur rainfall (in.) ⁻ (ft./ft.) n hr, Tt = [0.007	ft.)	L=	1,085	AB Pavement 0.012 100 4.27 0.022 0.018 0.02	
7. Surface descr 8. Flow length, L 9. Watercourse 10. Average velo 11. Compute Tt i Subtotal	0.5 (fps)			Unpaved 985 0.003 0.83 0.33 0.33		
Channel & Pipe Flow Segment ID 12. Segment Typ 13. Pipe Diamete 14. Cross section 15. Wetted perim 16. Hydraulic rad 17. Channel/Pipe 18. Manning's ro 19. V = 1.486(r^0 20. Flow length, I 21. Compute Tt ii 22. Subtotal	per (in.) nal flow area, a neter, Pw lius (ft), r = a/Pi e slope, s (ft./ft. ughness coeff. 0.667)(s^0.50)/ft.) , n n, Compute V				
Time of Concentration	on, hr. (summa	ation of subtotals)		urs nutes tal	0.35 21.0 21.0	

Notes:

- † Values from Table 3-1 of Urban Hydrology for Small Watersheds, Technical Release of TR-55
- †† The 2-year, 24-hour rainfall was used based on TR-55 Figure B-3.
- ††† This equation is derived from TR-55

Crossing Input: CD-01_PR

Parameter	Value	Units
DISCHARGE DATA		
Discharge Method	User-Defined	
Discharge List	Define	
TAILWATER DATA		
Channel Type	Enter Constant Tailwater Elevation	
Channel Invert Elevation	10.900	ft
Constant Tailwater	13.900	ft
Elevation		
Rating Curve	View	
ROADWAY DATA		
Roadway Profile Shape	Constant Roadway	
	Elevation	_
First Roadway Station	0.000	ft
Crest Length	300.000	ft
Crest Elevation	37.000	ft
Roadway Surface	Paved	
Top Width	96.000	ft

Culvert Input: CD-01_PR

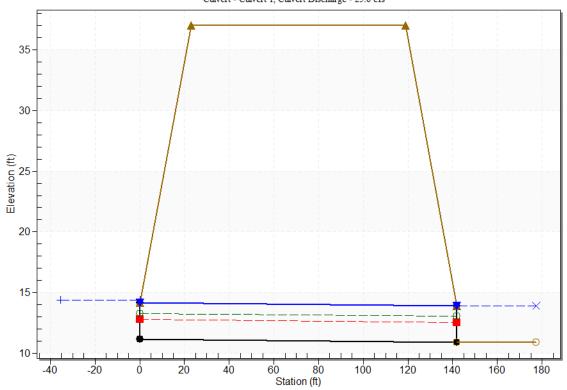
Parameter	Value	Units
CULVERT DATA		
Name	Culvert 1	
Shape	Circular	
Material	Concrete	
Diameter	3.000	ft
Embedment Depth	0.000	in
Manning's n	0.012	
Culvert Type	Straight	
Inlet Configuration	Square Edge with Headwall (Ke=0.5)	
Inlet Depression?	No	
SITE DATA		
Site Data Input Option	Culvert Invert Data	
Inlet Station	0.000	ft
Inlet Elevation	11.140	ft
Outlet Station	142.000	ft
Outlet Elevation	10.900	ft
Number of Barrels	1	
Computed Culvert Slope	0.001690	ft/ft

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	HW / D (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
50-yr	19.63	19.63	14.25	2.08	3.107	1.04	3- M1f	1.78	1.42	3.00	3.00	2.78	0.00
100-yr	22.09	22.09	14.35	2.23	3.212	1.07	3- M1f	1.92	1.51	3.00	3.00	3.13	0.00
500-yr	25.62	25.62	14.38	2.44	3.244	1.08	4-FFf	2.15	1.63	3.00	3.00	3.62	0.00
Overtopping	170.80	169.08	37.02	25.88	23.817	8.63	4-FFf	3.00	3.00	3.00	3.00	23.92	0.00

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - CD-01_PR, Design Discharge - 25.6 cfs Culvert - Culvert 1, Culvert Discharge - 25.6 cfs



CROSS DRAIN CD-02_PR

PROJECT:Sanford Airport ConnectorPREPARED:LCMDATE:02/03/25LOCATION:Seminole County, FloridaCHECKED:LCSDATE:02/03/25

Proposed Offsite Conveyance Calculations

Proposed Cross Drain at Sanford Airport Connector (Offsite CD-02_PR Basin)

Cross	Drain Name CD-02_PR
Affecte	ed Corridor(s) 2a
Pervi	vious C-Value 0.20
Imperv	vious C-value 0.95
Time of Concer	ntration (min) 138.6

Basin Runoff Calculations for Offsite CD-04_PR Basin

Basili Rulioli Calculations for Offsite CD-04_PR Basili					
Total Contributing Area (acres)	15.12				
Pervious Contributing Area (acres)	15.12				
Impervious Contributing Area (acres)	0.00				
Weighted Runoff Coefficient (C ₅₀) ¹	0.24				
Weighted Runoff Coefficient (C ₁₀₀₋₅₀₀) ¹	0.25				
Design Event ²	50-year				
Rainfall Intensities ³					
Design Event I ₅₀ (in/hr)	2.13				
I ₁₀₀ (in/hr)	2.31				
I ₅₀₀ (in/hr)	2.73				
Peak Flows					
Design Q ₅₀ (cfs)	7.73				
Q ₁₀₀ (cfs)	8.73				
Q ₅₀₀ (cfs)	10.32				

Total Peak Flow Draining to CD_04_PR

Basin	Q_{50}	Q ₁₀₀	Q ₅₀₀
*Sylvestri Lake North Drainage System	115.24	198.24	207.43
Offsite CD-02_PR Basin	7.73	8.73	10.32
Total Peak Flow	122.97	206.97	217.75

Note: *100-yr peak flows from Sylvestri Lake Drainage System Permit Documentation, other flows was estimated.

Cross Drain Sizing Calculations

Cross Brain Cizing Calculations	
Assumed Velocity (ft/s)	3
Cross-sectional Area Required (ft ²)	40.99
Number of Cells	1
Recommended Culvert Conveyance Size	9 ft x 5 ft
Provided Cross Sectional Area (ft ²)	45.00
Upstream Est. SHWL Elev (ft-NAVD88)	29.28
Upstream Est. Ground Elev (ft-NAVD88)	29.28
Downstream Est. Ground Elev (ft-NAVD88)	28.81
Additional Culvert Height Required	0 ft
Recommended Culvert Size (SpanxRise)	1-cell 9 ft x 5 ft
Tailwater (ft-NAVD88) ⁴	33.81
Length ⁵	156 ft

Notes:

^{**} Total Drainage Basin Area = Sylvestri Lakes North Drainage System + Offsite CD-02_PR

¹ Frequency Factor for Pervious Area Runoff Coefficients will be applied per Design Storm Event (Table B-5, FDOT Drainage Design Guide, January 2017).

² Per FDOT Drainage Manual, 50-year considered design event for mainline interstates and 100-year used if culvert proposed within regulated floodway.

³ Design Intensity calculated from NOAA IDF Curve (NOAA Atlas 14 Website).

⁴ Crown of culver

 $^{^{5}}$ Approximate Length = R/W Length - 10-ft each side for riprap / Culvert in skew.

Design Storm Frequency Factors for Pervious Area Runoff Coefficients

Table T-5 (FDOT Hydrology Handbook, Feb. 2012)

Return Period (years)	Design Storm Frequency
2 to 10	1.00
25	1.10
50	1.20
100	1.25

General Notes:

Sylvestri Lake North Drainage System Basin

¹⁻ The oufall flows from Sylvestri Lake North Drainage System for 50-yr and 500-yr recurrence intervals were estimates using a log-log procedure (See Sheet for Additional Flow Estimate from Sylvestri Lake South Drainage System).

PROJECT:	Sanford Airport Connector	PREPARED:	LCM	DATE : 4/28/2025
LOCATION:	Seminole County, Florida	_ CHECKED:	LCS	DATE: 4/28/2025
Proposed Offsi	te Time of Concentration Calculations			
EXISTING	or DEVELOPED / UNDEVELOPED		BASIN:	Offsite CD-02_PR
Тс	or Tt (through subarea)]		
Sheet flow (Applicab	le to Tc only)	L =	1,675 f	ft
Segment ID	ie to 10 only)		Γ	AB
Surface descr	iption [†]			Wood
2. Mannings roug	ghness coeff., n †			0.40
Flow length, L	(total L ≤ 100 ft.)			100
4. 2-year, 24-hoι				4.27
5. Land slope, s				0.002
	hr, Tt = $[0.007(nL)^{0.8}]/[P_{24hr}^{0.5} s^{0.4}]$ +++		-	0.831
Subtotal			L	0.83
Shallow Concentrate	d Flow		_	
Segment ID			_	BC
	iption (Paved or Unpaved)		-	Unpaved
8. Flow length, L			-	328
9. Watercourse s	city ^{†††} , V = kS^0.5 (fps)		-	0.0003
_	n hr, Tt = L/3600V		-	0.32
Subtotal	, 10 2,00000			0.32
Channel & Pipe Flow	,			
Segment ID			Γ	CD
12. Segment Typ	e			Channel
13. Pipe Diamete				
14. Cross section	al flow area, a (assumed d=0.5 ft for channel)			6
15. Wetted perim	eter, Pw			14.12
-	ius (ft), r = a/Pw, Compute r			0.42
17. Channel/Pipe	• • • •		_	0.0005
18. Manning's rou			-	0.06
19. V = 1.486(r^0 20. Flow length, l	.667)(s^0.50)/n, Compute V		-	0.30
-	- n hr, Tt = L/3600V			1,247 1.16
22. Subtotal	, 2,0000		-	1.16
			L	-
ime of Concentration	on, hr. (summation of subtotals)	Но	ours	2.31
		Mi	nutes	138 6

Notes:

- † Values from Table 3-1 of Urban Hydrology for Small Watersheds, Technical Release of TR-55
- †† The 2-year, 24-hour rainfall was used based on TR-55 Figure B-3.
- ††† This equation is derived from TR-55

138.6

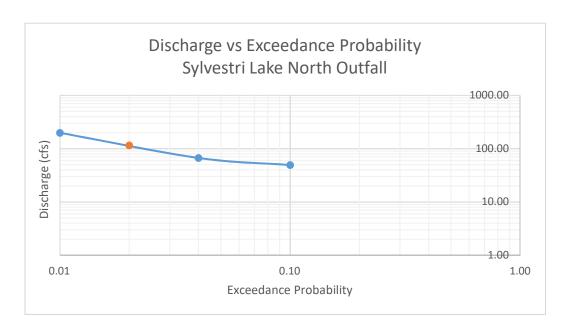
138.6

Minutes

Total

Additional Flow Estimate from Sylvestri Lake North Drainage System

RI	Prob	Discharge log Prol (cfs)		Log	
(yr)	PIOD			Discharge	
10	0.10	49.36	-1.000	1.693	
25	0.04	66.99	-1.398	1.826	
100	0.01	198.24	-2.000	2.297	
Slope1 =	-0.78262				
RI (yr)	Prob	log Prob	Log Discharge	Estimated Discharge (cfs)	
50	0.02	-1.699	2.062	115.24	



To determine Peak Flow for 500-yr Storm Event:

 Q_{500} = 207.43 cfs (Typical range Q_{500}/Q_{50} between 1.3 and 1.8, use 1.8)

Crossing Input: CD-02_PR

Parameter	Value	Units
DISCHARGE DATA		
Discharge Method	User-Defined	
Discharge List	Define	
TAILWATER DATA		
Channel Type	Enter Constant Tailwater Elevation	
Channel Invert Elevation	28.810	ft
Constant Tailwater	33.810	ft
Elevation		
Rating Curve	View	
ROADWAY DATA		
Roadway Profile Shape	Constant Roadway Elevation	
First Roadway Station	0.000	ft
Crest Length	300.000	ft
Crest Elevation	36.950	ft
Roadway Surface	Paved	
Top Width	96.000	ft

Culvert Input: CD-02_PR

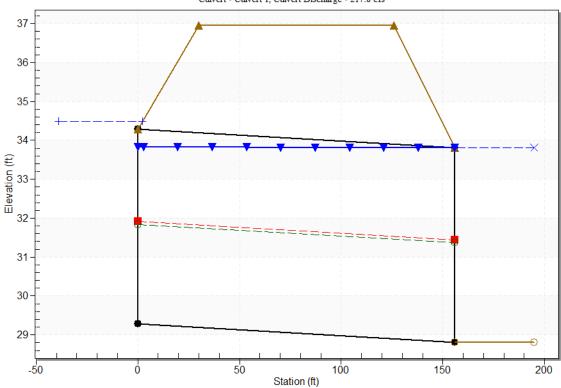
Parameter	Value	Units
CULVERT DATA		
Name	Culvert 1	
Shape	Concrete Box	
Material	Concrete	
Span	9.000	ft
Rise	5.000	ft
Embedment Depth	0.000	in
Manning's n	0.012	
Culvert Type	Straight	
Inlet Configuration	Square Edge (90º) Headwall (Ke=0.5)	
Inlet Depression?	No	
SITE DATA		
Site Data Input Option	Culvert Invert Data	
Inlet Station	0.000	ft
Inlet Elevation	29.280	ft
Outlet Station	156.000	ft
Outlet Elevation	28.810	ft
Number of Barrels	1	
Computed Culvert Slope	0.003013	ft/ft

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	HW / D (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
50-yr	122.97	122.97	34.02	3.06	4.745	0.95	1-S1f	1.73	1.80	5.00	5.00	2.73	0.00
100-yr	206.97	206.97	34.42	4.29	5.138	1.03	1-S1f	2.47	2.54	5.00	5.00	4.60	0.00
500-yr	217.75	217.75	34.48	4.44	5.203	1.04	1-S1f	2.56	2.63	5.00	5.00	4.84	0.00
Overtopping	508.08	445.73	37.12	7.84	7.342	1.57	4-FFf	4.30	4.24	5.00	5.00	9.91	0.00

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - CD-02_PR, Design Discharge - 217.8 cfs
Culvert - Culvert 1, Culvert Discharge - 217.8 cfs



CROSS DRAIN CD-03_PR

PROJECT:Sanford Airport ConnectorPREPARED:LCMDATE:05/02/25LOCATION:Seminole County, FloridaCHECKED:LCSDATE:05/02/25

Proposed Offsite Conveyance Calculations

Proposed Cross Drain at Sanford Airport Connector

(Total Drainage Basin Area = Drainage Basin CD-03_EX + Drainage Basin CD-04_EX + Offsite CD-03_PR Basin)

Cross Drain Name	CD-03_PR
Affected Corridor(s)	2a
Pervious C-Value	0.20
Impervious C-value	0.95
Time of Concentration (min)	49.1

Basin Runoff Calculations for Offsite CD-03 PR Basin

Dasin Runon Calculations for Offsite CD-03_FR Basin	
Total Contributing Area (acres)	23.85
Pervious Contributing Area (acres)	23.85
Impervious Contributing Area (acres)	0.00
Weighted Runoff Coefficient (C ₅₀) ¹	0.24
Weighted Runoff Coefficient (C ₁₀₀₋₅₀₀) ¹	0.25
Design Event ²	50-year
Rainfall Intensities ³	
Design Event I ₅₀ (in/hr)	4.27
I ₁₀₀ (in/hr)	4.62
I ₅₀₀ (in/hr)	5.37
Peak Flows	
Design Q ₅₀ (cfs)	24.44
Q ₁₀₀ (cfs)	27.55
Q ₅₀₀ (cfs)	32.02

Total Peak Flow Draining to CD_03_PR

Basin	Q ₅₀	Q ₁₀₀	Q ₅₀₀
*Existing Cross Drains CD-3A_EX and CD-3B_EX	70.33	84.40	105.50
*Existing Cross Drain CD-4_EX	45.90	55.08	68.85
Offsite CD-03_PR Basin	24.44	27.55	32.02
Total Peak Flow	140.68	167.03	206.37

Notes:

Cross Drain Sizing Calculations

Cross Drain Sizing Calculations	
Assumed Velocity (ft/s)	3
Cross-sectional Area Required (ft ²)	46.89
Number of Cells	1
Recommended Culvert Conveyance Size	8 ft x 6 ft
Provided Cross Sectional Area (ft ²)	48.00
Upstream Est. SHWL Elev (ft-NAVD88)	29.46
Upstream Est. Ground Elev (ft-NAVD88)	29.46
Downstream Est. Ground Elev (ft-NAVD88)	28.61
Additional Culvert Height Required	0 ft
Recommended Culvert Size (SpanxRise)	1-cell 8 ft x 6 ft
Tailwater (ft-NAVD88) ⁴	34.61
Length ⁵	283 ft

Notes:

^{**}Estimated using the velocity method

¹ Frequency Factor for Pervious Area Runoff Coefficients will be applied per Design Storm Event (Table B-5, FDOT Drainage Design Guide, January 2017).

² Per FDOT Drainage Manual, 50-year considered design event for mainline interstates and 100-year used if culvert proposed within regulated floodway.

 $^{^{\}rm 3}$ Design Intensity calculated from NOAA IDF Curve (NOAA Atlas 14 Website).

⁴ Crown of culvert

⁵ Approximate Length = R/W Length - 10-ft each side for riprap / Culvert in skew.

Design Storm Frequency Factors for Pervious Area Runoff Coefficients

Table T-5 (FDOT Hydrology Handbook, Feb. 2012)

Return Period (years)	Design Storm Frequency
2 to 10	1.00
25	1.10
50	1.20
100	1.25

General Notes:

Existing Cross Drains CD-3A_EX and CD-3B_EX Basin

1- Existing Cross Drains CD-3A_EX and CD-3B_EX are connected in an existing drainage system that runs within the North Sylvertri Lake Development and conveys the offsite basin runoff to a wetland area located on east of the community.

Existing Cross Drain CD-4 Basin

1- Although the cross drain is shown in the construction plans, it is not included in the drainage report of the permit document. Therefore, no design flow was provided in the permit documentation. The 50-yr flow rate was estimated using the velocity method.

Location: Seminole County, Florida	PROJECT:		rport Connector	PREPARED:	LCM	DATE:	
EXISTING Or DEVELOPED / UNDEVELOPED BASIN: Offsite CD-03_PR	LOCATION:	Seminole C	Jounty, Florida	CHECKED:	LCS	DATE:	04/28/25
L = 2,310 ft Sheet flow (Applicable to Tc only)	Proposed Off	site Time of C	oncentration Calculations				
L = 2,310 ft	EXISTING	or	DEVELOPED / UNDEVELOPED		BASIN:	Offsite CD	-03_PR
Segment ID	Тс	or	Tt (through subarea)	l			
AB				L =	2,310	ft	
1. Surface description 2. Mannings roughness coeff., n +		ible to Tc only)			г		
2. Mannings roughness coeff., n † 3. Flow length, L (total L ≤ 100 ft.) 4. 2-year, 24-hour rainfall (in.) +† 5. Land slope, s (ft./ft.) 6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{24hr} . 0.5 s ^{0.4}] +++ 5. Subtotal 3. Subtotal 3. Subtotal 5. Surface description (Paved or Unpaved) 8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft.) 10. Average velocity ^{1+†} , V = KS*0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft/ft.) 18. Manning's roughness coeff., n 19. V = 1.488(*0.667)(s*0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes Minutes 49.1		ariatian†			-		
3. Flow length, L (total L ≤ 100 ft.) 4. 2-year, 24-hour rainfall (in.) ++ 5. Land slope, s (ft/ft.) 6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{24tt} . 0.5 s. 0.4] +++ 5. Substal 0.318 Subtotal 0.32 Shallow Concentrated Flow Segment ID 7. Surface description (Paved or Unpaved) 8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft) 10. Average velocity 117, V = kS^0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal 0.50 Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft/ft.) 18. Manning's roughness coeff., n 19. V = 1.486(n^0.667)(s^0.50)in, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal			4		-		
4. 2-year, 24-hour rainfall (in.) ++ 5. Land slope, s (ft/ft.) 6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{28lll} 0.5 s ^{0.4}] +++ Subtotal 3.31 Subtotal 3.32 Shallow Concentrated Flow Segment ID 7. Surface description (Paved or Unpaved) 8. Flow length, L (ft.) 9. Watercourse slope, s (ft/ft.) 10. Average velocity ^{1+†} , V = kS^0.5 (fps.) 11. Compute Tt in hr, Tt = L/3600V Subtotal Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1	_	-			-		
5. Land slope, s (ft./ft.) 6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{24lm} ^{0.5} s ^{0.4}] +++ Subtotal 5. Land slope, s (ft./ft.) 6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{24lm} ^{0.5} s ^{0.4}] +++ Subtotal 5. Land slope, s (ft./ft.) 6. Compute Tt in hr, Tt = L/3600V Segment ID 7. Surface description (Paved or Unpaved) 8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft) 10. Average velocity ^{††} , V = kS ⁰ 0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal 6. Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r*0.667)(s*0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1	_				-		
6. Compute Tt in hr, Tt = [0.007(nL) ^{0.8}] / [P _{2-lip} ^{.0.5} s ^{0.4}] ††† Subtotal Shallow Concentrated Flow Segment ID 7. Surface description (Paved or Unpaved) 8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft) 10. Average velocity ^{1+†} , V = KS ⁰ 0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft/ft.) 18. Manning's roughness coeff., n 19. V = 1.486(f*0.667)(s*0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 0.318 0.32			11		-		
Shallow Concentrated Flow Segment ID BC Unpaved			7(pl) ^{0.8} 1/IP		-		
Shallow Concentrated Flow Segment ID 7. Surface description (Paved or Unpaved) Unpaved 8. Flow length, L (ft) 2,210 9. Watercourse slope, s (ft/ft) 0.006 10. Average velocity ^{††} , V = kS^0.5 (fps) 1.23 11. Compute Tt in hr, Tt = L/3600V 0.50 Subtotal 0.50 Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft/ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r*0.667)(s*0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1 Time of Concentration, hr. (summation of subtotals) Hours Minutes		111111, 11 - [0.007	(IIL)]/[i 24hr 3] · · ·		-		
Segment ID	Subtotal				L	0.32	
Segment ID	Shallow Concentra	ted Flow					
7. Surface description (Paved or Unpaved) 8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft) 10. Average velocity ^{†††} , V = kS^0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes Minutes Minutes					Г	ВС	
8. Flow length, L (ft) 9. Watercourse slope, s (ft/ft) 10. Average velocity ^{††} , V = kS^0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1	-	cription (Paved o	or Unpaved)		ļ		
9. Watercourse slope, s (ft/ft) 10. Average velocity ^{†††} , V = kS^0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal 11. Compute Tt in hr, Tt = L/3600V Subtotal 12. Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes 0.83			- 1 /		Ī		
10. Average velocity ^{†††} , V = kS^0.5 (fps) 11. Compute Tt in hr, Tt = L/3600V Subtotal Channel & Pipe Flow Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes					ļ		
Channel & Pipe Flow			0.5 (fps)		ľ	1.23	
Channel & Pipe Flow	11. Compute Tt	in hr, Tt = L/360	00V		ļ	0.50	
Segment ID 12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes 49.1						0.50	
12. Segment Type 13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes	Channel & Pipe Flo	w			-		
13. Pipe Diameter (in.) 14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 0.82 Minutes	-						
14. Cross sectional flow area, a (assumed d=0.5 ft for channel) 15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes							
15. Wetted perimeter, Pw 16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes 49.1							
16. Hydraulic radius (ft), r = a/Pw, Compute r 17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes			(assumed d=0.5 ft for channel)		-		
17. Channel/Pipe slope, s (ft./ft.) 18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes					-		
18. Manning's roughness coeff., n 19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes 49.1	-				-		
19. V = 1.486(r^0.667)(s^0.50)/n, Compute V 20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 0.82 Minutes	•		•		-		
20. Flow length, L 21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 0.82 Minutes					-		
21. Compute Tt in hr, Tt = L/3600V 22. Subtotal Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1			n, Compute v		-		
Time of Concentration, hr. (summation of subtotals) Hours Minutes 49.1			2017		-		
Time of Concentration, hr. (summation of subtotals) Hours 0.82 Minutes 49.1		. III III, Tt – L/300	50 V		-		
Minutes 49.1	ZZ. JUDIUIAI				L		
Minutes 49.1							
Minutes 49.1	Time of Concentrat	ion hr (eumm	ation of subtotals)	Но	urs [0.82	
	or Jonesiliat	, iii. (3uiiiiii	and. or outlotting		F		
					- F		

Notes:

- † Values from Table 3-1 of Urban Hydrology for Small Watersheds, Technical Release of TR-55
- †† The 2-year, 24-hour rainfall was used based on TR-55 Figure B-3.
- ††† This equation is derived from TR-55

Additional Flow Estimate from Existing Cross Drains (CD-03A_EX and CD-03B_EX)

Estimate Peak Flow (Alternative 1 - Using Q₂₅ Calculated Peak Flow from Permit)

From Permit document, $Q_{25} = 61.16 \text{ cfs}$

Calculated Q ₂₅	61.16	cfs
----------------------------	-------	-----

Estimate Q_{50} 70.33 cfs (Typical range Q_{50}/Q_{25} between 1.1 and 1.2, use 1.15) Estimate Q_{100} 84.40 cfs (Typical range Q_{100}/Q_{50} between 1.1 and 1.3, use 1.2) Estimate Q_{500} 105.50 cfs (Typical range Q_{500}/Q_{50} between 1.3 and 1.8, use 1.5)

Additional Flow Estimate from Existing Cross Drain CD-04_EX

Existing Structure	Triple 24"	x 38" ERCP
Opening Area	15.30	sf
Assume Velocity	3	fps
Estimate Q ₅₀	45.90	cfs
Estimate Q ₁₀₀	55.08	cfs (Typical range Q_{100}/Q_{50} between 1.1 and 1.3, use 1.2)
Estimate Q ₅₀₀	68.85	cfs (Typical range Q_{500}/Q_{50} between 1.3 and 1.8, use 1.5)

Crossing Input: CD-03_PR

Parameter	Value	Units			
DISCHARGE DATA					
Discharge Method	User-Defined				
Discharge List	Define				
TAILWATER DATA					
Channel Type	Enter Constant Tailwater Elevation				
Channel Invert Elevation	28.610	ft			
Constant Tailwater	34.610	ft			
Elevation					
Rating Curve	View				
ROADWAY DATA					
Roadway Profile Shape	Constant Roadway Elevation				
First Roadway Station	0.000	ft			
Crest Length	300.000	ft			
Crest Elevation	52.650	ft			
Roadway Surface	Paved				
Top Width	96.000	ft			

Culvert Input: CD-03_PR

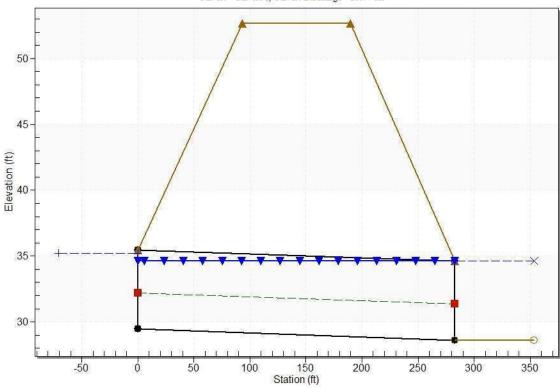
Parameter	Value	Units					
CULVERT DATA							
Name	Culvert 1						
Shape	Concrete Box						
Material	Concrete						
Span	8.000	ft					
Rise	6.000	ft					
Embedment Depth	0.000	in					
Manning's n	0.012						
Culvert Type	Straight						
Inlet Configuration	Square Edge (90º) Headwall (Ke=0.5)						
Inlet Depression?	No						
SITE DATA							
Site Data Input Option	Culvert Invert Data						
Inlet Station	0.000	ft					
Inlet Elevation	29.460 ft						
Outlet Station	283.000 ft						
Outlet Elevation	28.610	ft					
Number of Barrels	1						
Computed Culvert Slope	0.003004	ft/ft					

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	HW / D (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
50-yr	140.68	140.68	34.89	3.62	5.434	0.91	1-S1f	2.09	2.13	6.00	6.00	2.93	0.00
100-yr	167.03	167.03	35.01	4.04	5.550	0.93	1-S1f	2.36	2.38	6.00	6.00	3.48	0.00
500-yr	206.37	206.37	35.22	4.64	5.760	0.96	1-S1f	2.74	2.74	6.00	6.00	4.30	0.00
Overtopping	1031.85	1010.79	52.73	23.27	19.445	3.88	4-FFf	6.00	6.00	6.00	6.00	21.06	0.00

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - CD-03_PR, Design Discharge - 206.4 cfs
Culvert - Culvert 1, Culvert Discharge - 206.4 cfs



CROSS DRAIN CD-04_PR

HY-8 CALCULATION FOR PROPOSED CONDITION (TRIPLE 36-INCH RCP)

PROJECT:Sanford Airport ConnectorPREPARED:LCMDATE:06/20/25LOCATION:Seminole County, FloridaCHECKED:LCSDATE:06/20/25

Proposed Offsite Conveyance Calculations

Proposed Cross Drain at Sanford Airport Connector

Cross Drain Name	CD-04_PR
Affected Corridor(s)	2a

Basin Runoff Calculations for Offsite CD-05_PR Basin

Total Contributing Area (acres)	21.95
Design Q ₅₀ (cfs)	60.31
Q ₁₀₀ (cfs)	69.32
Q ₅₀₀ (cfs)	88.20

 Q_{50} , Q_{100} and Q_{500} from Permit SJRWMD ERP 4-117-22496-3 (See Excerpts in Appendix B Page 40)

Cross Drain Sizing Calculations

Assumed Velocity (ft/s)	3
Cross-sectional Area Required (ft ²)	20.10
Number of Cell	3
Recommended Culvert Conveyance Size	36 inch
Provided Cross Sectional Area (ft ²)	21.21
Upstream Est. SHWL Elev (ft-NAVD88)	28.96
Upstream Est. Ground Elev (ft-NAVD88)	28.96
Downstream Est. Ground Elev (ft-NAVD88)	28.56
Additional Culvert Height Required	0 ft
Recommended Culvert Size	36 inch
Tailwater (ft-NAVD88) ⁴	31.56
Length	220 ft

Notes:

¹ Frequency Factor for Pervious Area Runoff Coefficients will be applied per Design Storm Event (Table B-5, FDOT Drainage Design Guide, January 2017)

² Per FDOT Drainage Manual, 50-year considered design event for mainline interstates and 100-year used if culvert proposed within regulated floodway.

 $^{^{3}}$ Design Intensity calculated from NOAA IDF Curve (NOAA Atlas 14 Website).

⁴ Crown of culvert

A LUCO INTERNATIONAL LID. COMPANY	CALCULATION SHEET	PAGE OF
	proposed	PROJECT NO. 46547
CLIENT Seminole County	SUBJECT Cross Drain	Prepared By MG DATE 01/02/02
PROJECT East Lake Mary	Calculation	Reviewed By DATE
Bonlevard, Segment 2A		Approved By DATE

Intensity (
$$I_{50} = 7.0 \text{ in/hr} (C_{50} = 0.337 \times 1.2 = 0.404)$$

 $I_{100} = 7.5 \text{ in/hr} (C_{50} = 0.337 \times 1.25 = 0.421)$

$$Q_{50} = C_{5}I_{50}A$$

= 0.404 × 7.0 × 21.953 = 62.08 cfs

$$Q_{100} = C_{100} I_{100} A$$

= 0. $421 \times 7.5 \times 21.953 = 69.32$ cfs

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PDS ALTAMONTE SVC. CTR.

Crossing Input: CD-04_PR (Triple)

Parameter	Value	Units						
DISCHARGE DATA								
Discharge Method	User-Defined							
Discharge List	Define							
TAILWATER DATA								
Channel Type	Enter Constant Tailwater Elevation							
Channel Invert Elevation	28.560	ft						
Constant Tailwater	31.560	ft						
Elevation								
Rating Curve	View							
ROADWAY DATA								
Roadway Profile Shape	Constant Roadway Elevation							
First Roadway Station	0.000	ft						
Crest Length	300.000	ft						
Crest Elevation	38.200	ft						
Roadway Surface	Paved							
Top Width	96.000	ft						

Culvert Input: CD-04_PR (Triple)

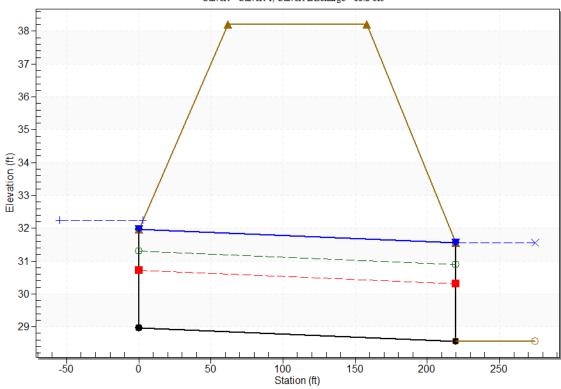
Parameter	Value	Units					
CULVERT DATA							
Name	Culvert 1						
Shape	Circular						
Material	Concrete						
Diameter	3.000	ft					
Embedment Depth	0.000	in					
Manning's n	0.012						
Culvert Type	Straight						
Inlet Configuration	Beveled Edge (1:1) (Ke=0.2)						
Inlet Depression?	No						
SITE DATA							
Site Data Input Option	Culvert Invert Data						
Inlet Station	0.000	ft					
Inlet Elevation	28.960	ft					
Outlet Station	220.000	ft					
Outlet Elevation	28.560	ft					
Number of Barrels	3						
Computed Culvert Slope	0.001818	ft/ft					

Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	HW / D (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
50-	60.31	60.31	31.94	2.06	2.981	0.99	3- M1f	1.76	1.44	3.00	3.00	2.84	0.00
100-	69.32	69.32	32.08	2.24	3.122	1.04	3- M1f	1.94	1.55	3.00	3.00	3.27	0.00
500-	88.20	88.20	32.24	2.57	3.285	1.09	4-FFf	2.34	1.76	3.00	3.00	4.16	0.00
Overtopping	294.00	276.22	38.27	7.95	9.314	3.10	4-FFf	3.00	2.86	3.00	3.00	13.03	0.00

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - CD-04_PR (Triple), Design Discharge - 88.2 cfs Culvert - Culvert 1, Culvert Discharge - 88.2 cfs



HY-8 CALCULATION FOR EXISTING CONDITION (TRIPLE 30-INCH RCP)

Crossing Input: CD_05_EX (NAVD) (Triple)

Parameter	Value	Units
DISCHARGE DATA		
Discharge Method	User-Defined	
Discharge List	Define	
TAILWATER DATA		
Channel Type	Enter Constant Tailwater Elevation	
Channel Invert Elevation	28.660	ft
Constant Tailwater	31.160	ft
Elevation		
Rating Curve	View	
ROADWAY DATA		
Roadway Profile Shape	Constant Roadway	
	Elevation	
First Roadway Station	0.000	ft
Crest Length	300.000	ft
Crest Elevation	39.240	ft
Roadway Surface	Paved	
Top Width	96.000	ft

Culvert Input: CD_05_EX (NAVD) (Triple)

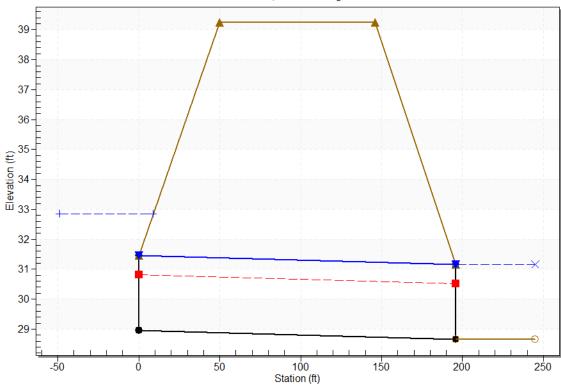
Parameter	Value	Units						
CULVERT DATA								
Name	Culvert 1							
Shape	Circular							
Material	Concrete							
Diameter	2.500	ft						
Embedment Depth	0.000	in						
Manning's n	0.012							
Culvert Type	Straight							
Inlet Configuration	Square Edge with Headwall (Ke=0.5)							
Inlet Depression?	No							
SITE DATA								
Site Data Input Option	Culvert Invert Data							
Inlet Station	0.000	ft						
Inlet Elevation	28.960	ft						
Outlet Station	196.000	ft						
Outlet Elevation	28.660	ft						
Number of Barrels	3							
Computed Culvert Slope	0.001531	ft/ft						

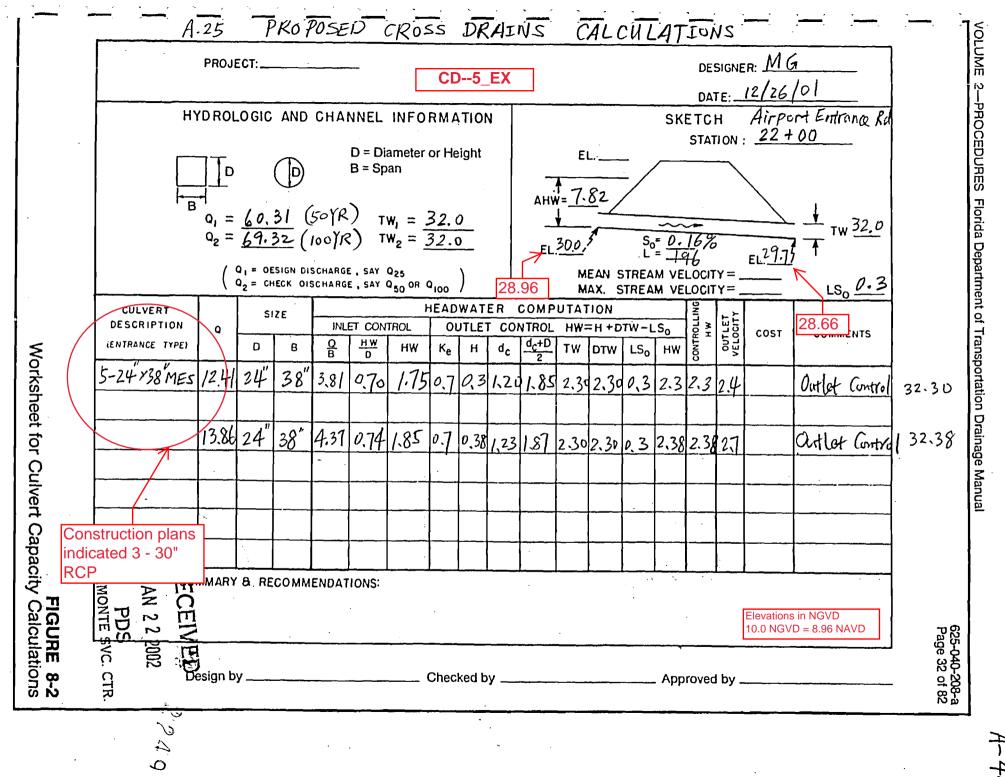
Table 2 - Culvert Summary Table: Culvert 1

Discharge Names	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	HW / D (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
50-yr	60.31	60.31	31.95	2.33	2.990	1.20	4-FFf	2.50	1.52	2.50	2.50	4.10	0.00
100-yr	69.32	69.32	32.20	2.57	3.243	1.30	4-FFf	2.50	1.64	2.50	2.50	4.71	0.00
500-yr	88.20	88.20	32.85	3.11	3.889	1.56	4-FFf	2.50	1.85	2.50	2.50	5.99	0.00
Overtopping	205.80	193.61	39.30	8.61	10.337	4.13	4-FFf	2.50	2.41	2.50	2.50	13.15	0.00

Water Surface Profile Plot for Culvert: Culvert 1

Crossing - CD_05_EX (NAVD) (Triple), Design Discharge - 88.2 cfs Culvert - Culvert 1, Culvert Discharge - 88.2 cfs





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